PARCO REGIONALE DELLA VALLE DEL LAMBRO
Via Vittorio Veneto, 19 - 20844 Triuggio (MB)

OPERE DI REGOLAZIONE DELLE PORTATE previste nell'intervento "Area di laminazione di Inverigo – interventi idraulici e di riqualificazione fluviale nei territori di Inverigo, Nibionno e Veduggio con Colzano"

APPALTO INTEGRATO - PROGETTO ESECUTIVO

INDICE	DATA	MODIFICHE	DISEGN.	CONTR.	APPROV.

CALCOLI ESECUTIVI
Calcoli esecutivi delle strutture

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GEOLOGIA: Geol. Pietro Alborghetti

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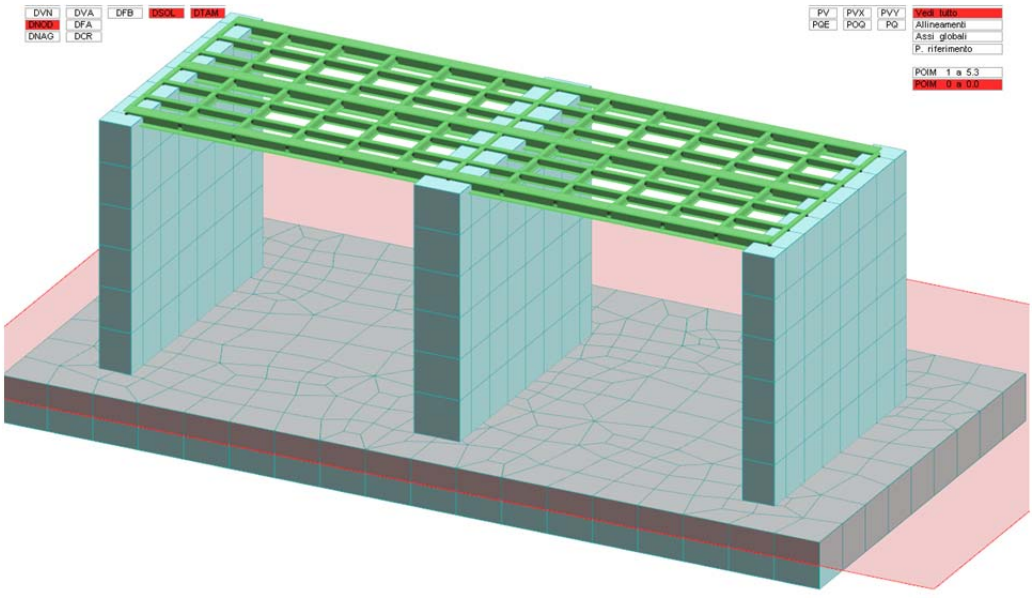
M-G-019

INDICE

1 INTRODUZIONE

La presente relazione riguarda la realizzazione di un ponte ciclopedonale a scavalco del torrente Lambro, attrezzato con doppie paratoie fluviali per controllo della portata di piena, per conto del Parco Regionale della Valle del Lambro. La struttura progettata prevede un impalcato costituente il ponte, composto da travi d'acciaio HEB280 e HEA280, con profili trasversali IPE 180 secondari e controventi diagonali Φ20, necessari a sostenere carichi in direzione trasversale all'asse dell'impalcato.
L'impalcato posa su spalle e su una pila centrale realizzate in cemento armato, aventi il compito anche di trasmettere in fondazione i carichi dovuti alla spinta dell'acqua che si genera allorquando entrino in azione una coppia di paratie di regolamentazione del flusso idrico.
Le fondazioni poggiano su pali trivellati di diametro 80 cm lunghi 14 m in accordo con la relazione geotecnica "Progetto definitivo opere strutturali relative all'intervento Area di laminazione di Inverigo - Interventi Idraulici e di riqualificazione fluviale nei territori di Inverigo, Nibionno e Veduggio con Colzano" dell'Aprile 2014 realizzata dal Dott. Geol. Pietro Alborghetti.
In prossimità dell'impalcato da ponte verrà inoltre realizzato un manufatto di sfioro, anch'esso gravante su pali di fondazione.

Nella presente relazione verranno riportati i calcoli effettuati per le verifiche ed il dimensionamento degli elementi strutturali, effettuando le principali verifiche descritte dalla normativa vigente. Si allega inoltre la relazione di calcolo riguardante il modello tridimensionale della struttura, realizzato con il software ad elementi finiti ModeSt 8.8.



2 PARAMETRI GENERALI DI PROGETTO

2.1 Premessa

A meno di diverse indicazioni i dati di seguito riportati sono da ritenersi validi per tutte le opere in progetto.

2.2 Quadro normativo

La normativa di riferimento è la seguente:

- D.M. 14 GENNAIO 2008 - Norme Tecniche per le Costruzioni.
- Circolare 617 del 02/02/2009 - Istruzioni per l'applicazione delle nuove Norme Tecniche per le Costruzioni di cui al D.M. 14 gennaio 2008.
- Legge 05/11/1971 – n. 1086 - G.U. 21-12-71 n.321 – "Norme per la disciplina delle opere in conglomerato cementizio armato, normale e precompresso ed a struttura metallica."

2.3 Vita nominale (V_N)

La vita nominale, intesa come il periodo di tempo nel quale la struttura, purché soggetta alla manutenzione ordinaria, deve poter essere utilizzata per lo scopo al quale è destinata, è stata valutate in comune accordo tra committente e progettista in **100 anni**.

Appartengono infatti a tale categoria grandi opere, ponti, opere infrastrutturali e dighe di grandi dimensioni o di importanza strategica (§2.4.1 NTC '08).

2.4 Classe d'uso

La classe d'uso di un edificio in presenza di azioni sismiche, è funzione delle conseguenze correlate ad una eventuale interruzione dell'operatività della struttura o di un suo collasso. Per il progetto corrente la categoria individuata è la numero **III** (§2.4.2 NTC '08).

2.5 Materiali utilizzati

2.5.1 Calcestruzzo

Si assume, per tutti gli elementi, **classe di esposizione XC4** (UNI 11104, in applicazione della UNI EN 206), da cui seguono:

1. resistenza minima: $R_{ck,min} = 40MPa;$
2. copriferro minimo: $c_{min} = 40mm.$

In fase di calcolo il calcestruzzo utilizzato è del tipo **C32/40,** i cui minimi parametri da garantire a 28 giorni dall'esecuzione del getto sono descritti nella tabella sotto riportata

- C32/40

Simbolo	Formula	Valore	
fck	Resistenza caratteristica a compressione cilindrica	32.00	MPa
Rck	Resistenza caratteristica a compressione cubica	40.00	MPa
fctm	Resistenza a trazione media	3.02	MPa
fctk_0.05	Resistenza a trazione caratteristica	2.12	MPa
Ecm	Modulo elastico medio	34922.82	MPa
ν	Coeff. di Poisson	0.20	-
γc	Coeff. di normativa	1.50	-
αcc	Coeff. di normativa per resistenze di lunga durata	0.85	-
fcd	Resistenza a compressione di progetto	18.13	MPa
ξcu	Deformazione ultima a rottura	0.35	%

2.5.2 Acciaio

L'acciaio impiegato per la realizzazione delle armature è del tipo **B450C** in barre ad aderenza migliorata le cui caratteristiche sono di seguito elencate:

Descrizione	Formula	B450C	
Diametri utilizzabili	-	da 6 a 40	mm
Resistenza caratteristica a trazione (≥ ft nom =540)	-	540	MPa
Tensione caratteristica di snervamento (≥ 450 fy nom = 450)	-	450	MPa
Rapporto di sovraresistenza	(ft/fy)k	≥ 1.15	-
		< 1.35	-
-	(fy/fy nom)k	≤ 1.25	-
Allungamento totale al carico massimo	-	≥ 7.5%	%
Modulo elastico longitudinale	-	210000	MPa
Fattore di sicurezza parziale proprietà acciaio	-	1.15	-
Resistenza a trazione caratteristica	fyd/γy	391.3	MPa

L'acciaio utilizzato per i profili metallici invece è del tipo **S355** (f_{yk} = 355 MPa, f_{yu} = 510 MPa).
I bulloni utilizzati per i collegamenti tra gli elementi strutturali sono invece di **classe 8.8** (f_{yk} = 640 MPa, f_{yu} = 800 MPa).

3 ANALISI DEI CARICHI GENERALE

L'individuazione dei diversi scenari di contingenza a cui l'opera potrà essere soggetta è stata determinata dal progettista in funzione dell'*ambiente di progetto*, del relativo *quadro normativo di riferimento*, di situazioni che introducono perturbazioni nello schema strutturale e di disposizioni non simmetriche dei carichi.

3.1 Carichi permanenti strutturali

A livello di carichi permanenti strutturali sono stati considerati i pesi propri degli elementi strutturali.

- IPE180 q= 18.8 daN/m
  interasse i_1 = 0.79 m
  interasse i_2 = 1.17 m → incidenza totale 40 daN/m^2

- HEB280 q= 103 daN/m
  interasse i = 5 m → incidenza totale 22 daN/m^2

- HEA280 q= 76.4 daN/m
  interasse i = 2.5 m → incidenza totale 32 daN/m^2

- Controventi Φ20
  q= 2.5 daN/m
  l_{tot} = 55m → incidenza totale 6 daN/m^2

- Spalle Dimensioni 5.74m x 5.3m x 0.7m

- Pila Dimensioni 5.74m x 5.3m x 1.0m

- Fondazioni Dimensioni 17.9m x 9.0m x 1.0m

- Pali Lunghezza 14m
  Diametro 0.8m – 0.7m

3.2 Carichi permanenti non strutturali

Alla stregua di carichi permanenti non strutturali sono state considerate le sollecitazioni dovute al peso degli elementi di camminamento oltre alle spinte provocate dal terreno sostenuto dalle spalle ed il peso dell'acqua transitante al di sotto dell'impalcato.

- Piastra metallica Peso specifico 7850 daN/m^3
  Spessore 0.011 m → carico 90 daN/m^2

- Parapetto → carico 50 daN/m

- Spinta terreno Peso specifico terreno 1700 daN/m^3
  Angolo di attrito 30° (coefficiente di spinta attiva k_a = 0.333)
  → Pressione terreno alla base spalla 3000 daN/m^2

- Peso acqua fondazione Peso specifico 1100 daN/m^3

Spessore 2.5m → carico 2500 daN/m^2

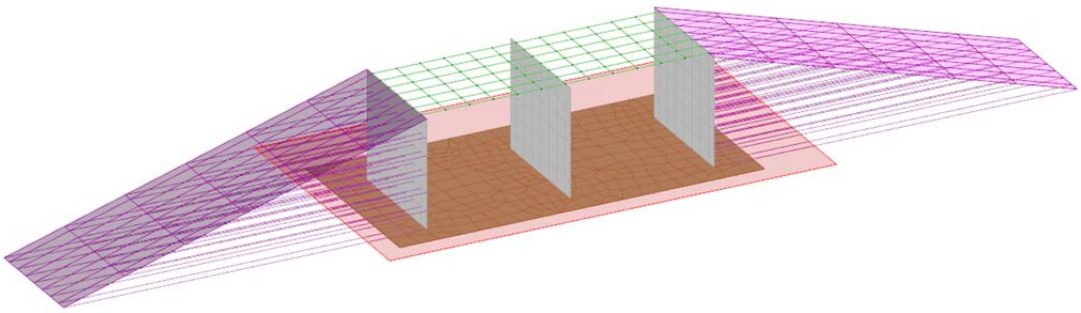


Figura 1 - Spinta del terreno

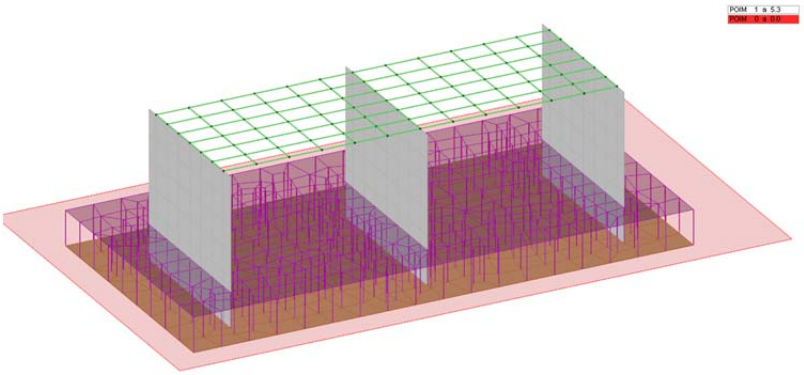


Figura 2 - Carico acqua in fondazione

3.3 Carichi variabili

Nel rispetto delle richieste effettuate dalla Committenza, a livello di carichi variabili sull'impalcato per simulare il peso della folla è stato assunto un valore pari a 1000 daN/m^2; data l'intensità di quest'ultimo carico è stato evitato di considerare l'effetto del sovraccarico da neve.
Sono stati anche considerati gli effetti dovuti alla spinta generata dalla presenza di un carico da folla in prossimità delle spalle del ponte, assunti in fase di predimensionamento pari a 330 daN/m^2, mentre in fase di modellazione tridimensionale ad elementi finiti, nella quale si tiene in conto degli effetti di tipo piastra degli elementi bidimensionali, è stato assunto pari a 1000 daN/m^2 .
Sono state tenute in conto anche le disposizioni relative al passaggio di mezzi di soccorso/manutenzione, così come indicato nella Circolare al paragrafo §C5.1.4.9, considerando una combinazione di carico caratterizzata da due assi di peso complessivo pari a 4000 daN e 8000 daN. Automaticamente non è stato quindi utilizzato lo schema di carico 4 previsto dal paragrafo §5.1.3.3.3 delle NTC in quanto caratterizzato da un carico concentrato di intensità inferiore (1000 daN).
Inoltre, in relazione ai dati forniti dagli studi idrologici, sono stati inseriti carichi agenti su spalle e pila centrale dovuti alle spinte dell'acqua, in relazione ad eventi naturali con periodo di ritorno di T = 200 anni e T = 500 anni.
Nel caso di scenario con T = 200 anni, è stata valutata la spinta dell'acqua, calcolata in regime idrostatico, considerando un'altezza del tirante idraulico pari a 4.3 m rispetto all'estradosso delle fondazioni ed un peso specifico dell'acqua pari a 1000 daN/m^3 , incrementato di un coefficiente γ = 1.1 per tenere in conto di possibili effetti dinamici. In questa situazione la spinta dell'acqua si

scarica sia sulla pila centrale che sulla spalle laterali in quanto è previsto che entrambe le paratoie, di cui la passerella è dotata, possano abbassarsi per regimare il deflusso di acqua.

Nel caso di scenario con T = 500 anni, è stata valutata la spinta dell'acqua, calcolata in regime idrostatico, considerando un'altezza del tirante idraulico pari a 4.68 m rispetto all'estradosso delle fondazioni ed un peso specifico dell'acqua pari a 1000 daN/m^3 , incrementato di un coefficiente γ = 1.1 per tenere in conto di possibili effetti dinamici. In questa situazione però la spinta si scarica solo sulla pila centrale ed una spalla, in quanto solo una delle due paratoie risulta essere abbassata per controllare il deflusso di acqua.
In entrambi i tipi di scenario, è stato assunto un sovraccarico dovuto alla presenza di un livello di acqua più elevato pari a 2800 daN/m^2.

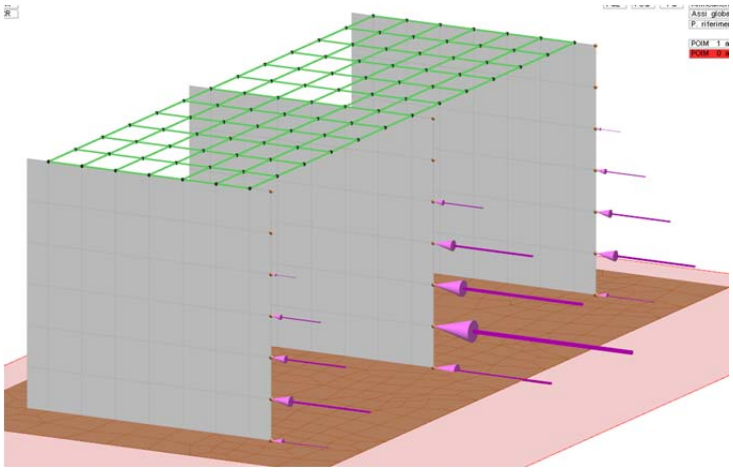


Figura 3 – Spinta acqua, scenario T = 200 anni

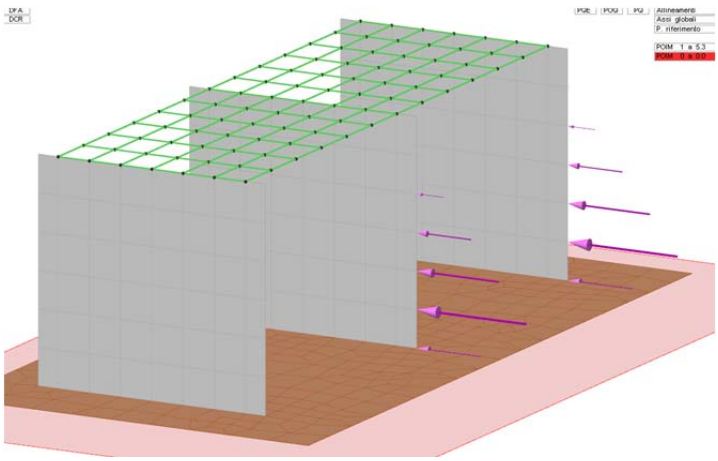


Figura 4 - Spinta acqua, scenario T = 500 anni

3.4 Azione sismica - § 3.2 NTC '08

La **pericolosità sismica di base** del sito di costruzione in funzione dello stato limite considerato dipende sia dall'accelerazione orizzontale massima in condizioni di campo libero su suolo orizzontale di categoria A, che dallo spettro di risposta elastico a quest'ultima corrispondente.

A loro volta le forme spettrali per ciascuna **probabilità di superamento** (**P_{vr}**) prevista dalla norma possono essere ricavate grazie ai parametri **a_g** (*Accelerazione orizzontale massima del sito),* **F_0** **(***Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale) e* **T^*_C** **(***Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale)* definiti

dalla normativa italiana a seconda della localizzazione dell'area di costruzione all'interno del **Reticolo Nazionale di Riferimento**.

Nei paragrafi a seguire verranno progressivamente ricavati tutti i valori necessari per la costruzione degli spettri ali **SL** di **Vita**, **SL** di **Danno** e di **Operatività**.

3.4.1 Localizzazione del sito d'intervento

Località	*Comune di Inverigo*
Latitudine	45.73292° N
Longitudine	9.23529° E
ID punti reticolo d'appartenenza	11152 11151 10930 10929

3.4.2 Periodo di riferimento (V_R) per l'azione sismica

Il periodo $\mathbf{V_R}$ rispetto il quale sono valutate le azioni sismiche viene ricavato moltiplicando la **vita nominale** della struttura per il **coefficiente d'uso** ($\mathbf{C_U}$), a sua volta funzione della **classe d'uso**:

Classe III: $C_U = 1.5$

$V_R = V_N \cdot C_U = 100 \cdot 1.5 = 150$ anni

3.4.3 Probabilità di superamento e Periodo di ritorno

La **probabilità di superamento** ($\mathbf{P_{VR}}$) del **periodo di riferimento** ($\mathbf{V_R}$) per l'individuazione dell'azione sismica è funzione dello stato limite considerato. A meno di particolari indicazioni a riguardo, gli **SL** richiesti per la verifica strutturale e le relative $\mathbf{P_{VR}}$ sono:

STATI LIMITE D'ESERCIZIO	di **Operatività** (**SLO**)	**81%**
	di **Danno** (**SLD**)	**63%**
STATI LIMITE ULTIMI* :	di **salvaguardia della Vita** (**SLV**)	**10%**
*: A tale categoria appartiene anche il caso degli SL di collasso, che tuttavia non è richiesto ai fini della verifica.		

A questo punto, grazie all'espressione $T_R = -\dfrac{V_R}{\ln(1-P_{VR})}$, è possibile valutare il **periodo di ritorno** ($\mathbf{T_R}$) dei corrispondenti terremoti:

$\mathbf{P_{VR}}$	$\mathbf{T_R}$ [anni]
81%	90
63%	151
10%	1424

3.4.4 Definizione dei parametri a_g, F_0 e T^*_C

I valori forniti dal **D.M. 2008** di $\mathbf{a_g}$, $\mathbf{F_0}$ *e* $\mathbf{T^*_C}$ in funzione dei valori di **Latitudine**, **Longitudine** e **Periodo di ritorno** determinati ai punti precedenti sono:

Stato limite considerato	$\mathbf{a_g}$ **[g]**	$\mathbf{F_0}$	$\mathbf{T^*_C}$
SLD	0.0344	2.608	0.226
SLV	0.0653	2.697	0.306

3.4.5 Coefficiente di amplificazione stratigrafica

La definizione dell'azione sismica, oltre che dipendere dalla zonazione di progetto, risulta influenzata anche dalla categoria del sottosuolo ivi presente; nel caso in esame sono stati considerati terreni appartenenti alla **categoria C.**

Stato limite	ag [g]	F0	T*C		Ss	Cc	
SLD	0.0344	2.608	0.226		1.5	1.715	
SLV	0.0653	2.697	0.306		1.5	1.552	

Categoria	Descrizione	Ss	Cc
C	Depositi di terreni a grana grossa mediamente addensati o terreni a grana fina mediamente consistenti, con spessori superiori a 30 m, caratterizzati da un graduale miglioramento delle proprietà meccaniche con la profondità e da valori di Vs,30 compresi tra 180 m/s e 360 m/s (ovvero 15<NSPT,30 <50 nei terreni a grana grossa e 70<cu,30 < 250 kPa nei terreni a grana fina).	1.0≤ 1.7-0.6*F0*ag/g ≤ 1.5	1.05*(Tc*)^-0.33

3.4.6 Coefficiente di amplificazione topografica

Per la completa definizione dello spettro elastico di risposta deve essere inoltre determinata la configurazione superficiale del sito in oggetto; nel caso corrente la categoria è la **T1**, ossia *pendii con inclinazione media i<15°*, cui è associato il seguente **coefficiente di amplificazione topografica** (S_T):

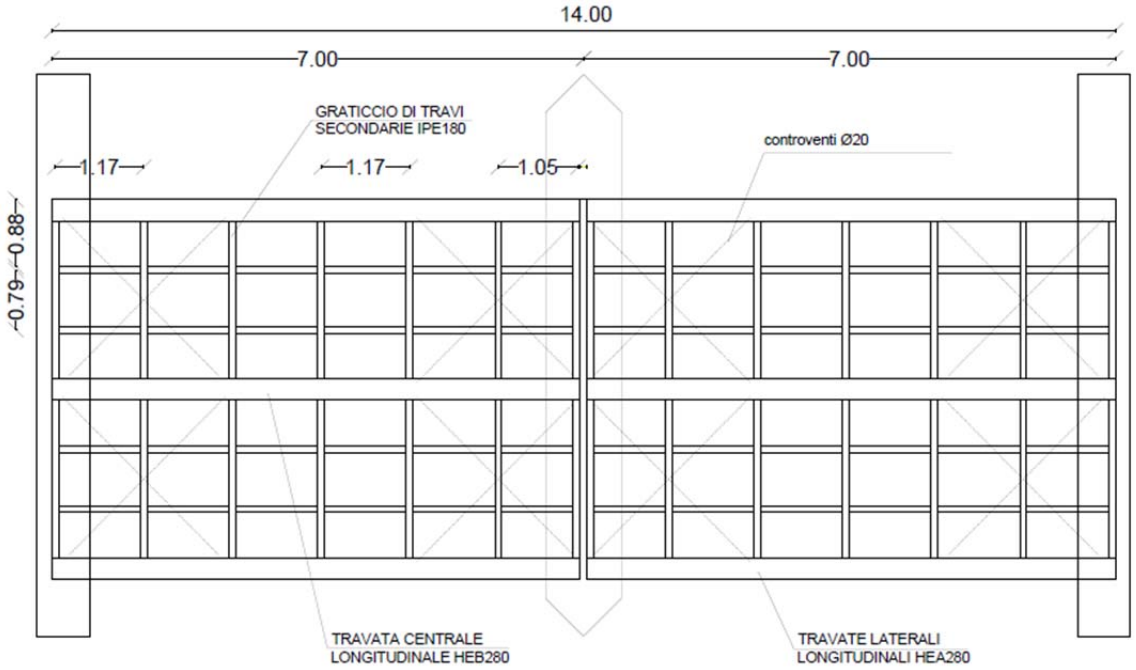
Categoria	Caratteristiche della superficie topografica	St
T1	Superficie pianeggiante, pendii e rilievi isolati con inclinazione media i ≤ 15°	1

3.4.7 Categoria di sottosuolo

La combinazione dei parametri S_S ed S_T porta alla definizione del parametro **S**, ossia, la **categoria di sottosuolo**:

Stato limite considerato	S_s	S_T	S
SLD	1.50	1.00	1.50
SLV	1.50	1.00	1.50

4 ANALISI



4.1 Verifiche piastra di camminamento

4.1.1 Introduzione

La verifica sulla piastra di camminamento è stata effettuata tramite il metodo di Grahof, tramite il quale la piastra viene studiata alla stregua di due travi perpendicolari tra loro e soggette rispettivamente ad un carico q_x e q_y tali per cui $q_x\, l_x + q_y\, l_y = q\, l_x\, l_y$; inoltre le due travi sono tali da avere una deformata identica in mezzeria $f\,(l_x/2) = f\,(l_y/2)$. Stesso ragionamento vale per un carico concentrato nel centro della piastra.
Svolgendo i calcoli del caso, definiti q_{tot} e P_{tot} i carichi distribuiti e concentrati agenti sulla piastra, si ottengono i seguenti risultati:

- $q_y = q_{tot}\, l_x^5 / (l_x^4 + l_y^4)$ $\qquad$ $q_x = q_y\, l_y^5 / l_x^5$
- $P_y = P_{tot}\, l_x^4 / (l_x^4 + l_y^4)$ $\qquad$ $P_x = P_y\, l_y^4 / l_x^4$

4.1.2 Calcoli

Dati generali

- Luci $l_x = 1.17$ m $\quad l_y = 0.79$ m
- Schema statico trave in semplice appoggio (Metodo di Grashof)
- Azioni resistenti di progetto $M_{x,RD} = 807.9$ daNm
  $T_{x,RD} = 169628$ daN

  $M_{y,RD} = 1196.6$ daNm
  $T_{y,RD} = 251221$ daN
- Rapporto limite SLE L / f = 300

Caso 1: peso proprio + peso folla

- Carico g_1 90 daN/m^2

- Coefficiente γ_{g1} = 1.35

→ g_1 = 125 daN/m^2

- Carico q 1000 daN/m^2
- Coefficiente γ_{g1} = 1.35

→ q = 1350 daN/m^2

$q_{tot\ SLU}$ = 1475 daN/m^2
$q_{tot\ SLE}$ = 1090 daN/m^2

$q_{x\ SLU}$ = 200 daN/m	$M_{x,ED}$ = 34.2 daNm	VERIFICATO
	$T_{x,ED}$ = 117 daN	VERIFICATO
$q_{y\ SLU}$ = 1428 daN/m	$M_{y,ED}$ = 111 daNm	VERIFICATO
	$T_{y,ED}$ = 564 daN	VERIFICATO
$q_{x\ SLE}$ = 148.1 daN/m	f_{max} = 0.00196 m	
	L / f = 596	VERIFICATO
$q_{y\ SLE}$ = 1057.8 daN/m	f_{max} = 0.00196 m	
	L / f = 403	VERIFICATO

Caso 2: peso proprio + peso mezzi soccorso/manutenzione

- Carico g_1 90 daN/m^2
- Coefficiente γ_{g1} = 1.35

→ **$q_{tot\ SLU}$ = 125 daN/m^2**
$q_{tot\ SLE}$ = 90 daN/m^2

- Carico P 4000 daN
- Coefficiente γ_{g1} = 1.35

→ **$P_{tot\ SLU}$ = 5400 daN/m^2**
$P_{tot\ SLE}$ = 4000 daN/m^2

$q_{x\ SLU}$ = 17.0 daN/m		
$P_{x\ SLU}$ = 929.3 daN		
	$M_{x,ED}$ = 275 daNm	VERIFICATO
	$T_{x,ED}$ = 938.9 daN	VERIFICATO
$q_{y\ SLU}$ = 121.1 daN/m		
$P_{y\ SLU}$ = 4470.7 daN		
	$M_{y,ED}$ = 892 daNm	VERIFICATO
	$T_{y,ED}$ = 4517.2 daN	VERIFICATO

Non sono previste verifiche in termini deformativi in quanto si presuppone che la situazione di carico dovuto a mezzi di manutenzione/soccorso sia limitata nel tempo.

4.2 Verifiche profili impalcato

4.2.1 Introduzione

Sono state effettuate le seguenti verifiche sui profili metallici costituenti l'impalcato:

- Verifica di resistenza a flessione
- Verifica di resistenza a taglio
- Verifica di deformabilità
- Verifiche legate a variazioni termiche $\Delta T = \pm 30°C$

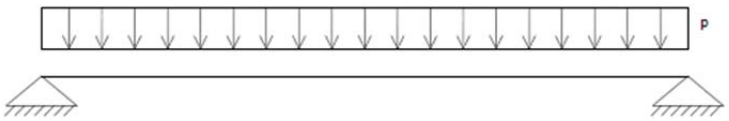
Non sono state effettuate verifiche legate all'instabilità flesso-torsionale degli elementi strutturali in quanto si ritiene che la limitata luce di libera inflessione e il contributo irrigidente della piastra di camminamento determinino un effetto benefico nei riguardi dell'instabilità.
Verrà invece effettuata una verifica a presso-flessione considerando l'azione di compressione dovuta a fenomeni di espansione termica, nell'ipotesi di impossibilità da parte del profilo metallico di potersi allungare liberamente.

4.2.2 Verifica IPE180 tipo A

Dati generali

- Luce l = 1.17 m
- Interasse i = 0.79 m
- Schema statico trave in semplice appoggio
- Azioni resistenti di progetto $M_{x,RD}$ = 5626 daNm
  $T_{x,RD}$ = 21970 daN
- Rapporto limite SLE L / f = 300
- Coefficiente di dilatazione termica $\alpha = 12 \times 10^{-6}$ 1/°C → deformazione ε = 0.036 %

Caso 1: peso proprio + peso lastra camminamento + peso folla



- Carico g_{1_SLE} 18.8 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 25.4 daN/m

- Carico g_{2_SLE} 71.1 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 106.7 daN/m

- Carico q_{SLE} 790 daN/m
- Coefficiente γ_q 1.35 → q_{SLU} = 1066.5 daN/m

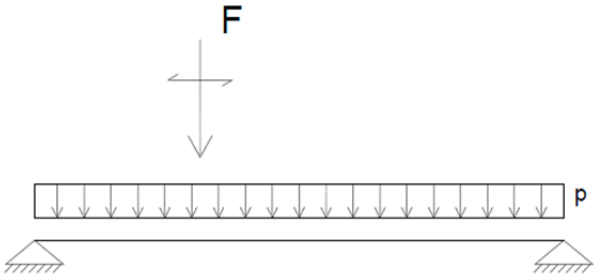
$q_{tot\ SLU}$ = 1198.6 daN/m
$q_{tot\ SLE}$ = 879.9 daN/m

M_{ED} = 205 daNm VERIFICATO
T_{ED} = 701 daN VERIFICATO

f_{max} = 0.00008 m
L / f = 15087 VERIFICATO

Caso 2: peso proprio + peso lastra camminamento + peso mezzi soccorso/manutenzione

Il carico concentrato F viene di volta in volta collocato nella posizione più sfavorevole per la verifica in corso di studio.



- Carico g_{1_SLE} 18.8 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 25.4 daN/m

- Carico g_{2_SLE} 71.1 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 106.7 daN/m

- Carico P_{SLE} 4000 daN
- Coefficiente γ_q 1.35 → P_{SLU} = 5400 daN

$q_{tot\ SLU}$ = 132.1 daN/m
$P_{tot\ SLU}$ = 5400 daN

$q_{tot\ SLE}$ = 89.9 daN/m
$P_{tot\ SLE}$ = 4000 daN

M_{ED} = 1602 daNm VERIFICATO
T_{ED} = 5477 daN VERIFICATO

f_{max} = 0.00049 m
L / f = 2385 VERIFICATO

Caso 3: effetto variazione termica ΔT, deformazione libera

Allungamento ΔL = 0.42 mm → Inferiore al gioco foro-bullone pari a 1.0 mm
VERIFICATO

Caso 4: effetto variazione termica ΔT, deformazione impedita

Incremento di sforzo assiale	$\Delta\sigma$ = 756 daN/cm^2	
Incremento di azione assiale	**ΔN = 18106.2 daN**	
Lunghezza libera inflessione L_0	117 cm	
Inerzia minima sezione I_{min}	100.9 cm^3	
	→	N_{crit} = 152770 daN
Snellezza adimensionale λ	0.746	
Curva di stabilità (Tab. 4.2.VI)	b	
	→	α = 0.34
Coefficiente Φ	0.871	
Coefficiente χ	0.757	

M_{RD} = 5626 daNm
χ N_{RD} = 0.757 x 80970 = 61294 daN
N_{ED} = 18106.2 daN
M_{ED} = 205 daNm

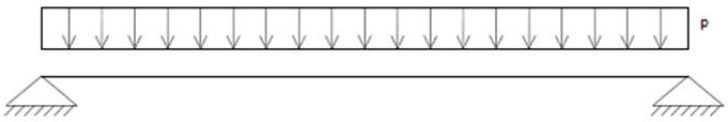
→ **F.S. = 0.33** VERIFICATO

4.2.3 Verifica IPE180 tipo B

Dati generali

- Luce l = 2.50 m
- Interasse i = 1.17 m
- Schema statico trave in semplice appoggio
- Azioni resistenti di progetto $M_{x,RD}$ = 5626 daNm
  $T_{x,RD}$ = 21970 daN
- Rapporto limite SLE L / f = 300
- Coefficiente di dilatazione termica $\alpha = 12 \times 10^{-6}$ 1/°C → deformazione ε = 0.036 %

Caso 1: peso proprio + peso lastra camminamento + peso folla



- Carico g_{1_SLE} 18.8 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 25.4 daN/m

- Carico g_{2_SLE} 105.3 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 157.9 daN/m

- Carico q_{SLE} 1170 daN/m
- Coefficiente γ_q 1.35 → q_{SLU} = 1579.5 daN/m

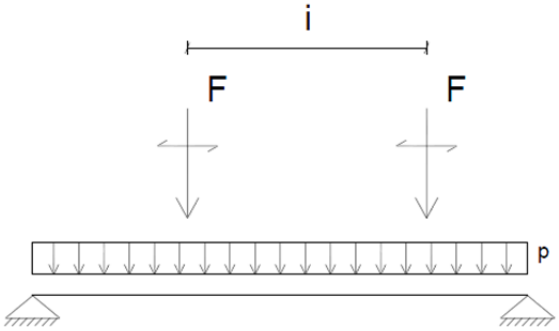
$q_{tot\ SLU}$ = 1762.8 daN/m
$q_{tot\ SLE}$ = 1294.1 daN/m

M_{ED} = 1377 daNm VERIFICATO
T_{ED} = 2203 daN VERIFICATO

f_{max} = 0.00023 m
L / f = 1050.5 VERIFICATO

Caso 2: peso proprio + peso lastra camminamento + peso mezzi soccorso/manutenzione

Il doppio carico concentrato F viene di volta in volta collocato nella posizione più sfavorevole per la verifica in corso di studio (interasse i = 1.30 m)



- Carico g_{1_SLE} 18.8 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 25.4 daN/m

- Carico g_{2_SLE} 105.3 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 157.9 daN/m

- Carico P_{SLE} 4000 daN
- Coefficiente γ_q 1.35 → P_{SLU} = 5400 daN

$q_{tot\ SLU}$ = 183.3 daN/m
$P_{tot\ SLU}$ = 5400 daN

$q_{tot\ SLE}$ = 124.1 daN/m
$P_{tot\ SLE}$ = 4000 daN

M_{ED} = 3900 daNm VERIFICATO
T_{ED} = 8200 daN VERIFICATO

f_{max} = 0.0065 m
L / f = 385 VERIFICATO

Caso 3: effetto variazione termica ΔT, deformazione libera

Allungamento ΔL = 0.90 mm → Inferiore al gioco foro-bullone pari a 1.0 mm
VERIFICATO

Caso 4: effetto variazione termica ΔT, deformazione impedita

Incremento di sforzo assiale $\Delta\sigma$ = 756 daN/cm^2
Incremento di azione assiale **ΔN = 18106.2 daN**

Lunghezza libera inflessione L_0	79 cm	
Inerzia minima sezione I_{min}	100.9 cm^3	
	→	N_{crit} = 335085 daN
Snellezza adimensionale λ	0.504	
Curva di stabilità (Tab. 4.2.VI)	b	
	→	α = 0.34
Coefficiente Φ	0.678	
Coefficiente χ	0.883	

M_{RD} = 5626 daNm
χ N_{RD} = 0.883 x 80970 = 71496.5 daN
N_{ED} = 18106.2 daN
M_{ED} = 1377 daNm

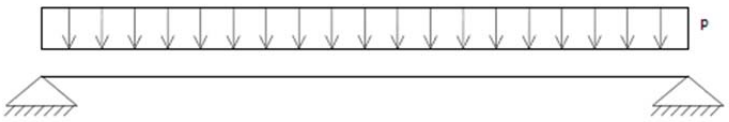
→ **F.S. = 0.49** VERIFICATO

4.2.4 Verifica HEA280

Dati generali

- Luce l = 7.00 m
- Interasse i = 1.25 m
- Schema statico trave in semplice appoggio
- Azioni resistenti di progetto $M_{x,RD}$ = 34250 daNm
  $T_{x,RD}$ = 61960 daN
- Rapporto limite SLE L / f = 300
- Coefficiente di dilatazione termica $\alpha = 12 \times 10^{-6}$ 1/°C → deformazione ε = 0.036 %

Caso 1: peso proprio + peso lastra camminamento + peso parapetto + peso folla



- Carico g_{1_SLE} 76.4 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 103.1 daN/m

- Carico g_{2_SLE} 165 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 247.5 daN/m

- Carico q_{SLE} 1250 daN/m
- Coefficiente γ_q 1.35 → q_{SLU} = 1687.5 daN/m

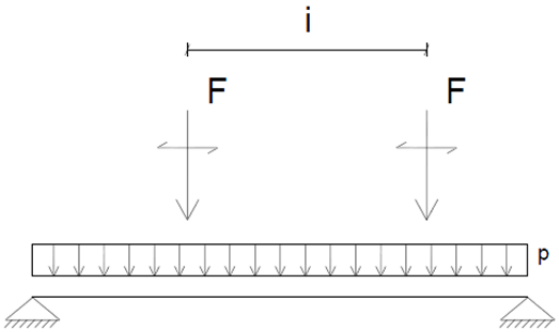
$q_{tot\ SLU}$ = 2038.1 daN/m
$q_{tot\ SLE}$ = 1491.4 daN/m

M_{ED} = 12483 daNm VERIFICATO
T_{ED} = 7133 daN VERIFICATO

f_{max} = 0.016 m
L / f = 431 VERIFICATO

Caso 2: peso proprio + peso lastra camminamento + peso parapetto + peso mezzi soccorso/manutenzione

Il doppio carico concentrato F viene di volta in volta collocato nella posizione più sfavorevole per la verifica in corso di studio (interasse i = 3.00 m). Inoltre, dato l'interasse tra gli elementi principali (travi HEA280 e HEB280), viene considerato il caso in cui due ruote del mezzo di soccorso/manutenzione si trovino effettivamente al di sopra del profilo HEA280, e al peso così determinato si somma la quota parte di carico che anche le altre due ruote scaricano sulla medesima trave.



- Carico g_{1_SLE} 76.4 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 103.1 daN/m

- Carico g_{2_SLE} 165 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 247.5 daN/m

- Carico $P1_{SLE}$ 2960 daN
- Coefficiente γ_q 1.35 → $P1_{SLU}$ = 3996 daN
- Carico $P2_{SLE}$ 5920 daN
- Coefficiente γ_q 1.35 → $P1_{SLU}$ = 7992 daN

$q_{tot\ SLU}$ = 350.6 daN/m
$P1_{tot\ SLU}$ = 3996 daN
$P2_{tot\ SLU}$ = 7992 daN

$q_{tot\ SLE}$ = 241.4 daN/m
$P1_{tot\ SLE}$ = 2960 daN
$P2_{tot\ SLE}$ = 5920 daN

M_{ED} = 17530 daNm VERIFICATO
T_{ED} = 11500 daN VERIFICATO

f_{max} = 0.0202 m
L / f = 345 VERIFICATO

Caso 3: effetto variazione termica ΔT, deformazione libera

Allungamento ΔL = 2.38 mm → Il foro di alloggio delle travi dovrà essere asolato per permettere questo tipo di deformazione

Caso 4: effetto variazione termica ΔT, deformazione impedita

Incremento di sforzo assiale $\Delta\sigma = 756$ daN/cm^2
Incremento di azione assiale **$\Delta N = 73528.5$ daN**

Lunghezza libera inflessione L_0 117 cm
Inerzia minima sezione I_{min} 4763 cm^3
→ $N_{crit} = 7211538$ daN

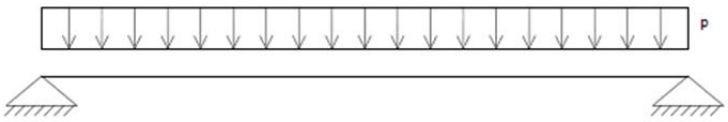
Rapporto N_{ED} / N_{crit} 0.01 < 0.04 (NTC §4.2.4.1.3.1)
→ Si trascurano gli effetti dovuti ad instabilità
VERIFICATO

4.2.5 Verifica HEB280

Dati generali

- Luce l = 7.00 m
- Interasse i = 2.5 m
- Schema statico trave in semplice appoggio
- Azioni resistenti di progetto $M_{x,RD}$ = 51860 daNm
  $T_{x,RD}$ = 80290 daN
- Rapporto limite SLE L / f = 300
- Coefficiente di dilatazione termica $\alpha = 12 \times 10^{-6}$ 1/°C → deformazione ε = 0.036 %

Caso 1: peso proprio + peso lastra camminamento + peso folla



- Carico g_{1_SLE} 103 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 139.1 daN/m

- Carico g_{2_SLE} 225 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 337.5 daN/m

- Carico q_{SLE} 2500 daN/m
- Coefficiente γ_q 1.35 → q_{SLU} = 3375 daN/m

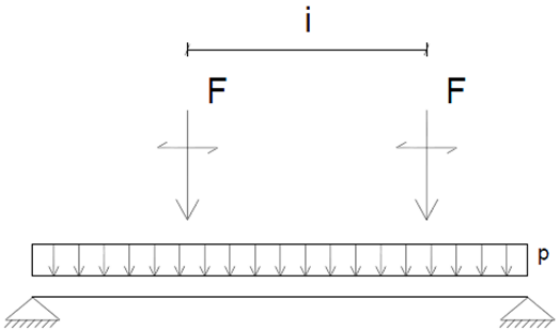
$q_{tot\ SLU}$ = 3851.6 daN/m
$q_{tot\ SLE}$ = 2828 daN/m

M_{ED} = 23587 daNm VERIFICATO
T_{ED} = 13479 daN VERIFICATO

f_{max} = 0.0218 m
L / f = 320 VERIFICATO

Caso 2: peso proprio + peso lastra camminamento + peso mezzi soccorso/manutenzione

Il doppio carico concentrato F viene di volta in volta collocato nella posizione più sfavorevole per la verifica in corso di studio (interasse i = 3.00 m). Inoltre, dato l'interasse tra gli elementi principali (travi HEA280 e HEB280), viene considerato il caso peggiore, determinato da un valore di carico concentrato massimo.



- Carico g_{1_SLE} 103 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 139.1 daN/m

- Carico g_{2_SLE} 225 daN/m
- Coefficiente γ_{g2} 1.50 → g_{2_SLU} = 337.5 daN/m

- Carico $P1_{SLE}$ 2960 daN
- Coefficiente γ_q 1.35 → $P1_{SLU}$ = 3996 daN
- Carico $P2_{SLE}$ 5920 daN
- Coefficiente γ_q 1.35 → $P1_{SLU}$ = 7992 daN

$q_{tot\ SLU}$ = 476.6 daN/m
$P1_{tot\ SLU}$ = 3996 daN
$P2_{tot\ SLU}$ = 7992 daN

$q_{tot\ SLE}$ = 328 daN/m
$P1_{tot\ SLE}$ = 2960 daN
$P2_{tot\ SLE}$ = 5920 daN

M_{ED} = 18300 daNm VERIFICATO
T_{ED} = 11949 daN VERIFICATO

f_{max} = 0.015 m
L / f = 465 VERIFICATO

Caso 3: effetto variazione termica ΔT, deformazione libera

Allungamento ΔL = 2.38 mm → Il foro di alloggio delle travi dovrà essere asolato per permettere questo tipo di deformazione

Caso 4: effetto variazione termica ΔT, deformazione impedita

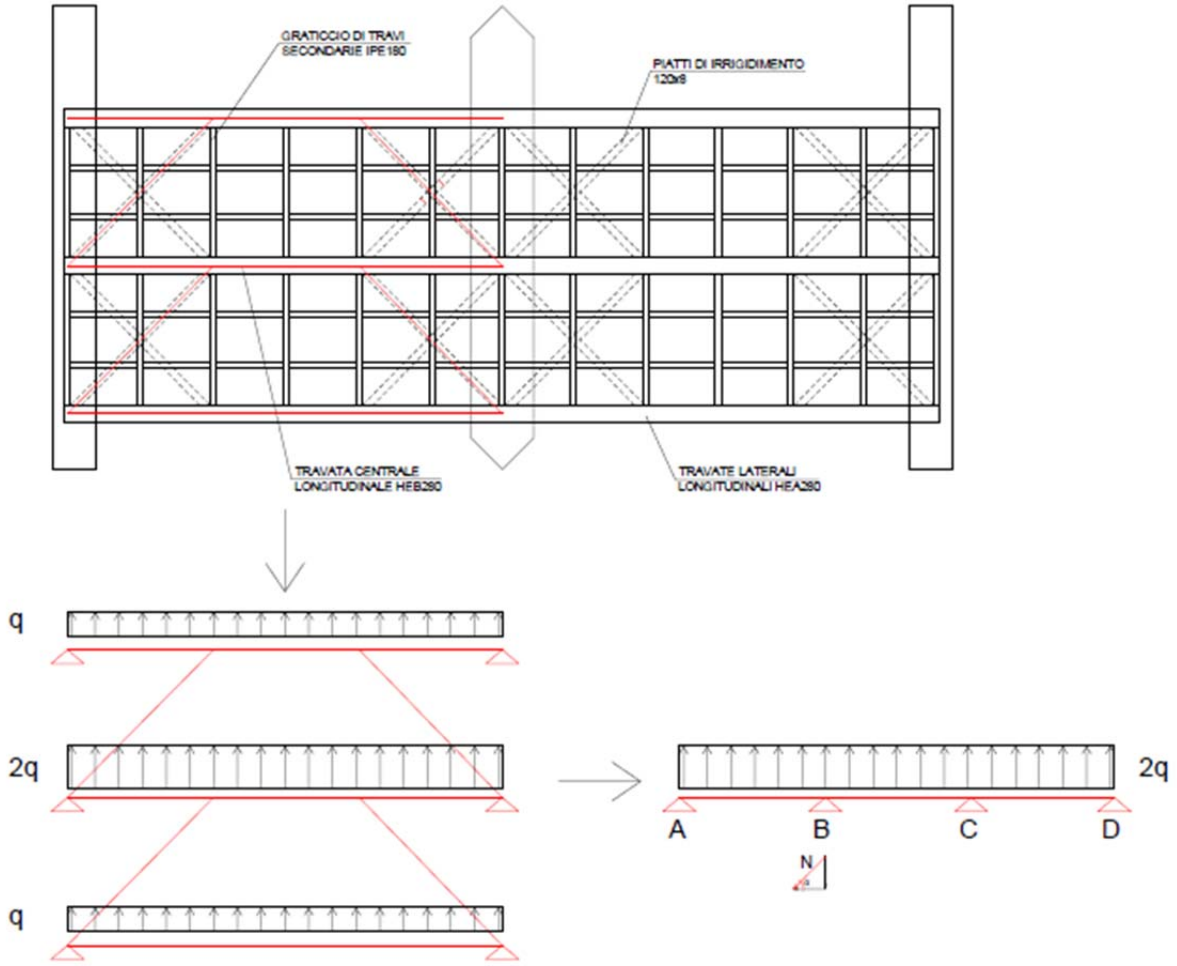
Incremento di sforzo assiale $\Delta\sigma$ = 756 daN/cm^2
Incremento di azione assiale **ΔN = 99338.4 daN**

Lunghezza libera inflessione L_0 117 cm
Inerzia minima sezione I_{min} 6595 cm^3
→ N_{crit} = 9985322.9 daN

Rapporto N_{ED} / N_{crit} 0.01 < 0.04 (NTC §4.2.4.1.3.1)
→ Si trascurano gli effetti dovuti ad instabilità
VERIFICATO

4.3 Verifica sismica impalcato

Il procedimento di calcolo eseguito per le verifiche sismiche sull'impalcato risulta il seguente: dopo aver calcolato la massa presente su una singola campata, è stata ricavata la forza dovuta al sisma avendo a disposizione l'accelerazione spettrale di riferimento. Per ipotesi la forza totale è stata poi divisa sui tre profili principali (HEA280 e HEB280), in particolare assegnando un carico doppio al profilo centrale.
Si è ricavato quindi uno schema di carico di trave su quattro appoggi, le cui reazioni vincolari sono state utilizzate per la verifica dei tiranti di controvento. Si sottolinea come non siano stati considerati i controventi soggetti a compressione, ma solo quelli a trazione.



MASSE PARTECIPANTI

- Lastra di camminamento	90 daN/m^2
- IPE180	40 daN/m^2
- HEA280	32 daN/m^2
- HEB 280	22 daN/m^2
- Controventi	6 daN/m^2
- Parapetto	25 daN/m^2
	215 daN/m^2

AREA IMPALCATO 7.0 m x 5.0 m = 35.0 m^2 → **MASSA TOT = 7525 daN**

ACCELERAZIONE SPETTRALE

- Fattore di struttura q = 1
- Accelerazione massima spettro 0.176 g

→ **FORZA TOT = 1324.4 daN**
Carico q = 47.3 daN/m
Carico 2q = 94.6 daN/m

ANALISI TRAVE CENTRALE HEB280

- Luce campate 2.35 m
- Carico 94.6 daN/m

→ **M_{ED_max} = 52.2 daNm**
V_{ED_max} = 133.4 daN → Sollecitazioni trascurabili ($M_{rd,z}$=24260daNm $T_{rd,z}$=196800 daN)

Reazione R_b = 244.5 daN
Angolo inclinazione α = 56°

→ **Azione assiale N = 294.9 daN**
Azione resistente N_{RD} = 27191 daN
VERIFICATO

4.4 Verifica collegamenti impalcato

4.4.1 Introduzione

Nel seguente paragrafo verranno svolte le verifiche dei collegamenti tra le varie parti strutturali, nel rispetto delle indicazioni fornite dalla normativa NTC '08 in riferimento ai dettami inseriti nel capitolo 4.

In particolare per le unioni con saldature a cordoni d'angolo, con riferimento all'altezza di gola 'a', la resistenza di progetto si determina attraverso la seguente formulazione (paragrafo §4.2.8.2.4):

$$\sqrt{\left(\sum \sigma_{\perp}\right)^2 + 3\left(\left(\sum \tau_{\perp}\right)^2 + \left(\sum \tau_{\parallel}\right)^2\right)} \leq \frac{f_{tk}}{\beta\, \gamma_{M2}}$$

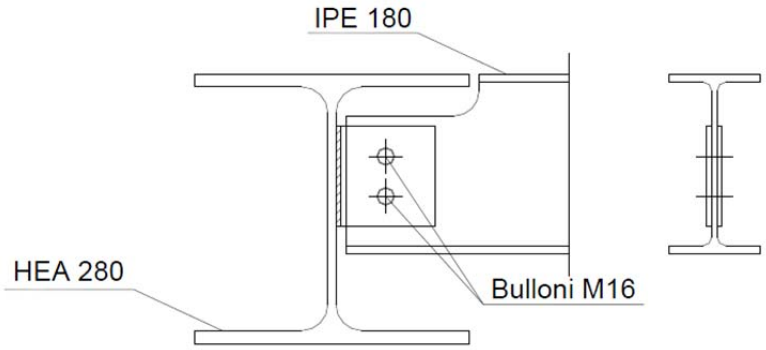
dove $\sigma_{\perp}, \tau_{\perp}, \tau_{\parallel}$ sono rispettivamente la tensione normale, tangenziale perpendicolare e tangenziale parallela all'asse del cordone d'angolo, f_{tk} è la resistenza a rottura del più debole degli elementi collegati, β è un coefficiente che assume valore pari a 0.80 per acciaio S235, 0.85 per acciaio S275 e 0.90 per acciaio S355, infine γ_{M2}=1.25.

Per quanto riguarda le unioni bullonate verranno effettuate le seguenti verifiche (paragrafo §4.2.8.1.1):

- Verifica a taglio $F_{v,Rd} = 0.6 * f_{tb} * A_{res}/\gamma_{M2}$ per bulloni di classe 8.8; f_{tb} rappresenta la resistenza a rottura del materiale, A_{res} l'area di calcolo;
- Verifica resistenza al rifollamento $F_{b,rd} = k * \alpha * f_{tu} * d * t/\gamma_{m2}$; d rappresenta il diametro del foro, t è lo spessore della piastra, f_{tk} la resistenza a rottura del materiale; considerando i bulloni presenti alla stregua di bulloni di bordo, risulta che $\alpha = \min\begin{cases} e_1/(3d_0) \\ f_{tb}/f_t \\ 1 \end{cases}$, mentre $k = \min\begin{cases} 2.8\frac{e_2}{d_0} - 1.7 \\ 2.5 \end{cases}$, con e_1 ed e_2 distanze dal bordo della piastra dei bulloni, d_0 diametro nominale del foro di alloggiamento del bullone, f_{tb} e f_t rispettivamente le resistenze del bullone e della piastra;

4.4.2 Verifica collegamento tipo

Si effettuano le verifiche relative al collegamento tipo, mostrato in figura. Le sollecitazioni di taglio di progetto sono state ricavate dal caso peggiore tra quelli studiati nei paragrafi precedenti, di conseguenza i risultati sono validi per tutti i collegamenti previsti.
T_{max} = 8200 daN



Verifica a taglio bulloni
Dati:

- Area resistente : A_{res} = 1.57 cm^2
- Acciaio bullone M8.8 : f_{tb} = 8000 daN/ cm^2
- N° bulloni: n = 2
- N° superfici di taglio per bullone: n_f = 2
- Resistenza a taglio bullone: $F_{v,Rd}$ = 6029 daN

→ **$F_{v,Rd}$ = 6029 daN**
$V_{ed\_bullone}$ = 2050 daN VERIFICATO

Verifica a rifollamento IPE180
Dati:

- Spessore : t = 0.53 cm
- Acciaio profilo S355 : f_{tk} = 5100 daN/cmq
- Distanza da bordo 1 : e_1 = 3.0 cm
- Distanza da bordo 2 : e_2 = 5.0 cm

→ α = 0.588 k = 2.50

→ **$F_{b,Rd}$ = 5088 daN**
V_{ed} = 4100 daN VERIFICATO

Verifica a rifollamento piastra di collegamento
Dati:

- Spessore : t = 0.5 cm

- Acciaio profilo S355 : f_{tk} = 5100 daN/cmq
- Distanza da bordo 1 : e_1 = 3.0 cm
- Distanza da bordo 2 : e_2 = 5.0 cm

→ α = 0.588 k = 2.50

→ **F_{b,Rd_TOT} = 4800 daN**
$V_{ed\_bullone}$ = 2050 daN VERIFICATO

Verifica saldatura piastra
Dati:

- Altezza di gola : a = 0.3 cm
- Lunghezza cordone: l =10 cm
- Acciaio S355 : f_{tk} = 5100 daN/cmq → β = 0.90
- N° cordoni: n = 3

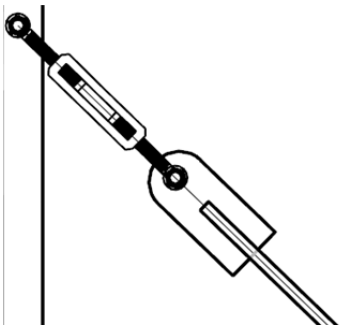
- Taglio agente su singolo cordone V_{ED} = 2735 daN
- Distanza tra punto applicazione taglio e saldatura 5.0 cm → M_{ED} = 137 daNm

→ $\tau_{\parallel}$ = 912 daN/cm^2
$\sigma_{\perp} = \tau_{\perp}$ =1938 daN/cm^2

→ Verifica **FS: 1.08**

4.4.3 Verifica collegamento controvento

Si effettuano le verifiche relative al collegamento dei controventi, mostrato in figura. Come sollecitazione di progetto è stato considerato il valore azione determinata dal sisma.
N_{RD} = 294.9 daN



Verifica saldatura piastra
Dati:

- Altezza di gola : a = 0.3 cm
- Lunghezza cordone: l =11 cm
- Acciaio S355 : f_{tk} = 5100 daN/cmq → β = 0.90
- N° cordoni: n = 4

→ $\tau_{\parallel}$ = 22.3 daN/cm^2
→ Verifica **FS: 117.4**

Verifica trazione piastra
Dati:

- Sezione piastra 10.0 cm x 1.0 cm
- Diametro foro 2.15 cm → Area netta 7.85 cm x 1.0 cm
  N_{rd} =26540 daN
  VERIFICATO

Verifica a taglio bulloni
Dati:

- Area resistente : A_{res} = 2.45 cm^2
- Acciaio bullone M8.8 : f_{tb} = 8000 daN/cm^2
- N° bulloni: n = 1
- N° superfici di taglio per bullone: n_f = 1
- Resistenza a taglio bullone: $F_{v,Rd}$ = 6029 daN

→ **$F_{v,Rd}$ = 6029 daN**
$V_{ed\_bullone}$ = 294.9 daN VERIFICATO

Verifica a rifollamento piastra di collegamento
Dati:

- Spessore : t = 1.0 cm

- Acciaio profilo S355 : f_{tk} = 5100 daN/cmq
- Distanza da bordo 1 : e_1 = 4.0 cm
- Distanza da bordo 2 : e_2 = 5.0 cm

→ α = 0.635 k = 2.50

→ **F_{b,Rd_TOT} = 12952 daN**

$V_{ed\_bullone}$ = 294.9 daN VERIFICATO

Verifica saldatura piastra collegamento profilo HE

Dati:

- Altezza di gola : a = 0.3 cm
- Lunghezza cordone: l =7 cm
- Acciaio S355 : f_{tk} = 5100 daN/cmq → β = 0.90
- N° cordoni: n = 2
- Angolo inclinazione forza α = 56°

→ $\tau_{\parallel}$ = 39.3 daN/cm^2

$\sigma_{\perp} = \tau_{\perp}$ =41.2 daN/cm^2

→ Verifica **FS: 42.4**

4.5 Appoggi neoprene

Gli appoggi in gomma armata sono stati progettati seguendo le disposizioni indicate nel catalogo Alga; in particolare è necessario conoscere i seguenti dati di input:

1. Valore massimo di azione verticale agente V_{Ed} ;
2. Valore massimo di azione orizzontale agente H_{Ed} ;
3. Valore massimo di spostamento s ;

Dall'analisi dei paragrafi precedenti si ricava un valore massimo di azione di compressione pari a:

→ Reazione massima all'appoggio **V_{Ed} = 13479 daN**

Per quanto riguarda il carico massimo orizzontale, è stato valutato l'effetto del sisma agente nella direzione perpendicolare all'asse del ponte; trascurando l'effetto dei controventi, si considera un asta di luce l=7.0 m, caricata con un carico q = 94.6 daN/m (vedi paragrafo azione sismica).

→ Reazione massima all'appoggio **H_{Ed} = 331.1 daN**

Inoltre dall'analisi della combinazione con variazione termica è scaturito un valore di spostamento massimo in corrispondenza dell'appoggio pari a **s = 2.38 mm**.

Noti i dati di input necessari, è possibile sfruttare il catalogo di riferimento per la scelta del prodotto più adatto; in particolare è necessario dapprima individuare la corretta combinazione di carico sfruttando il rapporto tra i carichi di progetto H_{Ed} e V_{Ed} : se il rapporto tra le forze risulta maggiore del 3% allora bisogna utilizzare i risultati forniti dalla cosiddetta Combo2 da catalogo, altrimenti si sfruttano i valori contenuti nella Combo1.

→ Rapporto **H_{Ed} / V_{Ed} = 2.4%** → Combo1

A questo punto è necessario calcolare i seguenti valori:

1. Carico orizzontale equivalente $H_{eq} = H_{Ed} + s * k_h$, con k_h rigidezza dell'elemento fornita dal catalogo
2. Spostamento orizzontale equivalente $s_{eq} = H_{Ed}/k_h + s$

Di seguito si riporta uno stralcio di catalogo con i valori del prodotto adottato:

DATA	Dimensioni			hg	Combo 1			Combo 2			Kh	W
	Ht	A	B		V	H	c*	V	H	c*		
	mm	mm	mm	mm	kN	kN	mm	kN	kN	mm	kN/mm	kG
NB 150x300xHt	21	150	300	10	1087	12	3,0	1029	61	15,0	4,05	3,0
	28	150	300	15	1225	11	4,0	1052	54	20,0	2,70	4,0
	35	150	300	20	1289	10	5,0	1039	51	25,0	2,03	5,0
	42	150	300	25	1231	10	6,0	1011	49	30,0	1,62	6,0
	49	150	300	30	1018	9	7,0	803	47	35,0	1,35	7,0
	56	150	300	35	865	9	8,0	655	46	40,0	1,16	8,0
	63	150	300	40	751	9	9,0	544	46	45,0	1,01	9,0
	70	150	300	45	662	9	10,0	458	45	50,0	0,90	10,0

L'appoggio in gomma scelto presenta le seguenti caratteristiche:

1. dimensioni in pianta 150 mm x 300 mm
2. altezza 28 mm
3. V_{Rd} 122500 daN

4. H_{Rd} 1100 daN
5. s^* 4.0 mm
6. k_h 270 daN/mm

Il valore del carico V_{ed} risulta pari a 13479 daN < 122500 daN, il valore del carico equivalente H_{eq} risulta pari a 973.7 KN < 1100 KN, mentre il valore dello spostamento equivalente s_{eq} risulta pari a 3.61 mm < 4.0 mm, pertanto le verifiche sono rispettate.

4.6 Tirafondi

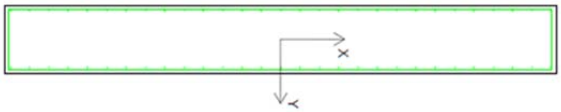
Per ipotesi, se la sollecitazione sismica agisse solo sulla trave principale centrale HEB280, si creerebbe un taglio all'appoggio pari a 3762.5 daN che, incrementato di un fattore di sicurezza pari a 1.5, risulterebbe pari a 5650 daN.
Si predispongono quattro tirafondi, aventi il compito di stabilizzare l'opera nei confronti delle azioni orizzontali.

- Tirafondo M20 Cl. 8.8
- Sezione resistente 245 mm^2
- Resistenza a taglio 9408 daN
- N° tirafondi 4

→ **Resistenza a taglio totale 37632 daN** VERIFICATO

4.7 Spalla

La spalla è stata armata con ferri verticali Φ14/20 e ferri orizzontali Φ10/20.



Per il pre-dimensionamento della spalla si tengono in conto quattro diverse condizioni di carico:

- Peso proprio e permanenti portati spalla ed impalcato
- Carico da folla agente su impalcato
- Spinta del terreno e sovraccarico a ridosso del manufatto
- Spinta idrostatica (scenario con tempo di ritorno T = 500 anni)

La spalla verrà studiata alla stregua di mensola incastrata alla base, con luce L= 5.30 m, sezione 5.74 m x 0.70 m.

Per le verifiche strutturali verranno considerate due condizioni di carico:

- Pesi propri e permanenti portati incrementati di un coefficiente secondo normativa + carico da folla sul ponte ed a ridosso del ponte + spinta terreno
- Pesi propri e permanenti portati moltiplicati per un coefficiente unitario + spinta terreno + spinta idrostatica

CONDIZIONI DI CARICO
PESI IMPALCATO g1 + g2

- Lastra di camminamento	90 daN/m^2
- IPE180	40 daN/m^2
- HEA280	32 daN/m^2
- HEB 280	22 daN/m^2
- Controventi	6 daN/m^2
- Parapetto	25 daN/m^2
	215 daN/m^2

Area influenza spalla 3.5 m x 5.0 m = 17.5 m^2

Peso spalla 53240 daN

→ Scenario A **γ = 1.35**
N = 76953.4 daN

Scenario B **γ = 1.0**
N = 57002.5 daN

CARICO DA FOLLA IMPALCATO

- Carico da folla 1000 daN/m^2

Area influenza spalla 3.5 m x 5.0 m = 17.5 m^2

→ Scenario A **γ = 1.35**
N = 23625 daN

Scenario B **γ = 0**
N = 0.0 daN

SPINTA TERRENO

- Peso specifico terreno 1700 daN/m^3
- Angolo di attrito 30° (coefficiente di spinta attiva k_a = 0.333)
→ Pressione terreno alla base spalla 3000 daN/m^2
- Sovraccarico → Pressione terreno alla base spalla 330 daN/m^2

→ Scenario A **$\gamma_{terreno}$ = 1.35 ; $\gamma_{sovraccarico}$ = 1.35**
T_x = 75943.2 daN
M_x = 146593.1 daNm

Scenario B **$\gamma_{terreno}$ = 1.35 ; $\gamma_{sovraccarico}$ = 0**
T_x = 62248.5 daN
M_x = 120347.1 daNm

SPINTA ACQUA

- Altezza tirante idraulico 4.68 m
- Peso specifico acqua 1100 daN/m^3

→ Scenario A **γ_{acqua} = 0.0**
T_y = 0.0 daN
M_y = 0.0 daNm

Scenario B **γ_{acqua} = 1.5**
T_y = 65050.1 daN
M_y = 101478.2 daNm

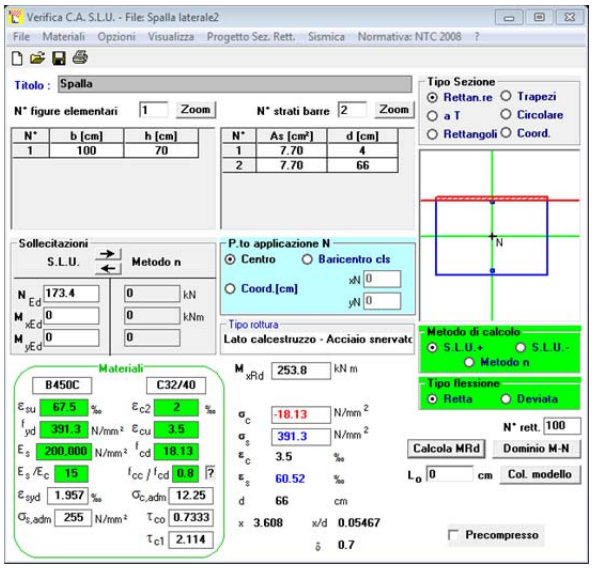
<u>SOLLECITAZIONI TOTALI</u>

SCENARIO A → N = 100578.4 daN
T_x = 75943.2 daN
M_x = 146593.1 daNm

T_y = 0.0 daN
M_y = 0.0 daNm

Resistenza a compressione f_{cd} = 181.3 daN/cm^2
Area resistente A_{res} = 39900 cm^2 → N_{rd} = 72338700 daN VERIFICATO

Il momento resistente rispetto all'asse X è stato valutato con il programma VCA_Slu, considerando una sezione di lunghezza unitaria ed altezza pari a 70 cm, pari allo spessore della spalla, soggetta ad azione assiale pari a 100578.4 daN / 5.8 m = 17341.1 daN/m. Il momento flettente resistente risulta pari a 25380 daNm/m, a fronte di un momento M_x = 146593 daNm /5.8 m = 25274.6 daNm/m.



VERIFICA TAGLIO

$V_{MAX} = \sqrt{V_x^2 + V_y^2}$ = 75943.2 daN

k_x = 1.55

v_{min} = 0.38 → V_{Xrdc} = 144039 daN

V_{max} / V_{xrd} = 1.89 VERIFICATO

SCENARIO B → N = 57002.5 daN
T_x = 62248.5 daN
M_x = 120347.1 daNm
T_y = 65050.1 daN
M_y = 101478.2 daNm

VERIFICA FLESSIONE DEVIATA
Momento resistente M_{xrd} = 22940 daNm/m x 5.8 m = 133052 daNm
Momento resistente M_{yrd} = 1158200 daNm

$M_{xed} / M_{xrd} + M_{yed} / M_{yrd}$ = 0.991 VERIFICATO

VERIFICA TAGLIO

$V_{MAX} = \sqrt{V_x^2 + V_y^2}$ = 90035.5 daN

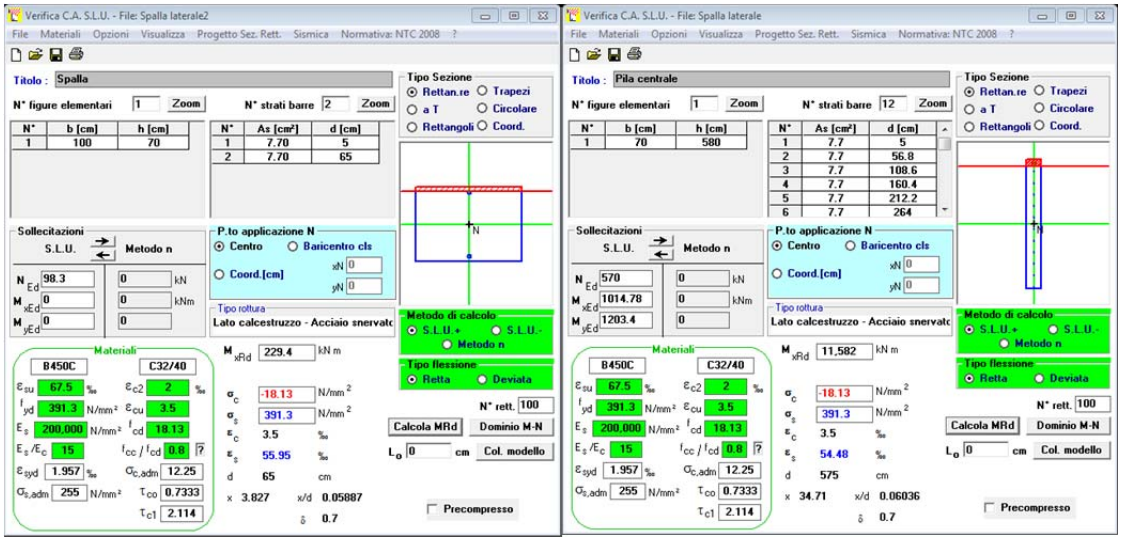
k_x = 1.55

v_{min} = 0.38 → V_{Xrdc} = 144039 daN

k_y = 1.18

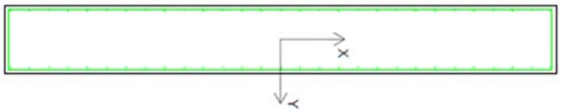
v_{min} = 0.25 → V_{yrdc} = 102148 daN

V_{max} / min(V_{xrd} ; V_{yrd})= 1.13 VERIFICATO



4.8 Pila centrale

La pila centrale è stata armata con ferri verticali Φ14/20 e ferri orizzontali Φ10/20.



Per il pre-dimensionamento della pila si tengono in conto tre diverse condizioni di carico:

- Peso proprio e permanenti portati spalla ed impalcato
- Carico da folla agente su impalcato
- Spinta idrostatica (scenario con tempo di ritorno T = 200 anni)

La pila verrà studiata alla stregua di mensola incastrata alla base, con luce L= 5.30 m, sezione 5.74 m x 1.00 m.

Per le verifiche strutturali verranno considerate due condizioni di carico:

- Pesi propri e permanenti portati incrementati di un coefficiente secondo normativa + carico da folla
- Pesi propri e permanenti portati moltiplicati per un coefficiente unitario + spinta idrostatica

CONDIZIONI DI CARICO
PESI IMPALCATO g1 + g2

- Lastra di camminamento	90 daN/m^2
- IPE180	40 daN/m^2
- HEA280	32 daN/m^2
- HEB 280	22 daN/m^2
- Controventi	6 daN/m^2
- Parapetto	25 daN/m^2
	215 daN/m^2

Area influenza spalla 7.0 m x 5.0 m = 35.0 m^2

Peso pila 76055 daN

→ Scenario A **γ = 1.35**
N = 112833 daN

Scenario B **γ = 1.0**
N = 83580 daN

CARICO DA FOLLA IMPALCATO

- Carico da folla 1000 daN/m^2

Area influenza spalla 7.0 m x 5.0 m = 35.0 m^2

→ Scenario A **γ = 1.35**
N = 47250 daN

Scenario B **γ = 0**
N = 0.0 daN

SPINTA ACQUA

- Altezza tirante idraulico 4.30 m
- Peso specifico acqua 1100 daN/m^3

→ Scenario A **γ_{acqua} = 0.0**
T_y = 0.0 daN
M_y = 0.0 daNm

Scenario B **γ_{acqua} = 1.5**
T_y = 109830.6 daN
M_y = 157423.9 daNm

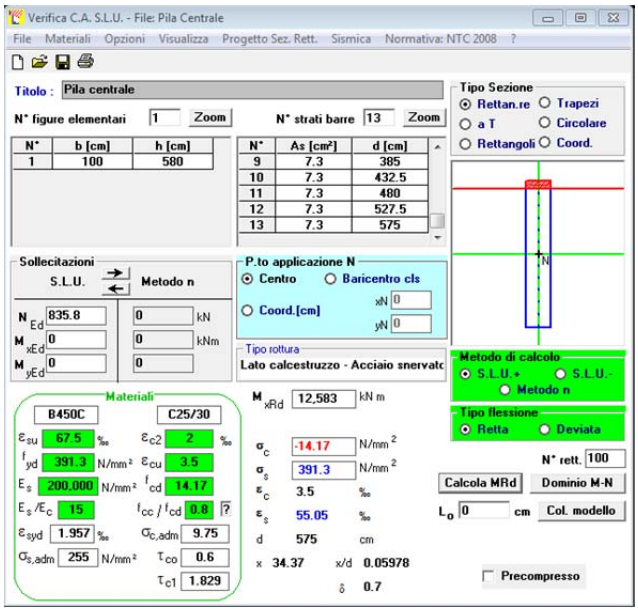
SOLLECITAZIONI TOTALI

SCENARIO A → N = 160083 daN
T_x = 0.0 daN
M_x = 0.0 daNm
T_y = 0.0 daN
M_y = 0.0 daNm

Resistenza a compressione f_{cd} = 181.3 daN/cm^2
Area resistente A_{res} = 57000 cm^2 → N_{rd} = 10334100 daN VERIFICATO

SCENARIO B → N = 83580 daN
T_x = 0.0 daN
M_x = 0.0 daNm
T_y = 109830.6 daN
M_y = 157423.9 daNm

VERIFICA FLESSIONE
Momento resistente M_{yrd} = 1258300 daNm
M_{yed} / M_{yrd} = 0.12 VERIFICATO



VERIFICA TAGLIO

$V_{MAX} = \sqrt{V_x^2 + V_y^2}$ = 109830.6 daN

k_y = 1.18

v_{min} = 0.25 → V_{yrdc} = 145000 daN

V_{max} / V_{xrd} = 1.33 VERIFICATO

4.9 Fondazione

4.9.1 Introduzione

La fondazione, essendo sostenuta da un sistema di pali, è stata studiata alla stregua di trave in semplice appoggio soggetta ad un carico distribuito, dovuto al peso proprio ed al carico massimo di acqua raggiungibile, stimato in 5.8 m. L'armatura inserita risulta la seguente: lembo inferiore Φ14/20 in entrambe le direzioni, lembo superiore Φ14/20 in entrambe le direzioni.

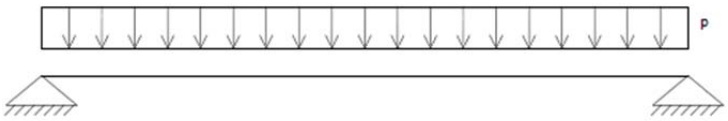
4.9.2 Calcoli

Dati generali

- Luce l = 2.45 m
- Interasse i = 1.00 m
- Sezione 1.00 m x 1.00 m
- Schema statico trave in semplice appoggio
- Azioni resistenti di progetto M_{RD} = 25741 daNm/m

k = 1.46
v_{min} = 0.35 → V_{rdc} = 33181 daN/m

Caso 1: peso proprio + peso acqua



- Carico g_{1_SLE} 2500 daN/m
- Coefficiente γ_{g1} 1.35 → g_{1_SLU} = 3375 daN/m

- Carico q_{acqua_SLE} 6380 daN/m
- Coefficiente γ_q 1.5 → q_{SLU} = 9570 daN/m

$q_{tot\ SLU}$ = 12945 daN/m

M_{ED} = 9712 daNm VERIFICATO
T_{ED} = 15857.6 daN VERIFICATO

4.10 Pali

4.10.1 Introduzione

L'analisi della palificata è stata svolta facendo affidamento su un foglio di calcolo opportunamente sviluppato per le verifiche strutturali e geotecniche di fondazioni profonde.
L'iter seguito per le verifiche è stato il seguente:

A) Inserimento dei parametri del terreno definiti tramite analisi MASW, per la determina dell'effetto di interazione cinematica sul palo dovuto al passaggio da uno strato all'altro di terreno;
B) Inserimento delle sollecitazioni di progetto: quest'ultime sono state ricavate da un apposito modello tridimensionale agli elementi finiti, inserendo le condizioni di carico descritte nei paragrafi precedenti. In particolare nel modello, ai nodi in corrispondenza della posizione dei pali, sono stati assegnati vincoli di tipo incastro, quindi in fase di post-processor, nel foglio di calcolo sui pali, sono state inserite le combinazioni di reazioni vincolari tali per cui risultasse:
    - N_{MAX}, con i relativi momenti M_x e M_y
    - N_{MIN}, con i relativi momenti M_x e M_y
    - Massima media geometrica tra M_x e M_y, con la relativa azione assiale N
    - Minima media geometrica tra M_x e M_y, con la relativa azione assiale N
    - Massima media geometrica tra V_x e V_y, con la relativa azione assiale N
    - Inserimento dei dati geometrici relativi alla palificata (dimensioni in pianta, interassi ecc.), questo per permettere al programma, nel caso venisse richiesta un'analisi globale della palificata e non solo sul singolo palo, di determinare la ripartizione delle azioni globali esterne, inserite nel precedente paragrafo;
C) Verifiche strutturali a presso/tenso – flessione ed a taglio, con inserimento delle caratteristiche geometriche del palo, tipo di materiali utilizzati, armature longitudinali e trasversali per determinare le resistenze di progetto;
D) Verifica strutturale a stabilità laterale del palo, con inserimento di coefficienti di reazione laterale per simulare l'effetto stabilizzante del terreno;
E) Verifica geotecnica per portanza trasversale del terreno per terreni coerenti o incoerenti;
F) Verifica geotecnica per portanza verticale del terreno per terreni coerenti o incoerenti;
G) Verifiche geotecniche di gruppo, ovvero considerando l'intera palificata;
H) Verifiche SLE nei riguardi di spostamenti limite traversali e verticali;

4.10.2 Analisi

Si riportano ora i calcoli effettuati con i relativi risultati per ciascuno dei punti precedentemente descritti.

A) Si considera l'azione cinematica, cioè l'effetto dovuto al passaggio tra uno strato di terreno e l'altro; inserendo i dati relativi alle caratteristiche del singolo palo (diametro 0.80 m, lunghezza 14 m, modulo elastico 33350 MPa) e relativi alle caratteristiche dei terreni attraversati, ricavati dalle prove MASW, si ricava un valore di momento di

interazione cinematica, per terreno catalogato di tipo C e seguendo le indicazioni del modello di Nikolaou et Alt, pari a 13908 daNm. Questo valore sarà utilizzato nelle verifiche strutturali successive.

Si considera l'interazione cinematica (M) ?	**si**
d = diametro palo= **m**	**0.80**
L = lunghezza palo= **m**	**14.00**
E_p = modulo elastico di rigidezza assiale del palo= **N/mmq**	**33,350.00**
STRATO 1	
tipo strato:	**-**
h_1 = altezza strato= **m**	**15.00**
$V_{S,1}$ = velocità delle onde di taglio= **m/s**	**127.00**
ρ_1 = densità (massa per unità di volume)= **kN s^2 / m^4**	**17.50**
ν_1 = coeff. di poisson=	**0.20**
STRATO 2	
tipo strato:	
h_2 = altezza strato= **m**	**18.20**
$V_{S,2}$ = velocità delle onde di taglio= **m/s**	**329.00**
ρ_2 = densità (massa per unità di volume)= **kN s^2 / m^4**	**25.00**
ν_2 = coeff. di poisson=	**0.23**
ACCELERAZIONE SISMICA DEL SITO	
a_g/g = (accelerazione massima attesa su sito di riferimento rigido) / g =	**0.065**
F_o = fattore amplif. spettrale massima, su sito di rif. rigido (se F_o< 2,2 occorre adottare 2,2) =	**2.664**
$V_{s,30} = V_{s,1}$ = m/s	127.00
Categoria di sottosuolo di progetto =	**C**
A: S_S=	1.000
B: S_S=	1.200
C: S_S=	1.500
D: S_S=	1.800
E: S_S=	1.600
S_S = effetto amplificazione stratigrafica sul sottosuolo in progetto:	1.500
Categoria topografica in progetto =	**T1**
S_T= effetto dell'amplificazione topografica (1,0 se T1; 1,2 se T2; 1,2 se T3; 1,4 se T4)=	1.000
$S = S_S S_T$=	1.500
Accelerazione massima al sito / g = $a_{max}/g = S\, a_g/g$ =	0.098
Accelerazione massima al sito = $a_{max}= (S\, a_g/g)$ g = m/sec^2	0.956
G_1 =Modulo di taglio dello strato 1 = $\rho_1 V_{s,1}^2$ = N/mmq	282.26
E_1 = Modulo di Young dello strato 1= 2 (1 + ν_1) G_1 = N/mmq	677.42
G_2 =Modulo di taglio dello strato 1 = $\rho_2 V_{s,2}^2$ = N/mmq	2,706.03
E_2 = Modulo di Young dello strato 1= 2 (1 + ν_2) G_2 = N/mmq	6,656.82
Rapporto di snellezza = L/d =	17.50
J_p = Momento di inerzia del palo = $\pi\, d^4 / 64$ = m^4	0.0201
E_p / E_1 =	49.23
L_a = Lunghezza attiva = 1,5 d $(E_p / E_1)^{0,25}$ =	3.18
$h_1 > L_a$?	si
(L'equazione a seguire per M è valida a rigore quando $h_1 > L_a$; ovvero quando l'interfaccia tra	
i due strati si trova a una profondità superiore alla Lunghezza attiva del palo)	
$V_{s,2} / V_{s,1}$ =	2.59
τ_c =Tensione di taglio all'interfaccia (contatto) tra i due strati = $a_{max}\, \rho_1\, h_1$ = kN/mq	251.07
Momento all'interfaccia (contatto) tra i due strati in condizioni di moto stazionario:	
$M = 0{,}042\, \tau_c\, d^3\, (L/d)^{0,30}\, (E_p/E_1)^{0,65}\, (V_{s,2}/V_{s,1})^{0,50}$ = kNm	258.16
VALUTAZIONE DEL FATTORE δ DI RIDUZIONE DEL MOMENTO	
funzione del numero di cicli effettivi e del periodo dominante dell'accelerogramma	
Valutazione 1) per δ:	
N_c = n.o di cicli effettivi dell'accelerogramma=	**-**
Periodo naturale del deposito prossimo ai periodi predominanti dell'eccitaz. sismica:	
$\delta = 0{,}04\, N_c + 0{,}23$=	0.23
Periodo naturale del deposito che si allontana dai periodi predominanti dell'eccitaz. sismica:	
$\delta = 0{,}015\, N_c + 0{,}17$=	0.17
δ scelto in base ai due valori calcolati =	**-**
Valutazione 2) per δ:	
δ nel campo dei valori frequenti (variabile in genere tra 0,17 e 0,50); risulta **δ =**	**0.50**
Valutazione adottata per δ=	**2)**
$\delta = \delta$ adottato=	0.50
M_{CIN} = Momento cinematico all'interfaccia tra i 2 strati (NIKOLAOU et Alt., 2001)= δ M = kNm	129.08
τ_{ff} = tensione tangenziale all'interfaccia da analisi di free-field= kN/mq	**-**
M_{CIN} = Momento cinematico all'interfaccia tra i 2 strati (MAIORANO et Alt., 2009):	
$0{,}071\, \tau_{ff}\, d^3\, (L/d)^{0,30}\, (E_p/E_1)^{0,65}\, (V_{s,2}/V_{s,1})^{0,50}$ = kNm	-
Valore adottato per M_{CIN}=	**NIKOLAOU et Alt 2001**
M_{CIN} = Momento cinematico all'interfaccia tra i 2 strati = valore adottato= kNm	129.08
M_{INERZ} (su monopalo o singolo palo della palificata) **= kNm**	**10.00**
Moto cinematico e inerziale: in fase oppure sfasati?	**fase**
M_{RIS} = Momento risultante (su monopalo o singolo palo della palificata) = kNm	139.08

B) Inserimento delle azioni sollecitanti: nel caso di analisi del singolo palo sono state analizzate le reazioni vincolari ottenute da un modello ad elementi finiti, la cui relazione risulta allegata. Di tutte le combinazioni sono state ricavate le situazioni peggiori come precedentemente descritto. Si riporta uno schema riassuntivo dei risultati ottenuti.

TOTALE	SLU									
Nodo	CC	Rx	Ry	Rz MAX	Mx	My	Mz	Rz MAX	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daN>	<daNm>	<daN>
-121.00	18	55.11	25525.8	126569.00	-2387.20	52.01	16.69	126569.00	2387.77	25525.86
Nodo	CC	Rx	Ry	Rz MIN	Mx	My	Mz	Rz MIN	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daN>	<daNm>	<daN>
-41.00	5	3176.85	-1516.58	20210.38	667.33	2701.15	-75.66	20210.38	2782.36	3520.28
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MAX (Mx^2+My^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-121.00	11	6944.77	-1971.82	60597.53	-456.46	19243.75	48.54	19249.16	19249.16	7219.27
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MIN (Mx^2+My^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-198.00	8	4514.12	-419.86	48915.72	-3.50	-26.99	30.69	27.22	27.22	4533.60
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MAX (Vx^2+Vy^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-196.00	18	1.35	43859.5	90457.80	-2280.27	5.95	1.80	43859.50	2280.28	43859.50
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MIN (Vx^2+Vy^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-38.00	8	2.7	-61.94	28959.69	354.70	453.66	-4.14	62.00	575.86	62.00
TOTALE	SLE									
Nodo	CC	Rx	Ry	Rz MAX	Mx	My	Mz	Rz MAX	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daN>	<daNm>	<daN>
-121.00	20	37.5	16962.6	88989.50	-1623.02	35.91	11.43	88989.50	1623.42	16962.64
Nodo	CC	Rx	Ry	Rz MIN	Mx	My	Mz	Rz MIN	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daN>	<daNm>	<daN>
-326.00	23	1404.7	603.12	22353.80	-1810.28	2363.33	14.94	22353.80	2976.99	1528.70
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MAX (Mx^2+My^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-117.00	21	-7150.41	6335.84	46194.00	-1144.10	-7716.75	-25.90	7801.10	7801.10	9553.60
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MIN (Mx^2+My^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-323.00	21	143.58	4678.09	36142.40	-134.23	16.68	-3.56	135.26	135.26	4680.29
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MAX (Vx^2+Vy^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-196.00	20	0.92	29145.7	64810.90	-1511.95	4.08	1.23	29145.70	1511.96	29145.70
Nodo	CC	Rx	Ry	Rz	Mx	My	Mz	MIN (Vx^2+Vy^2)^0.5	(Mx^2+My^2)^0.5	(Vx^2+Vy^2)^0.5
		<daN>	<daN>	<daN>	<daNm>	<daNm>	<daNm>	<daNm>	<daNm>	<daN>
-323.00	22	-0.19	452.07	26611.20	-1411.48	0.12	0.03	452.07	1411.48	452.07

Infine sono state valutate anche le sollecitazioni globali agenti sul manufatto, in modo da poter eseguire anche un'analisi globale della palificata; in particolare sono stati valutati i pesi verticali agli SLU e SLE oltre alle spinte dovute all'acqua nei diversi scenari con tempo di ritorno differente, ottenendo così le situazioni peggiori a livello di sollecitazioni. Anche in questo caso si riporta uno schema riassuntivo di calcolo

SPINTA ACQUA						SPINTA ACQUA			
SCENARIO T=200						SCENARIO T=500			
γw	1000.00	daN/mc				γw	1000.00	daN/mc	
γq	1.10	-				γq	1.10	-	
h	4.30	m				h	4.68	m	
l_pila	7.20	m				l_pila	3.60	m	
l_spalla	3.60	m				l_spalla	3.60	m	
Z [m]	**σw [daN/mq]**	**SPINTA_pila [daN]**	**SPINTA_spalla [daN]**			**Z [m]**	**σw [daN/mq]**	**SPINTA_pila [daN]**	**SPINTA_spalla [daN]**
0.00	0.00	732.20	366.10			0.00	0.00	433.67	433.67
0.43	473.00					0.47	514.80		
0.86	946.00	5857.63	2928.82			0.94	1029.60	3469.34	3469.34
1.29	1419.00					1.40	1544.40		
1.72	1892.00	11715.26	5857.63			1.87	2059.20	6938.68	6938.68
2.15	2365.00					2.34	2574.00		
2.58	2838.00	17572.90	8786.45			2.81	3088.80	10408.02	10408.02
3.01	3311.00					3.28	3603.60		
3.44	3784.00	23430.53	11715.26			3.74	4118.40	13877.36	13877.36
3.87	4257.00					4.21	4633.20		
4.30	4730.00	13911.88	6955.94			4.68	5148.00	8239.68	8239.68

Carichi gravitazionali	**SLU**	**SLE**
	daN	daN
Impalcato g1	9925.00	7350.00
Impalcato g2	8505.00	6300.00
Spalla	73875.00	54725.00
Pila	105540.00	78175.00
Fondazione	543715.00	402750.00
Pali	665000.00	492660.00
Acqua fissa	604125.00	402750.00
Folla	94500.00	70000.00
Acqua piena	676620.00	451080.00

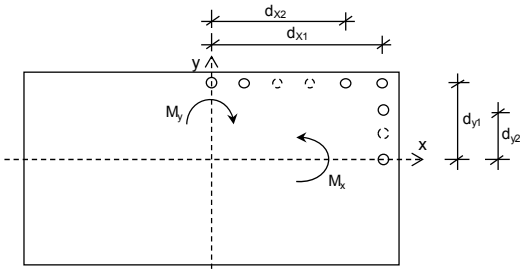
Carichi orizzontali	**SLU**	**SLE**	H [m]
Spinta piena 200	219665.00	146445.00	1.43
Spinta piena 500	130100.00	86740.00	1.56

Comb. 1	**g1+g2**			
	SLU		SLE	
	N [daN]	2084560.00	N [daN]	1499435.00
	Mx [daNm]	0.00	Mx [daNm]	0.00
	My [daNm]	0.00	My [daNm]	0.00
	T [daN]	0.00	T [daN]	0.00
Comb. 2	**g1+g2+folla**			
	SLU		SLE	
	N [daN]	2179060.00	N [daN]	1569435.00
	Mx [daNm]	0.00	Mx [daNm]	0.00
	My [daNm]	0.00	My [daNm]	0.00
	T [daN]	0.00	T [daN]	0.00
Comb. 3	**g1+g2+piena200**			
	SLU		SLE	
	N [daN]	2761180.00	N [daN]	1950515.00
	Mx [daNm]	314853.17	Mx [daNm]	209904.50
	My [daNm]	0.00	My [daNm]	0.00
	T [daN]	219665.00	T [daN]	146445.00
Comb. 4	**g1+g2+piena500**			
	SLU		SLE	
	N [daN]	2761180.00	N [daN]	1950515.00
	Mx [daNm]	202956.00	Mx [daNm]	135314.40
	My [daNm]	0.00	My [daNm]	0.00
	T [daN]	130100.00	T [daN]	86740.00

Si riporta quindi il foglio di calcolo relativo all'inserimento delle sollecitazioni su mono palo e su palificata.

Sollecitazioni su mono-Palo o Palificata ?		**mono-Palo**			
1) PER VERIFICHE SLU					
				Coefficienti parziali Azioni (A1, A2)	
				perm. γ_G (se fav.)	var. γ_Q (se fav.)
SLU: combinazioni NON SISMICHE tipo: $\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \Sigma_{i>1,n} (\gamma_{Qi} \psi_{oi} Q_{ki})$					
App. 1	Comb. 1 (STR): A1+M1+R1			1,30 (1,00)	1,50 (0,00)
	Comb. 2 (GEO) : A2+M1+R2			1,00 (1,00)	1,30 (0,00)
App. 2	Comb. unica (STR, GEO) : A1+M1+R3			1,30 (1,00)	1,50 (0,00)
SLU: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_j (\psi_{2j} Q_{kj})$					
App. 1	Comb. 1 (STR): A1+M1+R1			1.00	1.00
	Comb. 2 (GEO) : A2+M1+R2			1.00	1.00
App. 2	Comb. unica (STR, GEO) : A1+M1+R3			1.00	1.00
Approccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)		**2**			
			mono-Palo		Palificata
			Verifiche SLU_STR	Verifiche SLU_GEO	Verifiche SLU_STR	Verifiche SLU_GEO
Relativa Comb. associata all'Approccio scelto:			unica	unica	unica	unica
All'interno dell'app. scelto, riportare, per la comb. associata, i valori a seguire:						
Ai fini di SLU_STR_(N,M); resistenza SLU (N,M) dei pali						
N compressione (+), tra terne non sismiche e sismiche			Verifiche SLU_STR		Verifiche SLU_STR	
	$N=N_{min}$= kN		**378.05**		**20,845.60**	
	M_x = kNm		**6.67**		**-**	
	M_y = kNm		**27.01**		**-**	
	$N=N_{max}$= kN		**1,503.19**		**27,611.80**	
	M_x = kNm		**- 23.87**		**3,148.53**	
	M_y = kNm		**0.52**		**-**	
	N= kN		**726.65**		**27,611.80**	
$\{ (M_x^2 + M_y^2)^{1/2} \} = min$	**M_x = kNm**		**- 0.03**		**2,029.56**	
	M_y = kNm		**- 0.27**		**-**	
	N= kN		**843.47**		**27,611.80**	
$\{ (M_x^2 + M_y^2)^{1/2} \} = max$	**M_x = kNm**		**- 4.56**		**3,148.53**	
	M_y = kNm		**192.43**		**-**	
N trazione (-), tra terne non sismiche e sismiche			Verifiche SLU_STR		Verifiche SLU_STR	
	$N=N_{min}$= kN		-		-	
	M_x = kNm		-		-	
	M_y = kNm		-		-	
	$N=N_{max}$= kN		-		-	
	M_x = kNm		-		-	
	M_y = kNm		-		-	
	N= kN		-		-	
$\{ (M_x^2 + M_y^2)^{1/2} \} = min$	**M_x = kNm**		-		-	
	M_y = kNm		-		-	
	N= kN		-		-	
$\{ (M_x^2 + M_y^2)^{1/2} \} = max$	**M_x = kNm**		-		-	
	M_y = kNm		-		-	
Interazione cinematica			Verifiche SLU_STR		Verifiche SLU_STR	
M_{CIN} (su monopalo o singolo palo della palificata) = kNm			129.08		129.08	
M_{INERZ} (su monopalo o singolo palo della palificata) = kNm			10.00		10.00	
M_{RIS} (su monopalo o singolo palo della palificata) = kNm			139.08		139.08	
N (tra le combinazioni SLU_STR sismiche)= kN			**891.46**		**14,994.00**	
M_x = kNm					**-**	
M_y = kNm					**-**	
Ai fini di SLU_STR_(V); resistenza SLU a Taglio dei pali			Verifiche SLU_STR		Verifiche SLU_STR	
V tra combin. non sismiche e sismiche = max $\{ (V_x^2 + V_y^2)^{1/2} \}$ = kN			**438.59**		**2,196.65**	
Ai fini di SLU_STR_(N)_st_eq_el; stab. equilibrio elastico dei pali			Verifiche SLU_STR		Verifiche SLU_STR	
N= N di compressione (+) = kN			**1,503.19**		**27,611.80**	
M_x = kNm					**3,148.53**	
M_y = kNm					**-**	
Ai fini di SLU_GEO_qlim_trasv_t_c e SLU_GEO_qlim_trasv_t_i: portanza limite SLU trasversale				Verifiche SLU_GEO		Verifiche SLU_GEO
V tra combin. non sismiche e sismiche = kN				**438.59**		**2,196.65**
M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rdi} calcolato per						
a) N=0				-		-
b) N associato alla combinazione in cui opera V : N= kN				**1,142.07**		**27,611.80**
M_x = kNm						**3,148.53**
M_y = kNm						**-**
Ai fini di SLU_GEO_qlim_vert: portanza limite SLU verticale				Verifiche SLU_GEO		Verifiche SLU_GEO
N= N di compressione (+) tra terne non sismiche e sismiche= kN				**1,503.19**		**27,611.80**
M_x = kNm						**3,148.53**
M_y = kNm						**-**
N= N di trazione (-) tra terne non sismiche e sismiche= kN				-		-
M_x = kNm						-
M_y = kNm						-
Ai fini di SLU_GEO_Grup: portanze limiti SLU palificata per effetto di gruppo						Verifiche SLU_GEO
V tra combin. non sismiche e sismiche = kN						2,196.65
Valore (utente) = kN						-
Valore adottato = kN						2,196.65
N= N di compressione (+) tra terne non sismiche e sismiche= kN						27,611.80
Valore (utente) = kN						-
Valore adottato = kN						27,611.80
2) PER VERIFICHE SLE						
SLE: combinazioni NON SISMICHE tipo QUASI PERM. $G_1 + G_2 + \psi_{21} Q_{k1} + \Sigma_i (\psi_{2i} Q_{ki})$: per SLE combinazioni non sismiche, di regola solo questa per cedimenti e spostamenti						
SLE: combinazioni NON SISMICHE tipo FREQUENTE $G_1 + G_2 + \psi_{11} Q_{k1} + \Sigma_i (\psi_{2i} Q_{ki})$						
SLE: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_i (\psi_{2i} Q_{ki})$						
			mono-Palo		Palificata	
Riportare, per le comb. considerate i valori a seguire:						
Ai fini di SLE_ced_vert: cedimento max SLE verticale			Verifiche SLE		Verifiche SLE	
N= N di compressione (+) = kN			**889.89**		**19,505.15**	
M_x = kNm					**2,099.04**	
M_y = kNm					**-**	
Ai fini di SLE_sp_trasv: spostamento max SLE trasversale			Verifiche SLE		Verifiche SLE	
V tra combin. non sismiche e sismiche: V = max $\{ (V_x^2 + V_y^2)^{1/2} \}$ = kN			**291.45**		**1,464.45**	

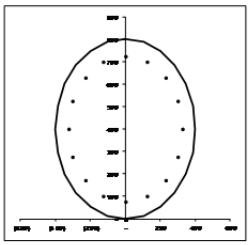
C) Vengono inseriti i dati per la distribuzione spaziale dei pali, in modo da ottenere le sollecitazioni agenti sui singoli elementi nel caso di verifiche globali.

Distribuzione dei pali nella palificata ?		uniforme
DISTRIBUZIONE UNIFORME E SIMMETRICA RISPETTO AI DUE ASSI DEI PALI NELLA PALIFICATA		
		
n_{px}= numero pali su una fila in direzione x :		7.00
n_{py}= numero pali su una fila in direzione y :		4.00
n_p = n.o totale pali della palificata =		28.00
d_{y1} = distanza asse x 1ª fila di pali = m		8.05
d_{y2} = distanza asse x 2ª fila di pali = m		5.65
d_{y3} = distanza asse x 3ª fila di pali = m		2.40
d_{y4} = distanza asse x 4ª fila di pali = m		-
d_{y5} = distanza asse x 5ª fila di pali = m	-	2.40
d_{y6} = distanza asse x 6ª fila di pali = m	-	5.65
d_{y7} = distanza asse x 7ª fila di pali = m	-	8.05
d_{y8} = distanza asse x 8ª fila di pali = m		-
d_{y9} = distanza asse x 9ª fila di pali = m		-
d_{y10} = distanza asse x 10ª fila di pali = m		-
d_{x1} = distanza asse y 1ª fila di pali = m		3.60
d_{x2} = distanza asse y 2ª fila di pali = m		1.20
d_{x3} = distanza asse y 3ª fila di pali = m	-	1.20
d_{x4} = distanza asse y 4ª fila di pali = m	-	3.60
d_{x5} = distanza asse y 5ª fila di pali = m		-
d_{x6} = distanza asse y 6ª fila di pali = m		-
d_{x7} = distanza asse y 7ª fila di pali = m		-
d_{x8} = distanza asse y 8ª fila di pali = m		-
d_{x9} = distanza asse y 9ª fila di pali = m		-
d_{x10} = distanza asse y 10ª fila di pali = m		-
d_{x11} = distanza asse y 11ª fila di pali = m		-
d_{x12} = distanza asse y 12ª fila di pali = m		-
d_{x13} = distanza asse y 13ª fila di pali = m		-
d_{x14} = distanza asse y 14ª fila di pali = m		-
d_{x15} = distanza asse y 15ª fila di pali = m		-
d_{x16} = distanza asse y 16ª fila di pali = m		-
d_{x17} = distanza asse y 17ª fila di pali = m		-
d_{x18} = distanza asse y 18ª fila di pali = m		-
d_{x19} = distanza asse y 19ª fila di pali = m		-
d_{x20} = distanza asse y 20ª fila di pali = m		-
$d_{ymax} = d_{y1}$ = m		8.05
d_{ymax} = m		-
d_{ymax} (adottato)= m		8.05
$d_{xmax} = d_{x1}$ = m		3.60
d_{xmax} = m		-
d_{xmax} (adottato)= m		3.60
$\Sigma_i d_{yi}^2 = d_{y1}^2 n_{px} 2 + d_{y2}^2 n_{px} 2 + \ldots + d_{y10}^2 n_{px} 2$ = mq		2,869.58
$\Sigma_i d_{yi}^2$ = mq		-
$\Sigma_i d_{yi}^2$ (adottato)= mq		2,869.58
$\Sigma_i d_{xi}^2 = d_{x1}^2 n_{py} 2 + d_{x2}^2 n_{py} 2 + \ldots + d_{x20}^2 n_{py} 2$ = mq		230.40
$\Sigma_i d_{xi}^2$ = mq		-
$\Sigma_i d_{xi}^2$ (adottato)= mq		230.40

1) PER VERIFICHE SLU			
	Palificata	**Singolo Palo della palificata**	
Ai fini di SLU_STR_(N,M); resistenza SLU (N,M) dei pali			
N compressione (+), tra terne non sismiche e sismiche		$N_{pmin} = N/n_p - M_x d_{ymax}/\Sigma_i d_{yi}^2 - M_y d_{xmax}/\Sigma d_{xi}^2$	
		$N_{pmax} = N/n_p + M_x d_{ymax}/\Sigma_i d_{yi}^2 + M_y d_{xmax}/\Sigma d_{xi}^2$	
	Verifiche SLU_STR		Verifiche SLU_STR
N= kN	20,845.60	N_{pmin}= kN	744.49
M_x = kNm	-	N_{pmax}= kN	744.49
M_y = kNm	-	**M_p = kNm**	**-**
N= kN	27,611.80	N_{pmin}= kN	977.30
M_x = kNm	3,148.53	N_{pmax}= kN	994.97
M_y = kNm	-	**M_p = kNm**	**78.45**
N= kN	27,611.80	N_{pmin}= kN	980.44
M_x = kNm	2,029.56	N_{pmax}= kN	991.83
M_y = kNm	-	**M_p = kNm**	**46.46**
N= kN	27,611.80	N_{pmin}= kN	977.30
M_x = kNm	3,148.53	N_{pmax}= kN	994.97
M_y = kNm	-	**M_p = kNm**	**78.45**
N trazione (-), tra terne non sismiche e sismiche		$N_{pmin} = N/n_p + M_x d_{ymax}/\Sigma_i d_{yi}^2 + M_y d_{xmax}/\Sigma d_{xi}^2$	
		$N_{pmax} = N/n_p - M_x d_{ymax}/\Sigma_i d_{yi}^2 - M_y d_{xmax}/\Sigma d_{xi}^2$	
	Verifiche SLU_STR		Verifiche SLU_STR
N= kN	-	N_{pmin}= kN	-
M_x = kNm	-	N_{pmax}= kN	-
M_y = kNm	-	**M_p = kNm**	**-**
N= kN	-	N_{pmin}= kN	-
M_x = kNm	-	N_{pmax}= kN	-
M_y = kNm	-	**M_p = kNm**	**-**
N= kN	-	N_{pmin}= kN	-
M_x = kNm	-	N_{pmax}= kN	-
M_y = kNm	-	**M_p = kNm**	**-**
N= kN	-	N_{pmin}= kN	-
M_x = kNm	-	N_{pmax}= kN	-
M_y = kNm	-	**M_p = kNm**	**-**
Interazione cinematica	Verifiche SLU_STR		
M_{CIN} (su monopalo o singolo palo della palificata) = kNm	129.08		
M_{INERZ} (su monopalo o singolo palo della palificata) = kNm	10.00		
M_{RIS} (su monopalo o singolo palo della palificata) = kNm	139.08		
N (tra le combinazioni SLU_STR sismiche)= kN	14,994.00	N_{pmin}= kN	535.50
M_x = kNm	-	N_{pmax}= kN	535.50
M_y = kNm	-		
Ai fini di SLU_STR_(V); resistenza SLU a Taglio dei pali	Verifiche SLU_STR		Verifiche SLU_STR
V tra combin. non sismiche e sismiche = max { $(V_x^2 + V_y^2)^{1/2}$ } = kN	2,196.65	$V_p = V / n_p$ = kN	78.45
Ai fini di SLU_STR_(N)_st_eq_el; stab. equilibrio elastico dei pali	Verifiche SLU_STR		Verifiche SLU_STR
		$N_{pmax} = N/n_p + M_x d_{ymax}/\Sigma_i d_{yi}^2 + M_y d_{xmax}/\Sigma d_{xi}^2$	
N= N di compressione (+) = kN	27,611.80	N_{pmax} = kN	994.97
M_x = kNm	3,148.53		
M_y = kNm	-		
Ai fini di SLU_GEO_qlim_trasv_t_c e SLU_GEO_qlim_trasv_t_i: portanza limite SLU trasversale	Verifiche SLU_GEO		Verifiche SLU_GEO
V tra combin. non sismiche e sismiche = kN	2,196.65	$V_p = V / n_p$ = kN	78.45
M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rd}, calcolato per			
a) N=0	-	$N_p = N / n_p$ = kN	-
b) N associato alla combinazione in cui opera V : N= kN	27,611.80	N_{pmin}= kN	977.30
M_x = kNm	3,148.53	N_{pmax} = kN	994.97
M_y = kNm	-		
Ai fini di SLU_GEO_qlim_vert: portanza limite SLU verticale	Verifiche SLU_GEO		Verifiche SLU_GEO
		$N_{pmax} = N/n_p + M_x d_{ymax}/\Sigma_i d_{yi}^2 + M_y d_{xmax}/\Sigma d_{xi}^2$	
N= N di compressione (+) tra terne non sismiche e sismiche= kN	27,611.80	N_{pmax} = kN	994.97
M_x = kNm	3,148.53		
M_y = kNm	-		
		$N_{pmax} = N/n_p - M_x d_{ymax}/\Sigma_i d_{yi}^2 - M_y d_{xmax}/\Sigma d_{xi}^2$	
N= N di trazione (-) tra terne non sismiche e sismiche= kN	-	N_{pmax} = kN	-
M_x = kNm	-		
M_y = kNm	-		
2) PER VERIFICHE SLE			
	Palificata	**Singolo Palo della palificata**	
Ai fini di SLE_ced_vert: cedimento max SLE verticale	Verifiche SLE		Verifiche SLE
		$N_{pmax} = N/n_p + M_x d_{ymax}/\Sigma_i d_{yi}^2 + M_y d_{xmax}/\Sigma d_{xi}^2$	
N= kN	19,505.15	N_{pmax} = kN	702.50
M_x = kNm	2,099.04	$N_{pmedio} = N/n_p$ = kN	696.61
M_y = kNm	-		
Ai fini di SLE_sp_trasv: spostamento max SLE trasversale	Verifiche SLE		Verifiche SLE
V tra combin. non sismiche e sismiche: V = max { $(V_x^2 + V_y^2)^{1/2}$ } = kN	1,464.45	$V_p = V / n_p$ = kN	52.30

D) Verifiche strutturali a presso-tenso flessione: vengono inserite le caratteristiche geometriche e meccaniche dei singoli pali, il numero ed il diametro delle armature longitudinali, determinando quindi il valore di momento resistente della sezione. In sintesi, sono stati scelti pali di diametro 0.80 m armati con 16Φ20 longitudinalmente. Si riportano i risultati relativi all'analisi su mono-palo e su palificata.

Cls				
f_{cd}= 0,83 R_{ck}= N/mmq	33.20			
R_{ck}= N/mmq	40.00			
γ_c =	1.50			
f_{cd}= α_{cc} f_{ck}/γ_c= 0,85 f_{ck}/γ_c= N/mmq	18.81			
Acciaio				
f_{yk}= N/mmq	450.00			
γ_s =	1.15			
f_{yd}= f_{yk}/γ_s= N/mmq	391.30			
E_s =N/mmq	200,000.00			
ε_{yd} = f_{yd}/E_s =	0.196%			
Copriferro	(EC2)		(Circ.-NTC)	
$c_{min,b}$ = mm	-	elemento:	Palo	
$c_{min,dur}$ = mm	-	vita nominale V_R:	100	
Δc_{dev} = mm	-	ambiente:	aggressivo	
$\Delta c_{dur,st}$ = mm	-	$c_{min,dur}$ = mm	45.00	
$\Delta c_{dur,add}$ = mm	-	Δc_{dur} = mm	-	
Δc_{dev} = mm	-	Δc_{dur} = mm	10.00	
$c_{min,b}$ + $\Delta c_{dev,g}$ - $\Delta c_{dur,st}$ - $\Delta c_{dur,add}$ = mm	-			
c_{min} = max{$c_{min,b}$; $c_{min,dur}$ + $\Delta c_{dev,g}$ - $\Delta c_{dur,st}$ - $\Delta c_{dur,add}$; 10 mm} = mm	-	c_{min}=$c_{min,dur}$ - Δc_{dur} =	45.00	
c_{nom} = c_{min} + Δc_{dev} = mm	55.00			
ϕ_{st} = ϕ staffa (max)= mm	10.00			
ϕ_b = ϕ barra (max)= mm	20.00			
c_{1_palo} = dist. min. da bordo a baric. barre strato 1 = c_{nom} + ϕ_{st} + ϕ_b/2 =mm	75.00			
Sezione				
d= diametro sezione palo = mm	800.00			
Ac = π(d/2)² = mmq	502,654.82			
Strato 1 (esterno)				
c_{b_1} = dist. da bordo a baricentro barre strato 1 = mm	75.00			
N.o barre = N_{b_1} =	16.00			
ϕ_{b_1} = mm	20.00			
Area totale barre= A_{sb_1} = mmq	5,026.55			
Strato 2 (intermedio)				
c_{b_2} = dist. da bordo a baricentro barre strato 2 = mm	-			
N.o barre = N_{b_2} =	-			
ϕ_{b_2} = mm	-			
Area totale barre= A_{sb_2} = mmq	-			
Strato 3 (interno)				
c_{b_3} = dist. da bordo a baricentro barre strato 3 = mm	-			
N.o barre = N_{b_3} =	-			
ϕ_{b_3} = mm	-			
Area totale barre= A_{sb_3} = mmq	-			
A_s = As totale = $\Sigma_{i=1,3} A_{sb\_i}$ =mmq	5,026.55			
ρ_s = As tot/Ac = %	1.00%			
ρ_{min} = (inf per 0,3% ; sup per 1%) = %	inf			
ρ_{min} (adottato) =	0.30%			
$\rho_s \geq \rho_{min}$ (adottato) ?	ok			
Calcola M_{Rd} per N assegnati				



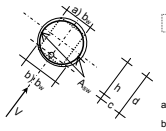
mono-Palo

Verifica SLU_STR_(N,M); resistenza SLU (N,M) dei pali

		Verifiche SLU_STR	$M_y = (M_x^2 + M_y^2)^{1/2}$	M_{Rd} (M) kNm	$M_{Rd} \geq M_y$?
N compressione (+), fra terne non sismiche e sismiche	N=N_{min}= kN	378.05			
	M_x = kNm	6.67			
	M_y = kNm	27.01	27.82	685.34	ok
	N=N_{max}= kN	1,503.19			
	M_x = kNm	- 23.87			
	M_y = kNm	0.52	23.88	902.82	ok
	N= kN	726.05			
	M_x = kNm	- 0.03			
	M_y = kNm	- 0.27	0.27	769.77	ok
	N= kN	843.47			
	M_x = kNm	- 4.56			
	M_y = kNm	192.43	192.48	784.38	ok
		Verifiche SLU_STR			
N frazione (-), fra terne non sismiche e sismiche	N=N_{min}= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	594.96	ok
	N=N_{max}= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	594.96	ok
	N= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	594.96	ok
	N= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	594.96	ok
		Verifiche SLU_STR			
Interazione cinematica	N = kN	891.46	M_y=M_{Rd}= kNm	M_{Rd} (M) kNm	$M_{Rd} \geq M_y$?
	M_{min} = kNm	139.08	139.08	793.86	ok
Ai fini di SLU_GEO_qlim_trasv_t_c e SLU_GEO_qlim_trasv_t_i: portanza limite SLU trasversale					
		Verifiche SLU_GEO			
V tra combin. non sismiche e sismiche = kN		438.59			
M_y = Momento di plasticizzazione della sezione (Broms) = M_{Rd}:					
	calcolato per			M_{Rd} (M) kNm	
	a) N=0	-		594.96	
	b) N associato alla combinazione in cui opera V: N= kN	1,142.07		841.22	

Singolo Palo della palificata (sollecitazioni per la distribuzione uniforme o sfalsata adottata)					
Verifica SLU_STR_(N,M); resistenza SLU (N,M) dei pali					
		Verifiche SLU_STR	**$M_d = M_p$=kNm**	**M_{Rd} (N) kNm**	**$M_{Rd} \geq M_d$?**
N compressione (+), tra terne non sismiche e sismiche	N_{pmin}= kN	744.49			
	M_p = kNm	-	-	594.96	ok
	N_{pmax}= kN	744.49			
	M_p = kNm	-	-	594.96	ok
	N_{pmin}= kN	977.30			
	M_p = kNm	78.45	78.45	594.96	ok
	N_{pmax}= kN	994.97			
	M_p = kNm	78.45	78.45	594.96	ok
	N_{pmin}= kN	980.44			
	M_p = kNm	46.46	46.46	594.96	ok
	N_{pmax}= kN	991.83			
	M_p = kNm	46.46	46.46	594.96	ok
	N_{pmin}= kN	977.30			
	M_p = kNm	78.45	78.45	594.96	ok
	N_{pmax}= kN	994.97			
	M_p = kNm	78.45	78.45	594.96	ok
		Verifiche SLU_STR	**$M_d = M_p$=kNm**	**M_{Rd} (N) kNm**	**$M_{Rd} \geq M_d$?**
N trazione (-), tra terne non sismiche e sismiche	N_{pmin}= kN	-			
	M_p = kNm	-	-	594.96	ok
	N_{pmax}= kN	-			
	M_p = kNm	-	-	594.96	ok
	N_{pmin}= kN	-			
	M_p = kNm	-	-	594.96	ok
	N_{pmax}= kN	-			
	M_p = kNm	-	-	594.96	ok
	N_{pmin}= kN	-			
	M_p = kNm	-	-	594.96	ok
	N_{pmax}= kN	-			
	M_p = kNm	-	-	594.96	ok
	N_{pmin}= kN	-			
	M_p = kNm	-	-	594.96	ok
	N_{pmax}= kN	-			
	M_p = kNm	-	-	594.96	ok
		Verifiche SLU_STR	**M_d=M_{RIS}=kNm**	**M_{Rd} (N) kNm**	**$M_{Rd} \geq M_d$?**
Interazione cinematica	N_{pmin}= kN	535.50			
	M_{RIS} = kNm	139.08	139.08	594.96	ok
	N_{pmax}= kN	535.50			
	M_{RIS} = kNm	139.08	139.08	594.96	ok
Ai fini di SLU_GEO_qlim_trasv_t_c e SLU_GEO_qlim_trasv_t_i: portanza limite SLU trasversale					
		Verifiche SLU_GEO			
	V tra combin. non sismiche e sismiche = V_p= kN	78.45			
	M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rd};				
	calcolato per			**M_{Rd} (N) kNm**	
	a) N=0	-		594.96	
	N associato alla combinazione in cui opera V : **b)** N_{pmin}= kN	977.30		594.96	
	c) N_{pmax}= kN	994.97		594.96	

E) Verifiche strutturali a taglio: vengono inserite le caratteristiche delle armature trasversali (diametro, passo) e si sceglie se valutare la resistenza del palo secondo i dettami delle NTC '08 al paragrafo §4.1.2.1.3.1, oppure se progettare le staffature resistenti a taglio. In definitiva vengono utilizzate staffe Φ10 passo 15 cm. Si riportano solo le verifiche relative al mono-palo, in quanto le sollecitazioni taglianti nel caso di palificata risultano notevolmente inferiori.

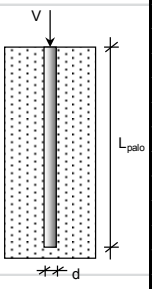


a) max inerzia: b_w=0,581 d

b) min corda: b_w=2 [(d/2)^2 - (d/2-c)^2]$^{1/2}$

Cls	
f_{ck}= N/mmq	33.20
R_{ck}= N/mmq	40.00
γ_c =	1.50
f_{cd} = α_{cc} f_{ck} /γ_c= 0,85 f_{ck} /γ_c= N/mmq	18.81
f_{ctm}= 0,30 $f_{ck}^{2/3}$ = N/mmq	3.10
$f_{ctk0.05}$ = 0,7 f_{ctm}= N/mmq	2.17
f_{ctd}= $f_{ctk0.05}$ / γ_c = N/mmq	1.45
Acciaio	
f_{yk}= N/mmq	450.00
γ_s =	1.15
f_{yd} = f_{yk}/γ_s= N/mmq	391.30
E_s =N/mmq	200,000.00
ε_{syd} = f_{yd}/E_s=	0.001957
Sollecitazioni	
Presenza di mono-Palo o Palificata ?	mono-Palo
V = kN	438.59
V = kN	-
V (adottato) = kN	438.59
d= diametro sezione palo = mm	800.00
Ac=π(d/2)^2= mmq	502,654.82
c = dist. da bordo a baricentro barre strato = mm	
strato 1° : $c_{s,1}$ = mm	72.00
strato 2° : $c_{s,2}$ = mm	-
strato 3° : $c_{s,3}$ = mm	-
c_{medio} = mm	72.00
c_{min}= mm	-
c_{max}= mm	72.00
c (adottato) = mm	**72.00**
h = d - c =mm	728.00
Per b_w si utilizza il criterio a)max inerzia, b)min corda, c)Min a) b)?	**c)Min a) b)**
b_w=mm	457.89
Si procede alle verifiche senza staffature resistenti a taglio?	**si**
Si procede al dimensionamento con staffature resistenti a taglio?	**si**
l_p= lunghezza palo= m	**14.00**
Vc= Ac l_p = mc	7.04
Verifica senza staffature resistenti a taglio	
V (adottato) = V_{Ed} = kN	438.6
k = min [1 + (200/h)$^{1/2}$; 2]=	1.524
N_{Ed}= forza assiale di calcolo di compressione (positiva)= kN	-
σ_{cp} = min [(N_{Ed}/Ac) ; 0,2 f_{cd}]= N/mmq	-
As_l= mmq	**2,002.00**
ρ_l = min [As_l /(b_w h); 0,02]=	0.0060
v_{min} = 0,035 $k^{3/2}$ $f_{ck}^{1/2}$= N/mmq	0.379
V_{Rd} = [v_{min} + 0,15 σ_{cp}] b_w h= kN	126.5
V^*_{Rd}= [0,18 k (100 ρ_l f_{ck})$^{1/3}$ / γ_c + 0,15 σ_{cp}] b_w h= kN	165.3
V_{Rd}= max [V_{Rd2}; V^*_{Rd}]= kN	165.3
V_{Rd} ≥ V_{Ed}?	No !
Dimensionamento con staffature resistenti a taglio	
Per gli N_{Ed}, si pone α_c=1 ?	**si**
N (kN)	-
σ_{cp} = N/Ac= N/mmq	-
1) α_c : [1+ σ_{cp}/f_{cd} se 0≤σ_{cp}<0,25f_{cd}; 1,25 se 0,25f_{cd}≤σ_{cp}≤0,5f_{cd}; 2,5(1- σ_{cp}/f_{cd}) se 0,5f_{cd}<σ_{cp}<f_{cd}]	-
2) α_c pari al minimo tra quelli valutati per tutti gli N di compress.	-
Procedere con la valutazione 1) oppure 2) ?	**1)**
α_c adottato.	1.000
V (adottato) =V_{Ed} = kN	438.6
s (passo staffe adottato)= **mm**	**150.00**
n_b (n.o bracci delle staffe adottato) =	**2.00**
Diametri adottati per le staffe:	
1° perimetro: ϕ_1 = mm	**10.00**
$A1_{\phi 1}$= π(ϕ_1/2)^2 = mmq	78.54
2° perimetro: ϕ_2 = mm	-
$A1_{\phi 2}$= π(ϕ_2/2)^2 = mmq	-
3° perimetro: ϕ_3 = mm	-
$A1_{\phi 3}$= π(ϕ_3/2)^2 = mmq	-
Asw = n_b [$A1_{\phi 1}$ + $A1_{\phi 2}$ + $A1_{\phi 3}$] = mmq	157.08
Asw f_{yd}/ b_ws=	0.89
1/2 α_c 0,5 f_{cd}=	4.70
Controllo che cotgϑ'≥1 (ϑ≤45°); con ϑ_{max}=45° : Asw f_{yd}/ b_ws ≤ 1/2 α_c 0,5 f_{cd} ?	ok
ϑ' = arcsin (Asw f_{yd}/ b_ws α_c 0,5 f_{cd})$^{1/2}$ = °	17.97
Controllo che cotgϑ'≤2,5 (ϑ'≥ϑ_{min}=21,8°); se ϑ'≥ϑ_{min} si assume ϑ=ϑ'; se ϑ'<ϑ_{min} si assume ϑ=21,8° : ϑ adottato=ϑ=	21.80
V_{Rsd} = 0,9 h (Asw/s) f_{yd} ctgϑ = kN	671.3
V_{Rcd} = 0,9 h b_w α_c (0,5 f_{cd}) ctgϑ / (1 + ctg$^2\vartheta$)= 0,9 h b_w α_c (0,5 f_{cd}) / (ctgϑ + tgϑ)= kN	973.1
V_{Rd} = [V_{Rsd} se ϑ'<21°,8 e ϑ=21°,8; altrimenti min(V_{Rsd} ; V_{Rcd})]= kN	671.3
V_{Rd} ≥ V_{Ed}?	ok
Prescrizioni armature	
Attivare prescrizioni armature ?	**si**
$\phi_{l,min}$ (diametro min. delle barre longitudinali)=mm	**14.00**
$\phi_{l,max}$ (diametro max delle barre longitudinali)=mm	**14.00**
s_{max}= passo max staffe= min(12 $\phi_{l,min}$; 250 mm) =mm	168.00
s ≤ s_{max}?	ok
ϕ_{min} = diametro min. staffa =max(6 mm; 1/4 $\phi_{l,max}$) =mm	6.00
1° perimetro: ϕ_1 ≥ ϕ_{min}?	ok
2° perimetro: ϕ_2 ≥ ϕ_{min}?	-
3° perimetro: ϕ_3 ≥ ϕ_{min}?	-

F) La verifica a stabilità del palo si effettua inserendo, oltre alle caratteristiche geometriche dell'opera, anche il coefficiente di reazione laterale del mono-palo, valutato attraverso la formulazione di Davisson (1970) $k_{h\_int} = 67\,\frac{c_u}{D}$, dove D = 0.80m e c_u = 63.15 KN/m^2; quest'ultimo valore di coesione non drenata è stato ottenuto dall'analisi delle informazioni geotecniche a disposizione, in particolare è stato opportunamente ottenuto un valore mediato, modellando di fatto il palo come se fosse inserito all'interno di un terreno equivalente: è stato infatti dapprima ottenuto un valore di coesione medio relativo agli strati di terreno attraversati dal palo, valore che è stato poi redistribuito lungo tutta la luce dell'opera, essendo la somma degli spessori degli strati di terreno dotati di coesione non drenata inferiore alla lunghezza totale del palo. Di seguito si riportano i risultati ottenuti dalle analisi. Si riportano solo le verifiche relative al mono-palo, in quanto le sollecitazioni assiali nel caso di palificata risultano inferiori.

VERIFICA SLU CON FORZA DI COMPRESSIONE PER LA STABILITA' DELL'EQUILIBRIO ELASTICO		
Presenza di mono-Palo o Palificata ?	mono-Palo	
d = diametro sezione palo = m	0.80	
d = diametro (utente) = m	-	
d=diametro adottato = m	0.80	
N= Carico verticale agente in Combinazione SLU :		
N = N_{max} = carico assiale max su mono-Palo = kN	1,503.19	
N = N_{pmax} = carico assiale max su singolo palo della Palificata = kN	-	
N = N_{Ed}=kN	1,503.19	
Calcolo del carico critico elastico		
Carico critico di asta caricata da N e vincolata lateralmente a un mezzo elastico;		
Relazione da Timoshenko, Gere, in Theory of elastic stability (1961):		
$N_{cr} = (\pi^2 E J/ L^2) [m^2 + \beta L^4/(m^2 \pi^4 EJ)]$		
Con m = n.o di semionde della deformata sinusoidale caricata dal carico di punta,		
posto λ =semilunghezza d'onda= L / m, risulta:		
$N_{cr} = \pi^2 E J (1/\lambda^2 + \lambda^2 \beta/(\pi^4 EJ)]$		
Al variare di λ si ottiene il minimo N_{cr} con: d (N_{cr}/dλ)=0, che porge:		
$\lambda^* = (EJ/\beta)^{1/4}$		
$N_{cr} = N_{cr}(\lambda^*) = 2\ (\beta EJ)^{1/2}$		
Calcolo di N_{cr}		
K_{h_int}= coefficiente di reazione laterale del terreno se mono-palo = N/cm^3	5.29	
K_{h_rid}= coefficiente di reazione laterale del terreno se palificata = N/cm^3	5.29	
K_h= (K_{h_int} se mono-Palo; K_{h_rid} se Palificata)= N/cm^3	5.29	
D= dimensione adottata = d = mm	800.00	
β = reazione laterale terreno per unità di spostamento laterale e per unità di lunghezza= k_h D= N/mm^2	4.23	
f_{ck}= 0,83 R_{ck}= N/mmq	33.20	
R_{ck}= N/mmq	40.00	
E_{cm} = 22.000 [f_{cm}/10]$^{0.3}$ = 22.000 [(f_{ck}+8) /10]$^{0.3}$ =N/mmq	33,642.78	
E= Modulo di elasticità (utente) = N/mm^2	33,350.00	
E= Modulo di elasticità adottato= N/mm^2	33,350.00	
J = π d^4 / 64 = mm^4	20,106,192,982.97	
J = Momento di inerzia (utente) = mm^4	-	
J= Momento di inerzia adottato= mm^4	20,106,192,982.97	
$N_{cr} = 2\ (\beta EJ)^{1/2}$ = kN	106,540.73	
N_{cr} (utente) = kN	-	
N_{cr} (adottato) = kN	106,540.73	
VERIFICA (Analisi Elastica)		
N_{Ed} =kN	1,503.19	
N_{cr} = N_{cr} (adottato) = kN	106,540.73	
α_{cr} = N_{cr}/ N_{Ed} =	70.88	
Fs =	5.00	
Analisi elastica: $\alpha_{cr} \geq$ Fs ?	ok	

G) La verifica a portanza trasversale del palo si effettua sulla falsariga del procedimento svolto nel caso di verifica a stabilità. Infatti, siccome la palificata attraversa strati di terreno di tipologia diversa (coerente ed incoerente), sono stati opportunamente ottenuti valori mediati relativi alle caratteristiche geotecniche (peso specifico, coesione non drenata), modellando di fatto il palo come se fosse inserito all'interno di un terreno equivalente: è stato infatti ottenuto un valore di coesione e di peso specifico medio relativo agli strati di terreno attraversati dal palo, valore che è stato poi redistribuito lungo tutta la luce dell'opera, essendo la somma degli spessori degli strati di terreno coerenti ed incoerenti inferiore alla lunghezza totale del palo. La portanza trasversale finale è quindi data dalla somma delle portanza tra terreni coerenti ed incoerenti. Di seguito si riportano i risultati ottenuti dalle analisi.

VERIFICA SLU-GEO PER CARICO LIMITE TRASVERSALE DI UN PALO CON ROTAZIONE IN TESTA IMPEDITA. TERRENI COESIVI.

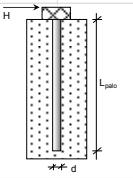
Sollecitazioni su mono-Palo o Palificata ?		mono-Palo				
		Coefficienti parziali Azioni, Materiali, Resistenze				
		A1, A2		M1	R1, R2, R3	
		perm. γ_G (se fav.)	var. γ_G (se fav.)	γ_{cu}	γ_T	
SLU: combinazioni NON SISMICHE tipo: $\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \Sigma_{i>1} (\gamma_{Qi} \psi_{oi} Q_{ki})$						
App. 1	Comb. 1 (STR): A1+M1+R1	1,30 (1,00)	1,50 (0,00)	1.00	1.00	
	Comb. 2 (GEO) : A2+M1+R2	**1,00 (1,00)**	**1,30 (0,00)**	**1.00**	**1.60**	
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**	**1,30 (1,00)**	**1,50 (0,00)**	**1.00**	**1.30**	
SLU: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_j (\psi_{2j} Q_{kj})$						
App. 1	Comb. 1 (STR): A1+M1+R1	1.00	1.00	1.00	1.00	
	Comb. 2 (GEO) : A2+M1+R2	**1.00**	**1.00**	**1.00**	**1.60**	
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**	**1.00**	**1.00**	**1.00**	**1.30**	

Approccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)	2
Relativa Comb. GEO associata all'Approccio scelto:	unica
γ_{cu} =	1.00
γ_T =	1.30

	mono-Palo		Palificata	
	Verifiche SLU_STR	Verifiche SLU_GEO	Verifiche SLU_STR	Verifiche SLU_GEO
Relativa Comb. associata all'Approccio scelto:		unica		unica
All'interno dell'app. scelto, a seguire i valori, per la comb. associata.				
Verifiche SLU-GEO				
portanza limite SLU trasversale		Verifiche SLU_GEO		Verifiche SLU_GEO
V (V_p se palificata) tra combin. non sismiche e sismiche = kN		438.59		-
M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rd} calcolato per				
mono-Palo				
a) N=0		-		
M_{Rd} = kNm =		597.65		
b) N associato alla combinazione in cui opera V : N= kN =		1,142.07		
M_{Rd} = kNm =		844.47		
Palificata				
a) N=0				-
M_{Rd} = kNm =				-
N associato alla combinazione in cui opera V :				
b) N_{min}= kN				-
M_{Rd} = kNm =				-
c) N_{max}= kN				-
M_{Rd} = kNm =				-

Fattori di correlazione ξ per il calcolo della resistenza caratteristica, condotto per via analitica (n = n.o verticali indagate)							
n	**1**	**2**	**3**	**4**	**5**	**7**	**≥10**
ξ_3	1.70	1.65	1.60	1.55	1.50	1.45	1.40
ξ_4	1.70	1.55	1.48	1.42	1.34	1.28	1.21

n = (1, 2, 3, 4, 5, 7, ≥10)	**1**
ξ_3 =	1.70
ξ_4 =	1.70
d = diametro sezione palo = m	0.80
L_{palo} = L= Lunghezza del palo = m	**14.00**
Coesione non drenata media= $c_{u\,med}$ = kN/mq	**63.15**
Coesione non drenata minima= $c_{u\,min}$ = kN/mq	**57.25**
Coesione non drenata media di progetto = $c_{u\,med,d} = c_{u\,med} / \gamma_{cu}$ = kN/mq	63.15
Coesione non drenata minima di progetto = $c_{u\,min,d} = c_{u\,min} / \gamma_{cu}$ = kN/mq	57.25



mono-Palo: calcolo effettuato per ciascuno dei 2 valori del Momento di plasticizzazione:		**a)**	**b)**
M_y = Momento di plasticizzazione della sezione = M_{Rd} = kNm		597.65	844.47
P. corto: H1 = 9 c_u d^2 (L/d - 1,5)	$H1_{med}$ (c_u= $c_{u\,med,d}$) =kN	5,819.90	5,819.90
	$H1_{min}$ (c_u= $c_{u\,min,d}$) =kN	5,276.16	5,276.16
P. intermedio: H2 = -9 c_u d^2 (L/d +1,5) + 9c_u d^2 [2 (L/d)^2 + 4/9 M_y/c_u d^3 +4,5]$^{1/2}$	$H2_{med}$ (c_u= $c_{u\,med,d}$) =kN	2,184.03	2,208.67
	$H2_{min}$ (c_u= $c_{u\,min,d}$) =kN	1,985.56	2,010.18
P. lungo: H3 = -13,5 c_u d^2 + c_u d^2 (182,25 + 36 M_y/c_u d^3)$^{1/2}$	$H3_{med}$ (c_u= $c_{u\,med,d}$) =kN	631.10	808.47
	$H3_{min}$ (c_u= $c_{u\,min,d}$) =kN	614.45	784.83
H_{med} = min ($H1_{med}$; $H2_{med}$; $H3_{med}$)= kN		631.10	808.47
		P. lungo	P. lungo
H_{min} = min ($H1_{min}$; $H2_{min}$; $H3_{min}$)= kN		614.45	784.83
		P. lungo	P. lungo
H_k = Min(H_{med}/ξ_3 ; H_{min}/ξ_4) = kN		361.44	461.66
$R_{T,d} = H_d = H_k/\gamma_T$ = kN		278.03	355.12
		a	**b**
Si procede alla verifica con il seguente $R_{T,d}$:			
a opp. b ?		**b**	
$R_{T,d}$ = kN		355.12	
$F_{T,d}$ = V = kN		438.59	
$R_{T,d}$ / $F_{T,d}$ =		**0.81**	
$F_{T,d} \leq R_{T,d}$?		**No!**	

VERIFICA SLU-GEO PER CARICO LIMITE TRASVERSALE DI UN PALO CON ROTAZIONE IN TESTA IMPEDITA. TERRENI INCOERENTI.

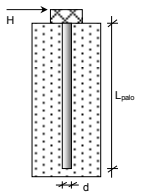
		Coefficienti parziali Azioni, Materiali, Resistenze			
		A1, A2		M1	R1, R2, R3
		perm. γ_G (se fav.)	var. γ_Q (se fav.)	γ_{γ} , $\gamma_{\varphi'}$	γ_T
SLU: combinazioni NON SISMICHE tipo: $\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \Sigma_{i=2,n} (\gamma_{Qi} \psi_{0i} Q_{ki})$					
App. 1	Comb. 1 (STR): A1+M1+R1	1,30 (1,00)	1,50 (0,00)	1.00	1.00
	Comb. 2 (GEO) : A2+M1+R2	**1,00 (1,00)**	**1,30 (0,00)**	**1.00**	**1.60**
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**	**1,30 (1,00)**	**1,50 (0,00)**	**1.00**	**1.30**
SLU: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_j (\psi_{2j} Q_{kj})$					
App. 1	Comb. 1 (STR): A1+M1+R1	1.00	1.00	1.00	1.00
	Comb. 2 (GEO) : A2+M1+R2	**1.00**	**1.00**	**1.00**	**1.60**
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**	**1.00**	**1.00**	**1.00**	**1.30**

Approccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)	2
Relativa Comb. GEO associata all'Approccio scelto:	unica
γ_{γ} , $\gamma_{\varphi'}$ =	1.00
γ_T =	1.30

	mono-Palo		Palificata	
	Verifiche SLU_STR	Verifiche SLU_GEO	Verifiche SLU_STR	Verifiche SLU_GEO
Relativa Comb. associata all'Approccio scelto:		unica		unica
All'interno dell'app. scelto, a seguire i valori, per la comb. associata.				
Verifiche SLU-GEO portanza limite SLU trasversale		Verifiche SLU_GEO		Verifiche SLU_GEO
V (V_p se palificata) tra combin. non sismiche e sismiche = kN		438.59		-
M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rd} calcolato per				
mono-Palo				
a) N=0		-		
M_{Rd} = kNm =		597.65		
b) N associato alla combinazione in cui opera V : N= kN =		1,142.07		
M_{Rd} = kNm =		844.47		
Palificata				
a) N=0				-
M_{Rd} = kNm =				-
N associato alla combinazione in cui opera V :				
b) N_{pmin}= kN				-
M_{Rd} = kNm =				-
c) N_{pmax}= kN				-
M_{Rd} = kNm =				-

Fattori di correlazione ξ_3 per il calcolo della resistenza caratteristica, condotto per via analitica (n = n.o verticali indagate)							
n	**1**	**2**	**3**	**4**	**5**	**7**	**≥10**
ξ_3	1.70	1.65	1.60	1.55	1.50	1.45	1.40
ξ_4	1.70	1.55	1.48	1.42	1.34	1.28	1.21

n = (1, 2, 3, 4, 5, 7, ≥10)	**1**
ξ_3 =	1.70
ξ_4 =	1.70
d = diametro sezione palo = m	0.80
L_{palo} = L= Lunghezza del palo = m	**14.00**
Peso di unità di volume γ (se falda $\gamma = \gamma'$) = kN/m^3 =	**7.85**
Angolo medio di attrito del terreno = φ'_{med} = °	**45.11**
Angolo minimo di attrito del terreno = φ'_{min} °	**44.29**
Peso di unità di volume di progetto $\gamma_d = \gamma/\gamma_{\gamma}$ = kN/m^3 =	7.85
Angolo medio di attrito del terreno, di progetto = $\varphi'_{med,d} = \varphi'_{med}/\gamma_{\varphi'}$ = °	45.11
Angolo minimo di attrito del terreno, di progetto = $\varphi_{min,d} = \varphi_{min}/\gamma_{\varphi'}$ = °	44.29
Coeff. medio di spinta passiva $k_{p\,med,d} = (1 + \sin\varphi'_{med,d})/(1 - \sin\varphi'_{med,d})$ =	5.86
Coeff. minimo di spinta passiva $k_{p\,min,d} = (1 + \sin\varphi'_{min,d})/(1 - \sin\varphi'_{min,d})$ =	5.63



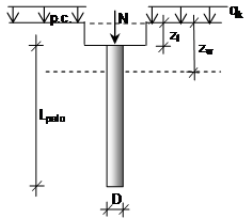
mono-Palo: calcolo effettuato per ciascuno dei 2 valori del Momento di plasticizzazione:		**a)**	**b)**
M_y = Momento di plasticizzazione della sezione = M_{Rd} = kNm		597.65	844.47
P. corto: $H1 = 1{,}5\ k_p\ \gamma_d\ d^3\ (L/d)^2$	$H1_{med}$ (k_p= $k_{p\,med,d}$) =kN	10,819.79	10,819.79
	$H1_{min}$ (k_p= $k_{p\,min,d}$) =kN	10,392.73	10,392.73
P. intermedio: $H2 = 1/2\ k_p\ \gamma_d\ d^3\ (L/d)^2 + M_y/L$	$H2_{med}$ (k_p= $k_{p\,med,d}$) =kN	3,649.29	3,666.92
	$H2_{min}$ (k_p= $k_{p\,min,d}$) =kN	3,506.93	3,524.56
P. lungo: $H3 = k_p\ \gamma_d\ d^3\ [(3{,}676\ M_y / k_p\ \gamma_d\ d^4)^2]^{1/3}$	$H3_{med}$ (k_p= $k_{p\,med,d}$) =kN	562.13	707.83
	$H3_{min}$ (k_p= $k_{p\,min,d}$) =kN	554.64	698.39
H_{med} = min ($H1_{med}$; $H2_{med}$; $H3_{med}$)= kN		562.13	707.83
		P. lungo	P. lungo
H_{min} = min ($H1_{min}$; $H2_{min}$; $H3_{min}$)= kN		554.64	698.39
		P. lungo	P. lungo
H_k = Min(H_{med}/ξ_3 ; H_{min}/ξ_4) = kN		326.26	410.82
$R_{tr,d} = H_d = H_k/\gamma_T$ = kN		250.97	316.02
		a	**b**
Si procede alla verifica con il seguente $R_{tr,d}$:			
a opp. b ?		**b**	
$R_{tr,d}$ = kN		316.02	
$F_{tr,d}$ = V = kN		438.59	
$R_{tr,d}$ / $F_{tr,d}$ =		**0.72**	
$F_{tr,d} \le R_{tr,d}$?		**No!**	

Sommando il contributo garantito dai terreni coerenti (F.S. = 0.81) con quello garantito dai terreni incoerenti (F.S. = 0.72), si ottiene un coefficiente di sicurezza pari a 1.53, pertanto la verifica risulta soddisfatta.

H) La verifica a portanza verticale del palo si effettua dapprima scegliendo il tipo di modello matematico per il calcolo dei parametri di portanza alla base e la tipologia di infissione, che determina le definizione di coefficienti di sicurezza differenti. Si inseriscono poi le caratteristiche degli spessori di terreno attraversati dal palo, dapprima introducendo i parametri medi e poi i parametri minimi; è così possibile ottenere i valori di portanza di base e laterale del terreno.

PALI SOGGETTI A CARICHI ASSIALI

Sollecitazioni su mono-Palo o Palificata ?	mono-Palo
D = Diametro sezione palo = m	0.80
Tecnologia, tipologia Diametro palo (e valori di calcolo N_q) =	Trivel. GD (Nq AGI/1984)
Tecnologia palo ?	Trivellati
z_t = Quota testa Palo da p.c. = m	1.00
z_w = Quota falda da p.c. = m	2.00
q_k = kN/mq	25.00
Applicare il fattore χ di riduzione capacità portante di base =	si
N_{str} = Numero strati = (Numero Strati)	4.00
A_p = Area Palo = $\pi(D/2)^2$ = mq	0.50265
$L_{palo} = \Sigma_{1\text{-}10}$ Sp strati = m	14.00



		Coefficienti parziali (A, R)				
		Azioni (A1, A2)		Resistenze (R1, R2, R3) base, laterale per pali soggetti a carichi assiali		
Approccio e Combinazioni		perm. γ_G (se fav.)	var. γ_Q (se fav.)	γ_b	γ_s	γ_{st}
SLU: combinazioni NON SISMICHE						
App. 1	Comb. 1 (STR): A1+M1+R1	1,30 (1,00)	1,50 (0,00)	1.00	1.00	1.00
	Comb. 2 (GEO): A2+M1+R2	1,00 (1,00)	1,30 (0,00)	1.70	1.45	1.60
App. 2	Comb. unica (STR, GEO): A1+M1+R3	1,30 (1,00)	1,50 (0,00)	1.35	1.15	1.25
SLU: combinazioni SISMICHE						
App. 1	Comb. 1 (STR): A1+M1+R1	1.00	1.00	1.00	1.00	1.00
	Comb. 2 (GEO): A2+M1+R2	1.00	1.00	1.70	1.45	1.60
App. 2	Comb. unica (STR, GEO): A1+M1+R3	1.00	1.00	1.35	1.15	1.25

roccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)	2
Relativa Comb. GEO associata all'Approccio scelto:	unica

	γ_b	γ_s	γ_{st}
γ da associare nel calcolo delle resistenze:	1.35	1.15	1.25

N'_d = azione assiale max di progetto a compressione (positiva) = kN	1,503.19
N'_d = azione assiale max di progetto a trazione (negativa) = kN	-

	Fattori di correlazione ξ per il calcolo della resistenza caratteristica, condotto per via analitica (n = n.o verticali indagate)						
n	1	2	3	4	5	7	≥10
ξ_3	1.70	1.65	1.60	1.55	1.50	1.45	1.40
ξ_4	1.70	1.55	1.48	1.42	1.34	1.28	1.21

n = (1, 2, 3, 4, 5, 7, ≥10)	1
ξ_3 =	1.70
ξ_4 =	1.70

CALCOLO DELLA RESISTENZA (base e laterale) CON I PARAMETRI MEDI DEL TERRENO

				Parametri MEDI terreno			
Strato	Sp (m)	Tipo terreno	Attrito negativo ?	γ (kN/m^3)	c. dr: c'=c'$_{med}$ (kN/mq)	c. dr: φ'=φ'$_{med}$ (°)	c. n dr: c_u=$c_{u\,med}$ (kN/mq)
1	6.00	Coesivo	no	16.70	-	-	22.00
2	1.80	Coesivo	no	21.00	-	-	133.00
3	1.80	Coesivo	no	25.00	-	-	285.00
4	4.40	Incoerente	no	25.00	-	45.11	-

Tipo Infisso: -

Strato	k f(palo, terreno)	μ=coef. scabr. interfac. terreno-palo			
	c. dr: k	c. dr: μ	c. dr: $\beta_S = k\,\mu$	c. dr: β_{S_utente}	c. dr: β_{S_adott}
1	-	-	-	-	-
2	-	-	-	-	-
3	-	-	-	-	-
4	0.292	1.004	0.293	-	0.293

Strato	parametri a, α legati all'adesione		β_n
	c. dr: a	c. n. dr: α	(in caso di attrito negativo)
1	-	0.900	1.00
2	-	0.400	1.00
3	-	0.400	1.00
4	-	-	1.00

		σ_{vz}	u	σ'_{vz}	c. n dr	c. dr	
		pr. verticale totale	pr. Interstiziale	pr. vert. efficace litost.	Q_{S_j} =	$Q_{S\_j\ attr\_p\text{-}t}$ =	Q_{S_j}=$Q_{S\_j\ attr\_p\text{-}t}$ + $Q_{S\_j\ ades}$
		$\sigma_{vz} = q_{ik} + (\gamma_1 z_i) + \Sigma_i \gamma_i Sp_i$	$u = (\gamma_w z_i) + \Sigma_i \gamma_w Sp_i$	$\sigma'_{vz} = (\sigma_{vz} - u)$	π D (Sp α c_u)$_i$	π D (Sp β_S β_n σ'_{vz_m})$_i$	$Q_{S\_j\ attr\_p\text{-}t}$ + πD (Sp a c')$_i$
	3 valori a dx per $\alpha(z_i)$	41.70	-	41.70			
z	6.00	141.90	50.00	91.90	298.58	-	-
	7.80	179.70	68.00	111.70	240.67	-	-
	9.60	224.70	86.00	138.70	515.72	-	-
	14.00	334.70	130.00	204.70	-	555.68	555.68

Pali Infissi MD o GD e Trivellati MD: valori di N_q dedotti da Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =5)	N_q (L/D =10)	N_q (L/D =20)	N_q (L/D =50)	L/D (palo)=	17.50	N_q(interp. per L/D palo)
1	-	-	-	-			-
2	-	-	-	-			-
3	-	-	-	-			-
4	519.87	426.71	370.24	347.74			384.36
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-

Pali Trivellati GD (N_q AGI/1984): valori di N_q ridotti, raccomandati da AGI (1984), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)=	17.50	N_q(interp. per L/D palo)
1	-	-			-
2	-	-			-
3	-	-			-
4	54.51	57.64			56.02
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-

Pali Trivellati GD (N_q Vig./1999): valori di N_q ridotti, proposti da Viggiani (1999), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)=	17.50	N_q(interp. per L/D palo)
1	-	-			-
2	-	-			-
3	-	-			-
4	93.63	90.92			92.32
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-

		N_q (ottenuto)	N_q (utente)	N_q (adottato)
In c. dr.: valore ottenuto, rispetto ai valori che precedono, in base a		-	-	-
scelta effettuata per 'Tecnologia, tipologia Diametro palo (e valori di calcolo N_q)'		-	-	-
		-	-	-
		56.02	-	56.02
		-	-	-
		-	-	-
		-	-	-
		-	-	-
		-	-	-
		-	-	-

RESISTENZA (laterale Q_S e di base o alla punta Q_b) CON I PARAMETRI MEDI DEL TERRENO

Strato	Q_{S_j} (kN)	N_q = N_q (adottato)	N_c	q_{b_j} (kN/mq)	Q_{b_j} (kN)	$Q_{b\_j\_utente}$ (kN)	$Q_{b\_j\_adot}$ (kN)
			c. n dr c_u>0: 9	c. n dr c_u>0: $N_c c_u + \sigma_{vz}$			
			c. dr. c'>0: (N_q -1) ctgφ'	c_u=0: c'N_c + $N_q\sigma'_{vz}$	= q_{b_j} A_p		
1	298.58					-	
2	240.67					-	
3	515.72					-	
4	555.68	56.02	-	11,467.60	5,764.25	-	5,764.25
						-	
						-	
						-	
						-	
						-	

CAPACITA' PORTANTE MEDIA

χ = fattore di riduzione capacità portante di base =	0.692
Base (per azione assiale $N_d \geq 0$): $R_{b;cal\,med} = \chi\ \Sigma_i\ Q_{b\_j\_adott}$ = kN	3,990.63
Laterale: $R_{s;cal\,med} = \Sigma_i\ Q_{S\_j}$ = kN	1,610.65

CALCOLO DELLA RESISTENZA (base e laterale) CON I PARAMETRI MINIMI DEL TERRENO

				Parametri MINIMI terreno			
Strato	Sp (m)	Tipo terreno	Attrito negativo ?	γ (kN/m³)	c. dr.: $c' = c'_{min}$ (kN/mq)	c. dr.: $\varphi' = \varphi'_{min}$ (°)	c. n. dr.: $c_u = c_{u\,min}$ (kN/mq)
1	6.00	Coesivo	no	16.70	-	-	19.00
2	1.80	Coesivo	no	21.00	-	-	104.00
3	1.80	Coesivo	no	25.00	-	-	278.00
4	4.40	Incoerente	no	25.00	-	44.29	-

Incolla k dai parametri MEDI

Tipo Infisso: -

Strato	k f(palo, terreno)	μ=coef. scabr. interfac. terreno-palo			
	c. dr.: k	c. dr.: μ	c. dr.: $\beta_s = k\,\mu$	c. dr.: $\beta_{s,utente}$	c. dr.: $\beta_{s,adott}$
1	-	-	-	-	-
2	-	-	-	-	-
3	-	-	-	-	-
4	0.302	0.976	0.294	-	0.294

Incolla α dai parametri MEDI

Strato	parametri a, α legati all'adesione		β_n
	c. dr.: a	c. n. dr.: α	(in caso di attrito negativo)
1	-	0.900	1.000
2	-	0.400	1.000
3	-	0.400	1.000
4	-	-	1.000

		σ_{vz}	u	σ'_{vz}	c. n. dr.	c. dr.	
		pr. verticale totale	pr. interstiziale	pr. vert. efficace litost.	$Q_{l,i} =$	$Q_{l,i\,attr,p+t} =$	$Q_{l,i} = Q_{l,i\,attr,p+t} + Q_{l,i\,ades}$
		$\sigma_{vz} = q_s + (\gamma_1 z) + \Sigma_i \gamma_i Sp_i$	$u = (\gamma_w z) + \Sigma_i \gamma_w Sp_i$	$\sigma'_{vz} = (\sigma_{vz} - u)$	$\pi D\,(Sp\,\alpha\,c_u)_i$	$\pi D\,(Sp\,\beta_s\,\beta_n\,\sigma'_{vz,m})_i$	$Q_{l,i\,attr,p+t} + \pi D\,(Sp\,a\,c')_i$
	3 valori a dx per $\sigma(z)$	41.70	-	41.70			
z	6.00	141.90	50.00	91.90	257.86	-	-
	7.80	179.70	68.00	111.70	188.19	-	-
	9.60	224.70	86.00	138.70	503.06	-	-
	14.00	334.70	130.00	204.70	-	558.84	558.84

Pali Infissi MD o GD e Trivellati MD: valori di N_q dedotti da Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	Nq (L/D =5)	Nq (L/D =10)	Nq (L/D =20)	Nq (L/D =50)	L/D (palo)=	17.50	N_q(interp. per L/D palo)
1	-	-	-	-			-
2	-	-	-	-			-
3	-	-	-	-			-
4	448.28	366.85	317.06	293.89			329.50
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-

Pali Trivellati GD (N_q AGI1984): valori di N_q ridotti, raccomandati da AGI (1984), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)=	17.50	N_q(interp. per L/D palo)
1	-	-			-
2	-	-			-
3	-	-			-
4	50.11	51.21			50.64
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-

Pali Trivellati GD (N_q Vig./1999): valori di N_q ridotti, proposti da Viggiani (1999), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)=	17.50	N_q(interp. per L/D palo)
1	-	-			-
2	-	-			-
3	-	-			-
4	89.10	84.75			87.00
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-

In c. dr.: valore ottenuto, rispetto ai valori che precedono, in base a scelta effettuata per "Tecnologia, tipologia Diametro palo (e valori di calcolo N_q)"

N_q (ottenuto)	N_q (utente)	N_q (adottato)
-	-	-
-	-	-
-	-	-
50.64	-	50.64
-	-	-
-	-	-
-	-	-
-	-	-
-	-	-
-	-	-

RESISTENZA (laterale Q_{li} e di base o alla punta Q_b) CON I PARAMETRI MINIMI DEL TERRENO

Strato	$Q_{l,i}$ (kN)	$N_q = N_q$ (adottato)	N_c	$q_{b,i}$ (kN/mq)	$Q_{b,i}$ (kN)	$Q_{b,i,utente}$ (kN)	$Q_{b,i,adott}$ (kN)
			c. n. dr. $c_u>0$: 9	c. n. dr. $c_u>0$: $N_c c_u + \sigma_{vz}$			
			c. dr. $c'>0$: $(N_q - 1)\,\mathrm{ctg}\,\varphi'$	$c_u=0$: $c' N_c + N_q \sigma'_{vz}$	$= q_{b,i}\,A_p$		
1	257.86					-	
2	188.19					-	
3	503.06					-	
4	558.84	50.64	-	10,365.85	5,210.44	-	5,210.44
						-	
						-	
						-	
						-	
						-	
						-	

CAPACITA' PORTANTE MINIMA

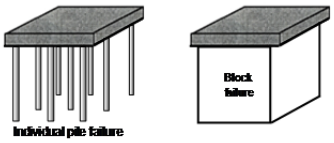
χ = fattore di riduzione capacità portante di base =	0.69
Base (per azione assiale $N_d \geq 0$): $R_{b,cal\,min} = \chi\, \Sigma_i Q_{b,i,adott}$ = kN	3,607.23
Laterale: $R_{s,cal\,min} = \Sigma_i Q_{l,i}$ = kN	1,507.95

CALCOLO DELLA RESISTENZA DI PROGETTO (CAPACITA PORTANTE)		
CARICO ASSIALE DI PROGETTO		
N'_d = azione assiale max di progetto = kN	1,503.19	-
	($N'_d \geq 0$)	($N'_d \leq 0$)
γ_g =	**1.00**	**1.00**
Valore assunto per $N_{at,n} = \Sigma\ (Q_{S,j\ attr\_p+1})_{<0}$ = kN	**a)medi**	**a)medi**
$N_{at,n} = \Sigma\ (Q_{S,j\ attr\_p+1})_{<0}$ = kN	-	-
$N''_d = \gamma_g\ I \Sigma\ (Q_{S,j\ attr\_p+1})_{<0}\ I$ = kN	-	-
	($N''_d \geq 0$)	($N''_d \geq 0$)
$N_d = N'_d + N''_d$ = kN	1,503.19	-
	(N_{d1}>0; sempre di compr.)	(N_{d2}> 0 opp. < 0)
RESISTENZA CARATTERISTICA	per N_{d1}	per N_{d2}
$R_{b,k} = Min(R_{b,cal\ med}/\xi_3\ ;\ R_{b,cal\ min}/\xi_4)$ = kN	2,121.90	-
$R_{s,k} = Min(R_{s,cal\ med}/\xi_3\ ;\ R_{s,cal\ min}/\xi_4)$ = kN	887.03	-
$R_{c,k} = R_{b,k} + R_{s,k}$ = kN	3,008.93	-
RESISTENZA DI PROGETTO (CAPACITA' PORTANTE)		
Per N_{d1}> 0 : $R_{c,d} = R_{bd}/\gamma_b + R_{sk}/\gamma_s$ = kN	2,343.11	
Per N_{d2}> 0 : $R_{c,d} = R_{bd}/\gamma_b + R_{sk}/\gamma_s$ = kN	-	
Per N_{d2}< 0 : $R_{t,d} = R_{bd}/\gamma_b + R_{sk}/\gamma_{st}$ = kN	-	
VERIFICA per N_{d1}>0		
$R_{c,d} / N_{d1}$ =	1.56	
$R_{c,d} \geq N_{d1}$?	ok	
VERIFICA per N_{d2}>0		
$R_{c,d} / N_{d2}$ =	-	
$R_{c,d} \geq N_{d2}$?	-	
VERIFICA per N_{d2}<0		
$R_{t,d} / I N_{d2} I$ =	-	
$R_{t,d} \geq I N_{d2} I$?	-	

I) Per il calcolo della portanza della palificata innanzitutto è necessario inserirne le caratteristiche geometriche (numero di pali, dimensioni in pianta, interassi ecc.); successivamente si sceglie per quali tipi di terreno effettuare le verifiche (terreni coerenti, incoerenti, entrambi). Nel caso in esame è stato scelto, a favore di sicurezza, di considerare per la portanza verticale solo l'effetto dei terreni incoerenti, assumendo un coefficiente di efficienza del gruppo di pali pari a 0.66, ovvero abbattendo la resistenza del singolo palo alla portanza verticale del 34%. Anche per quanto riguarda la portanza trasversale è stato scelto di verificare solo l'effetto indotto dai terreni incoerenti: è possibile scegliere tra l'approccio definito come MECCANISMI DI COLLASSO, dove la resistenza è valutata come il minimo tra la resistenza limite trasversale del singolo palo, moltiplicata per il numero di pali, e la resistenza del blocco, valutata con la relazione di Broms per palo corto, opportunamente calibrata per la palificata, oppure l'approccio MECCANISMO DI EFFICIENZA TRASVERSALE, dove la resistenza è valutata come il minimo tra la resistenza limite trasversale del singolo palo, moltiplicata per il numero di pali ed un coefficiente di efficienza in funzione del rapporto tra interasse e diametro del palo. Di seguito si riportano i risultati ottenuti.

PORTANZA LIMITE SLU-GEO DELLA PALIFICATA PER EFFETTO DI GRUPPO

NTC 6.4.3.1 ed EC7 7.7.1(4) Portanza limite SLU GEO della palificata per effetto di gruppo



1) Collasso per rottura del singolo palo — 2) Collasso per rottura del blocco

Sollecitazioni su mono-Palo o Palificata ?	**Palificata**
Dimensioni della palificata intesa come blocco	
B = m	9.00
H (H>B) = m	17.90
L = altezza della palificata = m	14.00
n_p = numero di pali della Palificata =	28.00
i = interasse dei pali = m	2.40
m = numero di file di pali =	4.00
n = n.o di pali in una fila =	7.00
Per la portata verticale si verifica su terreni: coerenti, incoerenti, entrambi ?	incoerenti
Per la portata trasversale si verifica su terreni: coerenti, incoerenti, entrambi ?	entrambi

Per portata VERTICALE della palificata

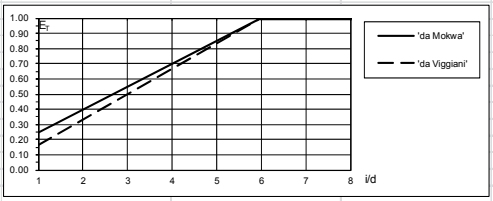
Terreni incoerenti

Collasso per rottura del singolo palo	
Resistenza limite verticale del singolo palo = $R_{c,d}$ = kN	2,343.11
n_p = numero di pali della Palificata =	28.00
Resistenza limite verticale palificata = R' = n_p x $R_{c,d}$ = kN	65,607.05
Resistenza limite verticale palificata = R'' = kN	-
Resistenza limite verticale palificata adottata = R_d = kN	65,607.05
Efficienza di gruppo = E_g =	**0.66**
Resistenza limite verticale palificata inclusiva effetti di gruppo= $R_{d,coll}$ = E_g R_d= kN	43,300.65
Verifica	
N_d = Forza verticale di progetto (di compressione) sulla palificata = kN	27,611.80
$R_{d,coll}$ / N_d =	1.57
$N_d \leq R_{d,coll}$?	ok

Per portata TRASVERSALE della palificata.

Terreni incoerenti

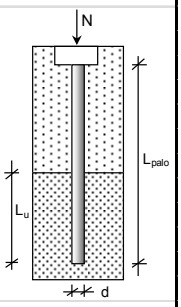
Dati a seguire dalla verifica SLU-GEO per carico limite trasversale di un palo con rotazione in testa impedita, su terreni incoerenti			
		γ_{γ} , $\gamma_{\varphi'}$ =	1.00
		γ_T =	1.30
		ξ_3 =	1.70
		ξ_4 =	1.70
		d = diametro sezione palo = m	0.80
		L_{palo} = Lunghezza del palo = m	14.00
		Peso di unità di volume γ (se falda $\gamma = \gamma'$) = kN/m^3 =	7.85
		Angolo medio di attrito del terreno = φ'_{med} = °	45.11
		Angolo minimo di attrito del terreno = φ'_{min} = °	44.29
		Peso di unità di volume di progetto $\gamma_d = \gamma/\gamma_{\gamma}$ = kN/m^3 =	7.85
		Angolo medio di attrito del terreno, di progetto = $\varphi'_{med,d} = \varphi'_{med}/\gamma_{\varphi'}$ = °	45.11
		Angolo minimo di attrito del terreno, di progetto = $\varphi'_{min,d} = \varphi'_{min}/\gamma_{\varphi'}$ = °	44.29
		Coeff. medio di spinta passiva $k_{p\,med,d} = (1 + \sin\varphi'_{med,d})/(1 - \sin\varphi'_{med,d})$ =	5.86
		Coeff. minimo di spinta passiva $k_{p\,min,d} = (1 + \sin\varphi'_{min,d})/(1 - \sin\varphi'_{min,d})$ =	5.63
		A) MECCANISMI DI COLLASSO	
		1) Collasso per rottura del singolo palo	
		Resistenza limite trasversale del singolo palo = $R_{tr,d}$ = kN	250.97
		n_p = numero di pali della Palificata =	28.00
		Resistenza limite trasversale palificata = $R'_1 = n_p \times R_{tr,d}$ = kN	7,027.09
		Resistenza limite trasversale palificata = R''_1 = kN	-
		Resistenza limite trasversale palificata adottata = R_1 = kN	7,027.09
		2) Collasso per rottura del blocco	
		Relazione di Broms per Palo corto: $H = 1{,}5\, k_p\, \gamma_d\, d\, L^2 = 1{,}5\, k_p\, \gamma_d\, d^3\, (L/d)^2$	
a) Forza in direzione X, direzione perpendicolare al lato B della palificata			
		d = B = m	9.00
		$H_{med} = H(k_p = k_{p\,med,d}) = 1{,}5\, k_{p\,med,d}\, \gamma_d\, B^3\, (L/B)^2$ = kN	121,722.66
		$H_{min} = H(k_p = k_{p\,min,d}) = 1{,}5\, k_{p\,min,d}\, \gamma_d\, B^3\, (L/B)^2$ = kN	116,918.24
		$H_k = \mathrm{Min}(H_{med}/\xi_3 ; H_{min}/\xi_4)$ = kN	68,775.43
		Resistenza limite trasversale palificata: $R_{2\_X} = H_k/\gamma_T$ = kN	52,904.18
b) Forza in direzione Y, direzione perpendicolare al lato H della palificata			
		d = H = m	17.90
		$H_{med} = H(k_p = k_{p\,med,d}) = 1{,}5\, k_{p\,med,d}\, \gamma_d\, H^3\, (L/H)^2$ = kN	242,092.85
		$H_{min} = H(k_p = k_{p\,min,d}) = 1{,}5\, k_{p\,min,d}\, \gamma_d\, H^3\, (L/H)^2$ = kN	232,537.38
		$H_k = \mathrm{Min}(H_{med}/\xi_3 ; H_{min}/\xi_4)$ = kN	136,786.70
		Resistenza limite trasversale palificata: $R_{2\_Y} = H_k/\gamma_T$ = kN	105,220.54
		Resistenza limite trasversale palificata: $R_2 = \min(R_{2\_X}, R_{2\_Y})$ = kN	52,904.18
A) Resistenza limite trasversale palificata = $R_{tr,d,coll} = \min(R_1, R_2)$ = kN			7,027.09
		B) MECCANISMO DI EFFICIENZA TRASVERSALE	
		Collasso per rottura del singolo palo	
		Resistenza limite trasversale del singolo palo = $R_{tr,d}$ = kN	250.97
		n_p = numero di pali della Palificata =	28.00
		Resistenza limite trasversale palificata = $R'_1 = n_p \times R_{tr,d}$ = kN	7,027.09
		Resistenza limite trasversale palificata = R'' = kN	-
		Resistenza limite trasversale palificata adottata = R_d = kN	7,027.09
		Metodi per calcolo Efficienza trasversale della palificata	
		1) MOKWA	
i/d =	1.00	6.00	
E_T =	0.25	1.00	
		i/d (in progetto)=	3.00
		i/d =	-
		i/d (adottato)=	3.00
E_T (calcolato per i/d adottato)= Efficienza Trasversale della palificata =			0.550
		2) VIGGIANI	
i/d =	3.00	6.00	
E_T =	0.50	1.00	
		i/d (in progetto)=	3.00
		i/d =	-
		i/d (adottato)=	3.00
E_T (calcolato per i/d adottato)= Efficienza Trasversale della palificata =			0.500
		3) Minimo tra 1) e 2)	0.500



		4) ALTRO	
		E_T = Efficienza Trasversale della palificata =	-
		Metodo scelto per adottare l'efficienza trasversale della palificata :	**3)Minimo tra 1) e 2)**
		$E_{T,ad}$ = Efficienza Trasversale adottata della palificata =	0.500
B) Resistenza limite trasversale palificata inclusiva effetti di gruppo= $R_{tr,d,coll} = E_{T,ad}\, R_d$ = kN			3,513.55
		C) Minimo tra A) e B): kN	3,513.55
		Meccanismo adottato ?	**C)Minimo tra A) e B)**
		$R_{tr,d,coll} = R_{tr,d,coll}$ adottata = kN	3,513.55
		Verifica	
		$F_{tr,d} = V$ = Forza trasversale di progetto sulla palificata = kN	2,196.65
		$R_{tr,d,coll} / F_{tr,d}$ =	1.60
		$F_{tr,d} \le R_{tr,d,coll}$?	ok

J) Per la valutazione dei cedimenti verticali si riportano i risultati ottenuti nel caso di analisi del mono-palo e di palificata

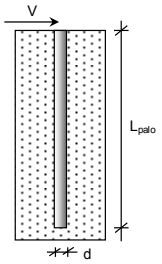
VERIFICA SLE PER CEDIMENTO VERTICALE		
Presenza di mono-Palo o Palificata ?	mono-Palo	
N= Carico verticale agente in Combinazione SLE :		
N = N_{max} = carico assiale max su mono-Palo = kN	889.89	
N = N_{pmedio} = carico assiale medio su singolo palo della Palificata = kN	-	
d = diametro sezione palo = m	0.80	
d = diametro sezione palo = m	-	
d = diametro sezione palo (adottato)=	0.80	
L = Lunghezza per valutare il coefficiente I_w = m	14.00	
E = Modulo di deformazione elastica del terreno = N/mmq	83.25	
In presenza di Palificata:		
i = interasse dei pali della Palificata = m	2.40	
L_{palo} = Lunghezza del palo = m	14.00	
n_p= numero di pali della Palificata =	-	
n_p= numero di pali della Palificata		
n_p= numero di pali della Palificata (adottato)=	-	
CEDIMENTO VERTICALE MASSIMO $\delta_{max,palo}$ DEL MONO PALO:		
I_w= Coefficiente di influenza = 0,5 + Log(L / D) =	1.74	
I_w= Coefficiente di influenza =	-	
I_w= Coefficiente di influenza (adottato) =	1.74	
$\delta_{max,palo}$ = $I_w N_{max}$ / (E L) = mm	1.33	
Verifica sul MONO PALO		
E_d= Cedimento verticale massimo su mono-palo, dovuto al carico agente in progetto = $\delta_{max,palo}$ = mm	1.33	
C_d= Cedimento verticale limite ammesso in progetto su mono-palo = mm	50.00	
$E_d \le C_d$	ok	



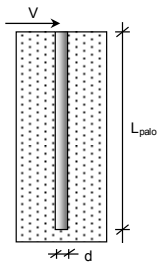
CEDIMENTO VERTICALE MASSIMO $\delta_{max,Palif}$ DELLA PALIFICATA:		
I_w= Coefficiente di influenza = 0,5 + Log(L / D) =	1.74	
I_w= Coefficiente di influenza =	-	
I_w= Coefficiente di influenza (adottato) =	1.74	
$\delta_{medio,palo}$ = I_w N_{pmedio} / (E L) = mm	1.04	
R = $(n_p \ i / L_{palo})^{1/2}$ =	2.19	
$R_{g,max}$ = coeff. di riduzione di gruppo = 0,5 / R + 0,13 / R^2 =	0.26	
$R_{g,max}$ = coeff. di riduzione di gruppo per calcolo $\delta_{max,Palif}$ =	-	
$R_{g,max}$ = coeff. di riduzione di gruppo (adottato)=	0.26	
$\delta_{max,Palif}$ = R_s δ = $(n_p \ R_{g,max})$ $\delta_{medio,palo}$ = mm	7.45	
CEDIMENTO VERTICALE MEDIO PIU' PROBABILE $\delta_{med,Palif}$ DELLA PALIFICATA:		
R_g = coeff. di riduzione di gruppo = 0,3 $R^{-1,2}$ =	0.12	
R_g = coeff. di riduzione di gruppo per calcolo $\delta_{med,Palif}$ =	-	
R_g = coeff. di riduzione di gruppo (adottato)=	0.12	
$\delta_{med,Palif}$ = R_s δ = $(n_p \ R_g)$ $\delta_{medio,palo}$ = mm	3.41	
CEDIMENTO VERTICALE DIFFERENZIALE MASSIMO $\Delta_{max,Palif}$ DELLA PALIFICATA:		
$R_{ds,max}$ = coeff. di riduzione di gruppo = 0,36 $R^{0,32}$ =	0.46	
$R_{ds,max}$ = coeff. di riduzione di gruppo per calcolo $\Delta_{max,Palif}$ =	-	
$R_{ds,max}$ = coeff. di riduzione di gruppo (adottato)=	0.46	
$\Delta_{max,Palif}$ = $R_{ds,max}$ $\delta_{med,Palif}$ = mm	1.58	
Verifiche sulla PALIFICATA		
E_d= Cedimento verticale massimo sulla palificata, dovuto al carico agente in progetto = $\delta_{max,Palif}$ = mm	7.45	
C_d= Corrispondente cedimento verticale limite, ammesso in progetto sulla palificata= mm	50.00	
$E_d \le C_d$?	ok	
E_d= Cedimento verticale medio più probabile sulla palificata, dovuto al carico in progetto = $\delta_{med,Palif}$ = mm	3.41	
C_d= Corrispondente cedimento verticale limite, ammesso in progetto sulla palificata= mm	30.00	
$E_d \le C_d$?	ok	
E_d= Cedimento verticale differenziale massimo sulla palificata, dovuto al carico in progetto = $\Delta_{max,Palif}$ = mm	1.58	
C_d= Corrispondente cedimento verticale differenziale limite, ammesso in progetto sulla palificata= mm	10.00	
$E_d \le C_d$?	ok	

K) Per la valutazione dei cedimenti orizzontali si riportano i risultati ottenuti nel caso di analisi del mono-palo e di palificata

VERIFICA SLE DELLO SPOSTAMENTO TRASVERSALE DI UN PALO CON ROTAZIONE IN TESTA IMPEDITA.	
Presenza di mono-Palo o Palificata ?	mono-Palo
V= Carico orizzontale agente in Combinazione SLE = kN	291.45
V= Carico orizzontale agente in Combinazione SLE = kN	-
V= Carico orizzontale agente in Combinazione SLE (adottato) = kN	291.45
d = diametro sezione palo = m	0.80
d = diametro sezione palo = m	-
d = diametro sezione palo (adottato)=	0.80
L_{palo} = Lunghezza del palo = m	**14.00**
In presenza di Palificata:	
n_p= numero di pali della Palificata =	-
n_p= numero di pali della Palificata	-
n_p= numero di pali della Palificata (adottato)=	-
K_{h_int}= coefficiente di reazione laterale del terreno = N/cm^3 =	**5.29**
r = fattore di riduzione di K_{h_int} in presenza di Palificata (Poulos e Davis, 1980) =	-
r = fattore di riduzione=	-
r = fattore di riduzione (adottato)=	-
K_{h_rid}= coefficiente di reazione laterale del terreno (Palificata)= r K_{h_int} = N/cm^3	-
K_h= (K_{h_int} se mono-Palo; K_{h_rid} se Palificata)= N/cm^3	5.29
f_{ck}= 0,83 R_{ck}= N/mmq	33.20
R_{ck}= N/mmq	**40.00**
E_{cm} = 22.000 $[f_{cm}/10]^{0,3}$ = 22.000 $[(f_{ck}+8)/10]^{0,3}$ =N/mmq	33,642.78
$J_p = \pi\, d^4 / 64$ = cm^4	2,010,619.30
λ = lunghezza elastica= $(4\, E_{cm} J_p / K_h d)^{1/4}$ = cm	502.84
VERIFICA SPOSTAMENTO TRASVERSALE DEL mono-Palo (spost. medio se Palificata)	
spostamento trasversale max dovuto al carico agente in progetto= spostamento y(z=0) = mm	13.696
C_d= spostamento trasversale limite ammesso in progetto = mm	**20.00**
$E_d \le C_d$?	ok



VERIFICA SLE DELLO SPOSTAMENTO TRASVERSALE DI UN PALO CON ROTAZIONE IN TESTA IMPEDITA.	
Presenza di mono-Palo o Palificata ?	Palificata
V= Carico orizzontale agente in Combinazione SLE = kN	52.30
V= Carico orizzontale agente in Combinazione SLE = kN	-
V= Carico orizzontale agente in Combinazione SLE (adottato) = kN	52.30
d = diametro sezione palo = m	0.80
d = diametro sezione palo = m	-
d = diametro sezione palo (adottato)=	0.80
L_{palo} = Lunghezza del palo = m	**14.00**
In presenza di Palificata:	
n_p= numero di pali della Palificata =	28.00
n_p= numero di pali della Palificata	-
n_p= numero di pali della Palificata (adottato)=	28.00
K_{h_int}= coefficiente di reazione laterale del terreno = N/cm^3 =	**5.29**
r = fattore di riduzione di K_{h_int} in presenza di Palificata (Poulos e Davis, 1980) =	0.25
r = fattore di riduzione=	-
r = fattore di riduzione (adottato)=	0.25
K_{h_rid}= coefficiente di reazione laterale del terreno (Palificata)= r K_{h_int} = N/cm^3	1.32
K_h= (K_{h_int} se mono-Palo; K_{h_rid} se Palificata)= N/cm^3	1.32
f_{ck}= 0,83 R_{ck}= N/mmq	33.20
R_{ck}= N/mmq	**40.00**
E_{cm} = 22.000 $[f_{cm}/10]^{0,3}$ = 22.000 $[(f_{ck}+8)/10]^{0,3}$ =N/mmq	33,642.78
$J_p = \pi\, d^4 / 64$ = cm^4	2,010,619.30
λ = lunghezza elastica= $(4\, E_{cm} J_p / K_h d)^{1/4}$ = cm	711.13
VERIFICA SPOSTAMENTO TRASVERSALE DEL mono-Palo (spost. medio se Palificata)	
spostamento trasversale max dovuto al carico agente in progetto= spostamento y(z=0) = mm	6.952
C_d= spostamento trasversale limite ammesso in progetto = mm	**20.00**
$E_d \le C_d$?	ok



4.11 Sfioratore laterale

4.11.1 Introduzione

L'analisi della struttura dello sfioratore è stata effettuata considerando lo scenario idrico peggiore, ovvero considerando un tempo di ritorno pari a 500 anni; in questo modo, nota la spinta dell'acqua, è stato possibile determinare le sollecitazioni e le armature necessarie per il manufatto di sfioro e per i pali di fondazione.
L'analisi dei pali è stata svolta sfruttando un foglio di calcolo opportunamente sviluppato per le verifiche strutturali e geotecniche di fondazioni profonde.
L'iter seguito per le verifiche è stato il seguente:

A) Inserimento dei parametri del terreno definiti tramite analisi MASW, per la determina dell'effetto di interazione cinematica sul palo dovuto al passaggio da uno strato all'altro di terreno;
B) Inserimento delle sollecitazioni di progetto: quest'ultime sono state ricavate da un apposito foglio di calcolo, inserendo le condizioni di carico descritte precedentemente. In particolare sono state inserite le azioni tali per cui risultasse:
    - N_{MAX}, con i relativi momenti M_x e M_y
    - N_{MIN}, con i relativi momenti M_x e M_y
    - Massima media geometrica tra M_x e M_y, con la relativa azione assiale N
    - Minima media geometrica tra M_x e M_y, con la relativa azione assiale N
    - Massima media geometrica tra V_x e V_y, con la relativa azione assiale N
C) Verifiche strutturali a presso/tenso – flessione ed a taglio, con inserimento delle caratteristiche geometriche del palo, tipo di materiali utilizzati, armature longitudinali e trasversali per determinare le resistenze di progetto;
D) Verifica strutturale a stabilità laterale del palo, con inserimento di coefficienti di reazione laterale per simulare l'effetto stabilizzante del terreno;
E) Verifica geotecnica per portanza trasversale del terreno per terreni coerenti o incoerenti;
F) Verifica geotecnica per portanza verticale del terreno per terreni coerenti o incoerenti;
G) Verifiche SLE nei riguardi di spostamenti limite traversali e verticali;

Non sono state effettuate in questo caso verifiche di tipo globale ma solo sul singolo palo.

4.11.2 Analisi

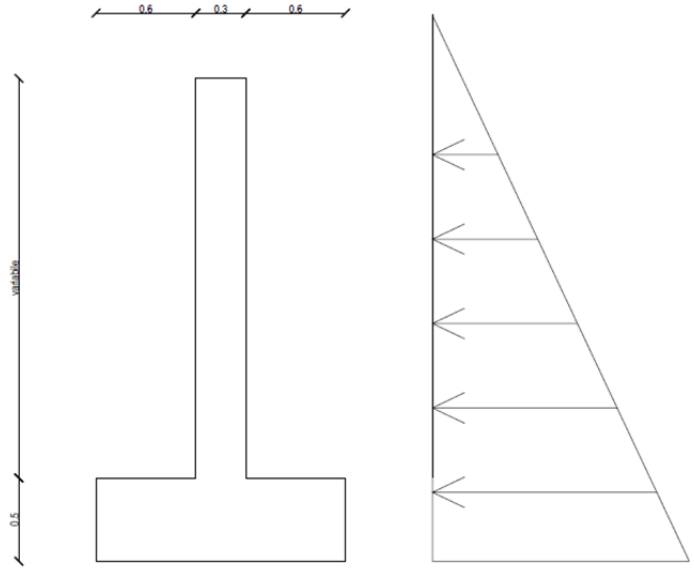
Le azioni sullo sfioratore sono state determinate secondo lo scenario T = 500 anni precedentemente descritto, e che prevede una quota del fronte d'acqua superiore di 38 cm rispetto alla sommità del manufatto.
Per quanto riguarda lo sfioratore sono state considerate le seguenti ipotesi di calcolo:

- Spessore in testa	0.30 m
- Altezza sfioratore	2.40 m
- Altezza fondazione	0.50 m
- Lunghezza ciabatte	0.60 m
- Altezza sfioro acqua al di sopra muro	0.38 m
- Diametro pali	0.70 m

- Altezza pali 14.0 m
- Interasse tra i pali 2.40 m
- Peso specifico acqua 1100 daN/m^3
- Peso specifico cls 2500 daN/m^3
- Peso specifico terreno 1700 daN/m^3
- Coefficiente amplificativo acqua 1.50
- Coefficiente amplificativo cls 1.35
- Coefficiente amplificativo terreno 1.35

Da ciò si ricavano le seguenti azioni sul singolo palo:

- N_{max} = 53777.7 daN
- N_{min} = 38163.3 daN
- M_{max} = 23289.8 daNm
- M_{min} = 0.0 daNm
- T_{max} = 21301.6 daN



A livello strutturale il paramento dello sfioratore viene verificato come se fosse una mensola incastrata alla base: considerando una distribuzione triangolare della spinta dell'acqua, si ottiene un valore di momento e taglio rispettivamente pari a M = 5908.4 daNm/m e T = 6375.9 daN/m. Avendo un'altezza utile di 240 mm si ottiene un'armatura minima pari a 699.6 mm^2/m, pertanto verranno inseriti 5 Φ 14 / m (770 mm^2 / m). A livello di taglio resistente si ricava un valore di k = 1.91 (NTC §4.1.2.1.3.1) e di conseguenza un valore di v_{min} = 0.52, pertanto il taglio resistente risulta essere pari a 12571.4 daN/m. Le verifiche risultano quindi soddisfatte.

La fondazione invece è stata considerata alla stregua di trave in semplice appoggio, di luce l=2.40m, soggetta ad un carico massimo q = 53777.7 daN / 2.4m = 22407.4 daN/m; si ottiene pertanto un momento e taglio rispettivamente pari a M = 16133.3 daNm e T = 26888.8 daN. Avendo un'altezza utile di 440 mm si ottiene un'armatura minima pari a 1041.9 mm^2, pertanto verranno inseriti 9 Φ 14 (1386 mm^2). A livello di taglio resistente si ricava un valore di k = 1.67 (NTC §4.1.2.1.3.1) e di conseguenza un valore di v_{min} = 0.43, pertanto il taglio resistente risulta essere pari a 28307.3 daN. Le verifiche risultano quindi soddisfatte.

Si riportano ora i calcoli effettuati con i relativi risultati per ciascuno dei punti precedentemente descritti in relazione alle verifiche sul singolo palo.

A) Si considera l'azione cinematica, cioè l'effetto dovuto al passaggio tra uno strato di terreno e l'altro; inserendo i dati relativi alle caratteristiche del singolo palo (diametro 0.70 m, lunghezza 14 m, modulo elastico 33350 MPa) e relativi alle caratteristiche dei terreni attraversati, ricavati dalle prove MASW, si ricava un valore di momento di interazione cinematica, per terreno catalogato di tipo C e seguendo le indicazioni del modello di Nikolaou et Alt, pari a 10001 daNm. Questo valore sarà utilizzato nelle verifiche strutturali successive.

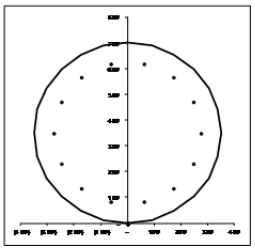
Si considera l'interazione cinematica (M) ?	**si**
d = diametro palo= **m**	**0.70**
L = lunghezza palo= **m**	**14.00**
E_p = modulo elastico di rigidezza assiale del palo= **N/mmq**	**33,350.00**
STRATO 1	
tipo strato:	**-**
h_1 = altezza strato= **m**	**15.00**
$V_{s,1}$ = velocità delle onde di taglio= **m/s**	**127.00**
ρ_1 = densità (massa per unità di volume)= **kN s^2 / m^4**	**17.50**
ν_1 = coeff. di poisson=	**0.20**
STRATO 2	
tipo strato:	
h_2 = altezza strato= **m**	**18.20**
$V_{s,2}$ = velocità delle onde di taglio= **m/s**	**329.00**
ρ_2 = densità (massa per unità di volume)= **kN s^2 / m^4**	**25.00**
ν_2 = coeff. di poisson=	**0.23**
ACCELERAZIONE SISMICA DEL SITO	
a_g/g = (accelerazione massima attesa su sito di riferimento rigido) / g =	**0.065**
F_o = fattore amplif. spettrale massima, su sito di rif. rigido (se F_o< 2,2 occorre adottare 2,2) =	**2.664**
$V_{s,30}$ = $V_{s,1}$ = m/s	127.00
Categoria di sottosuolo di progetto =	**C**
A: S_S=	1.000
B: S_S=	1.200
C: S_S=	1.500
D: S_S=	1.800
E: S_S=	1.600
S_S = effetto amplificazione stratigrafica sul sottosuolo in progetto:	1.500
Categoria topografica in progetto =	**T1**
S_T= effetto dell'amplificazione topografica (1,0 se T1; 1,2 se T2; 1,2 se T3; 1,4 se T4)=	1.000
S = S_S S_T=	1.500
Accelerazione massima al sito / g = a_{max}/g = S a_g/g =	0.098
Accelerazione massima al sito = a_{max}= (S a_g/g) g = m/sec^2	0.956
G_1 =Modulo di taglio dello strato 1 = ρ_1 $V_{s,1}^2$ = N/mmq	282.26
E_1 = Modulo di Young dello strato 1= 2 (1 + ν_1) G_1 = N/mmq	677.42
G_2 =Modulo di taglio dello strato 1 = ρ_2 $V_{s,2}^2$ = N/mmq	2,706.03
E_2 = Modulo di Young dello strato 1= 2 (1 + ν_2) G_2 = N/mmq	6,656.82
Rapporto di snellezza = L/d =	20.00
J_p = Momento di inerzia del palo = π d^4 / 64 = m^4	0.0118
E_p / E_1 =	49.23
L_a= Lunghezza attiva = 1,5 d (E_p / E_1)^{0,25} =	2.78
h_1 > L_a?	si
(L'equazione a seguire per M è valida a rigore quando h_1>L_a; ovvero quando l'interfaccia tra i due strati si trova a una profondità superiore alla Lunghezza attiva del palo)	
$V_{s,2}$ / $V_{s,1}$ =	2.59
τ_c =Tensione di taglio all'interfaccia (contatto) tra i due strati = a_{max} ρ_1 h_1 = kN/mq	251.07
Momento all'interfaccia (contatto) tra i due strati in condizioni di moto stazionario:	
M = 0,042 τ_c d^3 (L /d)^{0,30} (E_p/ E_1)^{0,65} ($V_{s,2}$/$V_{s,1}$)^{0,50} = kNm	180.01
VALUTAZIONE DEL FATTORE δ DI RIDUZIONE DEL MOMENTO	
funzione del numero di cicli effettivi e del periodo dominante dell'accelerogramma	
Valutazione 1) per δ:	
N_c = n.o di cicli effettivi dell'accelerogramma=	**-**
Periodo naturale del deposito prossimo ai periodi predominanti dell'eccitaz. sismica:	
δ = 0,04 N_c + 0,23=	0.23
Periodo naturale del deposito che si allontana dai periodi predominanti dell'eccitaz. sismica:	
δ = 0,015 N_c + 0,17=	0.17
δ scelto in base ai due valori calcolati =	**-**
Valutazione 2) per δ:	
δ nel campo dei valori frequenti (variabile in genere tra 0,17 e 0,50); risulta **δ =**	**0.50**
Valutazione adottata per δ=	**2)**
δ = δ adottato=	0.50
M_{CIN} = Momento cinematico all'interfaccia tra i 2 strati (NIKOLAOU et Alt., 2001)= δ M = kNm	90.01
τ_{ff} = tensione tangenziale all'interfaccia da analisi di free-field= kN/mq	**-**
M_{CIN} = Momento cinematico all'interfaccia tra i 2 strati (MAIORANO et Alt., 2009):	
0,071 τ_{ff} d^3 (L /d)^{0,30} (E_p/ E_1)^{0,65} ($V_{s,2}$/$V_{s,1}$)^{0,50} = kNm	-
Valore adottato per M_{CIN}=	**NIKOLAOU et Alt 2001**
M_{CIN} = Momento cinematico all'interfaccia tra i 2 strati = valore adottato= kNm	90.01
M_{INERZ} (su monopalo o singolo palo della palificata) **= kNm**	**10.00**
Moto cinematico e inerziale: in fase oppure sfasati?	**fase**
M_{RIS} = Momento risultante (su monopalo o singolo palo della palificata) = kNm	100.01

B) Inserimento delle azioni sollecitanti, riportate in precedenza.

Sollecitazioni su mono-Palo o Palificata ?			**mono-Palo**			
1) PER VERIFICHE SLU						
				Coefficienti parziali Azioni (A1, A2)		
				perm. γ_G (se fav.)	var. γ_Q (se fav.)	
SLU: combinazioni NON SISMICHE tipo: $\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \Sigma_{i=2,n} (\gamma_{Qi} \psi_{oi} Q_{ki})$						
App. 1	Comb. 1 (STR): A1+M1+R1			1,30 (1,00)	1,50 (0,00)	
	Comb. 2 (GEO) : A2+M1+R2			1,00 (1,00)	1,30 (0,00)	
App. 2	Comb. unica (STR, GEO) : A1+M1+R3			1,30 (1,00)	1,50 (0,00)	
SLU: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_i (\psi_{2i} Q_{ki})$						
App. 1	Comb. 1 (STR): A1+M1+R1			1.00	1.00	
	Comb. 2 (GEO) : A2+M1+R2			1.00	1.00	
App. 2	Comb. unica (STR, GEO) : A1+M1+R3			1.00	1.00	
Approccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)			**2**			
			mono-Palo		Palificata	
			Verifiche SLU_STR	Verifiche SLU_GEO	Verifiche SLU_STR	Verifiche SLU_GEO
Relativa Comb. associata all'Approccio scelto:			unica	unica	unica	unica
All'interno dell'app. scelto, riportare, per la comb. associata, i valori a seguire:						
Ai fini di SLU_STR_(N,M); resistenza SLU (N,M) dei pali						
N compressione (+), tra terne non sismiche e sismiche			Verifiche SLU_STR		Verifiche SLU_STR	
		$N=N_{min}$= kN	**381.63**			
		M_x = kNm	-			
		M_y = kNm	-			
		$N=N_{max}$= kN	**537.77**			
		M_x = kNm	**232.89**			
		M_y = kNm	-			
	$\{(M_x^2+M_y^2)^{1/2}\}$ = min	**N= kN**	**381.63**			
		M_x = kNm	-			
		M_y = kNm	-			
	$\{(M_x^2+M_y^2)^{1/2}\}$ = max	**N= kN**	**537.77**			
		M_x = kNm	**232.89**			
		M_y = kNm	-		-	
N trazione (-), tra terne non sismiche e sismiche			Verifiche SLU_STR		Verifiche SLU_STR	
		$N=N_{min}$= kN	-		-	
		M_x = kNm	-		-	
		M_y = kNm	-		-	
		$N=N_{max}$= kN	-		-	
		M_x = kNm	-		-	
		M_y = kNm	-		-	
	$\{(M_x^2+M_y^2)^{1/2}\}$ = min	**N= kN**	-		-	
		M_x = kNm	-		-	
		M_y = kNm	-		-	
	$\{(M_x^2+M_y^2)^{1/2}\}$ = max	**N= kN**	-		-	
		M_x = kNm	-		-	
		M_y = kNm	-		-	
		Interazione cinematica	Verifiche SLU_STR		Verifiche SLU_STR	
M_{CIN} (su monopalo o singolo palo della palificata) = kNm			90.01		90.01	
M_{INERZ} (su monopalo o singolo palo della palificata) = kNm			10.00		10.00	
M_{RIS} (su monopalo o singolo palo della palificata) = kNm			100.01		100.01	
N (tra le combinazioni SLU_STR sismiche)= kN			**381.63**			
M_x = kNm					-	
M_y = kNm					-	
Ai fini di SLU_STR_(V); resistenza SLU a Taglio dei pali			Verifiche SLU_STR		Verifiche SLU_STR	
V tra combin. non sismiche e sismiche = max $\{(V_x^2+V_y^2)^{1/2}\}$ = kN			**213.01**			
Ai fini di SLU_STR_(N)_st_eq_el; stab. equilibrio elastico dei pali			Verifiche SLU_STR		Verifiche SLU_STR	
N= N di compressione (+) = kN			**537.77**			
M_x = kNm						
M_y = kNm					-	
Ai fini di SLU_GEO_qlim_trasv_t_c e SLU_GEO_qlim_trasv_t_i: portanza limite SLU trasversale				Verifiche SLU_GEO		Verifiche SLU_GEO
V tra combin. non sismiche e sismiche = kN				**213.01**		
M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rd}; calcolato per						
a) N=0				-		-
b) N associato alla combinazione in cui opera V : N= kN				**537.77**		
M_x = kNm						
M_y = kNm						
Ai fini di SLU_GEO_qlim_vert: portanza limite SLU verticale				Verifiche SLU_GEO		Verifiche SLU_GEO
N= N di compressione (+) tra terne non sismiche e sismiche= kN				**537.77**		
M_x = kNm						
M_y = kNm						-
N= N di trazione (-) tra terne non sismiche e sismiche= kN				-		-
M_x = kNm						-
M_y = kNm						-
Ai fini di SLU_GEO_Grup: portanze limiti SLU palificata per effetto di gruppo						Verifiche SLU_GEO
V tra combin. non sismiche e sismiche = kN						-
Valore (utente) = kN						-
Valore adottato = kN						-
N= N di compressione (+) tra terne non sismiche e sismiche= kN						-
Valore (utente) = kN						-
Valore adottato = kN						-
2) PER VERIFICHE SLE						
SLE: combinazioni NON SISMICHE tipo QUASI PERM. $G_1 + G_2 + \psi_{21} Q_{k1} + \Sigma_i (\psi_{2i} Q_{ki})$; per SLE combinazioni non sismiche, di regola solo questa per cedimenti e spostamenti						
SLE: combinazioni NON SISMICHE tipo FREQUENTE $G_1 + G_2 + \psi_{11} Q_{k1} + \Sigma_i (\psi_{2i} Q_{ki})$						
SLE: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_i (\psi_{2i} Q_{ki})$						
			mono-Palo		Palificata	
Riportare, per le comb. considerate i valori a seguire:						
Ai fini di SLE_ced_vert: cedimento max SLE verticale			Verifiche SLE		Verifiche SLE	
N= N di compressione (+) = kN			**381.63**			
M_x = kNm						
M_y = kNm					-	
Ai fini di SLE_sp_trasv: spostamento max SLE trasversale			Verifiche SLE		Verifiche SLE	
V tra combin. non sismiche e sismiche: V = max $\{(V_x^2+V_y^2)^{1/2}\}$ = kN			**142.00**			

C) Verifiche strutturali a presso-tenso flessione: vengono inserite le caratteristiche geometriche e meccaniche dei singoli pali, il numero ed il diametro delle armature longitudinali, determinando quindi il valore di momento resistente della sezione. In sintesi, sono stati scelti pali di diametro 0.70 m armati con 14Φ20 longitudinalmente.

Cls				
f_{ck}= 0,83 R_{ck}= N/mmq	33.20			
R_{ck}= N/mmq	40.00			
γ_c =	1.50			
f_{cd}= α_{cc} f_{ck}/γ_c= 0,85 f_{ck}/γ_c= N/mmq	18.81			
Acciaio				
f_{yk}= N/mmq	450.00			
γ_s =	1.15			
f_{yd} = f_{yk}/γ_s= N/mmq	391.30			
E_s =N/mmq	200,000.00			
ε_{yd}= f_{yd}/E_s=	0.196%			
Copriferro	(EC2)			(Circ.-NTC)
$c_{min,b}$ = mm	-	elemento:		Palo
$c_{min,dur}$ = mm	-	vita nominale Vn:		100
$\Delta c_{dur,\gamma}$ = mm	-	ambiente:		aggressivo
$\Delta c_{dur,st}$ = mm	-	$c_{min,dur}$ = mm		45.00
$\Delta c_{dur,add}$ = mm	-	Δc_{dev} = mm		-
Δc_{dev} = mm	-	Δc_{dev} = mm		10.00
$c_{min,dur}$ + $\Delta c_{dur,\gamma}$ - $\Delta c_{dur,st}$ - $\Delta c_{dur,add}$= mm	-			
c_{min} = max{$c_{min,b}$; $c_{min,dur}$ + $\Delta c_{dur,\gamma}$ - $\Delta c_{dur,st}$ - $\Delta c_{dur,add}$; 10 mm} = mm	-	c_{min}=$c_{min,dur}$- Δc_{dur}=		45.00
c_{nom} = c_{min} + Δc_{dev} = mm	55.00			
ϕ_{st} = ϕ staffa (max)= mm	10.00			
ϕ_b = ϕ barra (max)= mm	20.00			
$c_{_{calc}}$ = dist. min. da bordo a baric. barre strato 1 = c_{nom} + ϕ_{st} + ϕ_b/2 =mm	75.00			
Sezione				
d= diametro sezione palo = mm	700.00			
Ac= π(d/2)^2= mmq	384,845.10			
Strato 1 (esterno)				
$c_{s,1}$= dist. da bordo a baricentro barre strato 1 = mm	75.00			
N.o barre = $N_{b,1}$=	14.00			
$\phi_{b,1}$ = mm	20.00			
Area totale barre= $A_{sk,1}$= mmq	4,398.23			
Strato 2 (intermedio)				
$c_{s,2}$= dist. da bordo a baricentro barre strato 2 = mm	-			
N.o barre = $N_{b,2}$=	-			
$\phi_{b,2}$ = mm	-			
Area totale barre= $A_{sk,2}$= mmq	-			
Strato 3 (interno)				
$c_{s,3}$= dist. da bordo a baricentro barre strato 3 = mm	-			
N.o barre = $N_{b,3}$=	-			
$\phi_{b,3}$ = mm	-			
Area totale barre= $A_{sk,3}$= mmq	-			
As= As totale = $\Sigma_{i=1,3} A_{sk,i}$= mmq	4,398.23			
ρ_s = As/Ac = %	1.14%			
ρ_{min} = (inf per 0,3% ; sup per 1%) = %	inf			
ρ_{min} (adottato) =	0.30%			
$\rho_s \geq \rho_{min}$ (adottato) ?	ok			
Calcola M_{Rd} per N assegnati				



mono-Palo

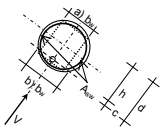
Verifica SLU_STR_(N,M); resistenza SLU (N,M) dei pali

		Verifiche SLU_STR	$M_R=(M_x^2+M_y^2)^{1/2}$	M_{Rd} (II) kNm	$M_{Rd} \geq M_R$?
N compressione (+), tra terne non sismiche e sismiche	N=N_{min}= kN	381.63			
	M_x = kNm	-			
	M_y = kNm	-	-	515.30	ok
	N=N_{max}= kN	537.77			
	M_x = kNm	232.89			
	M_y = kNm	-	232.89	543.10	ok
	N= kN	381.63			
	M_x = kNm	-			
	M_y = kNm	-	-	515.30	ok
	N= kN	537.77			
	M_x = kNm	232.89			
	M_y = kNm	-	232.89	543.10	ok
		Verifiche SLU_STR			
N trazione (-), tra terne non sismiche e sismiche	N=N_{min}= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	440.46	ok
	N=N_{max}= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	440.46	ok
	N= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	440.46	ok
	N= kN	-			
	M_x = kNm	-			
	M_y = kNm	-	-	440.46	ok
		Verifiche SLU_STR			
Interazione cinematica	N = kN	381.63	M_R=M_{Rx}= kNm	M_{Rd} (II) kNm	$M_{Rd} \geq M_R$?
	M_{Rx}= kNm	100.01	100.01	515.30	ok

Ai fini di SLU_GEO_qlim_trasv_t_c e SLU_GEO_qlim_trasv_t_i: portanza limite SLU trasversale

	Verifiche SLU_GEO		
V tra combin. non sismiche e sismiche = kN	213.01		
M_y = Momento di plasticizzazione della sezione (B cons)= M_{Rd}; calcolato per			M_{Rd} (II) kNm
a) N=0	-		440.46
b) N associato alla combinazione in cui opera V: N= kN	537.77		543.10

D) Verifiche strutturali a taglio: vengono inserite le caratteristiche delle armature trasversali (diametro, passo) e si sceglie se valutare la resistenza del palo secondo i dettami delle NTC ’08 al paragrafo §4.1.2.1.3.1, oppure se progettare le staffature resistenti a taglio. In definitiva vengono utilizzate staffe Φ10 passo 15 cm.



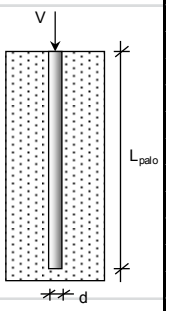
h=d-c

a) max inerzia: b_w=0,581 d

b) min corda: b_w=2 $[(d/2)^2 - (d/2-c)^2]^{1/2}$

Cls	
f_{ck}= N/mmq	33.20
R_{ck}= N/mmq	40.00
γ_c =	1.50
$f_{cd} = \alpha_{cc}\ f_{ck}/\gamma_c$= 0,85 f_{ck}/γ_c= N/mmq	18.81
f_{ctm}= 0,30 $f_{ck}^{2/3}$= N/mmq	3.10
$f_{ctk0.05}$ = 0,7 f_{ctm} = N/mmq	2.17
$f_{ctd} = f_{ctk0,05}/\gamma_c$ = N/mmq	1.45
Acciaio	
f_{yk}= N/mmq	450.00
γ_s =	1.15
$f_{yd} = f_{yk}/\gamma_s$= N/mmq	391.30
E_s =N/mmq	200,000.00
$\varepsilon_{syd} = f_{yd}/E_s$=	0.001957
Sollecitazioni	
Presenza di mono-Palo o Palificata ?	mono-Palo
V= kN	213.01
V = kN	-
V (adottato) = kN	213.01
d= diametro sezione palo = mm	700.00
Ac=$\pi(d/2)^2$= mmq	384,845.10
c = dist. da bordo a baricentro barre strato = mm	
strato 1° : $c_{b,1}$ = mm	75.00
strato 2° : $c_{b,2}$ = mm	-
strato 3° : $c_{b,3}$ = mm	-
c_{medio} = mm	75.00
c_{min}= mm	-
c_{max}= mm	75.00
c (adottato) = mm	**72.00**
h = d - c =mm	628.00
Per b_w si utilizza il criterio a)max inerzia, b)min corda, c)Min a) b)?	**c)Min a) b)**
b_w =mm	406.70
Si procede alle verifiche senza staffature resistenti a taglio?	**si**
Si procede al dimensionamento con staffature resistenti a taglio?	**si**
l_p= lunghezza palo= m	**14.00**
Vc= Ac l_p = mc	5.39
Verifica senza staffature resistenti a taglio	
V (adottato) = V_{Ed} = kN	213.0
k = min [1 + (200/h)$^{1/2}$; 2]=	1.564
N_{Ed}= forza assiale di calcolo di compressione (positiva)= kN	-
σ_{cp} = min [(N_{Ed}/Ac) ; 0,2 f_{cd}]= N/mmq	-
As_l= mmq	**2,002.00**
ρ_l = min [As_l/(b_w h); 0,02]=	0.0078
v_{min} = 0,035 $k^{3/2}$ $f_{ck}^{1/2}$= N/mmq	0.395
V_{Rd} = [v_{min} + 0,15 σ_{cp}] b_w h= kN	100.8
V^*_{Rd}= [0,18 k (100 ρ_l f_{ck})$^{1/3}$ / γ_c + 0,15 σ_{cp}] b_w h= kN	142.1
V_{Rd} = max [V_{Rd}; V^*_{Rd}]= kN	142.1
$V_{Rd} \geq V_{Ed}$?	No !
Dimensionamento con staffature resistenti a taglio	
Per gli N_{Ed}, si pone α_c=1 ?	**si**
N (kN)	-
σ_{cp} = N/Ac= N/mmq	-
1) α_c : [1+ σ_{cp}/f_{cd} se $0 \leq \sigma_{cp} < 0{,}25 f_{cd}$; 1,25 se $0{,}25 f_{cd} \leq \sigma_{cp} \leq 0{,}5 f_{cd}$; 2,5(1- σ_{cp}/f_{cd}) se $0{,}5 f_{cd} < \sigma_{cp} < f_{cd}$]	-
2) α_c pari al minimo tra quelli valutati per tutti gli N di compress.	-
Procedere con la valutazione 1) oppure 2) ?	**1)**
α_c adottato.	1.000
V (adottato) =V_{Ed} = kN	213.0
s (passo staffe adottato)= **mm**	**150.00**
n_b (n.o bracci delle staffe adottato) =	**2.00**
Diametri adottati per le staffe:	
1° perimetro: ϕ_1 = mm	**10.00**
$A1_{\phi 1}$= $\pi(\phi_1/2)^2$ = mmq	78.54
2° perimetro: ϕ_2 = mm	**-**
$A1_{\phi 2}$= $\pi(\phi_2/2)^2$ = mmq	-
3° perimetro: ϕ_3 = mm	**-**
$A1_{\phi 3}$= $\pi(\phi_3/2)^2$ = mmq	-
Asw = n_b [$A1_{\phi 1}$ + $A1_{\phi 2}$ + $A1_{\phi 3}$] = mmq	157.08
Asw f_{yd}/ b_ws=	1.01
1/2 α_c 0,5 f_{cd}=	4.70
Controllo che cotg$\vartheta \geq$1 ($\vartheta \leq$45°); con ϑ_{max}=45° : Asw f_{yd}/ b_ws ≤ 1/2 α_c 0,5 f_{cd} ?	ok
ϑ' = arcsin (Asw f_{yd}/ b_ws α_c 0,5 f_{cd})$^{1/2}$ = °	19.10
Controllo che cotg$\vartheta' \leq$2,5 ($\vartheta' \geq \vartheta_{min}$=21,8°); se $\vartheta' \geq \vartheta_{min}$ si assume ϑ=ϑ'; se $\vartheta' < \vartheta_{min}$ si assume ϑ=21,8° : ϑ adottato=ϑ=	21.80
V_{Rsd} = 0,9 h (Asw/s) f_{yd} ctgϑ = kN	579.1
V_{Rcd}= 0,9 h $b_w \alpha_c$ (0,5 f_{cd}) ctgϑ / (1 + ctg$^2\vartheta$)= 0,9 h $b_w \alpha_c$ (0,5 f_{cd}) / (ctgϑ + tgϑ)= kN	745.6
V_{Rd}= [V_{Rsd} se $\vartheta' \leq$21°,8 e ϑ=21°,8; altrimenti min(V_{Rsd} ; V_{Rcd})]= kN	579.1
$V_{Rd} \geq V_{Ed}$?	ok
Prescrizioni armature	
Attivare prescrizioni armature ?	**si**
$\phi_{L,min}$ (diametro min. delle barre longitudinali)=mm	**14.00**
$\phi_{L,max}$ (diametro max delle barre longitudinali)=mm	**14.00**
s_{max} = passo max staffe= min(12 ϕ_{Lmin}, 250 mm) =mm	168.00
s ≤ s_{max}?	ok
ϕ_{min} = diametro min. staffa =max(6 mm; 1/4 ϕ_{Lmax}) =mm	6.00
1° perimetro: $\phi_1 \geq \phi_{min}$?	ok
2° perimetro: $\phi_2 \geq \phi_{min}$?	-
3° perimetro: $\phi_3 \geq \phi_{min}$?	-

E) La verifica a stabilità del palo si effettua inserendo, oltre alle caratteristiche geometriche dell'opera, anche il coefficiente di reazione laterale del mono-palo, valutato attraverso la formulazione di Davisson (1970) $k_{h\_int} = 67\,\frac{c_u}{D}$, dove D = 0.70m e c_u = 63.15 KN/m^2; quest'ultimo valore di coesione non drenata è stato ottenuto dall'analisi delle informazioni geotecniche a disposizione, in particolare è stato opportunamente ottenuto un valore mediato, modellando di fatto il palo come se fosse inserito all'interno di un terreno equivalente: è stato infatti dapprima ottenuto un valore di coesione medio relativo agli strati di terreno attraversati dal palo, valore che è stato poi redistribuito lungo tutta la luce dell'opera, essendo la somma degli spessori degli strati di terreno dotati di coesione non drenata inferiore alla lunghezza totale del palo. Di seguito si riportano i risultati ottenuti dalle analisi.

VERIFICA SLU CON FORZA DI COMPRESSIONE PER LA STABILITA' DELL'EQUILIBRIO ELASTICO		
Presenza di mono-Palo o Palificata ?	mono-Palo	
d = diametro sezione palo = m	0.70	
d = diametro (utente) = m	-	
d=diametro adottato = m	0.70	
N= Carico verticale agente in Combinazione SLU :		
N = N_{max} = carico assiale max su mono-Palo = kN	537.77	
N = N_{pmax} = carico assiale max su singolo palo della Palificata = kN	-	
N = N_{Ed}=kN	537.77	
Calcolo del carico critico elastico		
Carico critico di asta caricata da N e vincolata lateralmente a un mezzo elastico;		
Relazione da Timoshenko, Gere, in Theory of elastic stability (1961):		
$N_{cr} = (\pi^2 E J / L^2)\,[m^2 + \beta L^4/(m^2 \pi^4 EJ)]$		
Con m = n.o di semionde della deformata sinusoidale caricata dal carico di punta,		
posto λ =semilunghezza d'onda= L / m, risulta:		
$N_{cr} = \pi^2 E J\,(1/\lambda^2 + \lambda^2 \beta/(\pi^4 EJ)]$		
Al variare di λ si ottiene il minimo N_{cr} con: d (N_{cr}/dλ)=0, che porge:		
$\lambda^* = (EJ/\beta)^{1/4}$		
$N_{cr} = N_{cr}(\lambda^*) = 2\ (\beta EJ)^{1/2}$		
Calcolo di N_{cr}		
K_{h_int}= coefficiente di reazione laterale del terreno se mono-palo = N/cm^3	6.04	
K_{h_rid}= coefficiente di reazione laterale del terreno se palificata = N/cm^3	-	
K_h= (K_{h_int} se mono-Palo; K_{h_rid} se Palificata)= N/cm^3	6.04	
D= dimensione adottata = d = mm	700.00	
β = reazione laterale terreno per unità di spostamento laterale e per unità di lunghezza= k_h D= N/mm^2	4.23	
f_{ck}= 0,83 R_{ck}= N/mmq	33.20	
R_{ck}= N/mmq	40.00	
E_{cm}= 22.000 [f_{cm}/10]^{0,3}= 22.000 [(f_{ck}+8) /10]^{0,3}=N/mmq	33,642.78	
E= Modulo di elasticità (utente) = N/mm^2	33,350.00	
E= Modulo di elasticità adottato= N/mm^2	33,350.00	
J = π d^4 / 64 = mm^4	11,785,881,189.48	
J = Momento di inerzia (utente) = mm^4	-	
J= Momento di inerzia adottato= mm^4	11,785,881,189.48	
$N_{cr} = 2\ (\beta EJ)^{1/2}$ = kN	81,531.69	
N_{cr} (utente) = kN	-	
N_{cr} (adottato) = kN	81,531.69	
VERIFICA (Analisi Elastica)		
N_{Ed}=kN	537.77	
N_{cr} = N_{cr} (adottato) = kN	81,531.69	
α_{cr} = N_{cr}/ N_{Ed} =	151.61	
Fs =	5.00	
Analisi elastica: $\alpha_{cr} \geq$ Fs ?	ok	

F) La verifica a portanza trasversale del palo si effettua sulla falsariga del procedimento svolto nel caso di verifica a stabilità. Infatti, siccome la palificata attraversa strati di terreno di tipologia diversa (coerente ed incoerente), sono stati opportunamente ottenuti valori mediati relativi alle caratteristiche geotecniche (peso specifico, coesione non drenata), modellando di fatto il palo come se fosse inserito all'interno di un terreno equivalente: è stato infatti ottenuto un valore di coesione e di peso specifico medio relativo agli strati di terreno attraversati dal palo, valore che è stato poi redistribuito lungo tutta la luce dell'opera, essendo la somma degli spessori degli strati di terreno coerenti ed incoerenti inferiore alla lunghezza totale del palo. La portanza trasversale finale è quindi data dalla somma delle portanza tra terreni coerenti ed incoerenti. Di seguito si riportano i risultati ottenuti dalle analisi.

VERIFICA SLU-GEO PER CARICO LIMITE TRASVERSALE DI UN PALO CON ROTAZIONE IN TESTA IMPEDITA. TERRENI COESIVI.

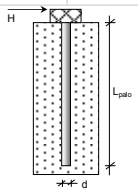
Sollecitazioni su mono-Palo o Palificata ?			mono-Palo			
			Coefficienti parziali Azioni, Materiali, Resistenze			
			A1, A2		M1	R1, R2, R3
			perm. γ_G (se fav.)	var. γ_Q (se fav.)	γ_{cu}	γ_T
SLU: combinazioni NON SISMICHE tipo: $\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \Sigma_{i=2,n} (\gamma_{Qi} \psi_{0i} Q_{ki})$						
App. 1	Comb. 1 (STR): A1+M1+R1		1,30 (1,00)	1,50 (0,00)	1.00	1.00
	Comb. 2 (GEO) : A2+M1+R2		**1,00 (1,00)**	**1,30 (0,00)**	**1.00**	**1.60**
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**		**1,30 (1,00)**	**1,50 (0,00)**	**1.00**	**1.30**
SLU: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_i (\psi_{2i} Q_{ki})$						
App. 1	Comb. 1 (STR): A1+M1+R1		1.00	1.00	1.00	1.00
	Comb. 2 (GEO) : A2+M1+R2		**1.00**	**1.00**	**1.00**	**1.60**
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**		**1.00**	**1.00**	**1.00**	**1.30**
Approccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)			2			
Relativa Comb. GEO associata all'Approccio scelto:			unica			
		γ_{cu} =	1.00			
		γ_T =	1.30			

	mono-Palo		Palificata	
	Verifiche SLU_STR	Verifiche SLU_GEO	Verifiche SLU_STR	Verifiche SLU_GEO
Relativa Comb. associata all'Approccio scelto:		unica		unica
All'interno dell'app. scelto, a seguire i valori, per la comb. associata.				
Verifiche SLU-GEO				
portanza limite SLU trasversale		Verifiche SLU_GEO		Verifiche SLU_GEO
V (V_p se palificata) tra combin. non sismiche e sismiche = kN		213.01		-
M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rd},				
calcolato per				
mono-Palo				
a) N=0		-		
M_{Rd} = kNm =		440.46		
b) N associato alla combinazione in cui opera V : N= kN =		537.77		
M_{Rd} = kNm =		543.10		
Palificata				
a) N=0				-
M_{Rd} = kNm =				-
N associato alla combinazione in cui opera V :				
b) N_{pmin}= kN				-
M_{Rd} = kNm =				-
c) N_{pmax}= kN				-
M_{Rd} = kNm =				-

Fattori di correlazione ξ per il calcolo della resistenza caratteristica, condotto per via analitica (n = n.o verticali indagate)

n	1	2	3	4	5	7	≥10
ξ_3	1.70	1.65	1.60	1.55	1.50	1.45	1.40
ξ_4	1.70	1.55	1.48	1.42	1.34	1.28	1.21

n = (1, 2, 3, 4, 5, 7, ≥10)		**1**	
	ξ_3 =	1.70	
	ξ_4 =	1.70	
d = diametro sezione palo = m		0.70	
L_{palo} = L= Lunghezza del palo = m		**14.00**	
Coesione non drenata media= $c_{u\,med}$ = kN/mq		**63.15**	
Coesione non drenata minima= $c_{u\,min}$ = kN/mq		**57.25**	
Coesione non drenata media di progetto = $c_{u\,med,d} = c_{u\,med} / \gamma_{cu}$ = kN/mq		63.15	
Coesione non drenata minima di progetto = $c_{u\,min,d} = c_{u\,min} / \gamma_{cu}$ = kN/mq		57.25	



mono-Palo: calcolo effettuato per ciascuno dei 2 valori del Momento di plasticizzazione:		**a)**	**b)**
M_y = Momento di plasticizzazione della sezione = M_{Rd}= kNm		440.46	543.10
P. corto: H1 = 9 c_u d^2 (L/d - 1,5)	$H1_{med}$ (c_u= $c_{u\,med,d}$) =kN	5,152.09	5,152.09
	$H1_{min}$ (c_u= $c_{u\,min,d}$) =kN	4,670.74	4,670.74
P. intermedio: H2 = -9 c_u d^2 (L/d +1,5) + 9c_u d^2 [2 (L/d)^2 + 4/9 M_y/c_u d^3 +4,5]$^{1/2}$	$H2_{med}$ (c_u= $c_{u\,med,d}$) =kN	1,955.73	1,966.00
	$H2_{min}$ (c_u= $c_{u\,min,d}$) =kN	1,777.13	1,787.40
P. lungo: H3 = -13,5 c_u d^2 + c_u d^2 (182,25 + 36 M_y/c_u d^3)$^{1/2}$	$H3_{med}$ (c_u= $c_{u\,med,d}$) =kN	517.91	601.47
	$H3_{min}$ (c_u= $c_{u\,min,d}$) =kN	503.83	584.07
H_{med} = min ($H1_{med}$; $H2_{med}$; $H3_{med}$)= kN		517.91	601.47
		P. lungo	P. lungo
H_{min} = min ($H1_{min}$; $H2_{min}$; $H3_{min}$)= kN		503.83	584.07
		P. lungo	P. lungo
H_k = Min(H_{med}/ξ_3 ; H_{min}/ξ_4) = kN		296.37	343.57
$R_{tr,d} = H_d = H_k/\gamma_T$ = kN		227.98	264.29
		a	**b**
Si procede alla verifica con il seguente $R_{tr,d}$:			
a opp. b ?		**b**	
$R_{tr,d}$ = kN		264.29	
$F_{tr,d}$ = V = kN		213.01	
$R_{tr,d}$ / $F_{tr,d}$ =		1.24	
$F_{tr,d} \le R_{tr,d}$?		ok	

VERIFICA SLU-GEO PER CARICO LIMITE TRASVERSALE DI UN PALO CON ROTAZIONE IN TESTA IMPEDITA. TERRENI INCOERENTI.

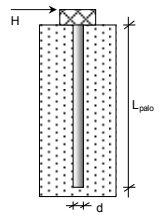
		Coefficienti parziali Azioni, Materiali, Resistenze			
		A1, A2		M1	R1, R2, R3
		perm. γ_G (se fav.)	var. γ_G (se fav.)	γ_{γ} , $\gamma_{\varphi'}$	γ_T
SLU: combinazioni NON SISMICHE tipo: $\gamma_{G1} G_1 + \gamma_{G2} G_2 + \gamma_{Q1} Q_{k1} + \Sigma_{i>2,n} (\gamma_{Qi} \psi_{oi} Q_{ki})$					
App. 1	Comb. 1 (STR): A1+M1+R1	1,30 (1,00)	1,50 (0,00)	1.00	1.00
	Comb. 2 (GEO) : A2+M1+R2	**1,00 (1,00)**	**1,30 (0,00)**	**1.00**	**1.60**
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**	**1,30 (1,00)**	**1,50 (0,00)**	**1.00**	**1.30**
SLU: combinazioni SISMICHE tipo : $E + G_1 + G_2 + \Sigma_j (\psi_{2j} Q_{kj})$					
App. 1	Comb. 1 (STR): A1+M1+R1	1.00	1.00	1.00	1.00
	Comb. 2 (GEO) : A2+M1+R2	**1.00**	**1.00**	**1.00**	**1.60**
App. 2	**Comb. unica (STR, GEO) : A1+M1+R3**	**1.00**	**1.00**	**1.00**	**1.30**

Approccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)	2
Relativa Comb. GEO associata all'Approccio scelto:	unica
γ_{γ} , $\gamma_{\varphi'}$ =	1.00
γ_T =	1.30

	mono-Palo		Palificata	
	Verifiche SLU_STR	Verifiche SLU_GEO	Verifiche SLU_STR	Verifiche SLU_GEO
Relativa Comb. associata all'Approccio scelto:		unica		unica
All'interno dell'app. scelto, a seguire i valori, per la comb. associata.				
Verifiche SLU-GEO portanza limite SLU trasversale		Verifiche SLU_GEO		Verifiche SLU_GEO
V (V_d se palificata) tra combin. non sismiche e sismiche = kN		213.01		-
M_y = Momento di plasticizzazione della sezione (Broms)= M_{Rd}, calcolato per				
mono-Palo				
a) N=0		-		
M_{Rd} = kNm =		440.46		
b) N associato alla combinazione in cui opera V : N= kN =		537.77		
M_{Rd} = kNm =		543.10		
Palificata				
a) N=0				-
M_{Rd} = kNm =				-
N associato alla combinazione in cui opera V :				
b) N_{pmin}= kN				-
M_{Rd} = kNm =				-
c) N_{pmax}= kN				-
M_{Rd} = kNm =				-

Fattori di correlazione ξ per il calcolo della resistenza caratteristica, condotto per via analitica (n = n.o verticali indagate)							
n	**1**	**2**	**3**	**4**	**5**	**7**	**≥10**
ξ_3	1.70	1.65	1.60	1.55	1.50	1.45	1.40
ξ_4	1.70	1.55	1.48	1.42	1.34	1.28	1.21

	n = (1, 2, 3, 4, 5, 7, ≥10)	**1**	
	ξ_3 =	1.70	
	ξ_4 =	1.70	
	d = diametro sezione palo = m	0.70	
	L_{palo} = L= Lunghezza del palo = m	**14.00**	
	Peso di unità di volume γ (se falda $\gamma = \gamma'$) = kN/m^3 =	**7.85**	
	Angolo medio di attrito del terreno = φ'_{med} = °	**45.11**	
	Angolo minimo di attrito del terreno = φ'_{min} = °	**44.29**	
	Peso di unità di volume di progetto $\gamma_d = \gamma/\gamma_\gamma$ = kN/m^3 =	7.85	
	Angolo medio di attrito del terreno, di progetto = $\varphi'_{med,d} = \varphi'_{med}/\gamma_{\varphi'}$ = °	45.11	
	Angolo minimo di attrito del terreno, di progetto = $\varphi'_{min,d} = \varphi'_{min}/\gamma_{\varphi'}$ = °	44.29	
	Coeff. medio di spinta passiva $k_{p\,med,d} = (1 + \sin\varphi'_{med,d})/(1 - \sin\varphi'_{med,d})$ =	5.86	
	Coeff. minimo di spinta passiva $k_{p\,min,d} = (1 + \sin\varphi'_{min,d})/(1 - \sin\varphi'_{min,d})$ =	5.63	



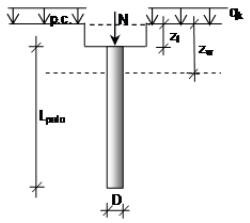
mono-Palo: calcolo effettuato per ciascuno dei 2 valori del Momento di plasticizzazione:		**a)**	**b)**
M_y = Momento di plasticizzazione della sezione = M_{Rd}= kNm		440.46	543.10
P. corto: $H1 = 1{,}5\ k_p\ \gamma_d\ d^3\ (L/d)^2$	$H1_{med}$ (k_p= $k_{p\,med,d}$) =kN	9,467.32	9,467.32
	$H1_{min}$ (k_p= $k_{p\,min,d}$) =kN	9,093.64	9,093.64
P. intermedio: $H2 = 1/2\ k_p\ \gamma_d\ d^3\ (L/d)^2 + M_y/L$	$H2_{med}$ (k_p= $k_{p\,med,d}$) =kN	3,187.23	3,194.57
	$H2_{min}$ (k_p= $k_{p\,min,d}$) =kN	3,062.67	3,070.01
P. lungo: $H3 = k_p\ \gamma_d\ d^3\ [(3{,}676\ M_y / k_p\ \gamma_d\ d^4)^2]^{1/3}$	$H3_{med}$ (k_p= $k_{p\,med,d}$) =kN	438.68	504.42
	$H3_{min}$ (k_p= $k_{p\,min,d}$) =kN	432.83	497.70
H_{med} = min ($H1_{med}$; $H2_{med}$; $H3_{med}$)= kN		438.68	504.42
		P. lungo	P. lungo
H_{min} = min ($H1_{min}$; $H2_{min}$; $H3_{min}$)= kN		432.83	497.70
		P. lungo	P. lungo
H_k = Min(H_{med}/ξ_3 ; H_{min}/ξ_4) = kN		254.60	292.76
$R_{tr,d} = H_d = H_k/\gamma_T$ = kN		195.85	225.20
		a	**b**
Si procede alla verifica con il seguente $R_{tr,d}$:			
a opp. b ?		**b**	
$R_{tr,d}$ = kN		225.20	
$F_{tr,d} = V$ = kN		213.01	
$R_{tr,d}$ / $F_{tr,d}$ =		1.06	
$F_{tr,d} \le R_{tr,d}$?		ok	

Sommando il contributo garantito dai terreni coerenti (F.S. = 1.24) con quello garantito dai terreni incoerenti (F.S. = 1.06), si ottiene un coefficiente di sicurezza pari a 2.30, pertanto la verifica risulta soddisfatta.

G) La verifica a portanza verticale del palo si effettua dapprima scegliendo il tipo di modello matematico per il calcolo dei parametri di portanza alla base e la tipologia di infissione, che determina le definizione di coefficienti di sicurezza differenti. Si inseriscono poi le caratteristiche degli spessori di terreno attraversati dal palo, dapprima introducendo i parametri medi e poi i parametri minimi; è così possibile ottenere i valori di portanza di base e laterale del terreno.

PALI SOGGETTI A CARICHI ASSIALI

Sollecitazioni su mono-Palo o Palificata ?	mono-Palo
D = Diametro sezione palo = m	0.70
Tecnologia, tipologia Diametro palo (e valori di calcolo N_{qk}) :	Trivel. GD (Nq AGI/1984)
Tecnologia palo :	Trivellati
z_t = Quota testa Palo da p.c. = m	1.00
z_w = Quota falda da p.c. = m	2.00
q_k = kN/mq	25.00
Applicare il fattore χ di riduzione capacità portante di base =	si
N_{sk} = Numero strati = (Numero Strati)	4.00
A_p = Area Palo = $\pi(D/2)^2$ = mq	0.38485
L_{palo} = $\Sigma_{1\text{-}10}$ Sp strati = m	14.00



		Coefficienti parziali (A, R)				
		Azioni (A1, A2)		Resistenze (R1, R2, R3) base, laterale per pali soggetti a carichi assiali		
Approccio e Combinazioni		perm. γ_G (se fav.)	var. γ_G (se fav.)	γ_b	γ_s	γ_{st}
SLU: combinazioni NON SISMICHE						
App. 1	Comb. 1 (STR): A1+M1+R1	1,30 (1,00)	1,50 (0,00)	1.00	1.00	1.00
	Comb. 2 (GEO): A2+M1+R2	1,00 (1,00)	1,30 (0,00)	1.70	1.45	1.60
App. 2	Comb. unica (STR, GEO): A1+M1+R3	1,30 (1,00)	1,50 (0,00)	1.35	1.15	1.25
SLU: combinazioni SISMICHE						
App. 1	Comb. 1 (STR): A1+M1+R1	1.00	1.00	1.00	1.00	1.00
	Comb. 2 (GEO): A2+M1+R2	1.00	1.00	1.70	1.45	1.60
App. 2	Comb. unica (STR, GEO): A1+M1+R3	1.00	1.00	1.35	1.15	1.25

roccio scelto nel calcolo Azioni su mono-Palo o Palificata (1 opp. 2)	2
Relativa Comb. GEO associata all'Approccio scelto:	unica

	γ_b	γ_s	γ_{st}
γ da associare nel calcolo delle resistenze:	1.35	1.15	1.25

N'_d = azione assiale max di progetto a compressione (positiva) = kN	537.77
N'_d = azione assiale max di progetto a trazione (negativa) = kN	-

Fattori di correlazione ξ per il calcolo della resistenza caratteristica, condotto per via analitica (n = n.o verticali indagate)

n	1	2	3	4	5	7	≥10
ξ_3	1.70	1.65	1.60	1.55	1.50	1.45	1.40
ξ_4	1.70	1.55	1.48	1.42	1.34	1.28	1.21

n = (1, 2, 3, 4, 5, 7, ≥10)	1
ξ_3 =	1.70
ξ_4 =	1.70

CALCOLO DELLA RESISTENZA (base e laterale) CON I PARAMETRI MEDI DEL TERRENO

Strato	Sp (m)	Tipo terreno	Attrito negativo ?	Parametri MEDI terreno: γ (kN/m^3)	c. dr: c'=c'$_{med}$ (kN/mq)	c. dr: φ'=φ'$_{med}$ (°)	c. n dr: c_u=$c_{u\,med}$ (kN/mq)
1	6.00	Coesivo	no	16.70	-	-	22.00
2	1.80	Coesivo	no	21.00	-	-	133.00
3	1.80	Coesivo	no	25.00	-	-	285.00
4	4.40	Incoerente	no	25.00	-	45.11	-

Tipo infisso?: -

Strato	k f(palo, terreno) c. dr: k	μ=coef. scabr. interfac. terreno-palo c. dr: μ	c. dr: $\beta_S = k\,\mu$	c. dr: β_{S_utente}	c. dr: β_{S_adott}
1	-	-	-	-	-
2	-	-	-	-	-
3	-	-	-	-	-
4	0.292	1.004	0.293	-	0.293

Strato	parametri a, α legati all'adesione c. dr: a	c. n. dr: α	β_n (in caso di attrito negativo)
1	-	0.900	1.00
2	-	0.400	1.00
3	-	0.400	1.00
4	-	-	1.00

		σ_{vz} pr. verticale totale $\sigma_{vz} = q_k + (\gamma_1 z_i) + \Sigma_i \gamma_i Sp_i$	u pr. Interstiziale $u = (\gamma_w z_i) + \Sigma_i \gamma_w Sp_i$	σ'_{vz} pr. vert. efficace litost. $\sigma'_{vz} = (\sigma_{vz} - u)$	c. n dr Q_{S_j} = π D (Sp α c_u)$_i$	c. dr $Q_{S\_j\ attr\_p-t}$ = π D (Sp β_S β_n σ'_{vz_mi})$_i$	c. dr $Q_{S\_j\ attr\_p-t} = Q_{S\_j\ attr\_p-t} + Q_{S\_j\ ados}$ $Q_{S_j\ attr_p-t} + \pi$D (Sp a c')$_i$
	3 valori a dx per $\sigma_{vz}(z_i)$	41.70	-	41.70			
z	6.00	141.90	50.00	91.90	261.25	-	-
	7.80	179.70	68.00	111.70	210.59	-	-
	9.60	224.70	86.00	138.70	451.26	-	-
	14.00	334.70	130.00	204.70	-	486.22	486.22

Pali Infissi MD o GD e Trivellati MD: valori di N_q dedotti da Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =5)	N_q (L/D =10)	N_q (L/D =20)	N_q (L/D =50)	L/D (palo)= 20.00	N_q(interp. per L/D palo)
1	-	-	-	-		-
2	-	-	-	-		-
3	-	-	-	-		-
4	519.87	426.71	370.24	347.74		370.24
	-	-	-	-		-
	-	-	-	-		-
	-	-	-	-		-
	-	-	-	-		-
	-	-	-	-		-
	-	-	-	-		-

Pali Trivellati GD (N_q AGI/1984): valori di N_q ridotti, raccomandati da AGI (1984), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)= 20.00	N_q(interp. per L/D palo)
1	-	-		-
2	-	-		-
3	-	-		-
4	54.51	57.64		56.30
	-	-		-
	-	-		-
	-	-		-
	-	-		-
	-	-		-
	-	-		-

Pali Trivellati GD (N_q Vig./1999): valori di N_q ridotti, proposti da Viggiani (1999), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)= 20.00	N_q(interp. per L/D palo)
1	-	-		-
2	-	-		-
3	-	-		-
4	93.63	90.92		92.08
	-	-		-
	-	-		-
	-	-		-
	-	-		-
	-	-		-
	-	-		-

In c. dr.: valore ottenuto, rispetto ai valori che precedono, in base a scelta effettuata per 'Tecnologia, tipologia Diametro palo (e valori di calcolo N_q)'	N_q (ottenuto)	N_q (utente)	N_q (adottato)
	-	-	-
	-	-	-
	-	-	-
	56.30	-	56.30
	-	-	-
	-	-	-
	-	-	-
	-	-	-
	-	-	-
	-	-	-

RESISTENZA (laterale Q_S e di base o alla punta Q_b) CON I PARAMETRI MEDI DEL TERRENO

Strato	Q_{S_j} (kN)	$N_q = N_q$ (adottato)	N_c c. n dr c_u>0: 9 c. dr. c'>0: $(N_q - 1)\,ctg\varphi'$	q_{b_j} (kN/mq) c. n dr c_u>0: $N_c c_u + \sigma_{vz}$ c_u=0: $c'N_c + N_q\sigma'_{vz}$	Q_{b_j} (kN) $= q_{b\_j}\,A_p$	$Q_{b\_j\ utente}$ (kN)	$Q_{b\_j\ adot}$ (kN)
1	261.25					-	
2	210.59					-	
3	451.26					-	
4	486.22	56.30	-	11,524.85	4,435.28	-	4,435.28
						-	
						-	
						-	
						-	
						-	

CAPACITA' PORTANTE MEDIA

χ = fattore di riduzione capacità portante di base =	0.708
Base (per azione assiale $N_d \geq 0$): $R_{b;cal\,med} = \chi\ \Sigma_i\ Q_{b\_j\_adott}$ = kN	3,141.66
Laterale: $R_{S;cal\,med} = \Sigma_i\ Q_{S\_j}$ = kN	1,409.32

CALCOLO DELLA RESISTENZA (base e laterale) CON I PARAMETRI MINIMI DEL TERRENO

Strato	Sp (m)	Tipo terreno	Attrito negativo ?	Parametri MINIMI terreno: γ (kN/m³)	c. dr.: $c'=c'_{min}$ (kN/mq)	c. dr.: $\varphi'=\varphi'_{min}$ (°)	c. n.dr.: $c_u=c_{u,min}$ (kN/mq)
1	6.00	Coesivo	no	16.70	-	-	19.00
2	1.80	Coesivo	no	21.00	-	-	104.00
3	1.80	Coesivo	no	25.00	-	-	278.00
4	4.40	Incoerente	no	25.00	-	44.29	-

Incolla k dai parametri MEDI

Tipo Infisso: -

Strato	k f(palo, terreno) c. dr.: k	μ=coef. scabr. interfac. terreno-palo c. dr.: μ	c. dr.: $\beta_s = k\,\mu$	c. dr.: $\beta_{s\ utente}$	c. dr.: $\beta_{s\ adott}$
1	-	-	-	-	-
2	-	-	-	-	-
3	-	-	-	-	-
4	0.302	0.976	0.294	-	0.294

Incolla α dai parametri MEDI

Strato	parametri a, α legati all'adesione c. dr.: a	c. n. dr.: α	β_n (in caso di attrito negativo)
1	-	0.900	1.000
2	-	0.400	1.000
3	-	0.400	1.000
4	-	-	1.000

	σ_{vz} pr. verticale totale $\sigma_{vz} = q_s + (\gamma_i\, z_i) + \Sigma_i \gamma_i\, Sp_i$	u pr. interstiziale $u = (\gamma_w z_i) + \Sigma_i \gamma_w\, Sp_i$	σ'_{vz} pr. vert. efficace litost. $\sigma'_{vz} = (\sigma_{vz} - u)$	c. n.dr. $Q_{s,i} = \pi D\,(Sp\ \alpha\ c_u)_i$	c. dr. $Q_{s,i\,attr\,pos} = \pi D\,(Sp\ \beta_s\ \beta_n\ \sigma'_{vz\,m})_i$	c. dr. $Q_{s,i} = Q_{s,i\,attr\,pos} + Q_{s,i\,adesione}$; $Q_{s,i\,attr\,pos} + \pi D\,(Sp\ a\ c')_i$
3 valori a dx per $\sigma(z_i)$	41.70	-	41.70			
z 6.00	141.90	50.00	91.90	225.63	-	-
7.80	179.70	68.00	111.70	164.67	-	-
9.60	224.70	86.00	138.70	440.17	-	-
14.00	334.70	130.00	204.70	-	488.99	488.99

Pali Infissi MD o GD e Trivellati MD: valori di N_q dedotti da Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	Nq (L/D =5)	Nq (L/D=10)	Nq (L/D=20)	Nq (L/D =50)	L/D (palo)=	20.00	N_q(interp. per L/D palo)
1	-	-	-	-			-
2	-	-	-	-			-
3	-	-	-	-			-
4	448.28	366.85	317.06	293.89			317.06
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-
	-	-	-	-			-

Pali Trivellati GD (N_q AGI'1984): valori di N_q ridotti, raccomandati da AGI (1984), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)=	20.00	N_q(interp. per L/D palo)
1	-	-			-
2	-	-			-
3	-	-			-
4	50.11	51.21			50.74
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-

Pali Trivellati GD (N_q Vig.'1999): valori di N_q ridotti, proposti da Viggiani (1999), sulla base dei diagrammi di Berezantzev, in c. dr., per rapporti L/D prefissati e in funzione di φ'

Strato	N_q (L/D =4)	N_q (L/D =32)	L/D (palo)=	20.00	N_q(interp. per L/D palo)
1	-	-			-
2	-	-			-
3	-	-			-
4	89.10	84.75			86.61
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-
	-	-			-

In c. dr.: valore ottenuto, rispetto ai valori che precedono, in base a scelta effettuata per 'Tecnologia, tipologia Diametro palo (e valori di calcolo N_q)'

N_q (ottenuto)	N_q (utente)	N_q (adottato)
-	-	-
-	-	-
-	-	-
50.74	-	50.74
-	-	-
-	-	-
-	-	-
-	-	-
-	-	-
-	-	-

RESISTENZA (laterale Q_s e di base o alla punta Q_b) CON I PARAMETRI MINIMI DEL TERRENO

Strato	$Q_{s,i}$ (kN)	$N_q = N_q$ (adottato)	N_c c. n.dr. $c_u>0$: 9; c. dr. $c'>0$: $(N_q - 1)\,ctg\varphi'$	$q_{b,i}$ (kN/mq) c. n.dr. $c_u>0$: $N_c c_u + \sigma_{vz}$; $c_u=0$: $c'N_c + N_q\sigma'_{vz}$	$Q_{b,i}$ (kN) $= q_{b,i}\,.\,A_p$	$Q_{b,i\,utente}$ (kN)	$Q_{b,i\,adott}$ (kN)
1	225.63					-	
2	164.67					-	
3	440.17					-	
4	488.99	50.74	-	10,385.92	3,996.97	-	3,996.97
						-	
						-	
						-	
						-	
						-	
						-	

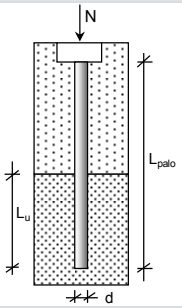
CAPACITA' PORTANTE MINIMA

χ = fattore di riduzione capacità portante di base =	0.71
Base (per azione assiale $N_d \geq 0$): $R_{b,cal\,min} = \chi\,\Sigma_i\,Q_{b,i\,adott}$ = kN	2,831.19
Laterale: $R_{s,cal\,min} = \Sigma_i\,Q_{s,i}$ = kN	1,319.46

CALCOLO DELLA RESISTENZA DI PROGETTO (CAPACITA PORTANTE)		
CARICO ASSIALE DI PROGETTO		
N'_d = azione assiale max di progetto = kN	537.77	-
	($N'_d \geq 0$)	($N'_d \leq 0$)
γ_g =	**1.00**	**1.00**
Valore assunto per $N_{att,n} = \Sigma (Q_{S,j\,attr\_p-1})_{>0}$ = kN	**a)medi**	**a)medi**
$N_{att,n} = \Sigma (Q_{S,j\,attr\_p-1})_{>0}$ = kN	-	-
$N''_d = \gamma_g \mid \Sigma (Q_{S,j\,attr\_p-1})_{<0} \mid$ = kN	-	-
	($N''_d \geq 0$)	($N''_d \geq 0$)
$N_d = N'_d + N''_d$ = kN	537.77	-
	(N_{d1}>0; sempre di compr.)	(N_{d2} > 0 opp. < 0)
RESISTENZA CARATTERISTICA	per N_{d1}	per N_{d2}
$R_{b,k} = Min(R_{b,cal\,med}/\xi_3 ; R_{b,cal\,min}/\xi_4)$ = kN	1,665.40	-
$R_{s,k} = Min(R_{s,cal\,med}/\xi_3 ; R_{s,cal\,min}/\xi_4)$ = kN	776.15	-
$R_{c,k} = R_{b,k} + R_{s,k}$ = kN	2,441.56	-
RESISTENZA DI PROGETTO (CAPACITA' PORTANTE)		
Per $N_{d1} > 0$: $R_{c,d} = R_{bk}/\gamma_b + R_{sk}/\gamma_s$ = kN	1,908.55	
Per $N_{d2} > 0$: $R_{c,d} = R_{bk}/\gamma_b + R_{sk}/\gamma_s$ = kN	-	
Per $N_{d2} < 0$: $R_{t,d} = R_{bk}/\gamma_b + R_{sk}/\gamma_{st}$ = kN	-	
VERIFICA per $N_{d1} > 0$		
$R_{c,d} / N_{d1}$ =	3.55	
$R_{c,d} \geq N_{d1}$?	ok	
VERIFICA per $N_{d2} > 0$		
$R_{c,d} / N_{d2}$ =	-	
$R_{c,d} \geq N_{d2}$?	-	
VERIFICA per $N_{d2} < 0$		
$R_{t,d} / \mid N_{d2} \mid$ =	-	
$R_{t,d} \geq \mid N_{d2} \mid$?	-	

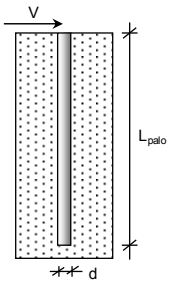
H) Per la valutazione dei cedimenti verticali si riportano i risultati ottenuti nel caso di analisi del mono-palo

VERIFICA SLE PER CEDIMENTO VERTICALE		
Presenza di mono-Palo o Palificata ?	mono-Palo	
N= Carico verticale agente in Combinazione SLE :		
N = N_{max} = carico assiale max su mono-Palo = kN	381.63	
N = N_{pmedio} = carico assiale medio su singolo palo della Palificata = kN	-	
d = diametro sezione palo = m	0.70	
d = diametro sezione palo = m	-	
d = diametro sezione palo (adottato)=	0.70	
L = Lunghezza per valutare il coefficiente I_w = m	14.00	
E = Modulo di deformazione elastica del terreno = N/mmq	83.25	
In presenza di Palificata:		
i = interasse dei pali della Palificata = m	2.40	
L_{palo} = Lunghezza del palo = m	14.00	
n_p= numero di pali della Palificata =	-	
n_p= numero di pali della Palificata		
n_p= numero di pali della Palificata (adottato)=	-	
CEDIMENTO VERTICALE MASSIMO $\delta_{max,palo}$ DEL MONO PALO:		
I_w= Coefficiente di influenza = 0,5 + Log(L / D) =	1.80	
I_w= Coefficiente di influenza =	-	
I_w= Coefficiente di influenza (adottato) =	1.80	
$\delta_{max,palo}$ = $I_w N_{max}$ / (E L) = mm	0.59	
Verifica sul MONO PALO		
E_d= Cedimento verticale massimo su mono-palo, dovuto al carico agente in progetto = $\delta_{max,palo}$ = mm	0.59	
C_d= Cedimento verticale limite ammesso in progetto su mono-palo = mm	50.00	
$E_d \leq C_d$	ok	



I) Per la valutazione dei cedimenti orizzontali si riportano i risultati ottenuti nel caso di analisi del mono-palo

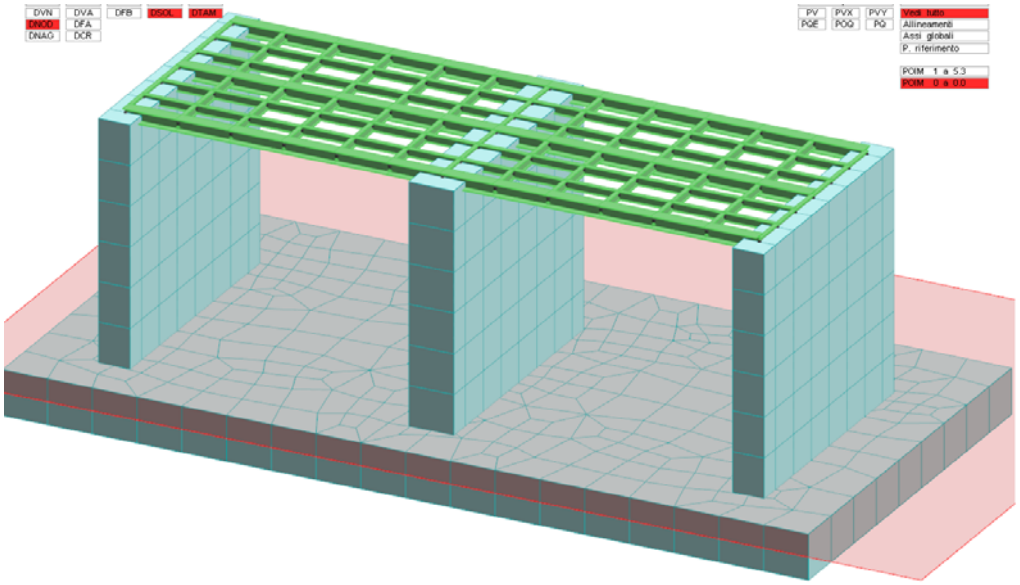
VERIFICA SLE DELLO SPOSTAMENTO TRASVERSALE DI UN PALO CON ROTAZIONE IN TESTA IMPEDITA.	
Presenza di mono-Palo o Palificata ?	mono-Palo
V= Carico orizzontale agente in Combinazione SLE = kN	142.00
V= Carico orizzontale agente in Combinazione SLE = kN	-
V= Carico orizzontale agente in Combinazione SLE (adottato) = kN	142.00
d = diametro sezione palo = m	0.70
d = diametro sezione palo = m	-
d = diametro sezione palo (adottato)=	0.70
L_{palo} = Lunghezza del palo = m	**14.00**
In presenza di Palificata:	
n_p= numero di pali della Palificata =	-
n_p= numero di pali della Palificata	-
n_p= numero di pali della Palificata (adottato)=	-
K_{h_int}= coefficiente di reazione laterale del terreno = N/cm^3 =	**6.04**
r = fattore di riduzione di K_{h_int} in presenza di Palificata (Poulos e Davis, 1980) =	-
r = fattore di riduzione=	-
r = fattore di riduzione (adottato)=	-
K_{h_rid}= coefficiente di reazione laterale del terreno (Palificata)= r K_{h_int} = N/cm^3	-
K_h= (K_{h_int} se mono-Palo; K_{h_rid} se Palificata)= N/cm^3	6.04
f_{ck}= 0,83 R_{ck}= N/mmq	33.20
R_{ck}= N/mmq	**40.00**
E_{cm} = 22.000 $[f_{cm}/10]^{0,3}$ = 22.000 $[(f_{ck}+8)/10]^{0,3}$ =N/mmq	33,642.78
$J_p = \pi\, d^4 / 64$ = cm^4	1,178,588.12
λ = lunghezza elastica= $(4\, E_{cm} J_p / K_h d)^{1/4}$ = cm	440.09
VERIFICA SPOSTAMENTO TRASVERSALE DEL mono-Palo (spost. medio se Palificata)	
spostamento trasversale max dovuto al carico agente in progetto= spostamento y(z=0) = mm	7.631
C_d= spostamento trasversale limite ammesso in progetto = mm	**20.00**
$E_d \le C_d$?	ok



Il Progettista

Sommario

La presente relazione riguarda la realizzazione di un ponte ciclopedonale a scavalco del torrente Lambro, attrezzato con doppie paratoie fluviali per controllo della portata di piena, per conto del Parco Regionale della Valle del Lambro. La struttura progettata prevede un impalcato costituente il ponte, composto da travi d'acciaio HEB280 e HEA280, con profili trasversali IPE 180 secondari e controventi diagonali Φ20, necessari a sostenere carichi in direzione trasversale all'asse dell'impalcato.
L'impalcato posa su spalle e su una pila centrale realizzate in cemento armato, aventi il compito anche di trasmettere in fondazione i carichi dovuti alla spinta dell'acqua che si genera allorquando entrino in azione una coppia di paratie di regolamentazione del flusso idrico.
Le fondazioni poggiano su pali trivellati di diametro 80 cm lunghi 14 m in accordo con la relazione geotecnica "Progetto definitivo opere strutturali relative all'intervento Area di laminazione di Inverigo - Interventi Idraulici e di riqualificazione fluviale nei territori di Inverigo, Nibionno e Veduggio con Colzano" dell'Aprile 2014 realizzata dal Dott. Geol. Pietro Alborghetti.



Introduzione

Sistemi di riferimento

Le coordinate, i carichi concentrati, i cedimenti, le reazioni vincolari e gli spostamenti dei NODI sono riferiti ad una terna destra cartesiana globale con l'asse Z verticale rivolto verso l'alto.
I carichi in coordinate locali e le sollecitazioni delle ASTE sono riferite ad una terna destra cartesiana locale così definita:
- origine nel nodo iniziale dell'asta;
- asse X coincidente con l'asse dell'asta e con verso dal nodo iniziale al nodo finale;
- immaginando la trave a sezione rettangolare l'asse Y è parallelo alla base e l'asse Z è parallelo all'altezza. La rotazione dell'asta comporta quindi una rotazione di tutta la terna locale.

Si può immaginare la terna locale di un'asta comunque disposta nello spazio come derivante da quella globale dopo una serie di trasformazioni:
- una rotazione intorno all'asse Z che porti l'asse X a coincidere con la proiezione dell'asse dell'asta sul piano orizzontale;
- una traslazione lungo il nuovo asse X così definito in modo da portare l'origine a coincidere con la proiezione del nodo iniziale dell'asta sul piano orizzontale;
- una traslazione lungo l'asse Z che porti l'origine a coincidere con il nodo iniziale dell'asta;
- una rotazione intorno all'asse Y così definito che porti l'asse X a coincidere con l'asse dell'asta;
- una rotazione intorno all'asse X così definito pari alla rotazione dell'asta.

In pratica le travi prive di rotazione avranno sempre l'asse Z rivolto verso l'alto e l'asse Y nel piano del solaio, mentre i pilastri privi di rotazione avranno l'asse Y parallelo all'asse Y globale e l'asse Z parallelo ma controverso all'asse X globale. Da notare quindi che per i pilastri la "base" è il lato parallelo a Y.

Le sollecitazioni ed i carichi in coordinate locali negli ELEMENTI BIDIMENSIONALI e nei MURI sono riferiti ad una terna destra cartesiana locale così definita:
- origine nel primo nodo dell'elemento;
- asse X coincidente con la congiungente il primo ed il secondo nodo dell'elemento;
- asse Y definito come prodotto vettoriale fra il versore dell'asse X e il versore della congiungente il primo e il quarto nodo. Asse Z a formare con gli altri due una terna destrorsa.

Praticamente un elemento verticale con l'asse X locale coincidente con l'asse X globale ha anche gli altri assi locali coincidenti con quelli globali.

Rotazioni e momenti

Seguendo il principio adottato per tutti i carichi che sono positivi se CONTROVERSI agli assi, anche i momenti concentrati e le rotazioni impresse in coordinate globali risultano positivi se CONTROVERSI al segno positivo delle rotazioni. Il segno positivo dei momenti e delle rotazioni è quello orario per l'osservatore posto nell'origine: X ruota su Y, Y ruota su Z, Z ruota su X. In pratica è sufficiente adottare la regola della mano destra: col pollice rivolto nella direzione dell'asse, la rotazione che porta a chiudere il palmo della mano corrisponde al segno positivo.

Normativa di riferimento

La normativa di riferimento è la seguente:
- Legge n. 64 del 2/2/1974 - Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche.

- D.M. del 24/1/1986 - Norme tecniche relative alle costruzioni sismiche.

- Legge n. 1086 del 5/11/1971 - Norme per la disciplina delle opere di conglomerato cementizio armato, normale e precompresso ed a struttura metallica.

- D.M. del 14/2/1992 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 9/1/1996 - Norme tecniche per l'esecuzione delle opere in c.a. normale e precompresso e per le strutture metalliche.

- D.M. del 16/1/1996 - Norme tecniche per le costruzioni in zone sismiche.

- Circolare n. 21745 del 30/7/1981 - Legge n. 219 del 14/5/1981 - Art. 10 - Istruzioni relative al rafforzamento degli edifici in muratura danneggiati dal sisma.

- Regione Autonoma Friuli Venezia Giulia - Legge Regionale n. 30 del 20/6/1977 - Documentazione tecnica per la progettazione e direzione delle opere di riparazione degli edifici - Documento Tecnico n. 2 - Raccomandazioni per la riparazione strutturale degli edifici in muratura.

- D.M. del 20/11/1987 - Norme Tecniche per la progettazione, esecuzione e collaudo degli edifici in muratura e per il loro consolidamento.

- Norme Tecniche C.N.R. n. 10011-85 del 18/4/1985 - Costruzioni di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Norme Tecniche C.N.R. n. 10025-84 del 14/12/1984 - Istruzioni per il progetto, l'esecuzione ed il controllo delle strutture prefabbricate in conglomerato cementizio e per le strutture costruite con sistemi industrializzati di acciaio - Istruzioni per il calcolo, l'esecuzione, il collaudo e la manutenzione.

- Circolare n. 65 del 10/4/1997 - Istruzioni per l'applicazione delle "Norme tecniche per le costruzioni in zone sismiche" di cui al D.M. del 16/1/1996.

- Eurocodice 5 - Progettazione delle strutture di legno.

- DIN 1052 - Metodi di verifica per il legno.

- D.M. del 14/1/2008 - Norme tecniche per le costruzioni. Le verifiche degli elementi di fondazione sono eseguite utilizzando l'Approccio 2.

- Circolare n. 617 del 2/2/2009 - Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al D.M. del 14/1/2008.

- Documento Tecnico CNR-DT 200 R1/2012 - Istruzioni per la Progettazione, l'Esecuzione ed il Controllo di Interventi di Consolidamento Statico mediante l'utilizzo di Compositi Fibrorinforzati.

- Eurocodice 3 - Progettazione delle strutture in acciaio.

Unità di misura

Le unità di misura adottate sono le seguenti:
- lunghezze : m
- forze : daN
- masse : kg
- temperature : gradi centigradi
- angoli : gradi sessadecimali o radianti

Geometria

Elenco vincoli nodi

Simbologia

Vn = Numero del vincolo nodo
Comm. = Commento
Sx = Spostamento in dir. X (L=libero, B=bloccato, E=elastico)
Sy = Spostamento in dir. Y (L=libero, B=bloccato, E=elastico)
Sz = Spostamento in dir. Z (L=libero, B=bloccato, E=elastico)
Rx = Rotazione intorno all'asse X (L=libera, B=bloccata, E=elastica)
Ry = Rotazione intorno all'asse Y (L=libera, B=bloccata, E=elastica)
Rz = Rotazione intorno all'asse Z (L=libera, B=bloccata, E=elastica)
RL = Rotazione libera
Ly = Lunghezza (dir. Y locale)
Lz = Larghezza (dir. Z locale)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Vn	Comm.	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>	Vn	Comm.	Sx	Sy	Sz	Rx	Ry	Rz	RL	Ly <m>	Lz <m>	Kt <daN/cmc>
1	Libero	L	L	L	L	L	L					2	Incastro	B	B	B	B	B	B				

Elenco nodi

Simbologia

Nodo = Numero del nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo
Z = Coordinata Z del nodo
Imp. = Numero dell'impalcato
Vn = Numero del vincolo nodo

Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn	Nodo	X <m>	Y <m>	Z <m>	Imp.	Vn
-502	14.04	5.24	5.30	1	1	-501	7.02	5.24	5.30	1	1	-500	0.00	5.24	5.30	1	1
-499	14.04	-0.50	5.30	1	1	-498	7.02	-0.50	5.30	1	1	-497	0.00	-0.50	5.30	1	1
-496	14.04	5.24	4.42	0	1	-495	7.02	5.24	4.42	0	1	-494	0.00	5.24	4.42	0	1
-493	14.04	4.74	4.42	0	1	-492	7.02	4.74	4.42	0	1	-491	0.00	4.74	4.42	0	1
-490	14.04	3.95	4.42	0	1	-489	7.02	3.95	4.42	0	1	-488	0.00	3.95	4.42	0	1
-487	14.04	3.16	4.42	0	1	-486	7.02	3.16	4.42	0	1	-485	0.00	3.16	4.42	0	1
-484	14.04	2.37	4.42	0	1	-483	7.02	2.37	4.42	0	1	-482	0.00	2.37	4.42	0	1
-481	14.04	1.58	4.42	0	1	-480	7.02	1.58	4.42	0	1	-479	0.00	1.58	4.42	0	1
-478	14.04	0.79	4.42	0	1	-477	7.02	0.79	4.42	0	1	-476	0.00	0.79	4.42	0	1
-475	14.04	0.00	4.42	0	1	-474	7.02	0.00	4.42	0	1	-473	0.00	0.00	4.42	0	1
-472	14.04	-0.50	4.42	0	1	-471	7.02	-0.50	4.42	0	1	-470	0.00	-0.50	4.42	0	1
-469	14.04	5.24	3.53	0	1	-468	7.02	5.24	3.53	0	1	-467	0.00	5.24	3.53	0	1
-466	14.04	4.74	3.53	0	1	-465	7.02	4.74	3.53	0	1	-464	0.00	4.74	3.53	0	1
-463	14.04	3.95	3.53	0	1	-462	7.02	3.95	3.53	0	1	-461	0.00	3.95	3.53	0	1
-460	14.04	3.16	3.53	0	1	-459	7.02	3.16	3.53	0	1	-458	0.00	3.16	3.53	0	1
-457	14.04	2.37	3.53	0	1	-456	7.02	2.37	3.53	0	1	-455	0.00	2.37	3.53	0	1

-454	14.04	1.58	3.53	0	1	-453	7.02	1.58	3.53	0	1	-452	0.00	1.58	3.53	0	1
-451	14.04	0.79	3.53	0	1	-450	7.02	0.79	3.53	0	1	-449	0.00	0.79	3.53	0	1
-448	14.04	0.00	3.53	0	1	-447	7.02	0.00	3.53	0	1	-446	0.00	0.00	3.53	0	1
-445	14.04	-0.50	3.53	0	1	-444	7.02	-0.50	3.53	0	1	-443	0.00	-0.50	3.53	0	1
-442	14.04	5.24	2.65	0	1	-441	7.02	5.24	2.65	0	1	-440	0.00	5.24	2.65	0	1
-439	14.04	4.74	2.65	0	1	-438	7.02	4.74	2.65	0	1	-437	0.00	4.74	2.65	0	1
-436	14.04	3.95	2.65	0	1	-435	7.02	3.95	2.65	0	1	-434	0.00	3.95	2.65	0	1
-433	14.04	3.16	2.65	0	1	-432	7.02	3.16	2.65	0	1	-431	0.00	3.16	2.65	0	1
-430	14.04	2.37	2.65	0	1	-429	7.02	2.37	2.65	0	1	-428	0.00	2.37	2.65	0	1
-427	14.04	1.58	2.65	0	1	-426	7.02	1.58	2.65	0	1	-425	0.00	1.58	2.65	0	1
-424	14.04	0.79	2.65	0	1	-423	7.02	0.79	2.65	0	1	-422	0.00	0.79	2.65	0	1
-421	14.04	0.00	2.65	0	1	-420	7.02	0.00	2.65	0	1	-419	0.00	0.00	2.65	0	1
-418	14.04	-0.50	2.65	0	1	-417	7.02	-0.50	2.65	0	1	-416	0.00	-0.50	2.65	0	1
-415	14.04	5.24	1.77	0	1	-414	7.02	5.24	1.77	0	1	-413	0.00	5.24	1.77	0	1
-412	14.04	4.74	1.77	0	1	-411	7.02	4.74	1.77	0	1	-410	0.00	4.74	1.77	0	1
-409	14.04	3.95	1.77	0	1	-408	7.02	3.95	1.77	0	1	-407	0.00	3.95	1.77	0	1
-406	14.04	3.16	1.77	0	1	-405	7.02	3.16	1.77	0	1	-404	0.00	3.16	1.77	0	1
-403	14.04	2.37	1.77	0	1	-402	7.02	2.37	1.77	0	1	-401	0.00	2.37	1.77	0	1
-400	14.04	1.58	1.77	0	1	-399	7.02	1.58	1.77	0	1	-398	0.00	1.58	1.77	0	1
-397	14.04	0.79	1.77	0	1	-396	7.02	0.79	1.77	0	1	-395	0.00	0.79	1.77	0	1
-394	14.04	0.00	1.77	0	1	-393	7.02	0.00	1.77	0	1	-392	0.00	0.00	1.77	0	1
-391	14.04	-0.50	1.77	0	1	-390	7.02	-0.50	1.77	0	1	-389	0.00	-0.50	1.77	0	1
-388	14.04	5.24	0.88	0	1	-387	7.02	5.24	0.88	0	1	-386	0.00	5.24	0.88	0	1
-385	14.04	4.74	0.88	0	1	-384	7.02	4.74	0.88	0	1	-383	0.00	4.74	0.88	0	1
-382	14.04	3.95	0.88	0	1	-381	7.02	3.95	0.88	0	1	-380	0.00	3.95	0.88	0	1
-379	14.04	3.16	0.88	0	1	-378	7.02	3.16	0.88	0	1	-377	0.00	3.16	0.88	0	1
-376	14.04	2.37	0.88	0	1	-375	7.02	2.37	0.88	0	1	-374	0.00	2.37	0.88	0	1
-373	14.04	1.58	0.88	0	1	-372	7.02	1.58	0.88	0	1	-371	0.00	1.58	0.88	0	1
-370	14.04	0.79	0.88	0	1	-369	7.02	0.79	0.88	0	1	-368	0.00	0.79	0.88	0	1
-367	14.04	0.00	0.88	0	1	-366	7.02	0.00	0.88	0	1	-365	0.00	0.00	0.88	0	1
-364	14.04	-0.50	0.88	0	1	-363	7.02	-0.50	0.88	0	1	-362	0.00	-0.50	0.88	0	1
-361	15.94	7.36	0.00	0	1	-360	14.95	7.36	0.00	0	1	-359	13.96	7.36	0.00	0	1
-358	12.97	7.36	0.00	0	1	-357	11.98	7.36	0.00	0	1	-356	10.98	7.36	0.00	0	1
-355	9.99	7.36	0.00	0	1	-354	9.00	7.36	0.00	0	1	-353	8.01	7.36	0.00	0	1
-352	7.02	7.36	0.00	0	1	-351	6.03	7.36	0.00	0	1	-350	5.04	7.36	0.00	0	1
-349	4.05	7.36	0.00	0	1	-348	3.06	7.36	0.00	0	1	-347	2.06	7.36	0.00	0	1
-346	1.07	7.36	0.00	0	1	-345	0.08	7.36	0.00	0	1	-344	-0.91	7.36	0.00	0	1
-343	-1.90	7.36	0.00	0	1	-342	13.62	6.89	0.00	0	1	-341	0.42	6.89	0.00	0	1
-340	13.25	6.88	0.00	0	1	-339	0.79	6.88	0.00	0	1	-338	8.85	6.77	0.00	0	1
-337	5.19	6.77	0.00	0	1	-336	8.45	6.76	0.00	0	1	-335	5.59	6.76	0.00	0	1
-334	10.14	6.67	0.00	0	1	-333	3.90	6.67	0.00	0	1	-332	10.94	6.64	0.00	0	1
-331	3.10	6.64	0.00	0	1	-330	11.83	6.59	0.00	0	1	-329	2.21	6.59	0.00	0	1
-328	14.21	6.53	0.00	0	1	-327	-0.17	6.53	0.00	0	1	-326	15.14	6.46	0.00	0	2
-325	12.74	6.46	0.00	0	2	-324	9.42	6.46	0.00	0	2	-323	7.02	6.46	0.00	0	2
-322	4.62	6.46	0.00	0	2	-321	1.30	6.46	0.00	0	2	-320	-1.10	6.46	0.00	0	2
-319	13.64	6.41	0.00	0	1	-318	0.40	6.41	0.00	0	1	-317	13.17	6.40	0.00	0	1
-316	0.87	6.40	0.00	0	1	-315	15.94	6.36	0.00	0	1	-314	-1.90	6.36	0.00	0	1
-313	7.80	6.24	0.00	0	1	-312	6.24	6.24	0.00	0	1	-311	10.23	6.24	0.00	0	1
-310	3.81	6.24	0.00	0	1	-309	9.11	6.17	0.00	0	1	-308	4.93	6.17	0.00	0	1
-307	8.50	6.17	0.00	0	1	-306	5.54	6.17	0.00	0	1	-305	9.79	6.11	0.00	0	1
-304	4.25	6.11	0.00	0	1	-303	9.51	6.01	0.00	0	1	-302	4.53	6.01	0.00	0	1
-301	10.72	5.95	0.00	0	1	-300	3.32	5.95	0.00	0	1	-299	14.62	5.90	0.00	0	1
-298	-0.58	5.90	0.00	0	1	-297	11.67	5.89	0.00	0	1	-296	2.37	5.89	0.00	0	1
-295	14.11	5.88	0.00	0	1	-294	-0.07	5.88	0.00	0	1	-293	12.47	5.85	0.00	0	1
-292	1.57	5.85	0.00	0	1	-291	13.58	5.84	0.00	0	1	-290	0.46	5.84	0.00	0	1
-289	13.05	5.83	0.00	0	1	-288	0.99	5.83	0.00	0	1	-287	7.02	5.81	0.00	0	1
-286	10.05	5.79	0.00	0	1	-285	3.99	5.79	0.00	0	1	-284	7.45	5.77	0.00	0	1
-283	6.59	5.77	0.00	0	1	-282	9.62	5.75	0.00	0	1	-281	4.42	5.75	0.00	0	1
-280	9.35	5.54	0.00	0	1	-279	4.69	5.54	0.00	0	1	-278	15.20	5.54	0.00	0	1
-277	-1.16	5.54	0.00	0	1	-276	8.64	5.51	0.00	0	1	-275	5.40	5.51	0.00	0	1
-274	8.03	5.47	0.00	0	1	-273	6.01	5.47	0.00	0	1	-272	14.61	5.38	0.00	0	1
-271	-0.57	5.38	0.00	0	1	-270	15.94	5.36	0.00	0	1	/Vc,	-1.90	5.36	0.00	0	1
-268	10.01	5.35	0.00	0	1	-267	4.03	5.35	0.00	0	1	-266	7.53	5.31	0.00	0	1
-265	6.51	5.31	0.00	0	1	-264	10.71	5.26	0.00	0	1	-263	3.33	5.26	0.00	0	1
-262	12.98	5.25	0.00	0	1	-261	1.06	5.25	0.00	0	1	-260	13.51	5.25	0.00	0	1
-259	0.53	5.25	0.00	0	1	-258	14.04	5.24	0.00	0	1	-257	7.02	5.24	0.00	0	1
-256	0.00	5.24	0.00	0	1	-255	12.35	5.22	0.00	0	1	-254	1.69	5.22	0.00	0	1
-253	11.59	5.21	0.00	0	1	-252	2.45	5.21	0.00	0	1	-251	15.52	4.97	0.00	0	1
-250	-1.48	4.97	0.00	0	1	-249	15.10	4.96	0.00	0	1	-248	-1.06	4.96	0.00	0	1
-247	9.38	4.95	0.00	0	1	-246	4.66	4.95	0.00	0	1	-245	9.96	4.94	0.00	0	1
-244	4.08	4.94	0.00	0	1	-243	8.73	4.93	0.00	0	1	-242	5.31	4.93	0.00	0	1
-241	8.14	4.89	0.00	0	1	-240	5.90	4.89	0.00	0	1	-239	14.58	4.87	0.00	0	1
-238	-0.54	4.87	0.00	0	1	-237	14.04	4.74	0.00	0	1	-236	7.64	4.74	0.00	0	1
-235	7.02	4.74	0.00	0	1	-234	6.40	4.74	0.00	0	1	-233	0.00	4.74	0.00	0	1
-232	12.91	4.70	0.00	0	1	-231	1.13	4.70	0.00	0	1	-230	13.45	4.67	0.00	0	1
-229	0.59	4.67	0.00	0	1	-228	12.34	4.64	0.00	0	1	-227	1.70	4.64	0.00	0	1
-226	15.52	4.60	0.00	0	1	-225	-1.48	4.60	0.00	0	1	-224	10.47	4.56	0.00	0	1
-223	3.57	4.56	0.00	0	1	-222	11.55	4.50	0.00	0	1	-221	2.49	4.50	0.00	0	1
-220	15.08	4.48	0.00	0	1	-219	-1.04	4.48	0.00	0	1	-218	9.50	4.46	0.00	0	1
-217	4.54	4.46	0.00	0	1	-216	8.25	4.45	0.00	0	1	-215	5.79	4.45	0.00	0	1
-214	8.76	4.44	0.00	0	1	-213	5.28	4.44	0.00	0	1	-212	14.57	4.43	0.00	0	1
-211	-0.53	4.43	0.00	0	1	-210	15.94	4.36	0.00	0	1	-209	-1.90	4.36	0.00	0	1

-208	12.90	4.28	0.00	0	1	-207	1.14	4.28	0.00	0	1	-206	12.43	4.12	0.00	0	1
-205	1.61	4.12	0.00	0	1	-204	7.85	4.09	0.00	0	1	-203	6.19	4.09	0.00	0	1
-202	13.29	4.01	0.00	0	1	-201	0.75	4.01	0.00	0	1	-200	15.14	3.95	0.00	0	2
-199	14.04	3.95	0.00	0	1	-198	12.74	3.95	0.00	0	2	-197	9.42	3.95	0.00	0	2
-196	7.02	3.95	0.00	0	2	-195	4.62	3.95	0.00	0	2	-194	1.30	3.95	0.00	0	2
-193	0.00	3.95	0.00	0	1	-192	-1.10	3.95	0.00	0	2	-191	8.60	3.95	0.00	0	1
-190	5.44	3.95	0.00	0	1	-189	10.56	3.71	0.00	0	1	-188	3.48	3.71	0.00	0	1
-187	11.77	3.65	0.00	0	1	-186	2.27	3.65	0.00	0	1	-185	15.94	3.36	0.00	0	1
-184	-1.90	3.36	0.00	0	1	-183	8.41	3.36	0.00	0	1	-182	5.63	3.36	0.00	0	1
-181	8.92	3.35	0.00	0	1	-180	5.12	3.35	0.00	0	1	-179	7.78	3.34	0.00	0	1
-178	6.26	3.34	0.00	0	1	-177	12.60	3.32	0.00	0	1	-176	1.44	3.32	0.00	0	1
-175	13.32	3.23	0.00	0	1	-174	0.72	3.23	0.00	0	1	-173	15.04	3.21	0.00	0	1
-172	-1.00	3.21	0.00	0	1	-171	14.04	3.16	0.00	0	1	-170	7.02	3.16	0.00	0	1
-169	0.00	3.16	0.00	0	1	-168	7.85	2.80	0.00	0	1	-167	6.19	2.80	0.00	0	1
-166	8.37	2.77	0.00	0	1	-165	7.43	2.76	0.00	0	1	-164	6.61	2.76	0.00	0	1
-163	5.67	2.77	0.00	0	1	-162	8.94	2.76	0.00	0	1	-161	5.10	2.76	0.00	0	1
-160	9.59	2.75	0.00	0	1	-159	4.45	2.75	0.00	0	1	-158	10.59	2.72	0.00	0	1
-157	3.45	2.72	0.00	0	1	-156	11.63	2.65	0.00	0	1	-155	2.41	2.65	0.00	0	1
-154	12.58	2.49	0.00	0	1	-153	1.46	2.49	0.00	0	1	-152	13.32	2.42	0.00	0	1
-151	0.72	2.42	0.00	0	1	-150	15.04	2.38	0.00	0	1	-149	-1.00	2.38	0.00	0	1
-148	14.04	2.37	0.00	0	1	-147	7.02	2.37	0.00	0	1	-146	0.00	2.37	0.00	0	1
-145	15.94	2.36	0.00	0	1	-144	-1.90	2.36	0.00	0	1	-143	7.43	2.35	0.00	0	1
-142	6.61	2.35	0.00	0	1	-141	7.85	2.30	0.00	0	1	-140	6.19	2.30	0.00	0	1
-139	8.31	2.17	0.00	0	1	-138	5.73	2.17	0.00	0	1	-137	8.89	2.17	0.00	0	1
-136	5.15	2.17	0.00	0	1	-135	7.42	1.94	0.00	0	1	-134	6.62	1.94	0.00	0	1
-133	7.80	1.90	0.00	0	1	-132	6.24	1.89	0.00	0	1	-131	10.56	1.81	0.00	0	1
-130	3.48	1.81	0.00	0	1	-129	11.61	1.77	0.00	0	1	-128	2.43	1.77	0.00	0	1
-127	13.35	1.60	0.00	0	1	-126	0.69	1.60	0.00	0	1	-125	15.14	1.58	0.00	0	2
-124	14.04	1.58	0.00	0	1	-123	12.74	1.58	0.00	0	2	-122	9.42	1.58	0.00	0	2
-121	7.02	1.58	0.00	0	2	-120	4.62	1.58	0.00	0	2	-119	1.30	1.58	0.00	0	2
-118	0.00	1.58	0.00	0	1	-117	-1.10	1.58	0.00	0	2	-116	8.14	1.42	0.00	0	1
-115	5.89	1.42	0.00	0	1	-114	15.94	1.36	0.00	0	1	-113	-1.90	1.36	0.00	0	1
-112	10.05	1.17	0.00	0	1	-111	3.99	1.17	0.00	0	1	-110	10.66	1.17	0.00	0	1
-109	3.38	1.17	0.00	0	1	-108	11.49	1.07	0.00	0	1	-107	2.55	1.07	0.00	0	1
-106	8.99	0.93	0.00	0	1	-105	5.05	0.93	0.00	0	1	-104	8.52	0.90	0.00	0	1
-103	5.51	0.89	0.00	0	1	-102	13.29	0.81	0.00	0	1	-101	0.75	0.81	0.00	0	1
-100	14.04	0.79	0.00	0	1	-99	7.02	0.79	0.00	0	1	-98	0.00	0.79	0.00	0	1
-97	12.40	0.78	0.00	0	1	-96	1.64	0.78	0.00	0	1	-95	10.07	0.74	0.00	0	1
-94	3.97	0.74	0.00	0	1	-93	10.60	0.64	0.00	0	1	-92	3.45	0.64	0.00	0	1
-91	11.26	0.52	0.00	0	1	-90	2.78	0.52	0.00	0	1	-89	11.87	0.42	0.00	0	1
-88	2.17	0.42	0.00	0	1	-87	7.75	0.41	0.00	0	1	-86	14.96	0.40	0.00	0	1
-85	9.66	0.40	0.00	0	1	-84	4.38	0.40	0.00	0	1	-83	-0.92	0.40	0.00	0	1
-82	6.24	0.39	0.00	0	1	-81	15.94	0.36	0.00	0	1	-80	-1.90	0.36	0.00	0	1
-79	8.42	0.30	0.00	0	1	-78	8.99	0.29	0.00	0	1	-77	5.04	0.29	0.00	0	1
-76	5.58	0.29	0.00	0	1	-75	13.34	0.07	0.00	0	1	-74	0.70	0.07	0.00	0	1
-73	10.38	0.06	0.00	0	1	-72	3.66	0.06	0.00	0	1	-71	7.40	0.03	0.00	0	1
-70	12.60	0.01	0.00	0	1	-69	1.44	0.01	0.00	0	1	-68	14.04	0.00	0.00	0	1
-67	7.02	0.00	0.00	0	1	-66	0.00	0.00	0.00	0	1	-65	14.52	-0.01	0.00	0	1
-64	-0.48	-0.01	0.00	0	1	-63	6.60	-0.04	0.00	0	1	-62	11.16	-0.06	0.00	0	1
-61	2.88	-0.06	0.00	0	1	-60	11.88	-0.10	0.00	0	1	-59	2.16	-0.10	0.00	0	1
-58	7.39	-0.33	0.00	0	1	-57	14.57	-0.41	0.00	0	1	-56	-0.53	-0.41	0.00	0	1
-55	8.36	-0.44	0.00	0	1	-54	5.61	-0.44	0.00	0	1	-53	8.90	-0.48	0.00	0	1
-52	5.12	-0.49	0.00	0	1	-51	14.04	-0.50	0.00	0	1	-50	7.02	-0.50	0.00	0	1
-49	0.00	-0.50	0.00	0	1	-48	6.56	-0.51	0.00	0	1	-47	7.72	-0.55	0.00	0	1
-46	6.10	-0.55	0.00	0	1	-45	13.41	-0.56	0.00	0	1	-44	0.63	-0.56	0.00	0	1
-43	15.94	-0.64	0.00	0	1	-42	-1.90	-0.64	0.00	0	1	-41	15.14	-0.74	0.00	0	2
-40	12.74	-0.74	0.00	0	2	-39	9.42	-0.74	0.00	0	2	-38	7.02	-0.74	0.00	0	2
-37	4.62	-0.74	0.00	0	2	-36	1.30	-0.74	0.00	0	2	-35	-1.10	-0.74	0.00	0	2
-34	10.22	-0.77	0.00	0	1	-33	3.82	-0.77	0.00	0	1	-32	11.92	-0.81	0.00	0	1
-31	11.06	-0.81	0.00	0	1	-30	2.98	-0.81	0.00	0	1	-29	2.12	-0.81	0.00	0	1
-28	6.53	-0.96	0.00	0	1	-27	14.16	-0.99	0.00	0	1	-26	-0.12	-0.99	0.00	0	1
-25	8.39	-1.05	0.00	0	1	-24	5.62	-1.05	0.00	0	1	-23	8.77	-1.06	0.00	0	1
-22	5.26	-1.06	0.00	0	1	-21	13.51	-1.06	0.00	0	1	-20	0.53	-1.06	0.00	0	1
-19	15.94	-1.64	0.00	0	1	-18	14.95	-1.64	0.00	0	1	-17	13.96	-1.64	0.00	0	1
-16	12.97	-1.64	0.00	0	1	-15	11.98	-1.64	0.00	0	1	-14	10.98	-1.64	0.00	0	1
-13	9.99	-1.64	0.00	0	1	-12	9.00	-1.64	0.00	0	1	-11	8.01	-1.64	0.00	0	1
-10	7.02	-1.64	0.00	0	1	-9	6.03	-1.64	0.00	0	1	-8	5.04	-1.64	0.00	0	1
-7	4.05	-1.64	0.00	0	1	-6	3.06	-1.64	0.00	0	1	-5	2.06	-1.64	0.00	0	1
-4	1.07	-1.64	0.00	0	1	-3	0.08	-1.64	0.00	0	1	-2	-0.91	-1.64	0.00	0	1
-1	-1.90	-1.64	0.00	0	1	101	0.00	0.00	5.30	1	1	102	1.17	0.00	5.30	1	1
103	2.34	0.00	5.30	1	1	104	3.51	0.00	5.30	1	1	105	4.68	0.00	5.30	1	1
106	5.85	0.00	5.30	1	1	107	7.02	0.00	5.30	1	1	108	8.19	0.00	5.30	1	1
109	9.36	0.00	5.30	1	1	110	10.53	0.00	5.30	1	1	111	11.70	0.00	5.30	1	1
112	12.87	0.00	5.30	1	1	113	14.04	0.00	5.30	1	1	114	0.00	0.79	5.30	1	1
115	1.17	0.79	5.30	1	1	116	2.34	0.79	5.30	1	1	117	3.51	0.79	5.30	1	1
118	4.68	0.79	5.30	1	1	119	5.85	0.79	5.30	1	1	120	7.02	0.79	5.30	1	1
121	8.19	0.79	5.30	1	1	122	9.36	0.79	5.30	1	1	123	10.53	0.79	5.30	1	1
124	11.70	0.79	5.30	1	1	125	12.87	0.79	5.30	1	1	126	14.04	0.79	5.30	1	1
127	0.00	1.58	5.30	1	1	128	1.17	1.58	5.30	1	1	129	2.34	1.58	5.30	1	1
130	3.51	1.58	5.30	1	1	131	4.68	1.58	5.30	1	1	132	5.85	1.58	5.30	1	1
133	7.02	1.58	5.30	1	1	134	8.19	1.58	5.30	1	1	135	9.36	1.58	5.30	1	1
136	10.53	1.58	5.30	1	1	137	11.70	1.58	5.30	1	1	138	12.87	1.58	5.30	1	1

139	14.04	1.58	5.30	1	1	140	0.00	2.37	5.30	1	1	141	1.17	2.37	5.30	1	1
142	2.34	2.37	5.30	1	1	143	3.51	2.37	5.30	1	1	144	4.68	2.37	5.30	1	1
145	5.85	2.37	5.30	1	1	146	7.02	2.37	5.30	1	1	147	8.19	2.37	5.30	1	1
148	9.36	2.37	5.30	1	1	149	10.53	2.37	5.30	1	1	150	11.70	2.37	5.30	1	1
151	12.87	2.37	5.30	1	1	152	14.04	2.37	5.30	1	1	153	0.00	3.16	5.30	1	1
154	1.17	3.16	5.30	1	1	155	2.34	3.16	5.30	1	1	156	3.51	3.16	5.30	1	1
157	4.68	3.16	5.30	1	1	158	5.85	3.16	5.30	1	1	159	7.02	3.16	5.30	1	1
160	8.19	3.16	5.30	1	1	161	9.36	3.16	5.30	1	1	162	10.53	3.16	5.30	1	1
163	11.70	3.16	5.30	1	1	164	12.87	3.16	5.30	1	1	165	14.04	3.16	5.30	1	1
166	0.00	3.95	5.30	1	1	167	1.17	3.95	5.30	1	1	168	2.34	3.95	5.30	1	1
169	3.51	3.95	5.30	1	1	170	4.68	3.95	5.30	1	1	171	5.85	3.95	5.30	1	1
172	7.02	3.95	5.30	1	1	173	8.19	3.95	5.30	1	1	174	9.36	3.95	5.30	1	1
175	10.53	3.95	5.30	1	1	176	11.70	3.95	5.30	1	1	177	12.87	3.95	5.30	1	1
178	14.04	3.95	5.30	1	1	179	0.00	4.74	5.30	1	1	180	1.17	4.74	5.30	1	1
181	2.34	4.74	5.30	1	1	182	3.51	4.74	5.30	1	1	183	4.68	4.74	5.30	1	1
184	5.85	4.74	5.30	1	1	185	7.02	4.74	5.30	1	1	186	8.19	4.74	5.30	1	1
187	9.36	4.74	5.30	1	1	188	10.53	4.74	5.30	1	1	189	11.70	4.74	5.30	1	1
190	12.87	4.74	5.30	1	1	191	14.04	4.74	5.30	1	1						

Elenco materiali

Simbologia

Mat. = Numero del materiale
Comm. = Commento
P = Peso specifico
E = Modulo elastico
G = Modulo elastico tangenziale
ν = Coeff. di Poisson
α = Coeff. di dilatazione termica

Mat.	Comm.	P <daN/mc>	E <daN/cmq>	G <daN/cmq>	ν	α
1	Calcestruzzo	2500	300000.00	130000.00	0.1	1.000000E-005
2	Acciaio	7850	2100000.00	800000.00	0.3	1.000000E-005

Elenco sezioni aste

Simbologia

Sez. = Numero della sezione
Comm. = Commento
Tipo = Tipologia
- 2C = Doppia C lato labbri
- 2Cdx = Doppia C lato costola
- 2I = Doppia I
- 2L = Doppia L lato labbri
- 2Ldx = Doppia L lato costole
- C = C
- Cdx = C destra
- Cir. = Circolare
- Cir.c = Circolare cava
- I = I
- L = L
- Ldx = L destra
- Om. = Omega
- Pg = Pi greco
- Pr = Poligono regolare
- Prc = Poligono regolare cavo
- Pc = Per coordinate
- Ia = Inerzie assegnate
- R = Rettangolare
- Rc = Rettangolare cava
- T = T
- U = U
- Ur = U rovescia
- V = V
- Vr = V rovescia
- Z = Z
- Zdx = Z destra
- Ts = T stondata
- Ls = L stondata
- Cs = C stondata
- Is = I stondata
- Dis. = Disegnata

Me = Membratura
- G = Generica
- T = Trave
- P = Pilastro

Ver. = Verifica prevista
- N = Nessuna

C = Cemento armato
A = Acciaio
L = Legno
B = Base
H = Altezza
s = Spessore ala
a = Spessore anima
r = Raggio raccordo anima-ala
r1 = Raggio in testa ala
Ma = Numero del materiale
C = Numero del criterio di progetto
Ccol = Numero del criterio di progetto collegamento

Sez.	Comm.	Tipo	Me	Ver.	B <cm>	H <cm>	s <cm>	a <cm>	r <cm>	r1 <cm>	Ma	C	Ccol
1	HEA280	Is	T	A	28.00	27.00	1.30	0.80	2.40	0.00	2	1	1
2	HEB280	Is	T	A	28.00	28.00	1.80	1.05	2.40	0.00	2	1	1
3	IPE180	Is	T	A	9.10	18.00	0.80	0.53	0.90	0.00	2	1	1

Elenco vincoli aste

Simbologia

Va = Numero del vincolo asta
Comm. = Commento
Tipo = Tipologia
SVI = Definizione di vincolamenti interni
ELA = Vincolo su suolo elastico alla Winkler
BIE-RTC = Biella resistente a trazione e a compressione
BIE-RC = Biella resistente solo a compressione
BIE-RT = Biella resistente solo a trazione
Ni = Sforzo normale nodo iniziale (0=sbloccato, 1=bloccato)
Tyi = Taglio in dir. Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Tzi = Taglio in dir. Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Mxi = Momento intorno all'asse X locale nodo iniziale (0=sbloccato, 1=bloccato)
Myi = Momento intorno all'asse Y locale nodo iniziale (0=sbloccato, 1=bloccato)
Mzi = Momento intorno all'asse Z locale nodo iniziale (0=sbloccato, 1=bloccato)
Nf = Sforzo normale nodo finale (0=sbloccato, 1=bloccato)
Tyf = Taglio in dir. Y locale nodo finale (0=sbloccato, 1=bloccato)
Tzf = Taglio in dir. Z locale nodo finale (0=sbloccato, 1=bloccato)
Mxf = Momento intorno all'asse X locale nodo finale (0=sbloccato, 1=bloccato)
Myf = Momento intorno all'asse Y locale nodo finale (0=sbloccato, 1=bloccato)
Mzf = Momento intorno all'asse Z locale nodo finale (0=sbloccato, 1=bloccato)
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Va	Comm.	Tipo	Ni	Tyi	Tzi	Mxi	Myi	Mzi	Nf	Tyf	Tzf	Mxf	Myf	Mzf	Kt <daN/cmc>
1	Inc+Inc	SVI	1	1	1	1	1	1	1	1	1	1	1	1	
4	Cer+Cer	SVI	1	1	1	0	0	0	1	1	1	1	0	0	
5	Inc+CerY	SVI	1	1	1	1	1	1	1	1	1	1	0	1	
6	CerY+Inc	SVI	1	1	1	1	0	1	1	1	1	1	1	1	

Elenco aste

Simbologia

Asta = Numero dell'asta
N1 = Nodo iniziale
N2 = Nodo finale
Sez. = Numero della sezione
Va = Numero del vincolo asta
Par. = Numero dei parametri aggiuntivi
Rot. = Rotazione
FF = Filo fisso
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Dz1 = Scost. filo fisso Z1
Dz2 = Scost. filo fisso Z2
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Asta	N1	N2	Sez.	Va	Par.	Rot. <grad>	FF	Dy1 <cm>	Dy2 <cm>	Dz1 <cm>	Dz2 <cm>	Kt <daN/cmc>
101	101	102	1	6		0.00	44	0.00	0.00	0.00	0.00	
101	102	103	1	1		0.00	44	0.00	0.00	0.00	0.00	
101	103	104	1	1		0.00	44	0.00	0.00	0.00	0.00	
101	104	105	1	1		0.00	44	0.00	0.00	0.00	0.00	
101	105	106	1	1		0.00	44	0.00	0.00	0.00	0.00	
101	106	107	1	5		0.00	44	0.00	0.00	0.00	0.00	
101	107	108	1	6		0.00	44	0.00	0.00	0.00	0.00	
101	108	109	1	1		0.00	44	0.00	0.00	0.00	0.00	
101	109	110	1	1		0.00	44	0.00	0.00	0.00	0.00	

101	110	111	1	1	0.00	44	0.00	0.00	0.00	0.00
101	111	112	1	1	0.00	44	0.00	0.00	0.00	0.00
101	112	113	1	5	0.00	44	0.00	0.00	0.00	0.00
102	114	115	3	4	0.00	44	0.00	0.00	0.00	0.00
102	115	116	3	4	0.00	44	0.00	0.00	0.00	0.00
102	116	117	3	4	0.00	44	0.00	0.00	0.00	0.00
102	117	118	3	4	0.00	44	0.00	0.00	0.00	0.00
102	118	119	3	4	0.00	44	0.00	0.00	0.00	0.00
102	119	120	3	4	0.00	44	0.00	0.00	0.00	0.00
102	120	121	3	4	0.00	44	0.00	0.00	0.00	0.00
102	121	122	3	4	0.00	44	0.00	0.00	0.00	0.00
102	122	123	3	4	0.00	44	0.00	0.00	0.00	0.00
102	123	124	3	4	0.00	44	0.00	0.00	0.00	0.00
102	124	125	3	4	0.00	44	0.00	0.00	0.00	0.00
102	125	126	3	4	0.00	44	0.00	0.00	0.00	0.00
103	127	128	3	4	0.00	44	0.00	0.00	0.00	0.00
103	128	129	3	4	0.00	44	0.00	0.00	0.00	0.00
103	129	130	3	4	0.00	44	0.00	0.00	0.00	0.00
103	130	131	3	4	0.00	44	0.00	0.00	0.00	0.00
103	131	132	3	4	0.00	44	0.00	0.00	0.00	0.00
103	132	133	3	4	0.00	44	0.00	0.00	0.00	0.00
103	133	134	3	4	0.00	44	0.00	0.00	0.00	0.00
103	134	135	3	4	0.00	44	0.00	0.00	0.00	0.00
103	135	136	3	4	0.00	44	0.00	0.00	0.00	0.00
103	136	137	3	4	0.00	44	0.00	0.00	0.00	0.00
103	137	138	3	4	0.00	44	0.00	0.00	0.00	0.00
103	138	139	3	4	0.00	44	0.00	0.00	0.00	0.00
104	140	141	2	6	0.00	44	0.00	0.00	0.00	0.00
104	141	142	2	1	0.00	44	0.00	0.00	0.00	0.00
104	142	143	2	1	0.00	44	0.00	0.00	0.00	0.00
104	143	144	2	1	0.00	44	0.00	0.00	0.00	0.00
104	144	145	2	1	0.00	44	0.00	0.00	0.00	0.00
104	145	146	2	5	0.00	44	0.00	0.00	0.00	0.00
104	146	147	2	6	0.00	44	0.00	0.00	0.00	0.00
104	147	148	2	1	0.00	44	0.00	0.00	0.00	0.00
104	148	149	2	1	0.00	44	0.00	0.00	0.00	0.00
104	149	150	2	1	0.00	44	0.00	0.00	0.00	0.00
104	150	151	2	1	0.00	44	0.00	0.00	0.00	0.00
104	151	152	2	5	0.00	44	0.00	0.00	0.00	0.00
105	153	154	3	4	0.00	44	0.00	0.00	0.00	0.00
105	154	155	3	4	0.00	44	0.00	0.00	0.00	0.00
105	155	156	3	4	0.00	44	0.00	0.00	0.00	0.00
105	156	157	3	4	0.00	44	0.00	0.00	0.00	0.00
105	157	158	3	4	0.00	44	0.00	0.00	0.00	0.00
105	158	159	3	4	0.00	44	0.00	0.00	0.00	0.00
105	159	160	3	4	0.00	44	0.00	0.00	0.00	0.00
105	160	161	3	4	0.00	44	0.00	0.00	0.00	0.00
105	161	162	3	4	0.00	44	0.00	0.00	0.00	0.00
105	162	163	3	4	0.00	44	0.00	0.00	0.00	0.00
105	163	164	3	4	0.00	44	0.00	0.00	0.00	0.00
105	164	165	3	4	0.00	44	0.00	0.00	0.00	0.00
106	166	167	3	4	0.00	44	0.00	0.00	0.00	0.00
106	167	168	3	4	0.00	44	0.00	0.00	0.00	0.00
106	168	169	3	4	0.00	44	0.00	0.00	0.00	0.00
106	169	170	3	4	0.00	44	0.00	0.00	0.00	0.00
106	170	171	3	4	0.00	44	0.00	0.00	0.00	0.00
106	171	172	3	4	0.00	44	0.00	0.00	0.00	0.00
106	172	173	3	4	0.00	44	0.00	0.00	0.00	0.00
106	173	174	3	4	0.00	44	0.00	0.00	0.00	0.00
106	174	175	3	4	0.00	44	0.00	0.00	0.00	0.00
106	175	176	3	4	0.00	44	0.00	0.00	0.00	0.00
106	176	177	3	4	0.00	44	0.00	0.00	0.00	0.00
106	177	178	3	4	0.00	44	0.00	0.00	0.00	0.00
107	179	180	1	6	0.00	44	0.00	0.00	0.00	0.00
107	180	181	1	1	0.00	44	0.00	0.00	0.00	0.00
107	181	182	1	1	0.00	44	0.00	0.00	0.00	0.00
107	182	183	1	1	0.00	44	0.00	0.00	0.00	0.00
107	183	184	1	1	0.00	44	0.00	0.00	0.00	0.00
107	184	185	1	5	0.00	44	0.00	0.00	0.00	0.00
107	185	186	1	6	0.00	44	0.00	0.00	0.00	0.00
107	186	187	1	1	0.00	44	0.00	0.00	0.00	0.00
107	187	188	1	1	0.00	44	0.00	0.00	0.00	0.00
107	188	189	1	1	0.00	44	0.00	0.00	0.00	0.00
107	189	190	1	1	0.00	44	0.00	0.00	0.00	0.00
107	190	191	1	5	0.00	44	0.00	0.00	0.00	0.00
108	101	114	3	1	0.00	44	0.00	0.00	0.00	0.00
108	114	127	3	1	0.00	44	0.00	0.00	0.00	0.00
108	127	140	3	1	0.00	44	0.00	0.00	0.00	0.00
108	140	153	3	1	0.00	44	0.00	0.00	0.00	0.00
108	153	166	3	1	0.00	44	0.00	0.00	0.00	0.00
108	166	179	3	1	0.00	44	0.00	0.00	0.00	0.00
109	102	115	3	6	0.00	44	0.00	0.00	0.00	0.00

109	115	128	3	1	0.00	44	0.00	0.00	0.00	0.00
109	128	141	3	5	0.00	44	0.00	0.00	0.00	0.00
109	141	154	3	6	0.00	44	0.00	0.00	0.00	0.00
109	154	167	3	1	0.00	44	0.00	0.00	0.00	0.00
109	167	180	3	5	0.00	44	0.00	0.00	0.00	0.00
110	103	116	3	6	0.00	44	0.00	0.00	0.00	0.00
110	116	129	3	1	0.00	44	0.00	0.00	0.00	0.00
110	129	142	3	5	0.00	44	0.00	0.00	0.00	0.00
110	142	155	3	6	0.00	44	0.00	0.00	0.00	0.00
110	155	168	3	1	0.00	44	0.00	0.00	0.00	0.00
110	168	181	3	5	0.00	44	0.00	0.00	0.00	0.00
111	104	117	3	6	0.00	44	0.00	0.00	0.00	0.00
111	117	130	3	1	0.00	44	0.00	0.00	0.00	0.00
111	130	143	3	5	0.00	44	0.00	0.00	0.00	0.00
111	143	156	3	6	0.00	44	0.00	0.00	0.00	0.00
111	156	169	3	1	0.00	44	0.00	0.00	0.00	0.00
111	169	182	3	5	0.00	44	0.00	0.00	0.00	0.00
112	105	118	3	6	0.00	44	0.00	0.00	0.00	0.00
112	118	131	3	1	0.00	44	0.00	0.00	0.00	0.00
112	131	144	3	5	0.00	44	0.00	0.00	0.00	0.00
112	144	157	3	6	0.00	44	0.00	0.00	0.00	0.00
112	157	170	3	1	0.00	44	0.00	0.00	0.00	0.00
112	170	183	3	5	0.00	44	0.00	0.00	0.00	0.00
113	106	119	3	6	0.00	44	0.00	0.00	0.00	0.00
113	119	132	3	1	0.00	44	0.00	0.00	0.00	0.00
113	132	145	3	5	0.00	44	0.00	0.00	0.00	0.00
113	145	158	3	6	0.00	44	0.00	0.00	0.00	0.00
113	158	171	3	1	0.00	44	0.00	0.00	0.00	0.00
113	171	184	3	5	0.00	44	0.00	0.00	0.00	0.00
114	107	120	3	1	0.00	44	0.00	0.00	0.00	0.00
114	120	133	3	1	0.00	44	0.00	0.00	0.00	0.00
114	133	146	3	1	0.00	44	0.00	0.00	0.00	0.00
114	146	159	3	1	0.00	44	0.00	0.00	0.00	0.00
114	159	172	3	1	0.00	44	0.00	0.00	0.00	0.00
114	172	185	3	1	0.00	44	0.00	0.00	0.00	0.00
115	108	121	3	6	0.00	44	0.00	0.00	0.00	0.00
115	121	134	3	1	0.00	44	0.00	0.00	0.00	0.00
115	134	147	3	5	0.00	44	0.00	0.00	0.00	0.00
115	147	160	3	6	0.00	44	0.00	0.00	0.00	0.00
115	160	173	3	1	0.00	44	0.00	0.00	0.00	0.00
115	173	186	3	5	0.00	44	0.00	0.00	0.00	0.00
116	109	122	3	6	0.00	44	0.00	0.00	0.00	0.00
116	122	135	3	1	0.00	44	0.00	0.00	0.00	0.00
116	135	148	3	5	0.00	44	0.00	0.00	0.00	0.00
116	148	161	3	6	0.00	44	0.00	0.00	0.00	0.00
116	161	174	3	1	0.00	44	0.00	0.00	0.00	0.00
116	174	187	3	5	0.00	44	0.00	0.00	0.00	0.00
117	110	123	3	6	0.00	44	0.00	0.00	0.00	0.00
117	123	136	3	1	0.00	44	0.00	0.00	0.00	0.00
117	136	149	3	5	0.00	44	0.00	0.00	0.00	0.00
117	149	162	3	6	0.00	44	0.00	0.00	0.00	0.00
117	162	175	3	1	0.00	44	0.00	0.00	0.00	0.00
117	175	188	3	5	0.00	44	0.00	0.00	0.00	0.00
118	111	124	3	6	0.00	44	0.00	0.00	0.00	0.00
118	124	137	3	1	0.00	44	0.00	0.00	0.00	0.00
118	137	150	3	5	0.00	44	0.00	0.00	0.00	0.00
118	150	163	3	6	0.00	44	0.00	0.00	0.00	0.00
118	163	176	3	1	0.00	44	0.00	0.00	0.00	0.00
118	176	189	3	5	0.00	44	0.00	0.00	0.00	0.00
119	112	125	3	6	0.00	44	0.00	0.00	0.00	0.00
119	125	138	3	1	0.00	44	0.00	0.00	0.00	0.00
119	138	151	3	5	0.00	44	0.00	0.00	0.00	0.00
119	151	164	3	6	0.00	44	0.00	0.00	0.00	0.00
119	164	177	3	1	0.00	44	0.00	0.00	0.00	0.00
119	177	190	3	5	0.00	44	0.00	0.00	0.00	0.00
120	113	126	3	1	0.00	44	0.00	0.00	0.00	0.00
120	126	139	3	1	0.00	44	0.00	0.00	0.00	0.00
120	139	152	3	1	0.00	44	0.00	0.00	0.00	0.00
120	152	165	3	1	0.00	44	0.00	0.00	0.00	0.00
120	165	178	3	1	0.00	44	0.00	0.00	0.00	0.00
120	178	191	3	1	0.00	44	0.00	0.00	0.00	0.00

Elenco tipi elementi bidimensionali

Simbologia

Tb = Numero del tipo muro/elemento bidimensionale
Comm. = Commento
Tipo = Tipologia
F = Flessionale
M = Membranale

W-RC = Winkler resistente solo a compressione
W-RTC = Winkler resistente a trazione e a compressione
Uso = Utilizzo
G = Generico
P = Parete
S = Soletta/Platea
N = Nucleo
M = Muratura ordinaria
L = Pilastro
MA = Muratura armata
Mat. = Numero del materiale
Crit. = Numero del criterio di progetto
Spess. = Spessore
Kt = Coeff. di sottofondo su suolo elastico alla Winkler

Tb	Comm.	Tipo	Uso	Mat.	Crit.	Spess. <cm>	Kt <daN/cmc>	Tb	Comm.	Tipo	Uso	Mat.	Crit.	Spess. <cm>	Kt <daN/cmc>
1	Spalla	F	P	1	1	70.00		2	Pila	F	P	1	1	100.00	
3	Fondazione	F	S	1	1	100.00									

Elenco elementi bidimensionali

Simbologia

Bid. = Numero del muro/elemento bidimensionale
Tb = Numero del tipo muro/elemento bidimensionale
FF = Filo fisso
Dy1 = Scost. filo fisso Y1
Dy2 = Scost. filo fisso Y2
Kt = Coeff. di sottofondo su suolo elastico alla Winkler
NN = Nodi

Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN	Bid.	Tb	FF	Dy1 <cm>	Dy2 <cm>	Kt <daN/cmc>	NN
102	2	22	0.00	0.00		-196 -170 -378 -381	102	2	22	0.00	0.00		-235 -196 -381 -384
102	2	22	0.00	0.00		-257 -235 -384 -387	102	2	22	0.00	0.00		-170 -147 -375 -378
102	2	22	0.00	0.00		-147 -121 -372 -375	102	2	22	0.00	0.00		-121 -99 -369 -372
102	2	22	0.00	0.00		-99 -67 -366 -369	102	2	22	0.00	0.00		-67 -50 -363 -366
102	2	22	0.00	0.00		-468 -465 -492 -495	102	2	22	0.00	0.00		-495 -492 185 -501
102	2	22	0.00	0.00		-384 -381 -408 -411	102	2	22	0.00	0.00		-411 -408 -435 -438
102	2	22	0.00	0.00		-438 -435 -462 -465	102	2	22	0.00	0.00		-465 -462 -489 -492
102	2	22	0.00	0.00		-492 -489 172 185	102	2	22	0.00	0.00		-381 -378 -405 -408
102	2	22	0.00	0.00		-408 -405 -432 -435	102	2	22	0.00	0.00		-435 -432 -459 -462
102	2	22	0.00	0.00		-462 -459 -486 -489	102	2	22	0.00	0.00		-489 -486 159 172
102	2	22	0.00	0.00		-378 -375 -402 -405	102	2	22	0.00	0.00		-405 -402 -429 -432
102	2	22	0.00	0.00		-432 -429 -456 -459	102	2	22	0.00	0.00		-459 -456 -483 -486
102	2	22	0.00	0.00		-486 -483 146 159	102	2	22	0.00	0.00		-375 -372 -399 -402
102	2	22	0.00	0.00		-402 -399 -426 -429	102	2	22	0.00	0.00		-429 -426 -453 -456
102	2	22	0.00	0.00		-456 -453 -480 -483	102	2	22	0.00	0.00		-483 -480 133 146
102	2	22	0.00	0.00		-372 -369 -396 -399	102	2	22	0.00	0.00		-399 -396 -423 -426
102	2	22	0.00	0.00		-426 -423 -450 -453	102	2	22	0.00	0.00		-453 -450 -477 -480
102	2	22	0.00	0.00		-480 -477 120 133	102	2	22	0.00	0.00		-369 -366 -393 -396
102	2	22	0.00	0.00		-396 -393 -420 -423	102	2	22	0.00	0.00		-423 -420 -447 -450
102	2	22	0.00	0.00		-450 -447 -474 -477	102	2	22	0.00	0.00		-477 -474 107 120
102	2	22	0.00	0.00		-366 -363 -390 -393	102	2	22	0.00	0.00		-393 -390 -417 -420
102	2	22	0.00	0.00		-420 -417 -444 -447	102	2	22	0.00	0.00		-447 -444 -471 -474
102	2	22	0.00	0.00		-474 -471 -498 107	102	2	22	0.00	0.00		-441 -438 -465 -468
102	2	22	0.00	0.00		-387 -384 -411 -414	102	2	22	0.00	0.00		-414 -411 -438 -441
103	1	22	0.00	0.00		-413 -410 -437 -440	103	1	22	0.00	0.00		-494 -491 179 -500
103	1	22	0.00	0.00		-440 -437 -464 -467	103	1	22	0.00	0.00		-467 -464 -491 -494
103	1	22	0.00	0.00		-386 -383 -410 -413	103	1	22	0.00	0.00		-464 -461 -488 -491
103	1	22	0.00	0.00		-491 -488 166 179	103	1	22	0.00	0.00		-380 -377 -404 -407
103	1	22	0.00	0.00		-407 -404 -431 -434	103	1	22	0.00	0.00		-434 -431 -458 -461
103	1	22	0.00	0.00		-461 -458 -485 -488	103	1	22	0.00	0.00		-488 -485 153 166
103	1	22	0.00	0.00		-377 -374 -401 -404	103	1	22	0.00	0.00		-404 -401 -428 -431
103	1	22	0.00	0.00		-431 -428 -455 -458	103	1	22	0.00	0.00		-458 -455 -482 -485
103	1	22	0.00	0.00		-383 -380 -407 -410	103	1	22	0.00	0.00		-410 -407 -434 -437
103	1	22	0.00	0.00		-437 -434 -461 -464	103	1	22	0.00	0.00		-256 -233 -383 -386
103	1	22	0.00	0.00		-233 -193 -380 -383	103	1	22	0.00	0.00		-193 -169 -377 -380
103	1	22	0.00	0.00		-169 -146 -374 -377	103	1	22	0.00	0.00		-146 -118 -371 -374
103	1	22	0.00	0.00		-118 -98 -368 -371	103	1	22	0.00	0.00		-98 -66 -365 -368
103	1	22	0.00	0.00		-66 -49 -362 -365	103	1	22	0.00	0.00		-395 -392 -419 -422
103	1	22	0.00	0.00		-422 -419 -446 -449	103	1	22	0.00	0.00		-449 -446 -473 -476
103	1	22	0.00	0.00		-476 -473 101 114	103	1	22	0.00	0.00		-365 -362 -389 -392
103	1	22	0.00	0.00		-392 -389 -416 -419	103	1	22	0.00	0.00		-419 -416 -443 -446
103	1	22	0.00	0.00		-446 -443 -470 -473	103	1	22	0.00	0.00		-473 -470 -497 101
103	1	22	0.00	0.00		-455 -452 -479 -482	103	1	22	0.00	0.00		-482 -479 127 140
103	1	22	0.00	0.00		-371 -368 -395 -398	103	1	22	0.00	0.00		-398 -395 -422 -425
103	1	22	0.00	0.00		-425 -422 -449 -452	103	1	22	0.00	0.00		-452 -449 -476 -479
103	1	22	0.00	0.00		-479 -476 114 127	103	1	22	0.00	0.00		-368 -365 -392 -395
103	1	22	0.00	0.00		-374 -371 -398 -401	103	1	22	0.00	0.00		-401 -398 -425 -428

103	1	22	0.00	0.00	-485	-482	140	153	103	1	22	0.00	0.00	-428	-425	-452	-455
104	1	22	0.00	0.00	-493	-490	178	191	104	1	22	0.00	0.00	-382	-379	-406	-409
104	1	22	0.00	0.00	-415	-412	-439	-442	104	1	22	0.00	0.00	-442	-439	-466	-469
104	1	22	0.00	0.00	-469	-466	-493	-496	104	1	22	0.00	0.00	-496	-493	191	-502
104	1	22	0.00	0.00	-385	-382	-409	-412	104	1	22	0.00	0.00	-412	-409	-436	-439
104	1	22	0.00	0.00	-439	-436	-463	-466	104	1	22	0.00	0.00	-466	-463	-490	-493
104	1	22	0.00	0.00	-457	-454	-481	-484	104	1	22	0.00	0.00	-484	-481	139	152
104	1	22	0.00	0.00	-373	-370	-397	-400	104	1	22	0.00	0.00	-400	-397	-424	-427
104	1	22	0.00	0.00	-427	-424	-451	-454	104	1	22	0.00	0.00	-454	-451	-478	-481
104	1	22	0.00	0.00	-481	-478	126	139	104	1	22	0.00	0.00	-370	-367	-394	-397
104	1	22	0.00	0.00	-397	-394	-421	-424	104	1	22	0.00	0.00	-424	-421	-448	-451
104	1	22	0.00	0.00	-451	-448	-475	-478	104	1	22	0.00	0.00	-478	-475	113	126
104	1	22	0.00	0.00	-367	-364	-391	-394	104	1	22	0.00	0.00	-394	-391	-418	-421
104	1	22	0.00	0.00	-421	-418	-445	-448	104	1	22	0.00	0.00	-448	-445	-472	-475
104	1	22	0.00	0.00	-475	-472	-499	113	104	1	22	0.00	0.00	-409	-406	-433	-436
104	1	22	0.00	0.00	-436	-433	-460	-463	104	1	22	0.00	0.00	-463	-460	-487	-490
104	1	22	0.00	0.00	-490	-487	165	178	104	1	22	0.00	0.00	-379	-376	-403	-406
104	1	22	0.00	0.00	-406	-403	-430	-433	104	1	22	0.00	0.00	-433	-430	-457	-460
104	1	22	0.00	0.00	-460	-457	-484	-487	104	1	22	0.00	0.00	-487	-484	152	165
104	1	22	0.00	0.00	-376	-373	-400	-403	104	1	22	0.00	0.00	-403	-400	-427	-430
104	1	22	0.00	0.00	-430	-427	-454	-457	104	1	22	0.00	0.00	-258	-237	-385	-388
104	1	22	0.00	0.00	-237	-199	-382	-385	104	1	22	0.00	0.00	-199	-171	-379	-382
104	1	22	0.00	0.00	-171	-148	-376	-379	104	1	22	0.00	0.00	-148	-124	-373	-376
104	1	22	0.00	0.00	-124	-100	-370	-373	104	1	22	0.00	0.00	-100	-68	-367	-370
104	1	22	0.00	0.00	-68	-51	-364	-367	104	1	22	0.00	0.00	-388	-385	-412	-415
401	3	11	0.00	0.00	-126	-118	-98	-101	401	3	11	0.00	0.00	-126	-101	-96	-119
401	3	11	0.00	0.00	-101	-98	-66	-74	401	3	11	0.00	0.00	-101	-74	-69	-96
401	3	11	0.00	0.00	-74	-66	-49	-44	401	3	11	0.00	0.00	-74	-44	-36	-69
401	3	11	0.00	0.00	-36	-44	-20	-4	401	3	11	0.00	0.00	-44	-49	-26	-20
401	3	11	0.00	0.00	-20	-26	-3	-4	401	3	11	0.00	0.00	-37	-84	-72	-33
401	3	11	0.00	0.00	-37	-33	-7	-8	401	3	11	0.00	0.00	-33	-72	-61	-30
401	3	11	0.00	0.00	-33	-30	-6	-7	401	3	11	0.00	0.00	-59	-69	-36	-29
401	3	11	0.00	0.00	-59	-29	-30	-61	401	3	11	0.00	0.00	-29	-36	-4	-5
401	3	11	0.00	0.00	-29	-5	-6	-30	401	3	11	0.00	0.00	-92	-109	-107	-90
401	3	11	0.00	0.00	-92	-90	-61	-72	401	3	11	0.00	0.00	-69	-59	-88	-96
401	3	11	0.00	0.00	-59	-61	-90	-88	401	3	11	0.00	0.00	-88	-90	-107	-96
401	3	11	0.00	0.00	-107	-109	-130	-128	401	3	11	0.00	0.00	-107	-128	-119	-96
401	3	11	0.00	0.00	-130	-109	-111	-120	401	3	11	0.00	0.00	-109	-92	-94	-111
401	3	11	0.00	0.00	-120	-111	-94	-84	401	3	11	0.00	0.00	-92	-72	-84	-94
401	3	11	0.00	0.00	-192	-209	-184	-172	401	3	11	0.00	0.00	-192	-172	-169	-193
401	3	11	0.00	0.00	-172	-184	-144	-149	401	3	11	0.00	0.00	-172	-149	-146	-169
401	3	11	0.00	0.00	-149	-144	-113	-117	401	3	11	0.00	0.00	-149	-117	-118	-146
401	3	11	0.00	0.00	-80	-42	-35	-83	401	3	11	0.00	0.00	-80	-83	-117	-113
401	3	11	0.00	0.00	-26	-49	-56	-35	401	3	11	0.00	0.00	-49	-66	-64	-56
401	3	11	0.00	0.00	-35	-56	-64	-83	401	3	11	0.00	0.00	-66	-98	-83	-64
401	3	11	0.00	0.00	-98	-118	-117	-83	401	3	11	0.00	0.00	-35	-42	-1	-2
401	3	11	0.00	0.00	-35	-2	-3	-26	401	3	11	0.00	0.00	-195	-217	-223	-188
401	3	11	0.00	0.00	-195	-188	-157	-159	401	3	11	0.00	0.00	-188	-223	-221	-186
401	3	11	0.00	0.00	-188	-186	-155	-157	401	3	11	0.00	0.00	-217	-246	-244	-223
401	3	11	0.00	0.00	-246	-279	-267	-244	401	3	11	0.00	0.00	-244	-267	-263	-223
401	3	11	0.00	0.00	-263	-252	-221	-223	401	3	11	0.00	0.00	-157	-155	-128	-130
401	3	11	0.00	0.00	-157	-130	-120	-159	401	3	11	0.00	0.00	-234	-240	-215	-203
401	3	11	0.00	0.00	-240	-242	-213	-215	401	3	11	0.00	0.00	-215	-213	-190	-203
401	3	11	0.00	0.00	-203	-196	-235	-234	401	3	11	0.00	0.00	-240	-234	-265	-273
401	3	11	0.00	0.00	-240	-273	-275	-242	401	3	11	0.00	0.00	-234	-235	-257	-265
401	3	11	0.00	0.00	-246	-217	-213	-242	401	3	11	0.00	0.00	-246	-242	-275	-279
401	3	11	0.00	0.00	-217	-195	-190	-213	401	3	11	0.00	0.00	-115	-138	-136	-120
401	3	11	0.00	0.00	-138	-163	-161	-136	401	3	11	0.00	0.00	-136	-161	-159	-120
401	3	11	0.00	0.00	-159	-161	-180	-195	401	3	11	0.00	0.00	-161	-163	-182	-180
401	3	11	0.00	0.00	-180	-182	-190	-195	401	3	11	0.00	0.00	-147	-142	-134	-121
401	3	11	0.00	0.00	-142	-140	-132	-134	401	3	11	0.00	0.00	-121	-134	-132	-115
401	3	11	0.00	0.00	-140	-138	-115	-132	401	3	11	0.00	0.00	-178	-167	-164	-170
401	3	11	0.00	0.00	-167	-140	-142	-164	401	3	11	0.00	0.00	-164	-142	-147	-170
401	3	11	0.00	0.00	-170	-196	-203	-178	401	3	11	0.00	0.00	-167	-178	-182	-163
401	3	11	0.00	0.00	-167	-163	-138	-140	401	3	11	0.00	0.00	-178	-203	-190	-182
401	3	11	0.00	0.00	-194	-205	-207	-201	401	3	11	0.00	0.00	-205	-227	-231	-207
401	3	11	0.00	0.00	-207	-231	-229	-201	401	3	11	0.00	0.00	-186	-221	-227	-205
401	3	11	0.00	0.00	-186	-205	-194	-176	401	3	11	0.00	0.00	-176	-153	-155	-186
401	3	11	0.00	0.00	-261	-259	-229	-231	401	3	11	0.00	0.00	-261	-231	-227	-254
401	3	11	0.00	0.00	-227	-221	-252	-254	401	3	11	0.00	0.00	-229	-259	-256	-233
401	3	11	0.00	0.00	-229	-233	-193	-201	401	3	11	0.00	0.00	-169	-146	-151	-174
401	3	11	0.00	0.00	-169	-174	-201	-193	401	3	11	0.00	0.00	-174	-151	-153	-176
401	3	11	0.00	0.00	-174	-176	-194	-201	401	3	11	0.00	0.00	-126	-151	-146	-118
401	3	11	0.00	0.00	-153	-151	-126	-119	401	3	11	0.00	0.00	-153	-119	-128	-155
401	3	11	0.00	0.00	-322	-308	-337	-350	401	3	11	0.00	0.00	-308	-306	-335	-337
401	3	11	0.00	0.00	-350	-337	-335	-351	401	3	11	0.00	0.00	-306	-312	-351	-335
401	3	11	0.00	0.00	-322	-304	-302	-308	401	3	11	0.00	0.00	-304	-285	-281	-302
401	3	11	0.00	0.00	-308	-302	-281	-279	401	3	11	0.00	0.00	-285	-267	-279	-281
401	3	11	0.00	0.00	-279	-275	-306	-308	401	3	11	0.00	0.00	-275	-273	-312	-306
401	3	11	0.00	0.00	-285	-300	-263	-267	401	3	11	0.00	0.00	-285	-304	-310	-300
401	3	11	0.00	0.00	-304	-322	-333	-310	401	3	11	0.00	0.00	-310	-333	-331	-300
401	3	11	0.00	0.00	-333	-322	-350	-349	401	3	11	0.00	0.00	-333	-349	-348	-331

401	3	11	0.00	0.00	-273	-265	-283	-312	401	3	11	0.00	0.00	-265	-257	-287	-283
401	3	11	0.00	0.00	-283	-287	-323	-312	401	3	11	0.00	0.00	-323	-352	-351	-312
401	3	11	0.00	0.00	-296	-329	-321	-292	401	3	11	0.00	0.00	-296	-292	-254	-252
401	3	11	0.00	0.00	-329	-347	-346	-321	401	3	11	0.00	0.00	-300	-331	-329	-296
401	3	11	0.00	0.00	-300	-296	-252	-263	401	3	11	0.00	0.00	-331	-348	-347	-329
401	3	11	0.00	0.00	-294	-256	-259	-290	401	3	11	0.00	0.00	-294	-290	-318	-327
401	3	11	0.00	0.00	-261	-254	-292	-288	401	3	11	0.00	0.00	-261	-288	-290	-259
401	3	11	0.00	0.00	-288	-292	-321	-316	401	3	11	0.00	0.00	-288	-316	-318	-290
401	3	11	0.00	0.00	-327	-318	-341	-345	401	3	11	0.00	0.00	-318	-316	-339	-341
401	3	11	0.00	0.00	-345	-341	-339	-346	401	3	11	0.00	0.00	-316	-321	-346	-339
401	3	11	0.00	0.00	-320	-327	-345	-344	401	3	11	0.00	0.00	-320	-344	-343	-314
401	3	11	0.00	0.00	-277	-320	-314	-269	401	3	11	0.00	0.00	-277	-271	-298	-320
401	3	11	0.00	0.00	-271	-256	-294	-298	401	3	11	0.00	0.00	-298	-294	-327	-320
401	3	11	0.00	0.00	-271	-277	-248	-238	401	3	11	0.00	0.00	-271	-238	-233	-256
401	3	11	0.00	0.00	-233	-238	-211	-193	401	3	11	0.00	0.00	-238	-248	-219	-211
401	3	11	0.00	0.00	-211	-219	-192	-193	401	3	11	0.00	0.00	-192	-219	-225	-209
401	3	11	0.00	0.00	-219	-248	-250	-225	401	3	11	0.00	0.00	-209	-225	-250	-269
401	3	11	0.00	0.00	-248	-277	-269	-250	401	3	11	0.00	0.00	-84	-77	-105	-120
401	3	11	0.00	0.00	-77	-76	-103	-105	401	3	11	0.00	0.00	-120	-105	-103	-115
401	3	11	0.00	0.00	-76	-82	-115	-103	401	3	11	0.00	0.00	-77	-84	-37	-52
401	3	11	0.00	0.00	-77	-52	-54	-76	401	3	11	0.00	0.00	-54	-46	-82	-76
401	3	11	0.00	0.00	-46	-54	-24	-9	401	3	11	0.00	0.00	-54	-52	-22	-24
401	3	11	0.00	0.00	-9	-24	-22	-8	401	3	11	0.00	0.00	-52	-37	-8	-22
401	3	11	0.00	0.00	-46	-48	-63	-82	401	3	11	0.00	0.00	-48	-50	-67	-63
401	3	11	0.00	0.00	-63	-67	-99	-82	401	3	11	0.00	0.00	-99	-121	-115	-82
401	3	11	0.00	0.00	-10	-38	-28	-9	401	3	11	0.00	0.00	-38	-50	-48	-28
401	3	11	0.00	0.00	-28	-48	-46	-9	401	3	11	0.00	0.00	-274	-266	-236	-241
401	3	11	0.00	0.00	-274	-241	-243	-276	401	3	11	0.00	0.00	-266	-257	-235	-236
401	3	11	0.00	0.00	-204	-236	-235	-196	401	3	11	0.00	0.00	-191	-214	-216	-204
401	3	11	0.00	0.00	-214	-243	-241	-216	401	3	11	0.00	0.00	-216	-241	-236	-204
401	3	11	0.00	0.00	-218	-214	-191	-197	401	3	11	0.00	0.00	-243	-214	-218	-247
401	3	11	0.00	0.00	-243	-247	-280	-276	401	3	11	0.00	0.00	-166	-183	-179	-168
401	3	11	0.00	0.00	-166	-168	-141	-139	401	3	11	0.00	0.00	-183	-191	-204	-179
401	3	11	0.00	0.00	-147	-143	-165	-170	401	3	11	0.00	0.00	-143	-141	-168	-165
401	3	11	0.00	0.00	-165	-168	-179	-170	401	3	11	0.00	0.00	-179	-204	-196	-170
401	3	11	0.00	0.00	-139	-141	-133	-116	401	3	11	0.00	0.00	-141	-143	-135	-133
401	3	11	0.00	0.00	-116	-133	-135	-121	401	3	11	0.00	0.00	-143	-147	-121	-135
401	3	11	0.00	0.00	-191	-183	-181	-197	401	3	11	0.00	0.00	-183	-166	-162	-181
401	3	11	0.00	0.00	-181	-162	-160	-197	401	3	11	0.00	0.00	-160	-162	-137	-122
401	3	11	0.00	0.00	-162	-166	-139	-137	401	3	11	0.00	0.00	-137	-139	-116	-122
401	3	11	0.00	0.00	-197	-160	-158	-189	401	3	11	0.00	0.00	-197	-189	-224	-218
401	3	11	0.00	0.00	-189	-158	-156	-187	401	3	11	0.00	0.00	-189	-187	-222	-224
401	3	11	0.00	0.00	-264	-268	-245	-224	401	3	11	0.00	0.00	-268	-280	-247	-245
401	3	11	0.00	0.00	-245	-247	-218	-224	401	3	11	0.00	0.00	-224	-222	-253	-264
401	3	11	0.00	0.00	-158	-160	-122	-131	401	3	11	0.00	0.00	-158	-131	-129	-156
401	3	11	0.00	0.00	-177	-154	-152	-175	401	3	11	0.00	0.00	-177	-175	-202	-198
401	3	11	0.00	0.00	-175	-152	-148	-171	401	3	11	0.00	0.00	-175	-171	-199	-202
401	3	11	0.00	0.00	-187	-177	-198	-206	401	3	11	0.00	0.00	-187	-206	-228	-222
401	3	11	0.00	0.00	-230	-232	-208	-202	401	3	11	0.00	0.00	-232	-228	-206	-208
401	3	11	0.00	0.00	-208	-206	-198	-202	401	3	11	0.00	0.00	-187	-156	-154	-177
401	3	11	0.00	0.00	-262	-255	-228	-232	401	3	11	0.00	0.00	-262	-232	-230	-260
401	3	11	0.00	0.00	-255	-253	-222	-228	401	3	11	0.00	0.00	-230	-202	-199	-237
401	3	11	0.00	0.00	-230	-237	-258	-260	401	3	11	0.00	0.00	-154	-156	-129	-123
401	3	11	0.00	0.00	-154	-123	-127	-152	401	3	11	0.00	0.00	-127	-124	-148	-152
401	3	11	0.00	0.00	-325	-317	-340	-358	401	3	11	0.00	0.00	-317	-319	-342	-340
401	3	11	0.00	0.00	-358	-340	-342	-359	401	3	11	0.00	0.00	-319	-328	-359	-342
401	3	11	0.00	0.00	-295	-328	-319	-291	401	3	11	0.00	0.00	-295	-291	-260	-258
401	3	11	0.00	0.00	-317	-325	-293	-289	401	3	11	0.00	0.00	-317	-289	-291	-319
401	3	11	0.00	0.00	-289	-293	-255	-262	401	3	11	0.00	0.00	-289	-262	-260	-291
401	3	11	0.00	0.00	-297	-330	-332	-301	401	3	11	0.00	0.00	-297	-301	-264	-253
401	3	11	0.00	0.00	-330	-357	-356	-332	401	3	11	0.00	0.00	-297	-253	-255	-293
401	3	11	0.00	0.00	-297	-293	-325	-330	401	3	11	0.00	0.00	-325	-358	-357	-330
401	3	11	0.00	0.00	-332	-334	-311	-301	401	3	11	0.00	0.00	-334	-324	-305	-311
401	3	11	0.00	0.00	-311	-305	-286	-301	401	3	11	0.00	0.00	-286	-268	-264	-301
401	3	11	0.00	0.00	-334	-332	-356	-355	401	3	11	0.00	0.00	-334	-355	-354	-324
401	3	11	0.00	0.00	-268	-286	-282	-280	401	3	11	0.00	0.00	-286	-305	-303	-282
401	3	11	0.00	0.00	-280	-282	-303	-309	401	3	11	0.00	0.00	-305	-324	-309	-303
401	3	11	0.00	0.00	-309	-307	-276	-280	401	3	11	0.00	0.00	-307	-313	-274	-276
401	3	11	0.00	0.00	-313	-307	-336	-353	401	3	11	0.00	0.00	-307	-309	-338	-336
401	3	11	0.00	0.00	-353	-336	-338	-354	401	3	11	0.00	0.00	-309	-324	-354	-338
401	3	11	0.00	0.00	-323	-287	-284	-313	401	3	11	0.00	0.00	-287	-257	-266	-284
401	3	11	0.00	0.00	-284	-266	-274	-313	401	3	11	0.00	0.00	-313	-353	-352	-323
401	3	11	0.00	0.00	-328	-295	-299	-326	401	3	11	0.00	0.00	-295	-258	-272	-299
401	3	11	0.00	0.00	-299	-272	-278	-326	401	3	11	0.00	0.00	-278	-270	-315	-326
401	3	11	0.00	0.00	-326	-315	-361	-360	401	3	11	0.00	0.00	-326	-360	-359	-328
401	3	11	0.00	0.00	-200	-220	-212	-199	401	3	11	0.00	0.00	-220	-249	-239	-212
401	3	11	0.00	0.00	-212	-239	-237	-199	401	3	11	0.00	0.00	-239	-249	-278	-272
401	3	11	0.00	0.00	-239	-272	-258	-237	401	3	11	0.00	0.00	-278	-249	-251	-270
401	3	11	0.00	0.00	-249	-220	-226	-251	401	3	11	0.00	0.00	-270	-251	-226	-210
401	3	11	0.00	0.00	-220	-200	-210	-226	401	3	11	0.00	0.00	-99	-87	-116	-121
401	3	11	0.00	0.00	-99	-67	-71	-87	401	3	11	0.00	0.00	-67	-50	-58	-71
401	3	11	0.00	0.00	-87	-71	-58	-47	401	3	11	0.00	0.00	-50	-38	-47	-58

401	3	11	0.00	0.00	-38	-10	-11	-47	401	3	11	0.00	0.00	-55	-79	-87	-47
401	3	11	0.00	0.00	-78	-79	-55	-53	401	3	11	0.00	0.00	-78	-53	-39	-85
401	3	11	0.00	0.00	-39	-53	-23	-12	401	3	11	0.00	0.00	-53	-55	-25	-23
401	3	11	0.00	0.00	-12	-23	-25	-11	401	3	11	0.00	0.00	-55	-47	-11	-25
401	3	11	0.00	0.00	-87	-79	-104	-116	401	3	11	0.00	0.00	-79	-78	-106	-104
401	3	11	0.00	0.00	-116	-104	-106	-122	401	3	11	0.00	0.00	-78	-85	-122	-106
401	3	11	0.00	0.00	-39	-12	-13	-34	401	3	11	0.00	0.00	-39	-34	-73	-85
401	3	11	0.00	0.00	-34	-13	-14	-31	401	3	11	0.00	0.00	-34	-31	-62	-73
401	3	11	0.00	0.00	-15	-16	-40	-32	401	3	11	0.00	0.00	-15	-32	-31	-14
401	3	11	0.00	0.00	-32	-40	-70	-60	401	3	11	0.00	0.00	-32	-60	-62	-31
401	3	11	0.00	0.00	-129	-131	-110	-108	401	3	11	0.00	0.00	-129	-108	-97	-123
401	3	11	0.00	0.00	-108	-91	-89	-97	401	3	11	0.00	0.00	-91	-62	-60	-89
401	3	11	0.00	0.00	-89	-60	-70	-97	401	3	11	0.00	0.00	-91	-108	-110	-93
401	3	11	0.00	0.00	-91	-93	-73	-62	401	3	11	0.00	0.00	-73	-93	-95	-85
401	3	11	0.00	0.00	-93	-110	-112	-95	401	3	11	0.00	0.00	-85	-95	-112	-122
401	3	11	0.00	0.00	-110	-131	-122	-112	401	3	11	0.00	0.00	-17	-27	-21	-16
401	3	11	0.00	0.00	-27	-51	-45	-21	401	3	11	0.00	0.00	-21	-45	-40	-16
401	3	11	0.00	0.00	-45	-51	-68	-75	401	3	11	0.00	0.00	-45	-75	-70	-40
401	3	11	0.00	0.00	-127	-123	-97	-102	401	3	11	0.00	0.00	-127	-102	-100	-124
401	3	11	0.00	0.00	-102	-97	-70	-75	401	3	11	0.00	0.00	-102	-75	-68	-100
401	3	11	0.00	0.00	-41	-27	-17	-18	401	3	11	0.00	0.00	-41	-18	-19	-43
401	3	11	0.00	0.00	-100	-68	-65	-86	401	3	11	0.00	0.00	-68	-51	-57	-65
401	3	11	0.00	0.00	-86	-65	-57	-41	401	3	11	0.00	0.00	-51	-27	-41	-57
401	3	11	0.00	0.00	-86	-125	-124	-100	401	3	11	0.00	0.00	-86	-41	-43	-81
401	3	11	0.00	0.00	-86	-81	-114	-125	401	3	11	0.00	0.00	-200	-199	-171	-173
401	3	11	0.00	0.00	-200	-173	-185	-210	401	3	11	0.00	0.00	-173	-171	-148	-150
401	3	11	0.00	0.00	-173	-150	-145	-185	401	3	11	0.00	0.00	-150	-148	-124	-125
401	3	11	0.00	0.00	-150	-125	-114	-145									

Carichi

Condizioni di carico elementari

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sicurezza = Contributo alla sicurezza
  F = a favore
  S = a sfavore
  A = ambigua
Variabilità = Tipo di variabilità
  B = di base
  I = indipendente
  A = ambigua

CCE	Comm.	Mx	My	Mz	Jpx	Jpy	Jpz	Tipo CCE	Sicurezza	Variabilità
1	Permanenti strutturali	1.00	1.00	0.00	0.00	0.00	1.00	21 D.M. 08 Permanenti strutturali PONTI	S	--
2	Permanenti non strutturali	1.00	1.00	0.00	0.00	0.00	1.00	2 D.M. 08 Permanenti non strutturali	S	--
3	Variabili folla	1.00	1.00	0.00	0.00	0.00	1.00	20 D.M. 08 Variabile Folla schema 5	S	B
4	Variabili temperatura	1.00	1.00	0.00	0.00	0.00	1.00	13 D.M. 08 Variabili Variazioni termiche	S	B
5	Variabile piena T=200	1.00	1.00	0.00	0.00	0.00	1.00	22 Azione di piena	S	--
6	Variabile piena T=500	1.00	1.00	0.00	0.00	0.00	1.00	22 Azione di piena	S	--

Elenco carichi nodi
Condizione di carico n. 5: Variabile piena T=200
Carichi concentrati

Simbologia

Nodo = Numero del nodo
Px = Componente X della forza applicata
Py = Componente Y della forza applicata
Pz = Componente Z della forza applicata
Mx = Momento intorno all'asse X
My = Momento intorno all'asse Y
Mz = Momento intorno all'asse Z

Nodo	Px <daN>	Py <daN>	Pz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>	Nodo	Px <daN>	Py <daN>	Pz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>
-496	0.00	370.00	0.00	0.00	0.00	0.00	-495	0.00	740.00	0.00	0.00	0.00	0.00
-494	0.00	370.00	0.00	0.00	0.00	0.00	-469	0.00	2930.00	0.00	0.00	0.00	0.00
-468	0.00	5860.00	0.00	0.00	0.00	0.00	-467	0.00	2930.00	0.00	0.00	0.00	0.00
-442	0.00	5860.00	0.00	0.00	0.00	0.00	-441	0.00	11720.00	0.00	0.00	0.00	0.00

-440	0.00	5860.00	0.00	0.00	0.00	0.00	-415	0.00	8790.00	0.00	0.00	0.00	0.00
-414	0.00	17580.00	0.00	0.00	0.00	0.00	-413	0.00	8790.00	0.00	0.00	0.00	0.00
-388	0.00	11720.00	0.00	0.00	0.00	0.00	-387	0.00	23430.00	0.00	0.00	0.00	0.00
-386	0.00	11720.00	0.00	0.00	0.00	0.00	-258	0.00	6960.00	0.00	0.00	0.00	0.00
-257	0.00	13920.00	0.00	0.00	0.00	0.00	-256	0.00	6960.00	0.00	0.00	0.00	0.00

Elenco carichi nodi
Condizione di carico n. 6: Variabile piena T=500
Carichi concentrati

Nodo	Px <daN>	Py <daN>	Pz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>	Nodo	Px <daN>	Py <daN>	Pz <daN>	Mx <daNm>	My <daNm>	Mz <daNm>
-495	0.00	435.00	0.00	0.00	0.00	0.00	-494	0.00	435.00	0.00	0.00	0.00	0.00
-468	0.00	3470.00	0.00	0.00	0.00	0.00	-467	0.00	3470.00	0.00	0.00	0.00	0.00
-441	0.00	6940.00	0.00	0.00	0.00	0.00	-440	0.00	6940.00	0.00	0.00	0.00	0.00
-414	0.00	10410.00	0.00	0.00	0.00	0.00	-413	0.00	10410.00	0.00	0.00	0.00	0.00
-387	0.00	13880.00	0.00	0.00	0.00	0.00	-386	0.00	13880.00	0.00	0.00	0.00	0.00
-257	0.00	8240.00	0.00	0.00	0.00	0.00	-256	0.00	8240.00	0.00	0.00	0.00	0.00

Elenco carichi aste
Condizione di carico n. 1: Permanenti strutturali
Carichi distribuiti

Simbologia

Asta = Numero dell'asta
N1 = Nodo iniziale
N2 = Nodo finale
E = Elemento provenienza del carico
  S = Solaio
  T = Tamponatura
NE = Numero elemento di provenienza del carico
T = Tipo di carico
  QA = Primo carico accidentale
  QA2 = Secondo carico accidentale
  QA3 = Terzo carico accidentale
  QPS = Carico permanente strutturale
  QPN = Carico permanente non strutturale
  PP = Peso proprio
  M = Manuale
DC = Direzione del carico
  XG,YG,ZG = secondo gli assi globali
  XL,YL,ZL = secondo gli assi locali
Xi = Distanza iniziale
Qi = Carico iniziale
Xf = Distanza finale
Qf = Carico finale

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
101	101	102	S	--	PP	ZG	0.00	76.35	1.17	76.35	101	102	103	S	--	PP	ZG	0.00	76.35	1.17	76.35
101	103	104	S	--	PP	ZG	0.00	76.35	1.17	76.35	101	104	105	S	--	PP	ZG	0.00	76.35	1.17	76.35
101	105	106	S	--	PP	ZG	0.00	76.35	1.17	76.35	101	106	107	S	--	PP	ZG	0.00	76.35	1.17	76.35
101	107	108	S	--	PP	ZG	0.00	76.35	1.17	76.35	101	108	109	S	--	PP	ZG	0.00	76.35	1.17	76.35
101	109	110	S	--	PP	ZG	0.00	76.35	1.17	76.35	101	110	111	S	--	PP	ZG	0.00	76.35	1.17	76.35
101	111	112	S	--	PP	ZG	0.00	76.35	1.17	76.35	101	112	113	S	--	PP	ZG	0.00	76.35	1.17	76.35
102	114	115	S	--	PP	ZG	0.00	18.80	1.17	18.80	102	115	116	S	--	PP	ZG	0.00	18.80	1.17	18.80
102	116	117	S	--	PP	ZG	0.00	18.80	1.17	18.80	102	117	118	S	--	PP	ZG	0.00	18.80	1.17	18.80
102	118	119	S	--	PP	ZG	0.00	18.80	1.17	18.80	102	119	120	S	--	PP	ZG	0.00	18.80	1.17	18.80
102	120	121	S	--	PP	ZG	0.00	18.80	1.17	18.80	102	121	122	S	--	PP	ZG	0.00	18.80	1.17	18.80
102	122	123	S	--	PP	ZG	0.00	18.80	1.17	18.80	102	123	124	S	--	PP	ZG	0.00	18.80	1.17	18.80
102	124	125	S	--	PP	ZG	0.00	18.80	1.17	18.80	102	125	126	S	--	PP	ZG	0.00	18.80	1.17	18.80
103	127	128	S	--	PP	ZG	0.00	18.80	1.17	18.80	103	128	129	S	--	PP	ZG	0.00	18.80	1.17	18.80
103	129	130	S	--	PP	ZG	0.00	18.80	1.17	18.80	103	130	131	S	--	PP	ZG	0.00	18.80	1.17	18.80
103	131	132	S	--	PP	ZG	0.00	18.80	1.17	18.80	103	132	133	S	--	PP	ZG	0.00	18.80	1.17	18.80
103	133	134	S	--	PP	ZG	0.00	18.80	1.17	18.80	103	134	135	S	--	PP	ZG	0.00	18.80	1.17	18.80
103	135	136	S	--	PP	ZG	0.00	18.80	1.17	18.80	103	136	137	S	--	PP	ZG	0.00	18.80	1.17	18.80
103	137	138	S	--	PP	ZG	0.00	18.80	1.17	18.80	103	138	139	S	--	PP	ZG	0.00	18.80	1.17	18.80
104	140	141	S	--	PP	ZG	0.00	103.12	1.17	103.12	104	141	142	S	--	PP	ZG	0.00	103.12	1.17	103.12
104	142	143	S	--	PP	ZG	0.00	103.12	1.17	103.12	104	143	144	S	--	PP	ZG	0.00	103.12	1.17	103.12
104	144	145	S	--	PP	ZG	0.00	103.12	1.17	103.12	104	145	146	S	--	PP	ZG	0.00	103.12	1.17	103.12
104	146	147	S	--	PP	ZG	0.00	103.12	1.17	103.12	104	147	148	S	--	PP	ZG	0.00	103.12	1.17	103.12
104	148	149	S	--	PP	ZG	0.00	103.12	1.17	103.12	104	149	150	S	--	PP	ZG	0.00	103.12	1.17	103.12
104	150	151	S	--	PP	ZG	0.00	103.12	1.17	103.12	104	151	152	S	--	PP	ZG	0.00	103.12	1.17	103.12
105	153	154	S	--	PP	ZG	0.00	18.80	1.17	18.80	105	154	155	S	--	PP	ZG	0.00	18.80	1.17	18.80
105	155	156	S	--	PP	ZG	0.00	18.80	1.17	18.80	105	156	157	S	--	PP	ZG	0.00	18.80	1.17	18.80
105	157	158	S	--	PP	ZG	0.00	18.80	1.17	18.80	105	158	159	S	--	PP	ZG	0.00	18.80	1.17	18.80
105	159	160	S	--	PP	ZG	0.00	18.80	1.17	18.80	105	160	161	S	--	PP	ZG	0.00	18.80	1.17	18.80
105	161	162	S	--	PP	ZG	0.00	18.80	1.17	18.80	105	162	163	S	--	PP	ZG	0.00	18.80	1.17	18.80
105	163	164	S	--	PP	ZG	0.00	18.80	1.17	18.80	105	164	165	S	--	PP	ZG	0.00	18.80	1.17	18.80

106	166	167	S	--	PP	ZG	0.00	18.80	1.17	18.80	106	167	168	S	--	PP	ZG	0.00	18.80	1.17	18.80
106	168	169	S	--	PP	ZG	0.00	18.80	1.17	18.80	106	169	170	S	--	PP	ZG	0.00	18.80	1.17	18.80
106	170	171	S	--	PP	ZG	0.00	18.80	1.17	18.80	106	171	172	S	--	PP	ZG	0.00	18.80	1.17	18.80
106	172	173	S	--	PP	ZG	0.00	18.80	1.17	18.80	106	173	174	S	--	PP	ZG	0.00	18.80	1.17	18.80
106	174	175	S	--	PP	ZG	0.00	18.80	1.17	18.80	106	175	176	S	--	PP	ZG	0.00	18.80	1.17	18.80
106	176	177	S	--	PP	ZG	0.00	18.80	1.17	18.80	106	177	178	S	--	PP	ZG	0.00	18.80	1.17	18.80
107	179	180	S	--	PP	ZG	0.00	76.35	1.17	76.35	107	180	181	S	--	PP	ZG	0.00	76.35	1.17	76.35
107	181	182	S	--	PP	ZG	0.00	76.35	1.17	76.35	107	182	183	S	--	PP	ZG	0.00	76.35	1.17	76.35
107	183	184	S	--	PP	ZG	0.00	76.35	1.17	76.35	107	184	185	S	--	PP	ZG	0.00	76.35	1.17	76.35
107	185	186	S	--	PP	ZG	0.00	76.35	1.17	76.35	107	186	187	S	--	PP	ZG	0.00	76.35	1.17	76.35
107	187	188	S	--	PP	ZG	0.00	76.35	1.17	76.35	107	188	189	S	--	PP	ZG	0.00	76.35	1.17	76.35
107	189	190	S	--	PP	ZG	0.00	76.35	1.17	76.35	107	190	191	S	--	PP	ZG	0.00	76.35	1.17	76.35
108	101	114	S	--	PP	ZG	0.00	18.80	0.79	18.80	108	114	127	S	--	PP	ZG	0.00	18.80	0.79	18.80
108	127	140	S	--	PP	ZG	0.00	18.80	0.79	18.80	108	140	153	S	--	PP	ZG	0.00	18.80	0.79	18.80
108	153	166	S	--	PP	ZG	0.00	18.80	0.79	18.80	108	166	179	S	--	PP	ZG	0.00	18.80	0.79	18.80
109	102	115	S	--	PP	ZG	0.00	18.80	0.79	18.80	109	115	128	S	--	PP	ZG	0.00	18.80	0.79	18.80
109	128	141	S	--	PP	ZG	0.00	18.80	0.79	18.80	109	141	154	S	--	PP	ZG	0.00	18.80	0.79	18.80
109	154	167	S	--	PP	ZG	0.00	18.80	0.79	18.80	109	167	180	S	--	PP	ZG	0.00	18.80	0.79	18.80
110	103	116	S	--	PP	ZG	0.00	18.80	0.79	18.80	110	116	129	S	--	PP	ZG	0.00	18.80	0.79	18.80
110	129	142	S	--	PP	ZG	0.00	18.80	0.79	18.80	110	142	155	S	--	PP	ZG	0.00	18.80	0.79	18.80
110	155	168	S	--	PP	ZG	0.00	18.80	0.79	18.80	110	168	181	S	--	PP	ZG	0.00	18.80	0.79	18.80
111	104	117	S	--	PP	ZG	0.00	18.80	0.79	18.80	111	117	130	S	--	PP	ZG	0.00	18.80	0.79	18.80
111	130	143	S	--	PP	ZG	0.00	18.80	0.79	18.80	111	143	156	S	--	PP	ZG	0.00	18.80	0.79	18.80
111	156	169	S	--	PP	ZG	0.00	18.80	0.79	18.80	111	169	182	S	--	PP	ZG	0.00	18.80	0.79	18.80
112	105	118	S	--	PP	ZG	0.00	18.80	0.79	18.80	112	118	131	S	--	PP	ZG	0.00	18.80	0.79	18.80
112	131	144	S	--	PP	ZG	0.00	18.80	0.79	18.80	112	144	157	S	--	PP	ZG	0.00	18.80	0.79	18.80
112	157	170	S	--	PP	ZG	0.00	18.80	0.79	18.80	112	170	183	S	--	PP	ZG	0.00	18.80	0.79	18.80
113	106	119	S	--	PP	ZG	0.00	18.80	0.79	18.80	113	119	132	S	--	PP	ZG	0.00	18.80	0.79	18.80
113	132	145	S	--	PP	ZG	0.00	18.80	0.79	18.80	113	145	158	S	--	PP	ZG	0.00	18.80	0.79	18.80
113	158	171	S	--	PP	ZG	0.00	18.80	0.79	18.80	113	171	184	S	--	PP	ZG	0.00	18.80	0.79	18.80
114	107	120	S	--	PP	ZG	0.00	18.80	0.79	18.80	114	120	133	S	--	PP	ZG	0.00	18.80	0.79	18.80
114	133	146	S	--	PP	ZG	0.00	18.80	0.79	18.80	114	146	159	S	--	PP	ZG	0.00	18.80	0.79	18.80
114	159	172	S	--	PP	ZG	0.00	18.80	0.79	18.80	114	172	185	S	--	PP	ZG	0.00	18.80	0.79	18.80
115	108	121	S	--	PP	ZG	0.00	18.80	0.79	18.80	115	121	134	S	--	PP	ZG	0.00	18.80	0.79	18.80
115	134	147	S	--	PP	ZG	0.00	18.80	0.79	18.80	115	147	160	S	--	PP	ZG	0.00	18.80	0.79	18.80
115	160	173	S	--	PP	ZG	0.00	18.80	0.79	18.80	115	173	186	S	--	PP	ZG	0.00	18.80	0.79	18.80
116	109	122	S	--	PP	ZG	0.00	18.80	0.79	18.80	116	122	135	S	--	PP	ZG	0.00	18.80	0.79	18.80
116	135	148	S	--	PP	ZG	0.00	18.80	0.79	18.80	116	148	161	S	--	PP	ZG	0.00	18.80	0.79	18.80
116	161	174	S	--	PP	ZG	0.00	18.80	0.79	18.80	116	174	187	S	--	PP	ZG	0.00	18.80	0.79	18.80
117	110	123	S	--	PP	ZG	0.00	18.80	0.79	18.80	117	123	136	S	--	PP	ZG	0.00	18.80	0.79	18.80
117	136	149	S	--	PP	ZG	0.00	18.80	0.79	18.80	117	149	162	S	--	PP	ZG	0.00	18.80	0.79	18.80
117	162	175	S	--	PP	ZG	0.00	18.80	0.79	18.80	117	175	188	S	--	PP	ZG	0.00	18.80	0.79	18.80
118	111	124	S	--	PP	ZG	0.00	18.80	0.79	18.80	118	124	137	S	--	PP	ZG	0.00	18.80	0.79	18.80
118	137	150	S	--	PP	ZG	0.00	18.80	0.79	18.80	118	150	163	S	--	PP	ZG	0.00	18.80	0.79	18.80
118	163	176	S	--	PP	ZG	0.00	18.80	0.79	18.80	118	176	189	S	--	PP	ZG	0.00	18.80	0.79	18.80
119	112	125	S	--	PP	ZG	0.00	18.80	0.79	18.80	119	125	138	S	--	PP	ZG	0.00	18.80	0.79	18.80
119	138	151	S	--	PP	ZG	0.00	18.80	0.79	18.80	119	151	164	S	--	PP	ZG	0.00	18.80	0.79	18.80
119	164	177	S	--	PP	ZG	0.00	18.80	0.79	18.80	119	177	190	S	--	PP	ZG	0.00	18.80	0.79	18.80
120	113	126	S	--	PP	ZG	0.00	18.80	0.79	18.80	120	126	139	S	--	PP	ZG	0.00	18.80	0.79	18.80
120	139	152	S	--	PP	ZG	0.00	18.80	0.79	18.80	120	152	165	S	--	PP	ZG	0.00	18.80	0.79	18.80
120	165	178	S	--	PP	ZG	0.00	18.80	0.79	18.80	120	178	191	S	--	PP	ZG	0.00	18.80	0.79	18.80

Elenco carichi aste

Condizione di carico n. 2: Permanenti non strutturali

Carichi distribuiti

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
101	101	102	S	--	M	ZG	0.00	35.60	1.17	35.60	101	101	102	S	--	M	ZG	0.00	50.00	1.17	50.00
101	102	103	S	--	M	ZG	0.00	35.60	1.17	35.60	101	102	103	S	--	M	ZG	0.00	50.00	1.17	50.00
101	103	104	S	--	M	ZG	0.00	35.60	1.17	35.60	101	103	104	S	--	M	ZG	0.00	50.00	1.17	50.00
101	104	105	S	--	M	ZG	0.00	35.60	1.17	35.60	101	104	105	S	--	M	ZG	0.00	50.00	1.17	50.00
101	105	106	S	--	M	ZG	0.00	35.60	1.17	35.60	101	105	106	S	--	M	ZG	0.00	50.00	1.17	50.00
101	106	107	S	--	M	ZG	0.00	35.60	1.17	35.60	101	106	107	S	--	M	ZG	0.00	50.00	1.17	50.00
101	107	108	S	--	M	ZG	0.00	35.60	1.17	35.60	101	107	108	S	--	M	ZG	0.00	50.00	1.17	50.00
101	108	109	S	--	M	ZG	0.00	35.60	1.17	35.60	101	108	109	S	--	M	ZG	0.00	50.00	1.17	50.00
101	109	110	S	--	M	ZG	0.00	35.60	1.17	35.60	101	109	110	S	--	M	ZG	0.00	50.00	1.17	50.00
101	110	111	S	--	M	ZG	0.00	35.60	1.17	35.60	101	110	111	S	--	M	ZG	0.00	50.00	1.17	50.00
101	111	112	S	--	M	ZG	0.00	35.60	1.17	35.60	101	111	112	S	--	M	ZG	0.00	50.00	1.17	50.00
101	112	113	S	--	M	ZG	0.00	35.60	1.17	35.60	101	112	113	S	--	M	ZG	0.00	50.00	1.17	50.00
102	114	115	S	--	M	ZG	0.00	71.10	1.17	71.10	102	115	116	S	--	M	ZG	0.00	71.10	1.17	71.10
102	116	117	S	--	M	ZG	0.00	71.10	1.17	71.10	102	117	118	S	--	M	ZG	0.00	71.10	1.17	71.10
102	118	119	S	--	M	ZG	0.00	71.10	1.17	71.10	102	119	120	S	--	M	ZG	0.00	71.10	1.17	71.10
102	120	121	S	--	M	ZG	0.00	71.10	1.17	71.10	102	121	122	S	--	M	ZG	0.00	71.10	1.17	71.10
102	122	123	S	--	M	ZG	0.00	71.10	1.17	71.10	102	123	124	S	--	M	ZG	0.00	71.10	1.17	71.10
102	124	125	S	--	M	ZG	0.00	71.10	1.17	71.10	102	125	126	S	--	M	ZG	0.00	71.10	1.17	71.10
103	127	128	S	--	M	ZG	0.00	71.10	1.17	71.10	103	128	129	S	--	M	ZG	0.00	71.10	1.17	71.10
103	129	130	S	--	M	ZG	0.00	71.10	1.17	71.10	103	130	131	S	--	M	ZG	0.00	71.10	1.17	71.10
103	131	132	S	--	M	ZG	0.00	71.10	1.17	71.10	103	132	133	S	--	M	ZG	0.00	71.10	1.17	71.10
103	133	134	S	--	M	ZG	0.00	71.10	1.17	71.10	103	134	135	S	--	M	ZG	0.00	71.10	1.17	71.10
103	135	136	S	--	M	ZG	0.00	71.10	1.17	71.10	103	136	137	S	--	M	ZG	0.00	71.10	1.17	71.10

103	137	138	S	--	M	ZG	0.00	71.10	1.17	71.10	103	138	139	S	--	M	ZG	0.00	71.10	1.17	71.10
104	140	141	S	--	M	ZG	0.00	71.10	1.17	71.10	104	141	142	S	--	M	ZG	0.00	71.10	1.17	71.10
104	142	143	S	--	M	ZG	0.00	71.10	1.17	71.10	104	143	144	S	--	M	ZG	0.00	71.10	1.17	71.10
104	144	145	S	--	M	ZG	0.00	71.10	1.17	71.10	104	145	146	S	--	M	ZG	0.00	71.10	1.17	71.10
104	146	147	S	--	M	ZG	0.00	71.10	1.17	71.10	104	147	148	S	--	M	ZG	0.00	71.10	1.17	71.10
104	148	149	S	--	M	ZG	0.00	71.10	1.17	71.10	104	149	150	S	--	M	ZG	0.00	71.10	1.17	71.10
104	150	151	S	--	M	ZG	0.00	71.10	1.17	71.10	104	151	152	S	--	M	ZG	0.00	71.10	1.17	71.10
105	153	154	S	--	M	ZG	0.00	71.10	1.17	71.10	105	154	155	S	--	M	ZG	0.00	71.10	1.17	71.10
105	155	156	S	--	M	ZG	0.00	71.10	1.17	71.10	105	156	157	S	--	M	ZG	0.00	71.10	1.17	71.10
105	157	158	S	--	M	ZG	0.00	71.10	1.17	71.10	105	158	159	S	--	M	ZG	0.00	71.10	1.17	71.10
105	159	160	S	--	M	ZG	0.00	71.10	1.17	71.10	105	160	161	S	--	M	ZG	0.00	71.10	1.17	71.10
105	161	162	S	--	M	ZG	0.00	71.10	1.17	71.10	105	162	163	S	--	M	ZG	0.00	71.10	1.17	71.10
105	163	164	S	--	M	ZG	0.00	71.10	1.17	71.10	105	164	165	S	--	M	ZG	0.00	71.10	1.17	71.10
106	166	167	S	--	M	ZG	0.00	71.10	1.17	71.10	106	167	168	S	--	M	ZG	0.00	71.10	1.17	71.10
106	168	169	S	--	M	ZG	0.00	71.10	1.17	71.10	106	169	170	S	--	M	ZG	0.00	71.10	1.17	71.10
106	170	171	S	--	M	ZG	0.00	71.10	1.17	71.10	106	171	172	S	--	M	ZG	0.00	71.10	1.17	71.10
106	172	173	S	--	M	ZG	0.00	71.10	1.17	71.10	106	173	174	S	--	M	ZG	0.00	71.10	1.17	71.10
106	174	175	S	--	M	ZG	0.00	71.10	1.17	71.10	106	175	176	S	--	M	ZG	0.00	71.10	1.17	71.10
106	176	177	S	--	M	ZG	0.00	71.10	1.17	71.10	106	177	178	S	--	M	ZG	0.00	71.10	1.17	71.10
107	179	180	S	--	M	ZG	0.00	35.60	1.17	35.60	107	179	180	S	--	M	ZG	0.00	50.00	1.17	50.00
107	180	181	S	--	M	ZG	0.00	35.60	1.17	35.60	107	180	181	S	--	M	ZG	0.00	50.00	1.17	50.00
107	181	182	S	--	M	ZG	0.00	35.60	1.17	35.60	107	181	182	S	--	M	ZG	0.00	50.00	1.17	50.00
107	182	183	S	--	M	ZG	0.00	35.60	1.17	35.60	107	182	183	S	--	M	ZG	0.00	50.00	1.17	50.00
107	183	184	S	--	M	ZG	0.00	35.60	1.17	35.60	107	183	184	S	--	M	ZG	0.00	50.00	1.17	50.00
107	184	185	S	--	M	ZG	0.00	35.60	1.17	35.60	107	184	185	S	--	M	ZG	0.00	50.00	1.17	50.00
107	185	186	S	--	M	ZG	0.00	35.60	1.17	35.60	107	185	186	S	--	M	ZG	0.00	50.00	1.17	50.00
107	186	187	S	--	M	ZG	0.00	35.60	1.17	35.60	107	186	187	S	--	M	ZG	0.00	50.00	1.17	50.00
107	187	188	S	--	M	ZG	0.00	35.60	1.17	35.60	107	187	188	S	--	M	ZG	0.00	50.00	1.17	50.00
107	188	189	S	--	M	ZG	0.00	35.60	1.17	35.60	107	188	189	S	--	M	ZG	0.00	50.00	1.17	50.00
107	189	190	S	--	M	ZG	0.00	35.60	1.17	35.60	107	189	190	S	--	M	ZG	0.00	50.00	1.17	50.00
107	190	191	S	--	M	ZG	0.00	35.60	1.17	35.60	107	190	191	S	--	M	ZG	0.00	50.00	1.17	50.00

Elenco carichi aste
Condizione di carico n. 3: Variabili folla
Carichi distribuiti

Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>	Asta	N1	N2	E	NE	T	DC	Xi <m>	Qi <daN/m>	Xf <m>	Qf <daN/m>
101	101	102	S	--	M	ZG	0.00	395.00	1.17	395.00	101	102	103	S	--	M	ZG	0.00	395.00	1.17	395.00
101	103	104	S	--	M	ZG	0.00	395.00	1.17	395.00	101	104	105	S	--	M	ZG	0.00	395.00	1.17	395.00
101	105	106	S	--	M	ZG	0.00	395.00	1.17	395.00	101	106	107	S	--	M	ZG	0.00	395.00	1.17	395.00
101	107	108	S	--	M	ZG	0.00	395.00	1.17	395.00	101	108	109	S	--	M	ZG	0.00	395.00	1.17	395.00
101	109	110	S	--	M	ZG	0.00	395.00	1.17	395.00	101	110	111	S	--	M	ZG	0.00	395.00	1.17	395.00
101	111	112	S	--	M	ZG	0.00	395.00	1.17	395.00	101	112	113	S	--	M	ZG	0.00	395.00	1.17	395.00
102	114	115	S	--	M	ZG	0.00	790.00	1.17	790.00	102	115	116	S	--	M	ZG	0.00	790.00	1.17	790.00
102	116	117	S	--	M	ZG	0.00	790.00	1.17	790.00	102	117	118	S	--	M	ZG	0.00	790.00	1.17	790.00
102	118	119	S	--	M	ZG	0.00	790.00	1.17	790.00	102	119	120	S	--	M	ZG	0.00	790.00	1.17	790.00
102	120	121	S	--	M	ZG	0.00	790.00	1.17	790.00	102	121	122	S	--	M	ZG	0.00	790.00	1.17	790.00
102	122	123	S	--	M	ZG	0.00	790.00	1.17	790.00	102	123	124	S	--	M	ZG	0.00	790.00	1.17	790.00
102	124	125	S	--	M	ZG	0.00	790.00	1.17	790.00	102	125	126	S	--	M	ZG	0.00	790.00	1.17	790.00
103	127	128	S	--	M	ZG	0.00	790.00	1.17	790.00	103	128	129	S	--	M	ZG	0.00	790.00	1.17	790.00
103	129	130	S	--	M	ZG	0.00	790.00	1.17	790.00	103	130	131	S	--	M	ZG	0.00	790.00	1.17	790.00
103	131	132	S	--	M	ZG	0.00	790.00	1.17	790.00	103	132	133	S	--	M	ZG	0.00	790.00	1.17	790.00
103	133	134	S	--	M	ZG	0.00	790.00	1.17	790.00	103	134	135	S	--	M	ZG	0.00	790.00	1.17	790.00
103	135	136	S	--	M	ZG	0.00	790.00	1.17	790.00	103	136	137	S	--	M	ZG	0.00	790.00	1.17	790.00
103	137	138	S	--	M	ZG	0.00	790.00	1.17	790.00	103	138	139	S	--	M	ZG	0.00	790.00	1.17	790.00
104	140	141	S	--	M	ZG	0.00	790.00	1.17	790.00	104	141	142	S	--	M	ZG	0.00	790.00	1.17	790.00
104	142	143	S	--	M	ZG	0.00	790.00	1.17	790.00	104	143	144	S	--	M	ZG	0.00	790.00	1.17	790.00
104	144	145	S	--	M	ZG	0.00	790.00	1.17	790.00	104	145	146	S	--	M	ZG	0.00	790.00	1.17	790.00
104	146	147	S	--	M	ZG	0.00	790.00	1.17	790.00	104	147	148	S	--	M	ZG	0.00	790.00	1.17	790.00
104	148	149	S	--	M	ZG	0.00	790.00	1.17	790.00	104	149	150	S	--	M	ZG	0.00	790.00	1.17	790.00
104	150	151	S	--	M	ZG	0.00	790.00	1.17	790.00	104	151	152	S	--	M	ZG	0.00	790.00	1.17	790.00
105	153	154	S	--	M	ZG	0.00	790.00	1.17	790.00	105	154	155	S	--	M	ZG	0.00	790.00	1.17	790.00
105	155	156	S	--	M	ZG	0.00	790.00	1.17	790.00	105	156	157	S	--	M	ZG	0.00	790.00	1.17	790.00
105	157	158	S	--	M	ZG	0.00	790.00	1.17	790.00	105	158	159	S	--	M	ZG	0.00	790.00	1.17	790.00
105	159	160	S	--	M	ZG	0.00	790.00	1.17	790.00	105	160	161	S	--	M	ZG	0.00	790.00	1.17	790.00
105	161	162	S	--	M	ZG	0.00	790.00	1.17	790.00	105	162	163	S	--	M	ZG	0.00	790.00	1.17	790.00
105	163	164	S	--	M	ZG	0.00	790.00	1.17	790.00	105	164	165	S	--	M	ZG	0.00	790.00	1.17	790.00
106	166	167	S	--	M	ZG	0.00	790.00	1.17	790.00	106	167	168	S	--	M	ZG	0.00	790.00	1.17	790.00
106	168	169	S	--	M	ZG	0.00	790.00	1.17	790.00	106	169	170	S	--	M	ZG	0.00	790.00	1.17	790.00
106	170	171	S	--	M	ZG	0.00	790.00	1.17	790.00	106	171	172	S	--	M	ZG	0.00	790.00	1.17	790.00
106	172	173	S	--	M	ZG	0.00	790.00	1.17	790.00	106	173	174	S	--	M	ZG	0.00	790.00	1.17	790.00
106	174	175	S	--	M	ZG	0.00	790.00	1.17	790.00	106	175	176	S	--	M	ZG	0.00	790.00	1.17	790.00
106	176	177	S	--	M	ZG	0.00	790.00	1.17	790.00	106	177	178	S	--	M	ZG	0.00	790.00	1.17	790.00
107	179	180	S	--	M	ZG	0.00	395.00	1.17	395.00	107	180	181	S	--	M	ZG	0.00	395.00	1.17	395.00
107	181	182	S	--	M	ZG	0.00	395.00	1.17	395.00	107	182	183	S	--	M	ZG	0.00	395.00	1.17	395.00
107	183	184	S	--	M	ZG	0.00	395.00	1.17	395.00	107	184	185	S	--	M	ZG	0.00	395.00	1.17	395.00
107	185	186	S	--	M	ZG	0.00	395.00	1.17	395.00	107	186	187	S	--	M	ZG	0.00	395.00	1.17	395.00
107	187	188	S	--	M	ZG	0.00	395.00	1.17	395.00	107	188	189	S	--	M	ZG	0.00	395.00	1.17	395.00
107	189	190	S	--	M	ZG	0.00	395.00	1.17	395.00	107	190	191	S	--	M	ZG	0.00	395.00	1.17	395.00

Elenco carichi aste
Condizione di carico n. 4: Variabili temperatura
Carichi distribuiti

Simbologia

Asta = Numero dell'asta
N1 = Nodo iniziale
N2 = Nodo finale
DT = Incremento di temperatura
Gy = Gradiente termico in dir. Y
Gz = Gradiente termico in dir. Z

Asta	N1	N2	DT <°C>	Gy <°C/m>	Gz <°C/m>	Asta	N1	N2	DT <°C>	Gy <°C/m>	Gz <°C/m>	Asta	N1	N2	DT <°C>	Gy <°C/m>	Gz <°C/m>
101	101	102	30.00			101	102	103	30.00			101	103	104	30.00		
101	104	105	30.00			101	105	106	30.00			101	106	107	30.00		
101	107	108	30.00			101	108	109	30.00			101	109	110	30.00		
101	110	111	30.00			101	111	112	30.00			101	112	113	30.00		
102	114	115	30.00			102	115	116	30.00			102	116	117	30.00		
102	117	118	30.00			102	118	119	30.00			102	119	120	30.00		
102	120	121	30.00			102	121	122	30.00			102	122	123	30.00		
102	123	124	30.00			102	124	125	30.00			102	125	126	30.00		
103	127	128	30.00			103	128	129	30.00			103	129	130	30.00		
103	130	131	30.00			103	131	132	30.00			103	132	133	30.00		
103	133	134	30.00			103	134	135	30.00			103	135	136	30.00		
103	136	137	30.00			103	137	138	30.00			103	138	139	30.00		
104	140	141	30.00			104	141	142	30.00			104	142	143	30.00		
104	143	144	30.00			104	144	145	30.00			104	145	146	30.00		
104	146	147	30.00			104	147	148	30.00			104	148	149	30.00		
104	149	150	30.00			104	150	151	30.00			104	151	152	30.00		
105	153	154	30.00			105	154	155	30.00			105	155	156	30.00		
105	156	157	30.00			105	157	158	30.00			105	158	159	30.00		
105	159	160	30.00			105	160	161	30.00			105	161	162	30.00		
105	162	163	30.00			105	163	164	30.00			105	164	165	30.00		
106	166	167	30.00			106	167	168	30.00			106	168	169	30.00		
106	169	170	30.00			106	170	171	30.00			106	171	172	30.00		
106	172	173	30.00			106	173	174	30.00			106	174	175	30.00		
106	175	176	30.00			106	176	177	30.00			106	177	178	30.00		
107	179	180	30.00			107	180	181	30.00			107	181	182	30.00		
107	182	183	30.00			107	183	184	30.00			107	184	185	30.00		
107	185	186	30.00			107	186	187	30.00			107	187	188	30.00		
107	188	189	30.00			107	189	190	30.00			107	190	191	30.00		
108	101	114	30.00			108	114	127	30.00			108	127	140	30.00		
108	140	153	30.00			108	153	166	30.00			108	166	179	30.00		
109	102	115	30.00			109	115	128	30.00			109	128	141	30.00		
109	141	154	30.00			109	154	167	30.00			109	167	180	30.00		
110	103	116	30.00			110	116	129	30.00			110	129	142	30.00		
110	142	155	30.00			110	155	168	30.00			110	168	181	30.00		
111	104	117	30.00			111	117	130	30.00			111	130	143	30.00		
111	143	156	30.00			111	156	169	30.00			111	169	182	30.00		
112	105	118	30.00			112	118	131	30.00			112	131	144	30.00		
112	144	157	30.00			112	157	170	30.00			112	170	183	30.00		
113	106	119	30.00			113	119	132	30.00			113	132	145	30.00		
113	145	158	30.00			113	158	171	30.00			113	171	184	30.00		
114	107	120	30.00			114	120	133	30.00			114	133	146	30.00		
114	146	159	30.00			114	159	172	30.00			114	172	185	30.00		
115	108	121	30.00			115	121	134	30.00			115	134	147	30.00		
115	147	160	30.00			115	160	173	30.00			115	173	186	30.00		
116	109	122	30.00			116	122	135	30.00			116	135	148	30.00		
116	148	161	30.00			116	161	174	30.00			116	174	187	30.00		
117	110	123	30.00			117	123	136	30.00			117	136	149	30.00		
117	149	162	30.00			117	162	175	30.00			117	175	188	30.00		
118	111	124	30.00			118	124	137	30.00			118	137	150	30.00		
118	150	163	30.00			118	163	176	30.00			118	176	189	30.00		
119	112	125	30.00			119	125	138	30.00			119	138	151	30.00		
119	151	164	30.00			119	164	177	30.00			119	177	190	30.00		
120	113	126	30.00			120	126	139	30.00			120	139	152	30.00		
120	152	165	30.00			120	165	178	30.00			120	178	191	30.00		

Elenco carichi elementi bidimensionali
Condizione di carico n. 1: Permanenti strutturali
Carichi uniformi

Simbologia

Bid. = Numero del muro/elemento bidimensionale
N1 = Nodo1
N2 = Nodo2

N3 = Nodo3
N4 = Nodo4
T = Tipo di carico
PP = Peso proprio
M = Manuale
DC = Direzione del carico
G = secondo gli assi globali
L = secondo gli assi locali
Qx = Carico in dir. X
Qy = Carico in dir. Y
Qz = Carico in dir. Z

Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
102	-196	-170	-378	-381	PP	G	0.00	0.00	2500.00
102	-235	-196	-381	-384	PP	G	0.00	0.00	2500.00
102	-257	-235	-384	-387	PP	G	0.00	0.00	2500.00
102	-170	-147	-375	-378	PP	G	0.00	0.00	2500.00
102	-147	-121	-372	-375	PP	G	0.00	0.00	2500.00
102	-121	-99	-369	-372	PP	G	0.00	0.00	2500.00
102	-99	-67	-366	-369	PP	G	0.00	0.00	2500.00
102	-67	-50	-363	-366	PP	G	0.00	0.00	2500.00
102	-468	-465	-492	-495	PP	G	0.00	0.00	2500.00
102	-495	-492	185	-501	PP	G	0.00	0.00	2500.00
102	-384	-381	-408	-411	PP	G	0.00	0.00	2500.00
102	-411	-408	-435	-438	PP	G	0.00	0.00	2500.00
102	-438	-435	-462	-465	PP	G	0.00	0.00	2500.00
102	-465	-462	-489	-492	PP	G	0.00	0.00	2500.00
102	-492	-489	172	185	PP	G	0.00	0.00	2500.00
102	-381	-378	-405	-408	PP	G	0.00	0.00	2500.00
102	-408	-405	-432	-435	PP	G	0.00	0.00	2500.00
102	-435	-432	-459	-462	PP	G	0.00	0.00	2500.00
102	-462	-459	-486	-489	PP	G	0.00	0.00	2500.00
102	-489	-486	159	172	PP	G	0.00	0.00	2500.00
102	-378	-375	-402	-405	PP	G	0.00	0.00	2500.00
102	-405	-402	-429	-432	PP	G	0.00	0.00	2500.00
102	-432	-429	-456	-459	PP	G	0.00	0.00	2500.00
102	-459	-456	-483	-486	PP	G	0.00	0.00	2500.00
102	-486	-483	146	159	PP	G	0.00	0.00	2500.00
102	-375	-372	-399	-402	PP	G	0.00	0.00	2500.00
102	-402	-399	-426	-429	PP	G	0.00	0.00	2500.00
102	-429	-426	-453	-456	PP	G	0.00	0.00	2500.00
102	-456	-453	-480	-483	PP	G	0.00	0.00	2500.00
102	-483	-480	133	146	PP	G	0.00	0.00	2500.00
102	-372	-369	-396	-399	PP	G	0.00	0.00	2500.00
102	-399	-396	-423	-426	PP	G	0.00	0.00	2500.00
102	-426	-423	-450	-453	PP	G	0.00	0.00	2500.00
102	-453	-450	-477	-480	PP	G	0.00	0.00	2500.00
102	-480	-477	120	133	PP	G	0.00	0.00	2500.00
102	-369	-366	-393	-396	PP	G	0.00	0.00	2500.00
102	-396	-393	-420	-423	PP	G	0.00	0.00	2500.00
102	-423	-420	-447	-450	PP	G	0.00	0.00	2500.00
102	-450	-447	-474	-477	PP	G	0.00	0.00	2500.00
102	-477	-474	107	120	PP	G	0.00	0.00	2500.00
102	-366	-363	-390	-393	PP	G	0.00	0.00	2500.00
102	-393	-390	-417	-420	PP	G	0.00	0.00	2500.00
102	-420	-417	-444	-447	PP	G	0.00	0.00	2500.00
102	-447	-444	-471	-474	PP	G	0.00	0.00	2500.00
102	-474	-471	-498	107	PP	G	0.00	0.00	2500.00
102	-441	-438	-465	-468	PP	G	0.00	0.00	2500.00
102	-387	-384	-411	-414	PP	G	0.00	0.00	2500.00
102	-414	-411	-438	-441	PP	G	0.00	0.00	2500.00
103	-413	-410	-437	-440	PP	G	0.00	0.00	1750.00
103	-494	-491	179	-500	PP	G	0.00	0.00	1750.00
103	-440	-437	-464	-467	PP	G	0.00	0.00	1750.00
103	-467	-464	-491	-494	PP	G	0.00	0.00	1750.00
103	-386	-383	-410	-413	PP	G	0.00	0.00	1750.00
103	-464	-461	-488	-491	PP	G	0.00	0.00	1750.00
103	-491	-488	166	179	PP	G	0.00	0.00	1750.00
103	-380	-377	-404	-407	PP	G	0.00	0.00	1750.00
103	-407	-404	-431	-434	PP	G	0.00	0.00	1750.00
103	-434	-431	-458	-461	PP	G	0.00	0.00	1750.00
103	-461	-458	-485	-488	PP	G	0.00	0.00	1750.00
103	-488	-485	153	166	PP	G	0.00	0.00	1750.00
103	-377	-374	-401	-404	PP	G	0.00	0.00	1750.00
103	-404	-401	-428	-431	PP	G	0.00	0.00	1750.00
103	-431	-428	-455	-458	PP	G	0.00	0.00	1750.00
103	-458	-455	-482	-485	PP	G	0.00	0.00	1750.00
103	-383	-380	-407	-410	PP	G	0.00	0.00	1750.00
103	-410	-407	-434	-437	PP	G	0.00	0.00	1750.00
103	-437	-434	-461	-464	PP	G	0.00	0.00	1750.00
103	-256	-233	-383	-386	PP	G	0.00	0.00	1750.00

103	-233	-193	-380	-383	PP	G	0.00	0.00	1750.00
103	-193	-169	-377	-380	PP	G	0.00	0.00	1750.00
103	-169	-146	-374	-377	PP	G	0.00	0.00	1750.00
103	-146	-118	-371	-374	PP	G	0.00	0.00	1750.00
103	-118	-98	-368	-371	PP	G	0.00	0.00	1750.00
103	-98	-66	-365	-368	PP	G	0.00	0.00	1750.00
103	-66	-49	-362	-365	PP	G	0.00	0.00	1750.00
103	-395	-392	-419	-422	PP	G	0.00	0.00	1750.00
103	-422	-419	-446	-449	PP	G	0.00	0.00	1750.00
103	-449	-446	-473	-476	PP	G	0.00	0.00	1750.00
103	-476	-473	101	114	PP	G	0.00	0.00	1750.00
103	-365	-362	-389	-392	PP	G	0.00	0.00	1750.00
103	-392	-389	-416	-419	PP	G	0.00	0.00	1750.00
103	-419	-416	-443	-446	PP	G	0.00	0.00	1750.00
103	-446	-443	-470	-473	PP	G	0.00	0.00	1750.00
103	-473	-470	-497	101	PP	G	0.00	0.00	1750.00
103	-455	-452	-479	-482	PP	G	0.00	0.00	1750.00
103	-482	-479	127	140	PP	G	0.00	0.00	1750.00
103	-371	-368	-395	-398	PP	G	0.00	0.00	1750.00
103	-398	-395	-422	-425	PP	G	0.00	0.00	1750.00
103	-425	-422	-449	-452	PP	G	0.00	0.00	1750.00
103	-452	-449	-476	-479	PP	G	0.00	0.00	1750.00
103	-479	-476	114	127	PP	G	0.00	0.00	1750.00
103	-368	-365	-392	-395	PP	G	0.00	0.00	1750.00
103	-374	-371	-398	-401	PP	G	0.00	0.00	1750.00
103	-401	-398	-425	-428	PP	G	0.00	0.00	1750.00
103	-485	-482	140	153	PP	G	0.00	0.00	1750.00
103	-428	-425	-452	-455	PP	G	0.00	0.00	1750.00
104	-493	-490	178	191	PP	G	0.00	0.00	1750.00
104	-382	-379	-406	-409	PP	G	0.00	0.00	1750.00
104	-415	-412	-439	-442	PP	G	0.00	0.00	1750.00
104	-442	-439	-466	-469	PP	G	0.00	0.00	1750.00
104	-469	-466	-493	-496	PP	G	0.00	0.00	1750.00
104	-496	-493	191	-502	PP	G	0.00	0.00	1750.00
104	-385	-382	-409	-412	PP	G	0.00	0.00	1750.00
104	-412	-409	-436	-439	PP	G	0.00	0.00	1750.00
104	-439	-436	-463	-466	PP	G	0.00	0.00	1750.00
104	-466	-463	-490	-493	PP	G	0.00	0.00	1750.00
104	-457	-454	-481	-484	PP	G	0.00	0.00	1750.00
104	-484	-481	139	152	PP	G	0.00	0.00	1750.00
104	-373	-370	-397	-400	PP	G	0.00	0.00	1750.00
104	-400	-397	-424	-427	PP	G	0.00	0.00	1750.00
104	-427	-424	-451	-454	PP	G	0.00	0.00	1750.00
104	-454	-451	-478	-481	PP	G	0.00	0.00	1750.00
104	-481	-478	126	139	PP	G	0.00	0.00	1750.00
104	-370	-367	-394	-397	PP	G	0.00	0.00	1750.00
104	-397	-394	-421	-424	PP	G	0.00	0.00	1750.00
104	-424	-421	-448	-451	PP	G	0.00	0.00	1750.00
104	-451	-448	-475	-478	PP	G	0.00	0.00	1750.00
104	-478	-475	113	126	PP	G	0.00	0.00	1750.00
104	-367	-364	-391	-394	PP	G	0.00	0.00	1750.00
104	-394	-391	-418	-421	PP	G	0.00	0.00	1750.00
104	-421	-418	-445	-448	PP	G	0.00	0.00	1750.00
104	-448	-445	-472	-475	PP	G	0.00	0.00	1750.00
104	-475	-472	-499	113	PP	G	0.00	0.00	1750.00
104	-409	-406	-433	-436	PP	G	0.00	0.00	1750.00
104	-436	-433	-460	-463	PP	G	0.00	0.00	1750.00
104	-463	-460	-487	-490	PP	G	0.00	0.00	1750.00
104	-490	-487	165	178	PP	G	0.00	0.00	1750.00
104	-379	-376	-403	-406	PP	G	0.00	0.00	1750.00
104	-406	-403	-430	-433	PP	G	0.00	0.00	1750.00
104	-433	-430	-457	-460	PP	G	0.00	0.00	1750.00
104	-460	-457	-484	-487	PP	G	0.00	0.00	1750.00
104	-487	-484	152	165	PP	G	0.00	0.00	1750.00
104	-376	-373	-400	-403	PP	G	0.00	0.00	1750.00
104	-403	-400	-427	-430	PP	G	0.00	0.00	1750.00
104	-430	-427	-454	-457	PP	G	0.00	0.00	1750.00
104	-258	-237	-385	-388	PP	G	0.00	0.00	1750.00
104	-237	-199	-382	-385	PP	G	0.00	0.00	1750.00
104	-199	-171	-379	-382	PP	G	0.00	0.00	1750.00
104	-171	-148	-376	-379	PP	G	0.00	0.00	1750.00
104	-148	-124	-373	-376	PP	G	0.00	0.00	1750.00
104	-124	-100	-370	-373	PP	G	0.00	0.00	1750.00
104	-100	-68	-367	-370	PP	G	0.00	0.00	1750.00
104	-68	-51	-364	-367	PP	G	0.00	0.00	1750.00
104	-388	-385	-412	-415	PP	G	0.00	0.00	1750.00
401	-126	-118	-98	-101	PP	G	0.00	0.00	2500.00
401	-126	-101	-96	-119	PP	G	0.00	0.00	2500.00
401	-101	-98	-66	-74	PP	G	0.00	0.00	2500.00
401	-101	-74	-69	-96	PP	G	0.00	0.00	2500.00
401	-74	-66	-49	-44	PP	G	0.00	0.00	2500.00
401	-74	-44	-36	-69	PP	G	0.00	0.00	2500.00

401	-36	-44	-20	-4	PP	G	0.00	0.00	2500.00
401	-44	-49	-26	-20	PP	G	0.00	0.00	2500.00
401	-20	-26	-3	-4	PP	G	0.00	0.00	2500.00
401	-37	-84	-72	-33	PP	G	0.00	0.00	2500.00
401	-37	-33	-7	-8	PP	G	0.00	0.00	2500.00
401	-33	-72	-61	-30	PP	G	0.00	0.00	2500.00
401	-33	-30	-6	-7	PP	G	0.00	0.00	2500.00
401	-59	-69	-36	-29	PP	G	0.00	0.00	2500.00
401	-59	-29	-30	-61	PP	G	0.00	0.00	2500.00
401	-29	-36	-4	-5	PP	G	0.00	0.00	2500.00
401	-29	-5	-6	-30	PP	G	0.00	0.00	2500.00
401	-92	-109	-107	-90	PP	G	0.00	0.00	2500.00
401	-92	-90	-61	-72	PP	G	0.00	0.00	2500.00
401	-69	-59	-88	-96	PP	G	0.00	0.00	2500.00
401	-59	-61	-90	-88	PP	G	0.00	0.00	2500.00
401	-88	-90	-107	-96	PP	G	0.00	0.00	2500.00
401	-107	-109	-130	-128	PP	G	0.00	0.00	2500.00
401	-107	-128	-119	-96	PP	G	0.00	0.00	2500.00
401	-130	-109	-111	-120	PP	G	0.00	0.00	2500.00
401	-109	-92	-94	-111	PP	G	0.00	0.00	2500.00
401	-120	-111	-94	-84	PP	G	0.00	0.00	2500.00
401	-92	-72	-84	-94	PP	G	0.00	0.00	2500.00
401	-192	-209	-184	-172	PP	G	0.00	0.00	2500.00
401	-192	-172	-169	-193	PP	G	0.00	0.00	2500.00
401	-172	-184	-144	-149	PP	G	0.00	0.00	2500.00
401	-172	-149	-146	-169	PP	G	0.00	0.00	2500.00
401	-149	-144	-113	-117	PP	G	0.00	0.00	2500.00
401	-149	-117	-118	-146	PP	G	0.00	0.00	2500.00
401	-80	-42	-35	-83	PP	G	0.00	0.00	2500.00
401	-80	-83	-117	-113	PP	G	0.00	0.00	2500.00
401	-26	-49	-56	-35	PP	G	0.00	0.00	2500.00
401	-49	-66	-64	-56	PP	G	0.00	0.00	2500.00
401	-35	-56	-64	-83	PP	G	0.00	0.00	2500.00
401	-66	-98	-83	-64	PP	G	0.00	0.00	2500.00
401	-98	-118	-117	-83	PP	G	0.00	0.00	2500.00
401	-35	-42	-1	-2	PP	G	0.00	0.00	2500.00
401	-35	-2	-3	-26	PP	G	0.00	0.00	2500.00
401	-195	-217	-223	-188	PP	G	0.00	0.00	2500.00
401	-195	-188	-157	-159	PP	G	0.00	0.00	2500.00
401	-188	-223	-221	-186	PP	G	0.00	0.00	2500.00
401	-188	-186	-155	-157	PP	G	0.00	0.00	2500.00
401	-217	-246	-244	-223	PP	G	0.00	0.00	2500.00
401	-246	-279	-267	-244	PP	G	0.00	0.00	2500.00
401	-244	-267	-263	-223	PP	G	0.00	0.00	2500.00
401	-263	-252	-221	-223	PP	G	0.00	0.00	2500.00
401	-157	-155	-128	-130	PP	G	0.00	0.00	2500.00
401	-157	-130	-120	-159	PP	G	0.00	0.00	2500.00
401	-234	-240	-215	-203	PP	G	0.00	0.00	2500.00
401	-240	-242	-213	-215	PP	G	0.00	0.00	2500.00
401	-215	-213	-190	-203	PP	G	0.00	0.00	2500.00
401	-203	-196	-235	-234	PP	G	0.00	0.00	2500.00
401	-240	-234	-265	-273	PP	G	0.00	0.00	2500.00
401	-240	-273	-275	-242	PP	G	0.00	0.00	2500.00
401	-234	-235	-257	-265	PP	G	0.00	0.00	2500.00
401	-246	-217	-213	-242	PP	G	0.00	0.00	2500.00
401	-246	-242	-275	-279	PP	G	0.00	0.00	2500.00
401	-217	-195	-190	-213	PP	G	0.00	0.00	2500.00
401	-115	-138	-136	-120	PP	G	0.00	0.00	2500.00
401	-138	-163	-161	-136	PP	G	0.00	0.00	2500.00
401	-136	-161	-159	-120	PP	G	0.00	0.00	2500.00
401	-159	-161	-180	-195	PP	G	0.00	0.00	2500.00
401	-161	-163	-182	-180	PP	G	0.00	0.00	2500.00
401	-180	-182	-190	-195	PP	G	0.00	0.00	2500.00
401	-147	-142	-134	-121	PP	G	0.00	0.00	2500.00
401	-142	-140	-132	-134	PP	G	0.00	0.00	2500.00
401	-121	-134	-132	-115	PP	G	0.00	0.00	2500.00
401	-140	-138	-115	-132	PP	G	0.00	0.00	2500.00
401	-178	-167	-164	-170	PP	G	0.00	0.00	2500.00
401	-167	-140	-142	-164	PP	G	0.00	0.00	2500.00
401	-164	-142	-147	-170	PP	G	0.00	0.00	2500.00
401	-170	-196	-203	-178	PP	G	0.00	0.00	2500.00
401	-167	-178	-182	-163	PP	G	0.00	0.00	2500.00
401	-167	-163	-138	-140	PP	G	0.00	0.00	2500.00
401	-178	-203	-190	-182	PP	G	0.00	0.00	2500.00
401	-194	-205	-207	-201	PP	G	0.00	0.00	2500.00
401	-205	-227	-231	-207	PP	G	0.00	0.00	2500.00
401	-207	-231	-229	-201	PP	G	0.00	0.00	2500.00
401	-186	-221	-227	-205	PP	G	0.00	0.00	2500.00
401	-186	-205	-194	-176	PP	G	0.00	0.00	2500.00
401	-176	-153	-155	-186	PP	G	0.00	0.00	2500.00
401	-261	-259	-229	-231	PP	G	0.00	0.00	2500.00
401	-261	-231	-227	-254	PP	G	0.00	0.00	2500.00

401	-227	-221	-252	-254	PP	G	0.00	0.00	2500.00
401	-229	-259	-256	-233	PP	G	0.00	0.00	2500.00
401	-229	-233	-193	-201	PP	G	0.00	0.00	2500.00
401	-169	-146	-151	-174	PP	G	0.00	0.00	2500.00
401	-169	-174	-201	-193	PP	G	0.00	0.00	2500.00
401	-174	-151	-153	-176	PP	G	0.00	0.00	2500.00
401	-174	-176	-194	-201	PP	G	0.00	0.00	2500.00
401	-126	-151	-146	-118	PP	G	0.00	0.00	2500.00
401	-153	-151	-126	-119	PP	G	0.00	0.00	2500.00
401	-153	-119	-128	-155	PP	G	0.00	0.00	2500.00
401	-322	-308	-337	-350	PP	G	0.00	0.00	2500.00
401	-308	-306	-335	-337	PP	G	0.00	0.00	2500.00
401	-350	-337	-335	-351	PP	G	0.00	0.00	2500.00
401	-306	-312	-351	-335	PP	G	0.00	0.00	2500.00
401	-322	-304	-302	-308	PP	G	0.00	0.00	2500.00
401	-304	-285	-281	-302	PP	G	0.00	0.00	2500.00
401	-308	-302	-281	-279	PP	G	0.00	0.00	2500.00
401	-285	-267	-279	-281	PP	G	0.00	0.00	2500.00
401	-279	-275	-306	-308	PP	G	0.00	0.00	2500.00
401	-275	-273	-312	-306	PP	G	0.00	0.00	2500.00
401	-285	-300	-263	-267	PP	G	0.00	0.00	2500.00
401	-285	-304	-310	-300	PP	G	0.00	0.00	2500.00
401	-304	-322	-333	-310	PP	G	0.00	0.00	2500.00
401	-310	-333	-331	-300	PP	G	0.00	0.00	2500.00
401	-333	-322	-350	-349	PP	G	0.00	0.00	2500.00
401	-333	-349	-348	-331	PP	G	0.00	0.00	2500.00
401	-273	-265	-283	-312	PP	G	0.00	0.00	2500.00
401	-265	-257	-287	-283	PP	G	0.00	0.00	2500.00
401	-283	-287	-323	-312	PP	G	0.00	0.00	2500.00
401	-323	-352	-351	-312	PP	G	0.00	0.00	2500.00
401	-296	-329	-321	-292	PP	G	0.00	0.00	2500.00
401	-296	-292	-254	-252	PP	G	0.00	0.00	2500.00
401	-329	-347	-346	-321	PP	G	0.00	0.00	2500.00
401	-300	-331	-329	-296	PP	G	0.00	0.00	2500.00
401	-300	-296	-252	-263	PP	G	0.00	0.00	2500.00
401	-331	-348	-347	-329	PP	G	0.00	0.00	2500.00
401	-294	-256	-259	-290	PP	G	0.00	0.00	2500.00
401	-294	-290	-318	-327	PP	G	0.00	0.00	2500.00
401	-261	-254	-292	-288	PP	G	0.00	0.00	2500.00
401	-261	-288	-290	-259	PP	G	0.00	0.00	2500.00
401	-288	-292	-321	-316	PP	G	0.00	0.00	2500.00
401	-288	-316	-318	-290	PP	G	0.00	0.00	2500.00
401	-327	-318	-341	-345	PP	G	0.00	0.00	2500.00
401	-318	-316	-339	-341	PP	G	0.00	0.00	2500.00
401	-345	-341	-339	-346	PP	G	0.00	0.00	2500.00
401	-316	-321	-346	-339	PP	G	0.00	0.00	2500.00
401	-320	-327	-345	-344	PP	G	0.00	0.00	2500.00
401	-320	-344	-343	-314	PP	G	0.00	0.00	2500.00
401	-277	-320	-314	-269	PP	G	0.00	0.00	2500.00
401	-277	-271	-298	-320	PP	G	0.00	0.00	2500.00
401	-271	-256	-294	-298	PP	G	0.00	0.00	2500.00
401	-298	-294	-327	-320	PP	G	0.00	0.00	2500.00
401	-271	-277	-248	-238	PP	G	0.00	0.00	2500.00
401	-271	-238	-233	-256	PP	G	0.00	0.00	2500.00
401	-233	-238	-211	-193	PP	G	0.00	0.00	2500.00
401	-238	-248	-219	-211	PP	G	0.00	0.00	2500.00
401	-211	-219	-192	-193	PP	G	0.00	0.00	2500.00
401	-192	-219	-225	-209	PP	G	0.00	0.00	2500.00
401	-219	-248	-250	-225	PP	G	0.00	0.00	2500.00
401	-209	-225	-250	-269	PP	G	0.00	0.00	2500.00
401	-248	-277	-269	-250	PP	G	0.00	0.00	2500.00
401	-84	-77	-105	-120	PP	G	0.00	0.00	2500.00
401	-77	-76	-103	-105	PP	G	0.00	0.00	2500.00
401	-120	-105	-103	-115	PP	G	0.00	0.00	2500.00
401	-76	-82	-115	-103	PP	G	0.00	0.00	2500.00
401	-77	-84	-37	-52	PP	G	0.00	0.00	2500.00
401	-77	-52	-54	-76	PP	G	0.00	0.00	2500.00
401	-54	-46	-82	-76	PP	G	0.00	0.00	2500.00
401	-46	-54	-24	-9	PP	G	0.00	0.00	2500.00
401	-54	-52	-22	-24	PP	G	0.00	0.00	2500.00
401	-9	-24	-22	-8	PP	G	0.00	0.00	2500.00
401	-52	-37	-8	-22	PP	G	0.00	0.00	2500.00
401	-46	-48	-63	-82	PP	G	0.00	0.00	2500.00
401	-48	-50	-67	-63	PP	G	0.00	0.00	2500.00
401	-63	-67	-99	-82	PP	G	0.00	0.00	2500.00
401	-99	-121	-115	-82	PP	G	0.00	0.00	2500.00
401	-10	-38	-28	-9	PP	G	0.00	0.00	2500.00
401	-38	-50	-48	-28	PP	G	0.00	0.00	2500.00
401	-28	-48	-46	-9	PP	G	0.00	0.00	2500.00
401	-274	-266	-236	-241	PP	G	0.00	0.00	2500.00
401	-274	-241	-243	-276	PP	G	0.00	0.00	2500.00
401	-266	-257	-235	-236	PP	G	0.00	0.00	2500.00

401	-204	-236	-235	-196	PP	G	0.00	0.00	2500.00
401	-191	-214	-216	-204	PP	G	0.00	0.00	2500.00
401	-214	-243	-241	-216	PP	G	0.00	0.00	2500.00
401	-216	-241	-236	-204	PP	G	0.00	0.00	2500.00
401	-218	-214	-191	-197	PP	G	0.00	0.00	2500.00
401	-243	-214	-218	-247	PP	G	0.00	0.00	2500.00
401	-243	-247	-280	-276	PP	G	0.00	0.00	2500.00
401	-166	-183	-179	-168	PP	G	0.00	0.00	2500.00
401	-166	-168	-141	-139	PP	G	0.00	0.00	2500.00
401	-183	-191	-204	-179	PP	G	0.00	0.00	2500.00
401	-147	-143	-165	-170	PP	G	0.00	0.00	2500.00
401	-143	-141	-168	-165	PP	G	0.00	0.00	2500.00
401	-165	-168	-179	-170	PP	G	0.00	0.00	2500.00
401	-179	-204	-196	-170	PP	G	0.00	0.00	2500.00
401	-139	-141	-133	-116	PP	G	0.00	0.00	2500.00
401	-141	-143	-135	-133	PP	G	0.00	0.00	2500.00
401	-116	-133	-135	-121	PP	G	0.00	0.00	2500.00
401	-143	-147	-121	-135	PP	G	0.00	0.00	2500.00
401	-191	-183	-181	-197	PP	G	0.00	0.00	2500.00
401	-183	-166	-162	-181	PP	G	0.00	0.00	2500.00
401	-181	-162	-160	-197	PP	G	0.00	0.00	2500.00
401	-160	-162	-137	-122	PP	G	0.00	0.00	2500.00
401	-162	-166	-139	-137	PP	G	0.00	0.00	2500.00
401	-137	-139	-116	-122	PP	G	0.00	0.00	2500.00
401	-197	-160	-158	-189	PP	G	0.00	0.00	2500.00
401	-197	-189	-224	-218	PP	G	0.00	0.00	2500.00
401	-189	-158	-156	-187	PP	G	0.00	0.00	2500.00
401	-189	-187	-222	-224	PP	G	0.00	0.00	2500.00
401	-264	-268	-245	-224	PP	G	0.00	0.00	2500.00
401	-268	-280	-247	-245	PP	G	0.00	0.00	2500.00
401	-245	-247	-218	-224	PP	G	0.00	0.00	2500.00
401	-224	-222	-253	-264	PP	G	0.00	0.00	2500.00
401	-158	-160	-122	-131	PP	G	0.00	0.00	2500.00
401	-158	-131	-129	-156	PP	G	0.00	0.00	2500.00
401	-177	-154	-152	-175	PP	G	0.00	0.00	2500.00
401	-177	-175	-202	-198	PP	G	0.00	0.00	2500.00
401	-175	-152	-148	-171	PP	G	0.00	0.00	2500.00
401	-175	-171	-199	-202	PP	G	0.00	0.00	2500.00
401	-187	-177	-198	-206	PP	G	0.00	0.00	2500.00
401	-187	-206	-228	-222	PP	G	0.00	0.00	2500.00
401	-230	-232	-208	-202	PP	G	0.00	0.00	2500.00
401	-232	-228	-206	-208	PP	G	0.00	0.00	2500.00
401	-208	-206	-198	-202	PP	G	0.00	0.00	2500.00
401	-187	-156	-154	-177	PP	G	0.00	0.00	2500.00
401	-262	-255	-228	-232	PP	G	0.00	0.00	2500.00
401	-262	-232	-230	-260	PP	G	0.00	0.00	2500.00
401	-255	-253	-222	-228	PP	G	0.00	0.00	2500.00
401	-230	-202	-199	-237	PP	G	0.00	0.00	2500.00
401	-230	-237	-258	-260	PP	G	0.00	0.00	2500.00
401	-154	-156	-129	-123	PP	G	0.00	0.00	2500.00
401	-154	-123	-127	-152	PP	G	0.00	0.00	2500.00
401	-127	-124	-148	-152	PP	G	0.00	0.00	2500.00
401	-325	-317	-340	-358	PP	G	0.00	0.00	2500.00
401	-317	-319	-342	-340	PP	G	0.00	0.00	2500.00
401	-358	-340	-342	-359	PP	G	0.00	0.00	2500.00
401	-319	-328	-359	-342	PP	G	0.00	0.00	2500.00
401	-295	-328	-319	-291	PP	G	0.00	0.00	2500.00
401	-295	-291	-260	-258	PP	G	0.00	0.00	2500.00
401	-317	-325	-293	-289	PP	G	0.00	0.00	2500.00
401	-317	-289	-291	-319	PP	G	0.00	0.00	2500.00
401	-289	-293	-255	-262	PP	G	0.00	0.00	2500.00
401	-289	-262	-260	-291	PP	G	0.00	0.00	2500.00
401	-297	-330	-332	-301	PP	G	0.00	0.00	2500.00
401	-297	-301	-264	-253	PP	G	0.00	0.00	2500.00
401	-330	-357	-356	-332	PP	G	0.00	0.00	2500.00
401	-297	-253	-255	-293	PP	G	0.00	0.00	2500.00
401	-297	-293	-325	-330	PP	G	0.00	0.00	2500.00
401	-325	-358	-357	-330	PP	G	0.00	0.00	2500.00
401	-332	-334	-311	-301	PP	G	0.00	0.00	2500.00
401	-334	-324	-305	-311	PP	G	0.00	0.00	2500.00
401	-311	-305	-286	-301	PP	G	0.00	0.00	2500.00
401	-286	-268	-264	-301	PP	G	0.00	0.00	2500.00
401	-334	-332	-356	-355	PP	G	0.00	0.00	2500.00
401	-334	-355	-354	-324	PP	G	0.00	0.00	2500.00
401	-268	-286	-282	-280	PP	G	0.00	0.00	2500.00
401	-286	-305	-303	-282	PP	G	0.00	0.00	2500.00
401	-280	-282	-303	-309	PP	G	0.00	0.00	2500.00
401	-305	-324	-309	-303	PP	G	0.00	0.00	2500.00
401	-309	-307	-276	-280	PP	G	0.00	0.00	2500.00
401	-307	-313	-274	-276	PP	G	0.00	0.00	2500.00
401	-313	-307	-336	-353	PP	G	0.00	0.00	2500.00
401	-307	-309	-338	-336	PP	G	0.00	0.00	2500.00

401	-353	-336	-338	-354	PP	G	0.00	0.00	2500.00
401	-309	-324	-354	-338	PP	G	0.00	0.00	2500.00
401	-323	-287	-284	-313	PP	G	0.00	0.00	2500.00
401	-287	-257	-266	-284	PP	G	0.00	0.00	2500.00
401	-284	-266	-274	-313	PP	G	0.00	0.00	2500.00
401	-313	-353	-352	-323	PP	G	0.00	0.00	2500.00
401	-328	-295	-299	-326	PP	G	0.00	0.00	2500.00
401	-295	-258	-272	-299	PP	G	0.00	0.00	2500.00
401	-299	-272	-278	-326	PP	G	0.00	0.00	2500.00
401	-278	-270	-315	-326	PP	G	0.00	0.00	2500.00
401	-326	-315	-361	-360	PP	G	0.00	0.00	2500.00
401	-326	-360	-359	-328	PP	G	0.00	0.00	2500.00
401	-200	-220	-212	-199	PP	G	0.00	0.00	2500.00
401	-220	-249	-239	-212	PP	G	0.00	0.00	2500.00
401	-212	-239	-237	-199	PP	G	0.00	0.00	2500.00
401	-239	-249	-278	-272	PP	G	0.00	0.00	2500.00
401	-239	-272	-258	-237	PP	G	0.00	0.00	2500.00
401	-278	-249	-251	-270	PP	G	0.00	0.00	2500.00
401	-249	-220	-226	-251	PP	G	0.00	0.00	2500.00
401	-270	-251	-226	-210	PP	G	0.00	0.00	2500.00
401	-220	-200	-210	-226	PP	G	0.00	0.00	2500.00
401	-99	-87	-116	-121	PP	G	0.00	0.00	2500.00
401	-99	-67	-71	-87	PP	G	0.00	0.00	2500.00
401	-67	-50	-58	-71	PP	G	0.00	0.00	2500.00
401	-87	-71	-58	-47	PP	G	0.00	0.00	2500.00
401	-50	-38	-47	-58	PP	G	0.00	0.00	2500.00
401	-38	-10	-11	-47	PP	G	0.00	0.00	2500.00
401	-55	-79	-87	-47	PP	G	0.00	0.00	2500.00
401	-78	-79	-55	-53	PP	G	0.00	0.00	2500.00
401	-78	-53	-39	-85	PP	G	0.00	0.00	2500.00
401	-39	-53	-23	-12	PP	G	0.00	0.00	2500.00
401	-53	-55	-25	-23	PP	G	0.00	0.00	2500.00
401	-12	-23	-25	-11	PP	G	0.00	0.00	2500.00
401	-55	-47	-11	-25	PP	G	0.00	0.00	2500.00
401	-87	-79	-104	-116	PP	G	0.00	0.00	2500.00
401	-79	-78	-106	-104	PP	G	0.00	0.00	2500.00
401	-116	-104	-106	-122	PP	G	0.00	0.00	2500.00
401	-78	-85	-122	-106	PP	G	0.00	0.00	2500.00
401	-39	-12	-13	-34	PP	G	0.00	0.00	2500.00
401	-39	-34	-73	-85	PP	G	0.00	0.00	2500.00
401	-34	-13	-14	-31	PP	G	0.00	0.00	2500.00
401	-34	-31	-62	-73	PP	G	0.00	0.00	2500.00
401	-15	-16	-40	-32	PP	G	0.00	0.00	2500.00
401	-15	-32	-31	-14	PP	G	0.00	0.00	2500.00
401	-32	-40	-70	-60	PP	G	0.00	0.00	2500.00
401	-32	-60	-62	-31	PP	G	0.00	0.00	2500.00
401	-129	-131	-110	-108	PP	G	0.00	0.00	2500.00
401	-129	-108	-97	-123	PP	G	0.00	0.00	2500.00
401	-108	-91	-89	-97	PP	G	0.00	0.00	2500.00
401	-91	-62	-60	-89	PP	G	0.00	0.00	2500.00
401	-89	-60	-70	-97	PP	G	0.00	0.00	2500.00
401	-91	-108	-110	-93	PP	G	0.00	0.00	2500.00
401	-91	-93	-73	-62	PP	G	0.00	0.00	2500.00
401	-73	-93	-95	-85	PP	G	0.00	0.00	2500.00
401	-93	-110	-112	-95	PP	G	0.00	0.00	2500.00
401	-85	-95	-112	-122	PP	G	0.00	0.00	2500.00
401	-110	-131	-122	-112	PP	G	0.00	0.00	2500.00
401	-17	-27	-21	-16	PP	G	0.00	0.00	2500.00
401	-27	-51	-45	-21	PP	G	0.00	0.00	2500.00
401	-21	-45	-40	-16	PP	G	0.00	0.00	2500.00
401	-45	-51	-68	-75	PP	G	0.00	0.00	2500.00
401	-45	-75	-70	-40	PP	G	0.00	0.00	2500.00
401	-127	-123	-97	-102	PP	G	0.00	0.00	2500.00
401	-127	-102	-100	-124	PP	G	0.00	0.00	2500.00
401	-102	-97	-70	-75	PP	G	0.00	0.00	2500.00
401	-102	-75	-68	-100	PP	G	0.00	0.00	2500.00
401	-41	-27	-17	-18	PP	G	0.00	0.00	2500.00
401	-41	-18	-19	-43	PP	G	0.00	0.00	2500.00
401	-100	-68	-65	-86	PP	G	0.00	0.00	2500.00
401	-68	-51	-57	-65	PP	G	0.00	0.00	2500.00
401	-86	-65	-57	-41	PP	G	0.00	0.00	2500.00
401	-51	-27	-41	-57	PP	G	0.00	0.00	2500.00
401	-86	-125	-124	-100	PP	G	0.00	0.00	2500.00
401	-86	-41	-43	-81	PP	G	0.00	0.00	2500.00
401	-86	-81	-114	-125	PP	G	0.00	0.00	2500.00
401	-200	-199	-171	-173	PP	G	0.00	0.00	2500.00
401	-200	-173	-185	-210	PP	G	0.00	0.00	2500.00
401	-173	-171	-148	-150	PP	G	0.00	0.00	2500.00
401	-173	-150	-145	-185	PP	G	0.00	0.00	2500.00
401	-150	-148	-124	-125	PP	G	0.00	0.00	2500.00
401	-150	-125	-114	-145	PP	G	0.00	0.00	2500.00

Elenco carichi elementi bidimensionali
Condizione di carico n. 2: Permanenti non strutturali
Carichi uniformi

Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
401	-126	-118	-98	-101	M	G	0.00	0.00	2500.00
401	-101	-98	-66	-74	M	G	0.00	0.00	2500.00
401	-74	-66	-49	-44	M	G	0.00	0.00	2500.00
401	-36	-44	-20	-4	M	G	0.00	0.00	2500.00
401	-20	-26	-3	-4	M	G	0.00	0.00	2500.00
401	-37	-33	-7	-8	M	G	0.00	0.00	2500.00
401	-33	-30	-6	-7	M	G	0.00	0.00	2500.00
401	-59	-29	-30	-61	M	G	0.00	0.00	2500.00
401	-29	-5	-6	-30	M	G	0.00	0.00	2500.00
401	-92	-90	-61	-72	M	G	0.00	0.00	2500.00
401	-59	-61	-90	-88	M	G	0.00	0.00	2500.00
401	-107	-109	-130	-128	M	G	0.00	0.00	2500.00
401	-130	-109	-111	-120	M	G	0.00	0.00	2500.00
401	-120	-111	-94	-84	M	G	0.00	0.00	2500.00
401	-192	-209	-184	-172	M	G	0.00	0.00	2500.00
401	-172	-184	-144	-149	M	G	0.00	0.00	2500.00
401	-149	-144	-113	-117	M	G	0.00	0.00	2500.00
401	-80	-42	-35	-83	M	G	0.00	0.00	2500.00
401	-26	-49	-56	-35	M	G	0.00	0.00	2500.00
401	-35	-56	-64	-83	M	G	0.00	0.00	2500.00
401	-98	-118	-117	-83	M	G	0.00	0.00	2500.00
401	-35	-2	-3	-26	M	G	0.00	0.00	2500.00
401	-195	-188	-157	-159	M	G	0.00	0.00	2500.00
401	-188	-186	-155	-157	M	G	0.00	0.00	2500.00
401	-246	-279	-267	-244	M	G	0.00	0.00	2500.00
401	-263	-252	-221	-223	M	G	0.00	0.00	2500.00
401	-157	-130	-120	-159	M	G	0.00	0.00	2500.00
401	-240	-242	-213	-215	M	G	0.00	0.00	2500.00
401	-203	-196	-235	-234	M	G	0.00	0.00	2500.00
401	-240	-273	-275	-242	M	G	0.00	0.00	2500.00
401	-246	-217	-213	-242	M	G	0.00	0.00	2500.00
401	-217	-195	-190	-213	M	G	0.00	0.00	2500.00
401	-138	-163	-161	-136	M	G	0.00	0.00	2500.00
401	-159	-161	-180	-195	M	G	0.00	0.00	2500.00
401	-180	-182	-190	-195	M	G	0.00	0.00	2500.00
401	-142	-140	-132	-134	M	G	0.00	0.00	2500.00
401	-140	-138	-115	-132	M	G	0.00	0.00	2500.00
401	-167	-140	-142	-164	M	G	0.00	0.00	2500.00
401	-170	-196	-203	-178	M	G	0.00	0.00	2500.00
401	-167	-163	-138	-140	M	G	0.00	0.00	2500.00
401	-194	-205	-207	-201	M	G	0.00	0.00	2500.00
401	-207	-231	-229	-201	M	G	0.00	0.00	2500.00
401	-186	-205	-194	-176	M	G	0.00	0.00	2500.00
401	-261	-259	-229	-231	M	G	0.00	0.00	2500.00
401	-227	-221	-252	-254	M	G	0.00	0.00	2500.00
401	-229	-233	-193	-201	M	G	0.00	0.00	2500.00
401	-169	-174	-201	-193	M	G	0.00	0.00	2500.00
401	-174	-176	-194	-201	M	G	0.00	0.00	2500.00
401	-153	-151	-126	-119	M	G	0.00	0.00	2500.00
401	-322	-308	-337	-350	M	G	0.00	0.00	2500.00
401	-350	-337	-335	-351	M	G	0.00	0.00	2500.00
401	-322	-304	-302	-308	M	G	0.00	0.00	2500.00
401	-308	-302	-281	-279	M	G	0.00	0.00	2500.00
401	-279	-275	-306	-308	M	G	0.00	0.00	2500.00
401	-285	-300	-263	-267	M	G	0.00	0.00	2500.00
401	-304	-322	-333	-310	M	G	0.00	0.00	2500.00
401	-333	-322	-350	-349	M	G	0.00	0.00	2500.00
401	-273	-265	-283	-312	M	G	0.00	0.00	2500.00
401	-283	-287	-323	-312	M	G	0.00	0.00	2500.00
401	-296	-329	-321	-292	M	G	0.00	0.00	2500.00
401	-329	-347	-346	-321	M	G	0.00	0.00	2500.00
401	-300	-296	-252	-263	M	G	0.00	0.00	2500.00
401	-294	-256	-259	-290	M	G	0.00	0.00	2500.00
401	-261	-254	-292	-288	M	G	0.00	0.00	2500.00
401	-288	-292	-321	-316	M	G	0.00	0.00	2500.00
401	-327	-318	-341	-345	M	G	0.00	0.00	2500.00
401	-345	-341	-339	-346	M	G	0.00	0.00	2500.00
401	-320	-327	-345	-344	M	G	0.00	0.00	2500.00
401	-277	-320	-314	-269	M	G	0.00	0.00	2500.00
401	-271	-256	-294	-298	M	G	0.00	0.00	2500.00
401	-271	-277	-248	-238	M	G	0.00	0.00	2500.00
401	-233	-238	-211	-193	M	G	0.00	0.00	2500.00
401	-211	-219	-192	-193	M	G	0.00	0.00	2500.00
401	-219	-248	-250	-225	M	G	0.00	0.00	2500.00

Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
401	-126	-101	-96	-119	M	G	0.00	0.00	2500.00
401	-101	-74	-69	-96	M	G	0.00	0.00	2500.00
401	-74	-44	-36	-69	M	G	0.00	0.00	2500.00
401	-44	-49	-26	-20	M	G	0.00	0.00	2500.00
401	-37	-84	-72	-33	M	G	0.00	0.00	2500.00
401	-33	-72	-61	-30	M	G	0.00	0.00	2500.00
401	-59	-69	-36	-29	M	G	0.00	0.00	2500.00
401	-29	-36	-4	-5	M	G	0.00	0.00	2500.00
401	-92	-109	-107	-90	M	G	0.00	0.00	2500.00
401	-69	-59	-88	-96	M	G	0.00	0.00	2500.00
401	-88	-90	-107	-96	M	G	0.00	0.00	2500.00
401	-107	-128	-119	-96	M	G	0.00	0.00	2500.00
401	-109	-92	-94	-111	M	G	0.00	0.00	2500.00
401	-92	-72	-84	-94	M	G	0.00	0.00	2500.00
401	-192	-172	-169	-193	M	G	0.00	0.00	2500.00
401	-172	-149	-146	-169	M	G	0.00	0.00	2500.00
401	-149	-117	-118	-146	M	G	0.00	0.00	2500.00
401	-80	-83	-117	-113	M	G	0.00	0.00	2500.00
401	-49	-66	-64	-56	M	G	0.00	0.00	2500.00
401	-66	-98	-83	-64	M	G	0.00	0.00	2500.00
401	-35	-42	-1	-2	M	G	0.00	0.00	2500.00
401	-195	-217	-223	-188	M	G	0.00	0.00	2500.00
401	-188	-223	-221	-186	M	G	0.00	0.00	2500.00
401	-217	-246	-244	-223	M	G	0.00	0.00	2500.00
401	-244	-267	-263	-223	M	G	0.00	0.00	2500.00
401	-157	-155	-128	-130	M	G	0.00	0.00	2500.00
401	-234	-240	-215	-203	M	G	0.00	0.00	2500.00
401	-215	-213	-190	-203	M	G	0.00	0.00	2500.00
401	-240	-234	-265	-273	M	G	0.00	0.00	2500.00
401	-234	-235	-257	-265	M	G	0.00	0.00	2500.00
401	-246	-242	-275	-279	M	G	0.00	0.00	2500.00
401	-115	-138	-136	-120	M	G	0.00	0.00	2500.00
401	-136	-161	-159	-120	M	G	0.00	0.00	2500.00
401	-161	-163	-182	-180	M	G	0.00	0.00	2500.00
401	-147	-142	-134	-121	M	G	0.00	0.00	2500.00
401	-121	-134	-132	-115	M	G	0.00	0.00	2500.00
401	-178	-167	-164	-170	M	G	0.00	0.00	2500.00
401	-164	-142	-147	-170	M	G	0.00	0.00	2500.00
401	-167	-178	-182	-163	M	G	0.00	0.00	2500.00
401	-178	-203	-190	-182	M	G	0.00	0.00	2500.00
401	-205	-227	-231	-207	M	G	0.00	0.00	2500.00
401	-186	-221	-227	-205	M	G	0.00	0.00	2500.00
401	-176	-153	-155	-186	M	G	0.00	0.00	2500.00
401	-261	-231	-227	-254	M	G	0.00	0.00	2500.00
401	-229	-259	-256	-233	M	G	0.00	0.00	2500.00
401	-169	-146	-151	-174	M	G	0.00	0.00	2500.00
401	-174	-151	-153	-176	M	G	0.00	0.00	2500.00
401	-126	-151	-146	-118	M	G	0.00	0.00	2500.00
401	-153	-119	-128	-155	M	G	0.00	0.00	2500.00
401	-308	-306	-335	-337	M	G	0.00	0.00	2500.00
401	-306	-312	-351	-335	M	G	0.00	0.00	2500.00
401	-304	-285	-281	-302	M	G	0.00	0.00	2500.00
401	-285	-267	-279	-281	M	G	0.00	0.00	2500.00
401	-275	-273	-312	-306	M	G	0.00	0.00	2500.00
401	-285	-304	-310	-300	M	G	0.00	0.00	2500.00
401	-310	-333	-331	-300	M	G	0.00	0.00	2500.00
401	-333	-349	-348	-331	M	G	0.00	0.00	2500.00
401	-265	-257	-287	-283	M	G	0.00	0.00	2500.00
401	-323	-352	-351	-312	M	G	0.00	0.00	2500.00
401	-296	-292	-254	-252	M	G	0.00	0.00	2500.00
401	-300	-331	-329	-296	M	G	0.00	0.00	2500.00
401	-331	-348	-347	-329	M	G	0.00	0.00	2500.00
401	-294	-290	-318	-327	M	G	0.00	0.00	2500.00
401	-261	-288	-290	-259	M	G	0.00	0.00	2500.00
401	-288	-316	-318	-290	M	G	0.00	0.00	2500.00
401	-318	-316	-339	-341	M	G	0.00	0.00	2500.00
401	-316	-321	-346	-339	M	G	0.00	0.00	2500.00
401	-320	-344	-343	-314	M	G	0.00	0.00	2500.00
401	-277	-271	-298	-320	M	G	0.00	0.00	2500.00
401	-298	-294	-327	-320	M	G	0.00	0.00	2500.00
401	-271	-238	-233	-256	M	G	0.00	0.00	2500.00
401	-238	-248	-219	-211	M	G	0.00	0.00	2500.00
401	-192	-219	-225	-209	M	G	0.00	0.00	2500.00
401	-209	-225	-250	-269	M	G	0.00	0.00	2500.00

401	-248	-277	-269	-250	M	G	0.00	0.00	2500.00
401	-77	-76	-103	-105	M	G	0.00	0.00	2500.00
401	-76	-82	-115	-103	M	G	0.00	0.00	2500.00
401	-77	-52	-54	-76	M	G	0.00	0.00	2500.00
401	-46	-54	-24	-9	M	G	0.00	0.00	2500.00
401	-9	-24	-22	-8	M	G	0.00	0.00	2500.00
401	-46	-48	-63	-82	M	G	0.00	0.00	2500.00
401	-63	-67	-99	-82	M	G	0.00	0.00	2500.00
401	-10	-38	-28	-9	M	G	0.00	0.00	2500.00
401	-28	-48	-46	-9	M	G	0.00	0.00	2500.00
401	-274	-241	-243	-276	M	G	0.00	0.00	2500.00
401	-204	-236	-235	-196	M	G	0.00	0.00	2500.00
401	-214	-243	-241	-216	M	G	0.00	0.00	2500.00
401	-218	-214	-191	-197	M	G	0.00	0.00	2500.00
401	-243	-247	-280	-276	M	G	0.00	0.00	2500.00
401	-166	-168	-141	-139	M	G	0.00	0.00	2500.00
401	-147	-143	-165	-170	M	G	0.00	0.00	2500.00
401	-165	-168	-179	-170	M	G	0.00	0.00	2500.00
401	-139	-141	-133	-116	M	G	0.00	0.00	2500.00
401	-116	-133	-135	-121	M	G	0.00	0.00	2500.00
401	-191	-183	-181	-197	M	G	0.00	0.00	2500.00
401	-181	-162	-160	-197	M	G	0.00	0.00	2500.00
401	-162	-166	-139	-137	M	G	0.00	0.00	2500.00
401	-197	-160	-158	-189	M	G	0.00	0.00	2500.00
401	-189	-158	-156	-187	M	G	0.00	0.00	2500.00
401	-264	-268	-245	-224	M	G	0.00	0.00	2500.00
401	-245	-247	-218	-224	M	G	0.00	0.00	2500.00
401	-158	-160	-122	-131	M	G	0.00	0.00	2500.00
401	-177	-154	-152	-175	M	G	0.00	0.00	2500.00
401	-175	-152	-148	-171	M	G	0.00	0.00	2500.00
401	-187	-177	-198	-206	M	G	0.00	0.00	2500.00
401	-230	-232	-208	-202	M	G	0.00	0.00	2500.00
401	-208	-206	-198	-202	M	G	0.00	0.00	2500.00
401	-262	-255	-228	-232	M	G	0.00	0.00	2500.00
401	-255	-253	-222	-228	M	G	0.00	0.00	2500.00
401	-230	-237	-258	-260	M	G	0.00	0.00	2500.00
401	-154	-123	-127	-152	M	G	0.00	0.00	2500.00
401	-325	-317	-340	-358	M	G	0.00	0.00	2500.00
401	-358	-340	-342	-359	M	G	0.00	0.00	2500.00
401	-295	-328	-319	-291	M	G	0.00	0.00	2500.00
401	-317	-325	-293	-289	M	G	0.00	0.00	2500.00
401	-289	-293	-255	-262	M	G	0.00	0.00	2500.00
401	-297	-330	-332	-301	M	G	0.00	0.00	2500.00
401	-330	-357	-356	-332	M	G	0.00	0.00	2500.00
401	-297	-293	-325	-330	M	G	0.00	0.00	2500.00
401	-332	-334	-311	-301	M	G	0.00	0.00	2500.00
401	-311	-305	-286	-301	M	G	0.00	0.00	2500.00
401	-334	-332	-356	-355	M	G	0.00	0.00	2500.00
401	-268	-286	-282	-280	M	G	0.00	0.00	2500.00
401	-280	-282	-303	-309	M	G	0.00	0.00	2500.00
401	-309	-307	-276	-280	M	G	0.00	0.00	2500.00
401	-313	-307	-336	-353	M	G	0.00	0.00	2500.00
401	-353	-336	-338	-354	M	G	0.00	0.00	2500.00
401	-323	-287	-284	-313	M	G	0.00	0.00	2500.00
401	-284	-266	-274	-313	M	G	0.00	0.00	2500.00
401	-328	-295	-299	-326	M	G	0.00	0.00	2500.00
401	-299	-272	-278	-326	M	G	0.00	0.00	2500.00
401	-326	-315	-361	-360	M	G	0.00	0.00	2500.00
401	-200	-220	-212	-199	M	G	0.00	0.00	2500.00
401	-212	-239	-237	-199	M	G	0.00	0.00	2500.00
401	-239	-272	-258	-237	M	G	0.00	0.00	2500.00
401	-249	-220	-226	-251	M	G	0.00	0.00	2500.00
401	-220	-200	-210	-226	M	G	0.00	0.00	2500.00
401	-99	-67	-71	-87	M	G	0.00	0.00	2500.00
401	-87	-71	-58	-47	M	G	0.00	0.00	2500.00
401	-38	-10	-11	-47	M	G	0.00	0.00	2500.00
401	-78	-79	-55	-53	M	G	0.00	0.00	2500.00
401	-39	-53	-23	-12	M	G	0.00	0.00	2500.00
401	-12	-23	-25	-11	M	G	0.00	0.00	2500.00
401	-87	-79	-104	-116	M	G	0.00	0.00	2500.00
401	-116	-104	-106	-122	M	G	0.00	0.00	2500.00
401	-39	-12	-13	-34	M	G	0.00	0.00	2500.00
401	-34	-13	-14	-31	M	G	0.00	0.00	2500.00
401	-15	-16	-40	-32	M	G	0.00	0.00	2500.00
401	-32	-40	-70	-60	M	G	0.00	0.00	2500.00
401	-129	-131	-110	-108	M	G	0.00	0.00	2500.00
401	-108	-91	-89	-97	M	G	0.00	0.00	2500.00
401	-89	-60	-70	-97	M	G	0.00	0.00	2500.00
401	-91	-93	-73	-62	M	G	0.00	0.00	2500.00
401	-93	-110	-112	-95	M	G	0.00	0.00	2500.00
401	-110	-131	-122	-112	M	G	0.00	0.00	2500.00
401	-27	-51	-45	-21	M	G	0.00	0.00	2500.00
401	-84	-77	-105	-120	M	G	0.00	0.00	2500.00
401	-120	-105	-103	-115	M	G	0.00	0.00	2500.00
401	-77	-84	-37	-52	M	G	0.00	0.00	2500.00
401	-54	-46	-82	-76	M	G	0.00	0.00	2500.00
401	-54	-52	-22	-24	M	G	0.00	0.00	2500.00
401	-52	-37	-8	-22	M	G	0.00	0.00	2500.00
401	-48	-50	-67	-63	M	G	0.00	0.00	2500.00
401	-99	-121	-115	-82	M	G	0.00	0.00	2500.00
401	-38	-50	-48	-28	M	G	0.00	0.00	2500.00
401	-274	-266	-236	-241	M	G	0.00	0.00	2500.00
401	-266	-257	-235	-236	M	G	0.00	0.00	2500.00
401	-191	-214	-216	-204	M	G	0.00	0.00	2500.00
401	-216	-241	-236	-204	M	G	0.00	0.00	2500.00
401	-243	-214	-218	-247	M	G	0.00	0.00	2500.00
401	-166	-183	-179	-168	M	G	0.00	0.00	2500.00
401	-183	-191	-204	-179	M	G	0.00	0.00	2500.00
401	-143	-141	-168	-165	M	G	0.00	0.00	2500.00
401	-179	-204	-196	-170	M	G	0.00	0.00	2500.00
401	-141	-143	-135	-133	M	G	0.00	0.00	2500.00
401	-143	-147	-121	-135	M	G	0.00	0.00	2500.00
401	-183	-166	-162	-181	M	G	0.00	0.00	2500.00
401	-160	-162	-137	-122	M	G	0.00	0.00	2500.00
401	-137	-139	-116	-122	M	G	0.00	0.00	2500.00
401	-197	-189	-224	-218	M	G	0.00	0.00	2500.00
401	-189	-187	-222	-224	M	G	0.00	0.00	2500.00
401	-268	-280	-247	-245	M	G	0.00	0.00	2500.00
401	-224	-222	-253	-264	M	G	0.00	0.00	2500.00
401	-158	-131	-129	-156	M	G	0.00	0.00	2500.00
401	-177	-175	-202	-198	M	G	0.00	0.00	2500.00
401	-175	-171	-199	-202	M	G	0.00	0.00	2500.00
401	-187	-206	-228	-222	M	G	0.00	0.00	2500.00
401	-232	-228	-206	-208	M	G	0.00	0.00	2500.00
401	-187	-156	-154	-177	M	G	0.00	0.00	2500.00
401	-262	-232	-230	-260	M	G	0.00	0.00	2500.00
401	-230	-202	-199	-237	M	G	0.00	0.00	2500.00
401	-154	-156	-129	-123	M	G	0.00	0.00	2500.00
401	-127	-124	-148	-152	M	G	0.00	0.00	2500.00
401	-317	-319	-342	-340	M	G	0.00	0.00	2500.00
401	-319	-328	-359	-342	M	G	0.00	0.00	2500.00
401	-295	-291	-260	-258	M	G	0.00	0.00	2500.00
401	-317	-289	-291	-319	M	G	0.00	0.00	2500.00
401	-289	-262	-260	-291	M	G	0.00	0.00	2500.00
401	-297	-301	-264	-253	M	G	0.00	0.00	2500.00
401	-297	-253	-255	-293	M	G	0.00	0.00	2500.00
401	-325	-358	-357	-330	M	G	0.00	0.00	2500.00
401	-334	-324	-305	-311	M	G	0.00	0.00	2500.00
401	-286	-268	-264	-301	M	G	0.00	0.00	2500.00
401	-334	-355	-354	-324	M	G	0.00	0.00	2500.00
401	-286	-305	-303	-282	M	G	0.00	0.00	2500.00
401	-305	-324	-309	-303	M	G	0.00	0.00	2500.00
401	-307	-313	-274	-276	M	G	0.00	0.00	2500.00
401	-307	-309	-338	-336	M	G	0.00	0.00	2500.00
401	-309	-324	-354	-338	M	G	0.00	0.00	2500.00
401	-287	-257	-266	-284	M	G	0.00	0.00	2500.00
401	-313	-353	-352	-323	M	G	0.00	0.00	2500.00
401	-295	-258	-272	-299	M	G	0.00	0.00	2500.00
401	-278	-270	-315	-326	M	G	0.00	0.00	2500.00
401	-326	-360	-359	-328	M	G	0.00	0.00	2500.00
401	-220	-249	-239	-212	M	G	0.00	0.00	2500.00
401	-239	-249	-278	-272	M	G	0.00	0.00	2500.00
401	-278	-249	-251	-270	M	G	0.00	0.00	2500.00
401	-270	-251	-226	-210	M	G	0.00	0.00	2500.00
401	-99	-87	-116	-121	M	G	0.00	0.00	2500.00
401	-67	-50	-58	-71	M	G	0.00	0.00	2500.00
401	-50	-38	-47	-58	M	G	0.00	0.00	2500.00
401	-55	-79	-87	-47	M	G	0.00	0.00	2500.00
401	-78	-53	-39	-85	M	G	0.00	0.00	2500.00
401	-53	-55	-25	-23	M	G	0.00	0.00	2500.00
401	-55	-47	-11	-25	M	G	0.00	0.00	2500.00
401	-79	-78	-106	-104	M	G	0.00	0.00	2500.00
401	-78	-85	-122	-106	M	G	0.00	0.00	2500.00
401	-39	-34	-73	-85	M	G	0.00	0.00	2500.00
401	-34	-31	-62	-73	M	G	0.00	0.00	2500.00
401	-15	-32	-31	-14	M	G	0.00	0.00	2500.00
401	-32	-60	-62	-31	M	G	0.00	0.00	2500.00
401	-129	-108	-97	-123	M	G	0.00	0.00	2500.00
401	-91	-62	-60	-89	M	G	0.00	0.00	2500.00
401	-91	-108	-110	-93	M	G	0.00	0.00	2500.00
401	-73	-93	-95	-85	M	G	0.00	0.00	2500.00
401	-85	-95	-112	-122	M	G	0.00	0.00	2500.00
401	-17	-27	-21	-16	M	G	0.00	0.00	2500.00
401	-21	-45	-40	-16	M	G	0.00	0.00	2500.00

401	-45	-51	-68	-75	M	G	0.00	0.00	2500.00	401	-45	-75	-70	-40	M	G	0.00	0.00	2500.00
401	-127	-123	-97	-102	M	G	0.00	0.00	2500.00	401	-127	-102	-100	-124	M	G	0.00	0.00	2500.00
401	-102	-97	-70	-75	M	G	0.00	0.00	2500.00	401	-102	-75	-68	-100	M	G	0.00	0.00	2500.00
401	-41	-27	-17	-18	M	G	0.00	0.00	2500.00	401	-41	-18	-19	-43	M	G	0.00	0.00	2500.00
401	-100	-68	-65	-86	M	G	0.00	0.00	2500.00	401	-68	-51	-57	-65	M	G	0.00	0.00	2500.00
401	-86	-65	-57	-41	M	G	0.00	0.00	2500.00	401	-51	-27	-41	-57	M	G	0.00	0.00	2500.00
401	-86	-125	-124	-100	M	G	0.00	0.00	2500.00	401	-86	-41	-43	-81	M	G	0.00	0.00	2500.00
401	-86	-81	-114	-125	M	G	0.00	0.00	2500.00	401	-200	-199	-171	-173	M	G	0.00	0.00	2500.00
401	-200	-173	-185	-210	M	G	0.00	0.00	2500.00	401	-173	-171	-148	-150	M	G	0.00	0.00	2500.00
401	-173	-150	-145	-185	M	G	0.00	0.00	2500.00	401	-150	-148	-124	-125	M	G	0.00	0.00	2500.00
401	-150	-125	-114	-145	M	G	0.00	0.00	2500.00											

Elenco carichi elementi bidimensionali
Condizione di carico n. 2: Permanenti non strutturali
Carichi idrostatici

Simbologia

Bid. = Numero del muro/elemento bidimensionale
N1 = Nodo1
N2 = Nodo2
N3 = Nodo3
N4 = Nodo4
Zi = Coordinata Z globale d'inizio carico
QYi = Componente iniziale del carico in direzione Y locale dell'elemento bidimensionale
MY = Coordinata Z globale di fine carico
QYf = Componente finale del carico in direzione Y locale dell'elemento bidimensionale

Bid.	N1	N2	N3	N4	Zi <m>	QYi <daN/m>	MY <m>	QYf <daN/m>	Bid.	N1	N2	N3	N4	Zi <m>	QYi <daN/m>	MY <m>	QYf <daN/m>
103	-413	-410	-437	-440	0.00	-3200.00	5.30	0.00	103	-494	-491	179	-500	0.00	-3200.00	5.30	0.00
103	-440	-437	-464	-467	0.00	-3200.00	5.30	0.00	103	-467	-464	-491	-494	0.00	-3200.00	5.30	0.00
103	-386	-383	-410	-413	0.00	-3200.00	5.30	0.00	103	-464	-461	-488	-491	0.00	-3200.00	5.30	0.00
103	-491	-488	166	179	0.00	-3200.00	5.30	0.00	103	-380	-377	-404	-407	0.00	-3200.00	5.30	0.00
103	-407	-404	-431	-434	0.00	-3200.00	5.30	0.00	103	-434	-431	-458	-461	0.00	-3200.00	5.30	0.00
103	-461	-458	-485	-488	0.00	-3200.00	5.30	0.00	103	-488	-485	153	166	0.00	-3200.00	5.30	0.00
103	-377	-374	-401	-404	0.00	-3200.00	5.30	0.00	103	-404	-401	-428	-431	0.00	-3200.00	5.30	0.00
103	-431	-428	-455	-458	0.00	-3200.00	5.30	0.00	103	-458	-455	-482	-485	0.00	-3200.00	5.30	0.00
103	-383	-380	-407	-410	0.00	-3200.00	5.30	0.00	103	-410	-407	-434	-437	0.00	-3200.00	5.30	0.00
103	-437	-434	-461	-464	0.00	-3200.00	5.30	0.00	103	-256	-233	-383	-386	0.00	-3200.00	5.30	0.00
103	-233	-193	-380	-383	0.00	-3200.00	5.30	0.00	103	-193	-169	-377	-380	0.00	-3200.00	5.30	0.00
103	-169	-146	-374	-377	0.00	-3200.00	5.30	0.00	103	-146	-118	-371	-374	0.00	-3200.00	5.30	0.00
103	-118	-98	-368	-371	0.00	-3200.00	5.30	0.00	103	-98	-66	-365	-368	0.00	-3200.00	5.30	0.00
103	-66	-49	-362	-365	0.00	-3200.00	5.30	0.00	103	-395	-392	-419	-422	0.00	-3200.00	5.30	0.00
103	-422	-419	-446	-449	0.00	-3200.00	5.30	0.00	103	-449	-446	-473	-476	0.00	-3200.00	5.30	0.00
103	-476	-473	101	114	0.00	-3200.00	5.30	0.00	103	-365	-362	-389	-392	0.00	-3200.00	5.30	0.00
103	-392	-389	-416	-419	0.00	-3200.00	5.30	0.00	103	-419	-416	-443	-446	0.00	-3200.00	5.30	0.00
103	-446	-443	-470	-473	0.00	-3200.00	5.30	0.00	103	-473	-470	-497	101	0.00	-3200.00	5.30	0.00
103	-455	-452	-479	-482	0.00	-3200.00	5.30	0.00	103	-482	-479	127	140	0.00	-3200.00	5.30	0.00
103	-371	-368	-395	-398	0.00	-3200.00	5.30	0.00	103	-398	-395	-422	-425	0.00	-3200.00	5.30	0.00
103	-425	-422	-449	-452	0.00	-3200.00	5.30	0.00	103	-452	-449	-476	-479	0.00	-3200.00	5.30	0.00
103	-479	-476	114	127	0.00	-3200.00	5.30	0.00	103	-368	-365	-392	-395	0.00	-3200.00	5.30	0.00
103	-374	-371	-398	-401	0.00	-3200.00	5.30	0.00	103	-401	-398	-425	-428	0.00	-3200.00	5.30	0.00
103	-485	-482	140	153	0.00	-3200.00	5.30	0.00	103	-428	-425	-452	-455	0.00	-3200.00	5.30	0.00
104	-493	-490	178	191	0.00	3200.00	5.30	0.00	104	-382	-379	-406	-409	0.00	3200.00	5.30	0.00
104	-415	-412	-439	-442	0.00	3200.00	5.30	0.00	104	-442	-439	-466	-469	0.00	3200.00	5.30	0.00
104	-469	-466	-493	-496	0.00	3200.00	5.30	0.00	104	-496	-493	191	-502	0.00	3200.00	5.30	0.00
104	-385	-382	-409	-412	0.00	3200.00	5.30	0.00	104	-412	-409	-436	-439	0.00	3200.00	5.30	0.00
104	-439	-436	-463	-466	0.00	3200.00	5.30	0.00	104	-466	-463	-490	-493	0.00	3200.00	5.30	0.00
104	-457	-454	-481	-484	0.00	3200.00	5.30	0.00	104	-484	-481	139	152	0.00	3200.00	5.30	0.00
104	-373	-370	-397	-400	0.00	3200.00	5.30	0.00	104	-400	-397	-424	-427	0.00	3200.00	5.30	0.00
104	-427	-424	-451	-454	0.00	3200.00	5.30	0.00	104	-454	-451	-478	-481	0.00	3200.00	5.30	0.00
104	-481	-478	126	139	0.00	3200.00	5.30	0.00	104	-370	-367	-394	-397	0.00	3200.00	5.30	0.00
104	-397	-394	-421	-424	0.00	3200.00	5.30	0.00	104	-424	-421	-448	-451	0.00	3200.00	5.30	0.00
104	-451	-448	-475	-478	0.00	3200.00	5.30	0.00	104	-478	-475	113	126	0.00	3200.00	5.30	0.00
104	-367	-364	-391	-394	0.00	3200.00	5.30	0.00	104	-394	-391	-418	-421	0.00	3200.00	5.30	0.00
104	-421	-418	-445	-448	0.00	3200.00	5.30	0.00	104	-448	-445	-472	-475	0.00	3200.00	5.30	0.00
104	-475	-472	-499	113	0.00	3200.00	5.30	0.00	104	-409	-406	-433	-436	0.00	3200.00	5.30	0.00
104	-436	-433	-460	-463	0.00	3200.00	5.30	0.00	104	-463	-460	-487	-490	0.00	3200.00	5.30	0.00
104	-490	-487	165	178	0.00	3200.00	5.30	0.00	104	-379	-376	-403	-406	0.00	3200.00	5.30	0.00
104	-406	-403	-430	-433	0.00	3200.00	5.30	0.00	104	-433	-430	-457	-460	0.00	3200.00	5.30	0.00
104	-460	-457	-484	-487	0.00	3200.00	5.30	0.00	104	-487	-484	152	165	0.00	3200.00	5.30	0.00
104	-376	-373	-400	-403	0.00	3200.00	5.30	0.00	104	-403	-400	-427	-430	0.00	3200.00	5.30	0.00
104	-430	-427	-454	-457	0.00	3200.00	5.30	0.00	104	-258	-237	-385	-388	0.00	3200.00	5.30	0.00
104	-237	-199	-382	-385	0.00	3200.00	5.30	0.00	104	-199	-171	-379	-382	0.00	3200.00	5.30	0.00
104	-171	-148	-376	-379	0.00	3200.00	5.30	0.00	104	-148	-124	-373	-376	0.00	3200.00	5.30	0.00
104	-124	-100	-370	-373	0.00	3200.00	5.30	0.00	104	-100	-68	-367	-370	0.00	3200.00	5.30	0.00
104	-68	-51	-364	-367	0.00	3200.00	5.30	0.00	104	-388	-385	-412	-415	0.00	3200.00	5.30	0.00

Elenco carichi elementi bidimensionali
Condizione di carico n. 3: Variabili folla
Carichi uniformi

Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
103	-413	-410	-437	-440	M	G	-1000.00	0.00	0.00
103	-440	-437	-464	-467	M	G	-1000.00	0.00	0.00
103	-386	-383	-410	-413	M	G	-1000.00	0.00	0.00
103	-491	-488	166	179	M	G	-1000.00	0.00	0.00
103	-407	-404	-431	-434	M	G	-1000.00	0.00	0.00
103	-461	-458	-485	-488	M	G	-1000.00	0.00	0.00
103	-377	-374	-401	-404	M	G	-1000.00	0.00	0.00
103	-431	-428	-455	-458	M	G	-1000.00	0.00	0.00
103	-383	-380	-407	-410	M	G	-1000.00	0.00	0.00
103	-437	-434	-461	-464	M	G	-1000.00	0.00	0.00
103	-233	-193	-380	-383	M	G	-1000.00	0.00	0.00
103	-169	-146	-374	-377	M	G	-1000.00	0.00	0.00
103	-118	-98	-368	-371	M	G	-1000.00	0.00	0.00
103	-66	-49	-362	-365	M	G	-1000.00	0.00	0.00
103	-422	-419	-446	-449	M	G	-1000.00	0.00	0.00
103	-476	-473	101	114	M	G	-1000.00	0.00	0.00
103	-392	-389	-416	-419	M	G	-1000.00	0.00	0.00
103	-446	-443	-470	-473	M	G	-1000.00	0.00	0.00
103	-455	-452	-479	-482	M	G	-1000.00	0.00	0.00
103	-371	-368	-395	-398	M	G	-1000.00	0.00	0.00
103	-425	-422	-449	-452	M	G	-1000.00	0.00	0.00
103	-479	-476	114	127	M	G	-1000.00	0.00	0.00
103	-374	-371	-398	-401	M	G	-1000.00	0.00	0.00
103	-485	-482	140	153	M	G	-1000.00	0.00	0.00
104	-493	-490	178	191	M	G	1000.00	0.00	0.00
104	-415	-412	-439	-442	M	G	1000.00	0.00	0.00
104	-469	-466	-493	-496	M	G	1000.00	0.00	0.00
104	-385	-382	-409	-412	M	G	1000.00	0.00	0.00
104	-439	-436	-463	-466	M	G	1000.00	0.00	0.00
104	-457	-454	-481	-484	M	G	1000.00	0.00	0.00
104	-373	-370	-397	-400	M	G	1000.00	0.00	0.00
104	-427	-424	-451	-454	M	G	1000.00	0.00	0.00
104	-481	-478	126	139	M	G	1000.00	0.00	0.00
104	-397	-394	-421	-424	M	G	1000.00	0.00	0.00
104	-451	-448	-475	-478	M	G	1000.00	0.00	0.00
104	-367	-364	-391	-394	M	G	1000.00	0.00	0.00
104	-421	-418	-445	-448	M	G	1000.00	0.00	0.00
104	-475	-472	-499	113	M	G	1000.00	0.00	0.00
104	-436	-433	-460	-463	M	G	1000.00	0.00	0.00
104	-490	-487	165	178	M	G	1000.00	0.00	0.00
104	-406	-403	-430	-433	M	G	1000.00	0.00	0.00
104	-460	-457	-484	-487	M	G	1000.00	0.00	0.00
104	-376	-373	-400	-403	M	G	1000.00	0.00	0.00
104	-430	-427	-454	-457	M	G	1000.00	0.00	0.00
104	-237	-199	-382	-385	M	G	1000.00	0.00	0.00
104	-171	-148	-376	-379	M	G	1000.00	0.00	0.00
104	-124	-100	-370	-373	M	G	1000.00	0.00	0.00
104	-68	-51	-364	-367	M	G	1000.00	0.00	0.00
103	-494	-491	179	-500	M	G	-1000.00	0.00	0.00
103	-467	-464	-491	-494	M	G	-1000.00	0.00	0.00
103	-464	-461	-488	-491	M	G	-1000.00	0.00	0.00
103	-380	-377	-404	-407	M	G	-1000.00	0.00	0.00
103	-434	-431	-458	-461	M	G	-1000.00	0.00	0.00
103	-488	-485	153	166	M	G	-1000.00	0.00	0.00
103	-404	-401	-428	-431	M	G	-1000.00	0.00	0.00
103	-458	-455	-482	-485	M	G	-1000.00	0.00	0.00
103	-410	-407	-434	-437	M	G	-1000.00	0.00	0.00
103	-256	-233	-383	-386	M	G	-1000.00	0.00	0.00
103	-193	-169	-377	-380	M	G	-1000.00	0.00	0.00
103	-146	-118	-371	-374	M	G	-1000.00	0.00	0.00
103	-98	-66	-365	-368	M	G	-1000.00	0.00	0.00
103	-395	-392	-419	-422	M	G	-1000.00	0.00	0.00
103	-449	-446	-473	-476	M	G	-1000.00	0.00	0.00
103	-365	-362	-389	-392	M	G	-1000.00	0.00	0.00
103	-419	-416	-443	-446	M	G	-1000.00	0.00	0.00
103	-473	-470	-497	101	M	G	-1000.00	0.00	0.00
103	-482	-479	127	140	M	G	-1000.00	0.00	0.00
103	-398	-395	-422	-425	M	G	-1000.00	0.00	0.00
103	-452	-449	-476	-479	M	G	-1000.00	0.00	0.00
103	-368	-365	-392	-395	M	G	-1000.00	0.00	0.00
103	-401	-398	-425	-428	M	G	-1000.00	0.00	0.00
103	-428	-425	-452	-455	M	G	-1000.00	0.00	0.00
104	-382	-379	-406	-409	M	G	1000.00	0.00	0.00
104	-442	-439	-466	-469	M	G	1000.00	0.00	0.00
104	-496	-493	191	-502	M	G	1000.00	0.00	0.00
104	-412	-409	-436	-439	M	G	1000.00	0.00	0.00
104	-466	-463	-490	-493	M	G	1000.00	0.00	0.00
104	-484	-481	139	152	M	G	1000.00	0.00	0.00
104	-400	-397	-424	-427	M	G	1000.00	0.00	0.00
104	-454	-451	-478	-481	M	G	1000.00	0.00	0.00
104	-370	-367	-394	-397	M	G	1000.00	0.00	0.00
104	-424	-421	-448	-451	M	G	1000.00	0.00	0.00
104	-478	-475	113	126	M	G	1000.00	0.00	0.00
104	-394	-391	-418	-421	M	G	1000.00	0.00	0.00
104	-448	-445	-472	-475	M	G	1000.00	0.00	0.00
104	-409	-406	-433	-436	M	G	1000.00	0.00	0.00
104	-463	-460	-487	-490	M	G	1000.00	0.00	0.00
104	-379	-376	-403	-406	M	G	1000.00	0.00	0.00
104	-433	-430	-457	-460	M	G	1000.00	0.00	0.00
104	-487	-484	152	165	M	G	1000.00	0.00	0.00
104	-403	-400	-427	-430	M	G	1000.00	0.00	0.00
104	-258	-237	-385	-388	M	G	1000.00	0.00	0.00
104	-199	-171	-379	-382	M	G	1000.00	0.00	0.00
104	-148	-124	-373	-376	M	G	1000.00	0.00	0.00
104	-100	-68	-367	-370	M	G	1000.00	0.00	0.00
104	-388	-385	-412	-415	M	G	1000.00	0.00	0.00

Elenco carichi elementi bidimensionali
Condizione di carico n. 5: Variabile piena T=200
Carichi uniformi

Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
401	-126	-118	-98	-101	M	G	0.00	0.00	2800.00
401	-101	-98	-66	-74	M	G	0.00	0.00	2800.00
401	-74	-66	-49	-44	M	G	0.00	0.00	2800.00
401	-36	-44	-20	-4	M	G	0.00	0.00	2800.00
401	-20	-26	-3	-4	M	G	0.00	0.00	2800.00
401	-37	-33	-7	-8	M	G	0.00	0.00	2800.00
401	-33	-30	-6	-7	M	G	0.00	0.00	2800.00
401	-59	-29	-30	-61	M	G	0.00	0.00	2800.00
401	-29	-5	-6	-30	M	G	0.00	0.00	2800.00
401	-92	-90	-61	-72	M	G	0.00	0.00	2800.00
401	-59	-61	-90	-88	M	G	0.00	0.00	2800.00
401	-107	-109	-130	-128	M	G	0.00	0.00	2800.00
401	-130	-109	-111	-120	M	G	0.00	0.00	2800.00
401	-120	-111	-94	-84	M	G	0.00	0.00	2800.00
401	-192	-209	-184	-172	M	G	0.00	0.00	2800.00
401	-172	-184	-144	-149	M	G	0.00	0.00	2800.00
401	-149	-144	-113	-117	M	G	0.00	0.00	2800.00
401	-80	-42	-35	-83	M	G	0.00	0.00	2800.00
401	-26	-49	-56	-35	M	G	0.00	0.00	2800.00
401	-35	-56	-64	-83	M	G	0.00	0.00	2800.00
401	-98	-118	-117	-83	M	G	0.00	0.00	2800.00
401	-126	-101	-96	-119	M	G	0.00	0.00	2800.00
401	-101	-74	-69	-96	M	G	0.00	0.00	2800.00
401	-74	-44	-36	-69	M	G	0.00	0.00	2800.00
401	-44	-49	-26	-20	M	G	0.00	0.00	2800.00
401	-37	-84	-72	-33	M	G	0.00	0.00	2800.00
401	-33	-72	-61	-30	M	G	0.00	0.00	2800.00
401	-59	-69	-36	-29	M	G	0.00	0.00	2800.00
401	-29	-36	-4	-5	M	G	0.00	0.00	2800.00
401	-92	-109	-107	-90	M	G	0.00	0.00	2800.00
401	-69	-59	-88	-96	M	G	0.00	0.00	2800.00
401	-88	-90	-107	-96	M	G	0.00	0.00	2800.00
401	-107	-128	-119	-96	M	G	0.00	0.00	2800.00
401	-109	-92	-94	-111	M	G	0.00	0.00	2800.00
401	-92	-72	-84	-94	M	G	0.00	0.00	2800.00
401	-192	-172	-169	-193	M	G	0.00	0.00	2800.00
401	-172	-149	-146	-169	M	G	0.00	0.00	2800.00
401	-149	-117	-118	-146	M	G	0.00	0.00	2800.00
401	-80	-83	-117	-113	M	G	0.00	0.00	2800.00
401	-49	-66	-64	-56	M	G	0.00	0.00	2800.00
401	-66	-98	-83	-64	M	G	0.00	0.00	2800.00
401	-35	-42	-1	-2	M	G	0.00	0.00	2800.00

401	-35	-2	-3	-26	M	G	0.00	0.00	2800.00
401	-195	-188	-157	-159	M	G	0.00	0.00	2800.00
401	-188	-186	-155	-157	M	G	0.00	0.00	2800.00
401	-246	-279	-267	-244	M	G	0.00	0.00	2800.00
401	-263	-252	-221	-223	M	G	0.00	0.00	2800.00
401	-157	-130	-120	-159	M	G	0.00	0.00	2800.00
401	-240	-242	-213	-215	M	G	0.00	0.00	2800.00
401	-203	-196	-235	-234	M	G	0.00	0.00	2800.00
401	-240	-273	-275	-242	M	G	0.00	0.00	2800.00
401	-246	-217	-213	-242	M	G	0.00	0.00	2800.00
401	-217	-195	-190	-213	M	G	0.00	0.00	2800.00
401	-138	-163	-161	-136	M	G	0.00	0.00	2800.00
401	-159	-161	-180	-195	M	G	0.00	0.00	2800.00
401	-180	-182	-190	-195	M	G	0.00	0.00	2800.00
401	-142	-140	-132	-134	M	G	0.00	0.00	2800.00
401	-140	-138	-115	-132	M	G	0.00	0.00	2800.00
401	-167	-140	-142	-164	M	G	0.00	0.00	2800.00
401	-170	-196	-203	-178	M	G	0.00	0.00	2800.00
401	-167	-163	-138	-140	M	G	0.00	0.00	2800.00
401	-194	-205	-207	-201	M	G	0.00	0.00	2800.00
401	-207	-231	-229	-201	M	G	0.00	0.00	2800.00
401	-186	-205	-194	-176	M	G	0.00	0.00	2800.00
401	-261	-259	-229	-231	M	G	0.00	0.00	2800.00
401	-227	-221	-252	-254	M	G	0.00	0.00	2800.00
401	-229	-233	-193	-201	M	G	0.00	0.00	2800.00
401	-169	-174	-201	-193	M	G	0.00	0.00	2800.00
401	-174	-176	-194	-201	M	G	0.00	0.00	2800.00
401	-153	-151	-126	-119	M	G	0.00	0.00	2800.00
401	-322	-308	-337	-350	M	G	0.00	0.00	2800.00
401	-350	-337	-335	-351	M	G	0.00	0.00	2800.00
401	-322	-304	-302	-308	M	G	0.00	0.00	2800.00
401	-308	-302	-281	-279	M	G	0.00	0.00	2800.00
401	-279	-275	-306	-308	M	G	0.00	0.00	2800.00
401	-285	-300	-263	-267	M	G	0.00	0.00	2800.00
401	-304	-322	-333	-310	M	G	0.00	0.00	2800.00
401	-333	-322	-350	-349	M	G	0.00	0.00	2800.00
401	-273	-265	-283	-312	M	G	0.00	0.00	2800.00
401	-283	-287	-323	-312	M	G	0.00	0.00	2800.00
401	-296	-329	-321	-292	M	G	0.00	0.00	2800.00
401	-329	-347	-346	-321	M	G	0.00	0.00	2800.00
401	-300	-296	-252	-263	M	G	0.00	0.00	2800.00
401	-294	-256	-259	-290	M	G	0.00	0.00	2800.00
401	-261	-254	-292	-288	M	G	0.00	0.00	2800.00
401	-288	-292	-321	-316	M	G	0.00	0.00	2800.00
401	-327	-318	-341	-345	M	G	0.00	0.00	2800.00
401	-345	-341	-339	-346	M	G	0.00	0.00	2800.00
401	-320	-327	-345	-344	M	G	0.00	0.00	2800.00
401	-277	-320	-314	-269	M	G	0.00	0.00	2800.00
401	-271	-256	-294	-298	M	G	0.00	0.00	2800.00
401	-271	-277	-248	-238	M	G	0.00	0.00	2800.00
401	-233	-238	-211	-193	M	G	0.00	0.00	2800.00
401	-211	-219	-192	-193	M	G	0.00	0.00	2800.00
401	-219	-248	-250	-225	M	G	0.00	0.00	2800.00
401	-248	-277	-269	-250	M	G	0.00	0.00	2800.00
401	-77	-76	-103	-105	M	G	0.00	0.00	2800.00
401	-76	-82	-115	-103	M	G	0.00	0.00	2800.00
401	-77	-52	-54	-76	M	G	0.00	0.00	2800.00
401	-46	-54	-24	-9	M	G	0.00	0.00	2800.00
401	-9	-24	-22	-8	M	G	0.00	0.00	2800.00
401	-46	-48	-63	-82	M	G	0.00	0.00	2800.00
401	-63	-67	-99	-82	M	G	0.00	0.00	2800.00
401	-10	-38	-28	-9	M	G	0.00	0.00	2800.00
401	-28	-48	-46	-9	M	G	0.00	0.00	2800.00
401	-274	-241	-243	-276	M	G	0.00	0.00	2800.00
401	-204	-236	-235	-196	M	G	0.00	0.00	2800.00
401	-214	-243	-241	-216	M	G	0.00	0.00	2800.00
401	-218	-214	-191	-197	M	G	0.00	0.00	2800.00
401	-243	-247	-280	-276	M	G	0.00	0.00	2800.00
401	-166	-168	-141	-139	M	G	0.00	0.00	2800.00
401	-147	-143	-165	-170	M	G	0.00	0.00	2800.00
401	-165	-168	-179	-170	M	G	0.00	0.00	2800.00
401	-139	-141	-133	-116	M	G	0.00	0.00	2800.00
401	-116	-133	-135	-121	M	G	0.00	0.00	2800.00
401	-191	-183	-181	-197	M	G	0.00	0.00	2800.00
401	-181	-162	-160	-197	M	G	0.00	0.00	2800.00
401	-162	-166	-139	-137	M	G	0.00	0.00	2800.00
401	-197	-160	-158	-189	M	G	0.00	0.00	2800.00
401	-189	-158	-156	-187	M	G	0.00	0.00	2800.00
401	-264	-268	-245	-224	M	G	0.00	0.00	2800.00
401	-245	-247	-218	-224	M	G	0.00	0.00	2800.00
401	-158	-160	-122	-131	M	G	0.00	0.00	2800.00
401	-177	-154	-152	-175	M	G	0.00	0.00	2800.00
401	-195	-217	-223	-188	M	G	0.00	0.00	2800.00
401	-188	-223	-221	-186	M	G	0.00	0.00	2800.00
401	-217	-246	-244	-223	M	G	0.00	0.00	2800.00
401	-244	-267	-263	-223	M	G	0.00	0.00	2800.00
401	-157	-155	-128	-130	M	G	0.00	0.00	2800.00
401	-234	-240	-215	-203	M	G	0.00	0.00	2800.00
401	-215	-213	-190	-203	M	G	0.00	0.00	2800.00
401	-240	-234	-265	-273	M	G	0.00	0.00	2800.00
401	-234	-235	-257	-265	M	G	0.00	0.00	2800.00
401	-246	-242	-275	-279	M	G	0.00	0.00	2800.00
401	-115	-138	-136	-120	M	G	0.00	0.00	2800.00
401	-136	-161	-159	-120	M	G	0.00	0.00	2800.00
401	-161	-163	-182	-180	M	G	0.00	0.00	2800.00
401	-147	-142	-134	-121	M	G	0.00	0.00	2800.00
401	-121	-134	-132	-115	M	G	0.00	0.00	2800.00
401	-178	-167	-164	-170	M	G	0.00	0.00	2800.00
401	-164	-142	-147	-170	M	G	0.00	0.00	2800.00
401	-167	-178	-182	-163	M	G	0.00	0.00	2800.00
401	-178	-203	-190	-182	M	G	0.00	0.00	2800.00
401	-205	-227	-231	-207	M	G	0.00	0.00	2800.00
401	-186	-221	-227	-205	M	G	0.00	0.00	2800.00
401	-176	-153	-155	-186	M	G	0.00	0.00	2800.00
401	-261	-231	-227	-254	M	G	0.00	0.00	2800.00
401	-229	-259	-256	-233	M	G	0.00	0.00	2800.00
401	-169	-146	-151	-174	M	G	0.00	0.00	2800.00
401	-174	-151	-153	-176	M	G	0.00	0.00	2800.00
401	-126	-151	-146	-118	M	G	0.00	0.00	2800.00
401	-153	-119	-128	-155	M	G	0.00	0.00	2800.00
401	-308	-306	-335	-337	M	G	0.00	0.00	2800.00
401	-306	-312	-351	-335	M	G	0.00	0.00	2800.00
401	-304	-285	-281	-302	M	G	0.00	0.00	2800.00
401	-285	-267	-279	-281	M	G	0.00	0.00	2800.00
401	-275	-273	-312	-306	M	G	0.00	0.00	2800.00
401	-285	-304	-310	-300	M	G	0.00	0.00	2800.00
401	-310	-333	-331	-300	M	G	0.00	0.00	2800.00
401	-333	-349	-348	-331	M	G	0.00	0.00	2800.00
401	-265	-257	-287	-283	M	G	0.00	0.00	2800.00
401	-323	-352	-351	-312	M	G	0.00	0.00	2800.00
401	-296	-292	-254	-252	M	G	0.00	0.00	2800.00
401	-300	-331	-329	-296	M	G	0.00	0.00	2800.00
401	-331	-348	-347	-329	M	G	0.00	0.00	2800.00
401	-294	-290	-318	-327	M	G	0.00	0.00	2800.00
401	-261	-288	-290	-259	M	G	0.00	0.00	2800.00
401	-288	-316	-318	-290	M	G	0.00	0.00	2800.00
401	-318	-316	-339	-341	M	G	0.00	0.00	2800.00
401	-316	-321	-346	-339	M	G	0.00	0.00	2800.00
401	-320	-344	-343	-314	M	G	0.00	0.00	2800.00
401	-277	-271	-298	-320	M	G	0.00	0.00	2800.00
401	-298	-294	-327	-320	M	G	0.00	0.00	2800.00
401	-271	-238	-233	-256	M	G	0.00	0.00	2800.00
401	-238	-248	-219	-211	M	G	0.00	0.00	2800.00
401	-192	-219	-225	-209	M	G	0.00	0.00	2800.00
401	-209	-225	-250	-269	M	G	0.00	0.00	2800.00
401	-84	-77	-105	-120	M	G	0.00	0.00	2800.00
401	-120	-105	-103	-115	M	G	0.00	0.00	2800.00
401	-77	-84	-37	-52	M	G	0.00	0.00	2800.00
401	-54	-46	-82	-76	M	G	0.00	0.00	2800.00
401	-54	-52	-22	-24	M	G	0.00	0.00	2800.00
401	-52	-37	-8	-22	M	G	0.00	0.00	2800.00
401	-48	-50	-67	-63	M	G	0.00	0.00	2800.00
401	-99	-121	-115	-82	M	G	0.00	0.00	2800.00
401	-38	-50	-48	-28	M	G	0.00	0.00	2800.00
401	-274	-266	-236	-241	M	G	0.00	0.00	2800.00
401	-266	-257	-235	-236	M	G	0.00	0.00	2800.00
401	-191	-214	-216	-204	M	G	0.00	0.00	2800.00
401	-216	-241	-236	-204	M	G	0.00	0.00	2800.00
401	-243	-214	-218	-247	M	G	0.00	0.00	2800.00
401	-166	-183	-179	-168	M	G	0.00	0.00	2800.00
401	-183	-191	-204	-179	M	G	0.00	0.00	2800.00
401	-143	-141	-168	-165	M	G	0.00	0.00	2800.00
401	-179	-204	-196	-170	M	G	0.00	0.00	2800.00
401	-141	-143	-135	-133	M	G	0.00	0.00	2800.00
401	-143	-147	-121	-135	M	G	0.00	0.00	2800.00
401	-183	-166	-162	-181	M	G	0.00	0.00	2800.00
401	-160	-162	-137	-122	M	G	0.00	0.00	2800.00
401	-137	-139	-116	-122	M	G	0.00	0.00	2800.00
401	-197	-189	-224	-218	M	G	0.00	0.00	2800.00
401	-189	-187	-222	-224	M	G	0.00	0.00	2800.00
401	-268	-280	-247	-245	M	G	0.00	0.00	2800.00
401	-224	-222	-253	-264	M	G	0.00	0.00	2800.00
401	-158	-131	-129	-156	M	G	0.00	0.00	2800.00
401	-177	-175	-202	-198	M	G	0.00	0.00	2800.00

401	-175	-152	-148	-171	M	G	0.00	0.00	2800.00	401	-175	-171	-199	-202	M	G	0.00	0.00	2800.00
401	-187	-177	-198	-206	M	G	0.00	0.00	2800.00	401	-187	-206	-228	-222	M	G	0.00	0.00	2800.00
401	-230	-232	-208	-202	M	G	0.00	0.00	2800.00	401	-232	-228	-206	-208	M	G	0.00	0.00	2800.00
401	-208	-206	-198	-202	M	G	0.00	0.00	2800.00	401	-187	-156	-154	-177	M	G	0.00	0.00	2800.00
401	-262	-255	-228	-232	M	G	0.00	0.00	2800.00	401	-262	-232	-230	-260	M	G	0.00	0.00	2800.00
401	-255	-253	-222	-228	M	G	0.00	0.00	2800.00	401	-230	-202	-199	-237	M	G	0.00	0.00	2800.00
401	-230	-237	-258	-260	M	G	0.00	0.00	2800.00	401	-154	-156	-129	-123	M	G	0.00	0.00	2800.00
401	-154	-123	-127	-152	M	G	0.00	0.00	2800.00	401	-127	-124	-148	-152	M	G	0.00	0.00	2800.00
401	-325	-317	-340	-358	M	G	0.00	0.00	2800.00	401	-317	-319	-342	-340	M	G	0.00	0.00	2800.00
401	-358	-340	-342	-359	M	G	0.00	0.00	2800.00	401	-319	-328	-359	-342	M	G	0.00	0.00	2800.00
401	-295	-328	-319	-291	M	G	0.00	0.00	2800.00	401	-295	-291	-260	-258	M	G	0.00	0.00	2800.00
401	-317	-325	-293	-289	M	G	0.00	0.00	2800.00	401	-317	-289	-291	-319	M	G	0.00	0.00	2800.00
401	-289	-293	-255	-262	M	G	0.00	0.00	2800.00	401	-289	-262	-260	-291	M	G	0.00	0.00	2800.00
401	-297	-330	-332	-301	M	G	0.00	0.00	2800.00	401	-297	-301	-264	-253	M	G	0.00	0.00	2800.00
401	-330	-357	-356	-332	M	G	0.00	0.00	2800.00	401	-297	-253	-255	-293	M	G	0.00	0.00	2800.00
401	-297	-293	-325	-330	M	G	0.00	0.00	2800.00	401	-325	-358	-357	-330	M	G	0.00	0.00	2800.00
401	-332	-334	-311	-301	M	G	0.00	0.00	2800.00	401	-334	-324	-305	-311	M	G	0.00	0.00	2800.00
401	-311	-305	-286	-301	M	G	0.00	0.00	2800.00	401	-286	-268	-264	-301	M	G	0.00	0.00	2800.00
401	-334	-332	-356	-355	M	G	0.00	0.00	2800.00	401	-334	-355	-354	-324	M	G	0.00	0.00	2800.00
401	-268	-286	-282	-280	M	G	0.00	0.00	2800.00	401	-286	-305	-303	-282	M	G	0.00	0.00	2800.00
401	-280	-282	-303	-309	M	G	0.00	0.00	2800.00	401	-305	-324	-309	-303	M	G	0.00	0.00	2800.00
401	-309	-307	-276	-280	M	G	0.00	0.00	2800.00	401	-307	-313	-274	-276	M	G	0.00	0.00	2800.00
401	-313	-307	-336	-353	M	G	0.00	0.00	2800.00	401	-307	-309	-338	-336	M	G	0.00	0.00	2800.00
401	-353	-336	-338	-354	M	G	0.00	0.00	2800.00	401	-309	-324	-354	-338	M	G	0.00	0.00	2800.00
401	-323	-287	-284	-313	M	G	0.00	0.00	2800.00	401	-287	-257	-266	-284	M	G	0.00	0.00	2800.00
401	-284	-266	-274	-313	M	G	0.00	0.00	2800.00	401	-313	-353	-352	-323	M	G	0.00	0.00	2800.00
401	-328	-295	-299	-326	M	G	0.00	0.00	2800.00	401	-295	-258	-272	-299	M	G	0.00	0.00	2800.00
401	-299	-272	-278	-326	M	G	0.00	0.00	2800.00	401	-278	-270	-315	-326	M	G	0.00	0.00	2800.00
401	-326	-315	-361	-360	M	G	0.00	0.00	2800.00	401	-326	-360	-359	-328	M	G	0.00	0.00	2800.00
401	-200	-220	-212	-199	M	G	0.00	0.00	2800.00	401	-220	-249	-239	-212	M	G	0.00	0.00	2800.00
401	-212	-239	-237	-199	M	G	0.00	0.00	2800.00	401	-239	-249	-278	-272	M	G	0.00	0.00	2800.00
401	-239	-272	-258	-237	M	G	0.00	0.00	2800.00	401	-278	-249	-251	-270	M	G	0.00	0.00	2800.00
401	-249	-220	-226	-251	M	G	0.00	0.00	2800.00	401	-270	-251	-226	-210	M	G	0.00	0.00	2800.00
401	-220	-200	-210	-226	M	G	0.00	0.00	2800.00	401	-99	-87	-116	-121	M	G	0.00	0.00	2800.00
401	-99	-67	-71	-87	M	G	0.00	0.00	2800.00	401	-67	-50	-58	-71	M	G	0.00	0.00	2800.00
401	-87	-71	-58	-47	M	G	0.00	0.00	2800.00	401	-50	-38	-47	-58	M	G	0.00	0.00	2800.00
401	-38	-10	-11	-47	M	G	0.00	0.00	2800.00	401	-55	-79	-87	-47	M	G	0.00	0.00	2800.00
401	-78	-79	-55	-53	M	G	0.00	0.00	2800.00	401	-78	-53	-39	-85	M	G	0.00	0.00	2800.00
401	-39	-53	-23	-12	M	G	0.00	0.00	2800.00	401	-53	-55	-25	-23	M	G	0.00	0.00	2800.00
401	-12	-23	-25	-11	M	G	0.00	0.00	2800.00	401	-55	-47	-11	-25	M	G	0.00	0.00	2800.00
401	-87	-79	-104	-116	M	G	0.00	0.00	2800.00	401	-79	-78	-106	-104	M	G	0.00	0.00	2800.00
401	-116	-104	-106	-122	M	G	0.00	0.00	2800.00	401	-78	-85	-122	-106	M	G	0.00	0.00	2800.00
401	-39	-12	-13	-34	M	G	0.00	0.00	2800.00	401	-39	-34	-73	-85	M	G	0.00	0.00	2800.00
401	-34	-13	-14	-31	M	G	0.00	0.00	2800.00	401	-34	-31	-62	-73	M	G	0.00	0.00	2800.00
401	-15	-16	-40	-32	M	G	0.00	0.00	2800.00	401	-15	-32	-31	-14	M	G	0.00	0.00	2800.00
401	-32	-40	-70	-60	M	G	0.00	0.00	2800.00	401	-32	-60	-62	-31	M	G	0.00	0.00	2800.00
401	-129	-131	-110	-108	M	G	0.00	0.00	2800.00	401	-129	-108	-97	-123	M	G	0.00	0.00	2800.00
401	-108	-91	-89	-97	M	G	0.00	0.00	2800.00	401	-91	-62	-60	-89	M	G	0.00	0.00	2800.00
401	-89	-60	-70	-97	M	G	0.00	0.00	2800.00	401	-91	-108	-110	-93	M	G	0.00	0.00	2800.00
401	-91	-93	-73	-62	M	G	0.00	0.00	2800.00	401	-73	-93	-95	-85	M	G	0.00	0.00	2800.00
401	-93	-110	-112	-95	M	G	0.00	0.00	2800.00	401	-85	-95	-112	-122	M	G	0.00	0.00	2800.00
401	-110	-131	-122	-112	M	G	0.00	0.00	2800.00	401	-17	-27	-21	-16	M	G	0.00	0.00	2800.00
401	-27	-51	-45	-21	M	G	0.00	0.00	2800.00	401	-21	-45	-40	-16	M	G	0.00	0.00	2800.00
401	-45	-51	-68	-75	M	G	0.00	0.00	2800.00	401	-45	-75	-70	-40	M	G	0.00	0.00	2800.00
401	-127	-123	-97	-102	M	G	0.00	0.00	2800.00	401	-127	-102	-100	-124	M	G	0.00	0.00	2800.00
401	-102	-97	-70	-75	M	G	0.00	0.00	2800.00	401	-102	-75	-68	-100	M	G	0.00	0.00	2800.00
401	-41	-27	-17	-18	M	G	0.00	0.00	2800.00	401	-41	-18	-19	-43	M	G	0.00	0.00	2800.00
401	-100	-68	-65	-86	M	G	0.00	0.00	2800.00	401	-68	-51	-57	-65	M	G	0.00	0.00	2800.00
401	-86	-65	-57	-41	M	G	0.00	0.00	2800.00	401	-51	-27	-41	-57	M	G	0.00	0.00	2800.00
401	-86	-125	-124	-100	M	G	0.00	0.00	2800.00	401	-86	-41	-43	-81	M	G	0.00	0.00	2800.00
401	-86	-81	-114	-125	M	G	0.00	0.00	2800.00	401	-200	-199	-171	-173	M	G	0.00	0.00	2800.00
401	-200	-173	-185	-210	M	G	0.00	0.00	2800.00	401	-173	-171	-148	-150	M	G	0.00	0.00	2800.00
401	-173	-150	-145	-185	M	G	0.00	0.00	2800.00	401	-150	-148	-124	-125	M	G	0.00	0.00	2800.00
401	-150	-125	-114	-145	M	G	0.00	0.00	2800.00											

Elenco carichi elementi bidimensionali
Condizione di carico n. 6: Variabile piena T=500
Carichi uniformi

Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>	Bid.	N1	N2	N3	N4	T	DC	Qx <daN/mq>	Qy <daN/mq>	Qz <daN/mq>
401	-126	-118	-98	-101	M	G	0.00	0.00	2800.00	401	-126	-101	-96	-119	M	G	0.00	0.00	2800.00
401	-101	-98	-66	-74	M	G	0.00	0.00	2800.00	401	-101	-74	-69	-96	M	G	0.00	0.00	2800.00
401	-74	-66	-49	-44	M	G	0.00	0.00	2800.00	401	-74	-44	-36	-69	M	G	0.00	0.00	2800.00
401	-36	-44	-20	-4	M	G	0.00	0.00	2800.00	401	-44	-49	-26	-20	M	G	0.00	0.00	2800.00
401	-20	-26	-3	-4	M	G	0.00	0.00	2800.00	401	-37	-84	-72	-33	M	G	0.00	0.00	2800.00
401	-37	-33	-7	-8	M	G	0.00	0.00	2800.00	401	-33	-72	-61	-30	M	G	0.00	0.00	2800.00
401	-33	-30	-6	-7	M	G	0.00	0.00	2800.00	401	-59	-69	-36	-29	M	G	0.00	0.00	2800.00
401	-59	-29	-30	-61	M	G	0.00	0.00	2800.00	401	-29	-36	-4	-5	M	G	0.00	0.00	2800.00
401	-29	-5	-6	-30	M	G	0.00	0.00	2800.00	401	-92	-109	-107	-90	M	G	0.00	0.00	2800.00
401	-92	-90	-61	-72	M	G	0.00	0.00	2800.00	401	-69	-59	-88	-96	M	G	0.00	0.00	2800.00

401	-59	-61	-90	-88	M	G	0.00	0.00	2800.00
401	-107	-109	-130	-128	M	G	0.00	0.00	2800.00
401	-130	-109	-111	-120	M	G	0.00	0.00	2800.00
401	-120	-111	-94	-84	M	G	0.00	0.00	2800.00
401	-192	-209	-184	-172	M	G	0.00	0.00	2800.00
401	-172	-184	-144	-149	M	G	0.00	0.00	2800.00
401	-149	-144	-113	-117	M	G	0.00	0.00	2800.00
401	-80	-42	-35	-83	M	G	0.00	0.00	2800.00
401	-26	-49	-56	-35	M	G	0.00	0.00	2800.00
401	-35	-56	-64	-83	M	G	0.00	0.00	2800.00
401	-98	-118	-117	-83	M	G	0.00	0.00	2800.00
401	-35	-2	-3	-26	M	G	0.00	0.00	2800.00
401	-195	-188	-157	-159	M	G	0.00	0.00	2800.00
401	-188	-186	-155	-157	M	G	0.00	0.00	2800.00
401	-246	-279	-267	-244	M	G	0.00	0.00	2800.00
401	-263	-252	-221	-223	M	G	0.00	0.00	2800.00
401	-157	-130	-120	-159	M	G	0.00	0.00	2800.00
401	-240	-242	-213	-215	M	G	0.00	0.00	2800.00
401	-203	-196	-235	-234	M	G	0.00	0.00	2800.00
401	-240	-273	-275	-242	M	G	0.00	0.00	2800.00
401	-246	-217	-213	-242	M	G	0.00	0.00	2800.00
401	-217	-195	-190	-213	M	G	0.00	0.00	2800.00
401	-138	-163	-161	-136	M	G	0.00	0.00	2800.00
401	-159	-161	-180	-195	M	G	0.00	0.00	2800.00
401	-180	-182	-190	-195	M	G	0.00	0.00	2800.00
401	-142	-140	-132	-134	M	G	0.00	0.00	2800.00
401	-140	-138	-115	-132	M	G	0.00	0.00	2800.00
401	-167	-140	-142	-164	M	G	0.00	0.00	2800.00
401	-170	-196	-203	-178	M	G	0.00	0.00	2800.00
401	-167	-163	-138	-140	M	G	0.00	0.00	2800.00
401	-194	-205	-207	-201	M	G	0.00	0.00	2800.00
401	-207	-231	-229	-201	M	G	0.00	0.00	2800.00
401	-186	-205	-194	-176	M	G	0.00	0.00	2800.00
401	-261	-259	-229	-231	M	G	0.00	0.00	2800.00
401	-227	-221	-252	-254	M	G	0.00	0.00	2800.00
401	-229	-233	-193	-201	M	G	0.00	0.00	2800.00
401	-169	-174	-201	-193	M	G	0.00	0.00	2800.00
401	-174	-176	-194	-201	M	G	0.00	0.00	2800.00
401	-153	-151	-126	-119	M	G	0.00	0.00	2800.00
401	-322	-308	-337	-350	M	G	0.00	0.00	2800.00
401	-350	-337	-335	-351	M	G	0.00	0.00	2800.00
401	-322	-304	-302	-308	M	G	0.00	0.00	2800.00
401	-308	-302	-281	-279	M	G	0.00	0.00	2800.00
401	-279	-275	-306	-308	M	G	0.00	0.00	2800.00
401	-285	-300	-263	-267	M	G	0.00	0.00	2800.00
401	-304	-322	-333	-310	M	G	0.00	0.00	2800.00
401	-333	-322	-350	-349	M	G	0.00	0.00	2800.00
401	-273	-265	-283	-312	M	G	0.00	0.00	2800.00
401	-283	-287	-323	-312	M	G	0.00	0.00	2800.00
401	-296	-329	-321	-292	M	G	0.00	0.00	2800.00
401	-329	-347	-346	-321	M	G	0.00	0.00	2800.00
401	-300	-296	-252	-263	M	G	0.00	0.00	2800.00
401	-294	-256	-259	-290	M	G	0.00	0.00	2800.00
401	-261	-254	-292	-288	M	G	0.00	0.00	2800.00
401	-288	-292	-321	-316	M	G	0.00	0.00	2800.00
401	-327	-318	-341	-345	M	G	0.00	0.00	2800.00
401	-345	-341	-339	-346	M	G	0.00	0.00	2800.00
401	-320	-327	-345	-344	M	G	0.00	0.00	2800.00
401	-277	-320	-314	-269	M	G	0.00	0.00	2800.00
401	-271	-256	-294	-298	M	G	0.00	0.00	2800.00
401	-271	-277	-248	-238	M	G	0.00	0.00	2800.00
401	-233	-238	-211	-193	M	G	0.00	0.00	2800.00
401	-211	-219	-192	-193	M	G	0.00	0.00	2800.00
401	-219	-248	-250	-225	M	G	0.00	0.00	2800.00
401	-248	-277	-269	-250	M	G	0.00	0.00	2800.00
401	-77	-76	-103	-105	M	G	0.00	0.00	2800.00
401	-76	-82	-115	-103	M	G	0.00	0.00	2800.00
401	-77	-52	-54	-76	M	G	0.00	0.00	2800.00
401	-46	-54	-24	-9	M	G	0.00	0.00	2800.00
401	-9	-24	-22	-8	M	G	0.00	0.00	2800.00
401	-46	-48	-63	-82	M	G	0.00	0.00	2800.00
401	-63	-67	-99	-82	M	G	0.00	0.00	2800.00
401	-10	-38	-28	-9	M	G	0.00	0.00	2800.00
401	-28	-48	-46	-9	M	G	0.00	0.00	2800.00
401	-274	-241	-243	-276	M	G	0.00	0.00	2800.00
401	-204	-236	-235	-196	M	G	0.00	0.00	2800.00
401	-214	-243	-241	-216	M	G	0.00	0.00	2800.00
401	-218	-214	-191	-197	M	G	0.00	0.00	2800.00
401	-243	-247	-280	-276	M	G	0.00	0.00	2800.00
401	-166	-168	-141	-139	M	G	0.00	0.00	2800.00
401	-147	-143	-165	-170	M	G	0.00	0.00	2800.00
401	-165	-168	-179	-170	M	G	0.00	0.00	2800.00
401	-88	-90	-107	-96	M	G	0.00	0.00	2800.00
401	-107	-128	-119	-96	M	G	0.00	0.00	2800.00
401	-109	-92	-94	-111	M	G	0.00	0.00	2800.00
401	-92	-72	-84	-94	M	G	0.00	0.00	2800.00
401	-192	-172	-169	-193	M	G	0.00	0.00	2800.00
401	-172	-149	-146	-169	M	G	0.00	0.00	2800.00
401	-149	-117	-118	-146	M	G	0.00	0.00	2800.00
401	-80	-83	-117	-113	M	G	0.00	0.00	2800.00
401	-49	-66	-64	-56	M	G	0.00	0.00	2800.00
401	-66	-98	-83	-64	M	G	0.00	0.00	2800.00
401	-35	-42	-1	-2	M	G	0.00	0.00	2800.00
401	-195	-217	-223	-188	M	G	0.00	0.00	2800.00
401	-188	-223	-221	-186	M	G	0.00	0.00	2800.00
401	-217	-246	-244	-223	M	G	0.00	0.00	2800.00
401	-244	-267	-263	-223	M	G	0.00	0.00	2800.00
401	-157	-155	-128	-130	M	G	0.00	0.00	2800.00
401	-234	-240	-215	-203	M	G	0.00	0.00	2800.00
401	-215	-213	-190	-203	M	G	0.00	0.00	2800.00
401	-240	-234	-265	-273	M	G	0.00	0.00	2800.00
401	-234	-235	-257	-265	M	G	0.00	0.00	2800.00
401	-246	-242	-275	-279	M	G	0.00	0.00	2800.00
401	-115	-138	-136	-120	M	G	0.00	0.00	2800.00
401	-136	-161	-159	-120	M	G	0.00	0.00	2800.00
401	-161	-163	-182	-180	M	G	0.00	0.00	2800.00
401	-147	-142	-134	-121	M	G	0.00	0.00	2800.00
401	-121	-134	-132	-115	M	G	0.00	0.00	2800.00
401	-178	-167	-164	-170	M	G	0.00	0.00	2800.00
401	-164	-142	-147	-170	M	G	0.00	0.00	2800.00
401	-167	-178	-182	-163	M	G	0.00	0.00	2800.00
401	-178	-203	-190	-182	M	G	0.00	0.00	2800.00
401	-205	-227	-231	-207	M	G	0.00	0.00	2800.00
401	-186	-221	-227	-205	M	G	0.00	0.00	2800.00
401	-176	-153	-155	-186	M	G	0.00	0.00	2800.00
401	-261	-231	-227	-254	M	G	0.00	0.00	2800.00
401	-229	-259	-256	-233	M	G	0.00	0.00	2800.00
401	-169	-146	-151	-174	M	G	0.00	0.00	2800.00
401	-174	-151	-153	-176	M	G	0.00	0.00	2800.00
401	-126	-151	-146	-118	M	G	0.00	0.00	2800.00
401	-153	-119	-128	-155	M	G	0.00	0.00	2800.00
401	-308	-306	-335	-337	M	G	0.00	0.00	2800.00
401	-306	-312	-351	-335	M	G	0.00	0.00	2800.00
401	-304	-285	-281	-302	M	G	0.00	0.00	2800.00
401	-285	-267	-279	-281	M	G	0.00	0.00	2800.00
401	-275	-273	-312	-306	M	G	0.00	0.00	2800.00
401	-285	-304	-310	-300	M	G	0.00	0.00	2800.00
401	-310	-333	-331	-300	M	G	0.00	0.00	2800.00
401	-333	-349	-348	-331	M	G	0.00	0.00	2800.00
401	-265	-257	-287	-283	M	G	0.00	0.00	2800.00
401	-323	-352	-351	-312	M	G	0.00	0.00	2800.00
401	-296	-292	-254	-252	M	G	0.00	0.00	2800.00
401	-300	-331	-329	-296	M	G	0.00	0.00	2800.00
401	-331	-348	-347	-329	M	G	0.00	0.00	2800.00
401	-294	-290	-318	-327	M	G	0.00	0.00	2800.00
401	-261	-288	-290	-259	M	G	0.00	0.00	2800.00
401	-288	-316	-318	-290	M	G	0.00	0.00	2800.00
401	-318	-316	-339	-341	M	G	0.00	0.00	2800.00
401	-316	-321	-346	-339	M	G	0.00	0.00	2800.00
401	-320	-344	-343	-314	M	G	0.00	0.00	2800.00
401	-277	-271	-298	-320	M	G	0.00	0.00	2800.00
401	-298	-294	-327	-320	M	G	0.00	0.00	2800.00
401	-271	-238	-233	-256	M	G	0.00	0.00	2800.00
401	-238	-248	-219	-211	M	G	0.00	0.00	2800.00
401	-192	-219	-225	-209	M	G	0.00	0.00	2800.00
401	-209	-225	-250	-269	M	G	0.00	0.00	2800.00
401	-84	-77	-105	-120	M	G	0.00	0.00	2800.00
401	-120	-105	-103	-115	M	G	0.00	0.00	2800.00
401	-77	-84	-37	-52	M	G	0.00	0.00	2800.00
401	-54	-46	-82	-76	M	G	0.00	0.00	2800.00
401	-54	-52	-22	-24	M	G	0.00	0.00	2800.00
401	-52	-37	-8	-22	M	G	0.00	0.00	2800.00
401	-48	-50	-67	-63	M	G	0.00	0.00	2800.00
401	-99	-121	-115	-82	M	G	0.00	0.00	2800.00
401	-38	-50	-48	-28	M	G	0.00	0.00	2800.00
401	-274	-266	-236	-241	M	G	0.00	0.00	2800.00
401	-266	-257	-235	-236	M	G	0.00	0.00	2800.00
401	-191	-214	-216	-204	M	G	0.00	0.00	2800.00
401	-216	-241	-236	-204	M	G	0.00	0.00	2800.00
401	-243	-214	-218	-247	M	G	0.00	0.00	2800.00
401	-166	-183	-179	-168	M	G	0.00	0.00	2800.00
401	-183	-191	-204	-179	M	G	0.00	0.00	2800.00
401	-143	-141	-168	-165	M	G	0.00	0.00	2800.00
401	-179	-204	-196	-170	M	G	0.00	0.00	2800.00

401	-139	-141	-133	-116	M	G	0.00	0.00	2800.00
401	-116	-133	-135	-121	M	G	0.00	0.00	2800.00
401	-191	-183	-181	-197	M	G	0.00	0.00	2800.00
401	-181	-162	-160	-197	M	G	0.00	0.00	2800.00
401	-162	-166	-139	-137	M	G	0.00	0.00	2800.00
401	-197	-160	-158	-189	M	G	0.00	0.00	2800.00
401	-189	-158	-156	-187	M	G	0.00	0.00	2800.00
401	-264	-268	-245	-224	M	G	0.00	0.00	2800.00
401	-245	-247	-218	-224	M	G	0.00	0.00	2800.00
401	-158	-160	-122	-131	M	G	0.00	0.00	2800.00
401	-177	-154	-152	-175	M	G	0.00	0.00	2800.00
401	-175	-152	-148	-171	M	G	0.00	0.00	2800.00
401	-187	-177	-198	-206	M	G	0.00	0.00	2800.00
401	-230	-232	-208	-202	M	G	0.00	0.00	2800.00
401	-208	-206	-198	-202	M	G	0.00	0.00	2800.00
401	-262	-255	-228	-232	M	G	0.00	0.00	2800.00
401	-255	-253	-222	-228	M	G	0.00	0.00	2800.00
401	-230	-237	-258	-260	M	G	0.00	0.00	2800.00
401	-154	-123	-127	-152	M	G	0.00	0.00	2800.00
401	-325	-317	-340	-358	M	G	0.00	0.00	2800.00
401	-358	-340	-342	-359	M	G	0.00	0.00	2800.00
401	-295	-328	-319	-291	M	G	0.00	0.00	2800.00
401	-317	-325	-293	-289	M	G	0.00	0.00	2800.00
401	-289	-293	-255	-262	M	G	0.00	0.00	2800.00
401	-297	-330	-332	-301	M	G	0.00	0.00	2800.00
401	-330	-357	-356	-332	M	G	0.00	0.00	2800.00
401	-297	-293	-325	-330	M	G	0.00	0.00	2800.00
401	-332	-334	-311	-301	M	G	0.00	0.00	2800.00
401	-311	-305	-286	-301	M	G	0.00	0.00	2800.00
401	-334	-332	-356	-355	M	G	0.00	0.00	2800.00
401	-268	-286	-282	-280	M	G	0.00	0.00	2800.00
401	-280	-282	-303	-309	M	G	0.00	0.00	2800.00
401	-309	-307	-276	-280	M	G	0.00	0.00	2800.00
401	-313	-307	-336	-353	M	G	0.00	0.00	2800.00
401	-353	-336	-338	-354	M	G	0.00	0.00	2800.00
401	-323	-287	-284	-313	M	G	0.00	0.00	2800.00
401	-284	-266	-274	-313	M	G	0.00	0.00	2800.00
401	-328	-295	-299	-326	M	G	0.00	0.00	2800.00
401	-299	-272	-278	-326	M	G	0.00	0.00	2800.00
401	-326	-315	-361	-360	M	G	0.00	0.00	2800.00
401	-200	-220	-212	-199	M	G	0.00	0.00	2800.00
401	-212	-239	-237	-199	M	G	0.00	0.00	2800.00
401	-239	-272	-258	-237	M	G	0.00	0.00	2800.00
401	-249	-220	-226	-251	M	G	0.00	0.00	2800.00
401	-220	-200	-210	-226	M	G	0.00	0.00	2800.00
401	-99	-67	-71	-87	M	G	0.00	0.00	2800.00
401	-87	-71	-58	-47	M	G	0.00	0.00	2800.00
401	-38	-10	-11	-47	M	G	0.00	0.00	2800.00
401	-78	-79	-55	-53	M	G	0.00	0.00	2800.00
401	-39	-53	-23	-12	M	G	0.00	0.00	2800.00
401	-12	-23	-25	-11	M	G	0.00	0.00	2800.00
401	-87	-79	-104	-116	M	G	0.00	0.00	2800.00
401	-116	-104	-106	-122	M	G	0.00	0.00	2800.00
401	-39	-12	-13	-34	M	G	0.00	0.00	2800.00
401	-34	-13	-14	-31	M	G	0.00	0.00	2800.00
401	-15	-16	-40	-32	M	G	0.00	0.00	2800.00
401	-32	-40	-70	-60	M	G	0.00	0.00	2800.00
401	-129	-131	-110	-108	M	G	0.00	0.00	2800.00
401	-108	-91	-89	-97	M	G	0.00	0.00	2800.00
401	-89	-60	-70	-97	M	G	0.00	0.00	2800.00
401	-91	-93	-73	-62	M	G	0.00	0.00	2800.00
401	-93	-110	-112	-95	M	G	0.00	0.00	2800.00
401	-110	-131	-122	-112	M	G	0.00	0.00	2800.00
401	-27	-51	-45	-21	M	G	0.00	0.00	2800.00
401	-45	-51	-68	-75	M	G	0.00	0.00	2800.00
401	-127	-123	-97	-102	M	G	0.00	0.00	2800.00
401	-102	-97	-70	-75	M	G	0.00	0.00	2800.00
401	-41	-27	-17	-18	M	G	0.00	0.00	2800.00
401	-100	-68	-65	-86	M	G	0.00	0.00	2800.00
401	-86	-65	-57	-41	M	G	0.00	0.00	2800.00
401	-86	-125	-124	-100	M	G	0.00	0.00	2800.00
401	-86	-81	-114	-125	M	G	0.00	0.00	2800.00
401	-200	-173	-185	-210	M	G	0.00	0.00	2800.00
401	-173	-150	-145	-185	M	G	0.00	0.00	2800.00
401	-150	-125	-114	-145	M	G	0.00	0.00	2800.00
401	-141	-143	-135	-133	M	G	0.00	0.00	2800.00
401	-143	-147	-121	-135	M	G	0.00	0.00	2800.00
401	-183	-166	-162	-181	M	G	0.00	0.00	2800.00
401	-160	-162	-137	-122	M	G	0.00	0.00	2800.00
401	-137	-139	-116	-122	M	G	0.00	0.00	2800.00
401	-197	-189	-224	-218	M	G	0.00	0.00	2800.00
401	-189	-187	-222	-224	M	G	0.00	0.00	2800.00
401	-268	-280	-247	-245	M	G	0.00	0.00	2800.00
401	-224	-222	-253	-264	M	G	0.00	0.00	2800.00
401	-158	-131	-129	-156	M	G	0.00	0.00	2800.00
401	-177	-175	-202	-198	M	G	0.00	0.00	2800.00
401	-175	-171	-199	-202	M	G	0.00	0.00	2800.00
401	-187	-206	-228	-222	M	G	0.00	0.00	2800.00
401	-232	-228	-206	-208	M	G	0.00	0.00	2800.00
401	-187	-156	-154	-177	M	G	0.00	0.00	2800.00
401	-262	-232	-230	-260	M	G	0.00	0.00	2800.00
401	-230	-202	-199	-237	M	G	0.00	0.00	2800.00
401	-154	-156	-129	-123	M	G	0.00	0.00	2800.00
401	-127	-124	-148	-152	M	G	0.00	0.00	2800.00
401	-317	-319	-342	-340	M	G	0.00	0.00	2800.00
401	-319	-328	-359	-342	M	G	0.00	0.00	2800.00
401	-295	-291	-260	-258	M	G	0.00	0.00	2800.00
401	-317	-289	-291	-319	M	G	0.00	0.00	2800.00
401	-289	-262	-260	-291	M	G	0.00	0.00	2800.00
401	-297	-301	-264	-253	M	G	0.00	0.00	2800.00
401	-297	-253	-255	-293	M	G	0.00	0.00	2800.00
401	-325	-358	-357	-330	M	G	0.00	0.00	2800.00
401	-334	-324	-305	-311	M	G	0.00	0.00	2800.00
401	-286	-268	-264	-301	M	G	0.00	0.00	2800.00
401	-334	-355	-354	-324	M	G	0.00	0.00	2800.00
401	-286	-305	-303	-282	M	G	0.00	0.00	2800.00
401	-305	-324	-309	-303	M	G	0.00	0.00	2800.00
401	-307	-313	-274	-276	M	G	0.00	0.00	2800.00
401	-307	-309	-338	-336	M	G	0.00	0.00	2800.00
401	-309	-324	-354	-338	M	G	0.00	0.00	2800.00
401	-287	-257	-266	-284	M	G	0.00	0.00	2800.00
401	-313	-353	-352	-323	M	G	0.00	0.00	2800.00
401	-295	-258	-272	-299	M	G	0.00	0.00	2800.00
401	-278	-270	-315	-326	M	G	0.00	0.00	2800.00
401	-326	-360	-359	-328	M	G	0.00	0.00	2800.00
401	-220	-249	-239	-212	M	G	0.00	0.00	2800.00
401	-239	-249	-278	-272	M	G	0.00	0.00	2800.00
401	-278	-249	-251	-270	M	G	0.00	0.00	2800.00
401	-270	-251	-226	-210	M	G	0.00	0.00	2800.00
401	-99	-87	-116	-121	M	G	0.00	0.00	2800.00
401	-67	-50	-58	-71	M	G	0.00	0.00	2800.00
401	-50	-38	-47	-58	M	G	0.00	0.00	2800.00
401	-55	-79	-87	-47	M	G	0.00	0.00	2800.00
401	-78	-53	-39	-85	M	G	0.00	0.00	2800.00
401	-53	-55	-25	-23	M	G	0.00	0.00	2800.00
401	-55	-47	-11	-25	M	G	0.00	0.00	2800.00
401	-79	-78	-106	-104	M	G	0.00	0.00	2800.00
401	-78	-85	-122	-106	M	G	0.00	0.00	2800.00
401	-39	-34	-73	-85	M	G	0.00	0.00	2800.00
401	-34	-31	-62	-73	M	G	0.00	0.00	2800.00
401	-15	-32	-31	-14	M	G	0.00	0.00	2800.00
401	-32	-60	-62	-31	M	G	0.00	0.00	2800.00
401	-129	-108	-97	-123	M	G	0.00	0.00	2800.00
401	-91	-62	-60	-89	M	G	0.00	0.00	2800.00
401	-91	-108	-110	-93	M	G	0.00	0.00	2800.00
401	-73	-93	-95	-85	M	G	0.00	0.00	2800.00
401	-85	-95	-112	-122	M	G	0.00	0.00	2800.00
401	-17	-27	-21	-16	M	G	0.00	0.00	2800.00
401	-21	-45	-40	-16	M	G	0.00	0.00	2800.00
401	-45	-75	-70	-40	M	G	0.00	0.00	2800.00
401	-127	-102	-100	-124	M	G	0.00	0.00	2800.00
401	-102	-75	-68	-100	M	G	0.00	0.00	2800.00
401	-41	-18	-19	-43	M	G	0.00	0.00	2800.00
401	-68	-51	-57	-65	M	G	0.00	0.00	2800.00
401	-51	-27	-41	-57	M	G	0.00	0.00	2800.00
401	-86	-41	-43	-81	M	G	0.00	0.00	2800.00
401	-200	-199	-171	-173	M	G	0.00	0.00	2800.00
401	-173	-171	-148	-150	M	G	0.00	0.00	2800.00
401	-150	-148	-124	-125	M	G	0.00	0.00	2800.00

Risultati del calcolo

Parametri di calcolo

La modellazione della struttura e la rielaborazione dei risultati del calcolo sono stati effettuati con:

ModeSt ver. 8.80, prodotto da Tecnisoft s.a.s. - Prato

La struttura è stata calcolata utilizzando come solutore agli elementi finiti:
Xfinest ver. 2015, prodotto da Ce.A.S. S.r.l. - Milano

Tipo di normativa: stati limite D.M. 08
Tipo di calcolo: analisi sismica dinamica
Vincoli esterni: Considera sempre vincoli assegnati in modellazione
Schematizzazione piani rigidi: metodo Master-Slave
Modalità di recupero masse secondarie: trasferire all'impalcato più vicino con modifica XY baricentro

Generazione combinazioni

- Lineari: si
- Valuta spostamenti e non sollecitazioni: no
- Buckling: no

Opzioni di calcolo

- Sono state considerate infinitamente rigide le zone di connessione fra travi, pilastri ed elementi bidimensionali con una riduzione del 20%
- Calcolo con offset rigidi dai nodi: no
- Uniformare i carichi variabili: no
- Massimizzare i carichi variabili: no
- Minimo carico da considerare: 0.00 <daN/m>
- Recupero carichi zone rigide: taglio e momento flettente
- Modalità di combinazione momento torcente: disaccoppiare le azioni

Opzioni del solutore

- Tipo di elemento bidimensionale: QF46
- Calcolo sforzo nei nodi: No
- Trascura deformabilità a taglio delle aste: Sì
- Analisi dinamica con metodo di Lanczos: Sì
- Check sequenza di Sturm: Sì
- Analisi non lineare con Newton modificato: No
- Usa formulazione secante per buckling: No
- Trascura buckling torsionale: No
- Soluzione matrice con metodo ver. 5.1: No

Dati struttura

- Zona sismica: zona 4
- Sito di costruzione: LON. 9.23529 LAT. 45.73292
  Contenuto tra ID reticolo: 11152 11151 10930 10929

Simbologia

TCC = Tipo di combinazione di carico
  SLU = Stato limite ultimo
  SLU S = Stato limite ultimo (azione sismica)
  SLE R = Stato limite d'esercizio, combinazione rara
  SLE F = Stato limite d'esercizio, combinazione frequente
  SLE Q = Stato limite d'esercizio, combinazione quasi permanente
  SLD = Stato limite di danno
  SLV = Stato limite di salvaguardia della vita
  SLC = Stato limite di prevenzione del collasso
  SLO = Stato limite di operatività
  SLU I = Stato limite di resistenza al fuoco
T_R = Periodo di ritorno <anni>
Ag = Accelerazione orizzontale massima al sito <g>
FO = Valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale
TC* = Periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale <sec>
S_S = Coefficiente di amplificazione stratigrafica
C_C = Coefficiente funzione della categoria del suolo

TCC	T_R	Ag	FO	TC*	S_S	C_C
SLD	151	0.0345	2.61	0.23	1.50	1.71
SLV	1424	0.0653	2.70	0.31	1.50	1.55

- Tipo di opera: Grande opera
- Vita nominale V_N: 100.00
- Classe d'uso: Classe III
- SL Esercizio: SLO-Pvr no, SLD-Pvr 63.00
- SL Ultimi: SLV-Pvr 10.00, SLC-Pvr no
- Classe di duttilità: Classe B
- Quota di riferimento: 0.00 <m>
- Altezza della struttura: 5.30 <m>
- Numero piani edificio: 1
- Coefficiente θ: 0.00
- Edificio regolare in altezza: si

- Edificio regolare in pianta: si
- Forze orizzontali convenzionali per stati limite non sismici: 1.00%
- Genera stati limite per verifiche di resistenza al fuoco: no

Dati di piano

Simbologia

Imp. = Numero dell'impalcato
Lx = Dimensione del piano in dir. X
Ly = Dimensione del piano in dir. Y
Ex = Eccentricità in dir. X
Ey = Eccentricità in dir. Y
Ea = Eccentricità complessiva

Imp.	Lx <m>	Ly <m>	Ex <m>	Ey <m>	Ea <m>
1	14.04	5.74	0.70	0.29	0.76

Dati di calcolo

- Categoria del suolo di fondazione: C
- Tipologia edificio: c.a. a pendolo inverso

Coeff. C_1	0.05
Periodo T_1	0.17465
Coeff. λ SLD	1.00
Coeff. λ SLV	1.00
Rapporto di sovraresistenza (α_u/α_1)	--
Valore di riferimento del fattore di struttura (q_0)	1.50
Fattore riduttivo (K_w)	1.00
Fattore riduttivo regolarità in altezza (KR)	1.00
Fattore di struttura (q)	1.50

- Categoria topografica: T1 - Superficie pianeggiante, pendii e rilievi isolati con inclinazione media i<=15°
- Coeff. amplificazione topografica S_T: 1.00
- Fattore di struttura per sisma verticale (qv): 1.50
- Modalità di calcolo modi di vibrare: Autovalori
  Numero modi: 3
- Modi da considerare: tali da movimentare una percentuale di massa pari a 85.00%
- Trascura modi con massa movimentata minore di: no

- Smorzamento spettro: 5.00

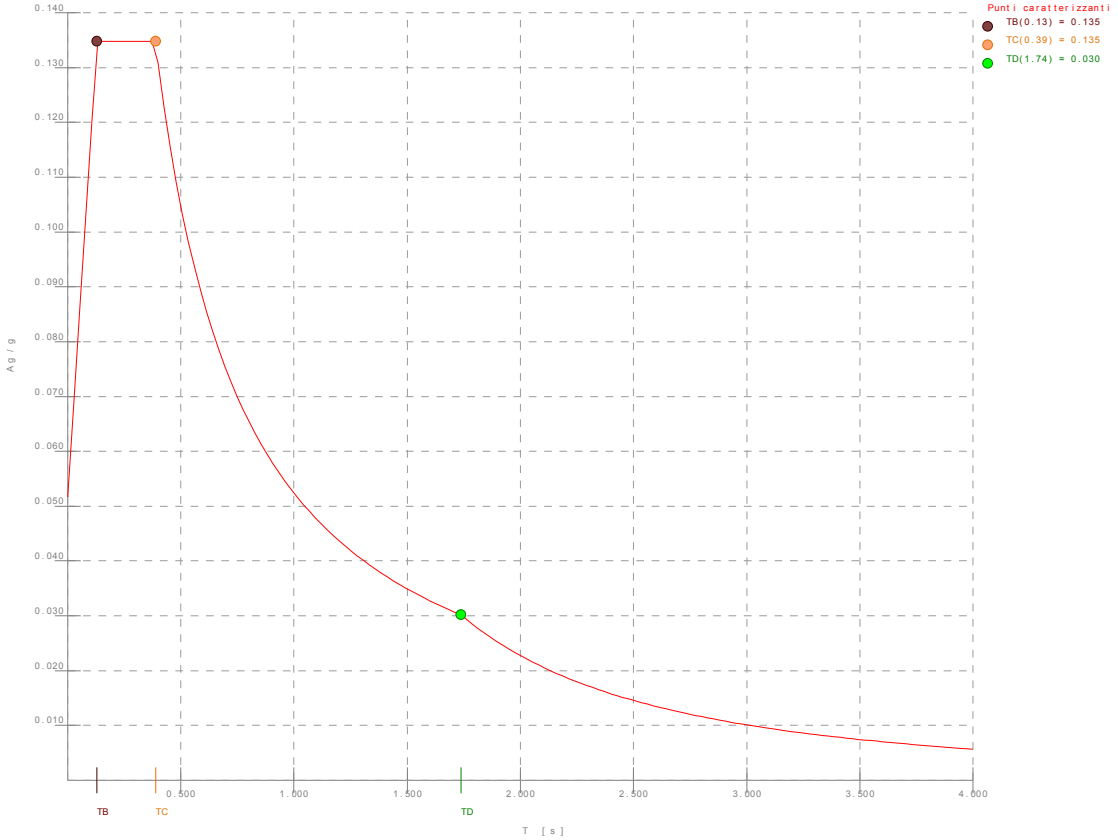


Figura numero 1: Spettro SLD

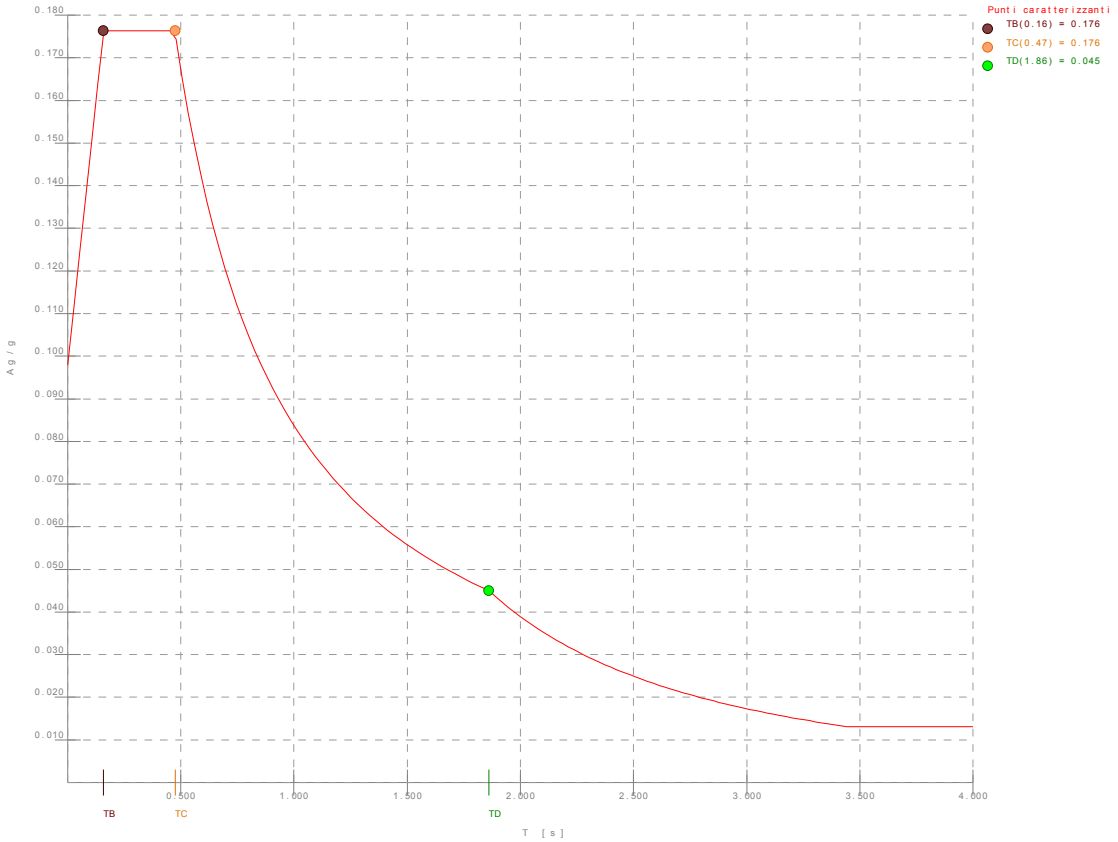


Figura numero 2: Spettro SLV

- Angolo di ingresso del sisma: 0.00 <grad>

Condizioni di carico elementari

Simbologia

CCE = Numero della condizione di carico elementare
Comm. = Commento
Mx = Moltiplicatore della massa in dir. X
My = Moltiplicatore della massa in dir. Y
Mz = Moltiplicatore della massa in dir. Z
Jpx = Moltiplicatore del momento d'inerzia intorno all'asse X
Jpy = Moltiplicatore del momento d'inerzia intorno all'asse Y
Jpz = Moltiplicatore del momento d'inerzia intorno all'asse Z
Tipo CCE = Tipo di CCE per calcolo agli stati limite
Sicurezza = Contributo alla sicurezza
F = a favore
S = a sfavore
A = ambigua
Variabilità = Tipo di variabilità
B = di base
I = indipendente
A = ambigua

CCE	Comm.	Mx	My	Mz	Jpx	Jpy	Jpz	Tipo CCE	Sicurezza	Variabilità
1	Permanenti strutturali	1.00	1.00	0.00	0.00	0.00	1.00	21	S	--
2	Permanenti non strutturali	1.00	1.00	0.00	0.00	0.00	1.00	2	S	--
3	Variabili folla	1.00	1.00	0.00	0.00	0.00	1.00	20	S	B
4	Variabili temperatura	1.00	1.00	0.00	0.00	0.00	1.00	13	S	B
5	Variabile piena T=200	1.00	1.00	0.00	0.00	0.00	1.00	22	S	--
6	Variabile piena T=500	1.00	1.00	0.00	0.00	0.00	1.00	22	S	--

Elenco tipi cce definiti

Simbologia

Tipo CCE = Tipo condizione di carico elementare
Comm. = Commento
Tipo = Tipologia
G = Permanente
Q = Variabile
I = Da ignorare
A = Azione eccezionale
P = Precompressione
Durata = Durata del carico
N = Non definita
P = Permanente
L = Lunga
M = Media
B = Breve
I = Istantanea
γ min. = Coeff. $\gamma_{min.}$
γ max = Coeff. γ_{max}
ψ_0 = Coeff. ψ_0
ψ_1 = Coeff. ψ_1
ψ_2 = Coeff. ψ_2
$\psi_{0,s}$ = Coeff. ψ_0 sismico (D.M. 96)

Tipo CCE	Comm.	Tipo	Durata	γ min.	γ max	ψ_0	ψ_1	ψ_2	$\psi_{0,s}$
1	D.M. 08 Permanenti strutturali	G	N	1.00	1.35				
2	D.M. 08 Permanenti non strutturali	G	N	0.00	1.50				
3	D.M. 08 Variabili Categoria A Ambienti ad uso residenziale	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
4	D.M. 08 Variabili Categoria B Uffici	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
5	D.M. 08 Variabili Categoria C Ambienti suscettibili di affollamento	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
6	D.M. 08 Variabili Categoria D Ambienti ad uso commerciale	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
7	D.M. 08 Variabili Categoria E Biblioteche, archivi, magazzini e ambienti ad uso industriale	Q	N	0.00	1.50	1.00	0.90	0.80	0.00
8	D.M. 08 Variabili Categoria F Rimesse e parcheggi (per autoveicoli di peso <= 30 kN)	Q	N	0.00	1.50	0.70	0.70	0.60	0.00
9	D.M. 08 Variabili Categoria G Rimesse e parcheggi (per autoveicoli di peso > 30 kN)	Q	N	0.00	1.50	0.70	0.50	0.30	0.00
10	D.M. 08 Variabili Vento	Q	N	0.00	1.50	0.60	0.20	0.00	0.00
11	D.M. 08 Variabili Neve (a quota <= 1000 m s.l.m.)	Q	N	0.00	1.50	0.50	0.20	0.00	0.00
12	D.M. 08 Variabili Neve (a quota > 1000 m s.l.m.)	Q	N	0.00	1.50	0.70	0.50	0.20	0.00
13	D.M. 08 Variabili Variazioni termiche	Q	N	0.00	1.50	0.60	0.50	0.00	0.00
14	D.M. 96 Permanenti	G	N	1.00	1.40				
15	D.M. 96 Variabili Abitazioni	Q	P	0.00	1.50	0.70	0.50	0.20	0.70
16	D.M. 96 Variabili Uffici, negozi, scuole, ecc.	Q	N	0.00	1.50	0.70	0.60	0.30	0.70
17	D.M. 96 Variabili Autorimesse	Q	N	0.00	1.50	0.70	0.70	0.60	0.70
18	D.M. 96 Variabili Vento	Q	N	0.00	1.50	0.70	0.20	0.00	0.00
19	D.M. 08 Variabili Categoria H - Coperture	Q	N	0.00	1.50	0.00	0.00	0.00	1.00
20	D.M. 08 Variabile Folla schema 5	Q	N	0.00	1.35	0.40	0.40	0.00	0.00
21	D.M. 08 Permanenti strutturali PONTI	G	N	1.00	1.35				
22	Azione di piena	A	N	0.00	1.50				

Ambienti di carico

Simbologia

N Numero
Comm. Commento
5 Variabile piena T=200

1 Permanenti strutturali
2 Permanenti non strutturali
3 Variabili folla
4 Variabili temperatura
5 Variabile piena T=200
6 Variabile piena T=500
F azioni orizzontali convenzionali
SLU Stato limite ultimo
SLR Stato limite per combinazioni rare
SLF Stato limite per combinazioni frequenti
SLQ Stato limite per combinazioni quasi permanenti o di danno

N	Comm.	1	2	3	4	5	6	S	SLU	SLR	SLF	SLQ
1	Calcolo sismico	si	si	si	si	si	si	si	si	no	no	no
2	Calcolo statico	si	si	si	si	si	si	no	si	si	si	si

Elenco combinazioni di carico simboliche

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco

CC	Comm.	TCC	1	2	3	4	5	6	S
1	Amb. 1 (Sisma)	SLU S	1	1	ψ_2	ψ_2	ψ_2	ψ_2	1
2	Amb. 2 (SLU)	SLU	γ max	γ max	γ max	γ max	1	1	-----
3	Amb. 2 (SLE R)	SLE R	1	1	1	1	1	1	-----
4	Amb. 2 (SLE F)	SLE F	1	1	ψ_1	ψ_1	1	1	-----
5	Amb. 2 (SLE Q)	SLE Q	1	1	ψ_2	ψ_2	1	1	-----

Genera le combinazioni con un solo carico di tipo variabile come di base: no

Considera sollecitazioni dinamiche con segno dei modi principali: no

Combinazioni delle cce

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Comm. = Commento
TCC = Tipo di combinazione di carico
SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco
An. = Tipo di analisi
L = Lineare
NL = Non lineare
Bk = Buckling
S = Si
N = No

CC	Comm.	TCC	An.	Bk	1	2	3	4	5	6	Mt	±S X	±S Y
1	CC 1 - Amb. 1 (SLU S) S Mt+X+0.3Y	SLV	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	1.00	0.30
2	CC 2 - Amb. 1 (SLE) S Mt+X+0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	1.00	0.30
3	CC 3 - Amb. 1 (SLU S) S Mt+X-0.3Y	SLV	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	1.00	-0.30
4	CC 4 - Amb. 1 (SLE) S Mt+X-0.3Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	1.00	-0.30
5	CC 5 - Amb. 1 (SLU S) S Mt+0.3X+Y	SLV	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	0.30	1.00
6	CC 6 - Amb. 1 (SLE) S Mt+0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	0.30	1.00
7	CC 7 - Amb. 1 (SLU S) S Mt-0.3X+Y	SLV	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	-0.30	1.00
8	CC 8 - Amb. 1 (SLE) S Mt-0.3X+Y	SLD	L	N	1.00	1.00	0.00	0.00	0.00	0.00	1.00	-0.30	1.00
9	CC 9 - Amb. 1 (SLU S) S -Mt+X+0.3Y	SLV	L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	1.00	0.30

10	CC 10 - Amb. 1 (SLE) S -Mt+X+0.3Y	SLD		L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	1.00	0.30
11	CC 11 - Amb. 1 (SLU S) S -Mt+X-0.3Y	SLV		L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	1.00	-0.30
12	CC 12 - Amb. 1 (SLE) S -Mt+X-0.3Y	SLD		L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	1.00	-0.30
13	CC 13 - Amb. 1 (SLU S) S -Mt+0.3X+Y	SLV		L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	0.30	1.00
14	CC 14 - Amb. 1 (SLE) S -Mt+0.3X+Y	SLD		L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	0.30	1.00
15	CC 15 - Amb. 1 (SLU S) S -Mt-0.3X+Y	SLV		L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	-0.30	1.00
16	CC 16 - Amb. 1 (SLE) S -Mt-0.3X+Y	SLD		L	N	1.00	1.00	0.00	0.00	0.00	0.00	-1.00	-0.30	1.00
17	CC 17 - Amb. 2 (SLU)	SLU		L	N	1.35	1.50	1.35	1.50	0.00	0.00	0.00	0.00	0.00
18	CC 18 - Amb. 2 (SLU)	SLU		L	N	1.35	1.50	0.00	0.00	1.50	0.00	0.00	0.00	0.00
19	CC 19 - Amb. 2 (SLU)	SLU		L	N	1.35	1.50	0.00	0.00	0.00	1.50	0.00	0.00	0.00
20	CC 20 - Amb. 2 (SLE R)	SLE	R	L	N	1.00	1.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00
21	CC 21 - Amb. 2 (SLE R)	SLE	R	L	N	1.00	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00
22	CC 22 - Amb. 2 (SLE F)	SLE	F	L	N	1.00	1.00	0.40	0.50	0.00	0.00	0.00	0.00	0.00
23	CC 23 - Amb. 2 (SLE Q)	SLE	Q	L	N	1.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Elenco baricentri e masse impalcati

Simbologia

Imp. = Numero dell'impalcato
X = Coordinata X
Y = Coordinata Y
Z = Coordinata Z
Mo = Massa orizzontale
Jpz = Momento d'inerzia polare intorno all'asse Z

Imp.	X <m>	Y <m>	Z <m>	Mo <kg>	Jpz <kg*mq>
1	7.02	2.37	5.30	184018.00	5647850.00

Totali masse impalcati

Mo <kg>	Jpz <kg*mq>
184018.00	5647850.00

Elenco forze sismiche di impalcato allo SLD

Simbologia

Imp. = Numero dell'impalcato
cx = Coeff. c in dir. X
cy = Coeff. c in dir. Y
Mz = Momento intorno all'asse Z

Imp.	cx	cy	Mz <daNm>
1	1.00	1.00	18457.30

Totali forze sismiche

Mz <daNm>
18457.30

Elenco forze sismiche di impalcato allo SLV

Imp.	cx	cy	Mz <daNm>
1	1.00	1.00	24132.30

Totali forze sismiche

Mz <daNm>
24132.30

Elenco modi di vibrare, masse partecipanti e coefficienti di partecipazione

Simbologia

Modo = Numero del modo di vibrare
C = * indica che il modo è stato considerato
Per. = Periodo
Diff. = Minima differenza percentuale dagli altri periodi
Φx = Coefficiente di partecipazione in dir. X
Φy = Coefficiente di partecipazione in dir. Y
Φz = Coefficiente di partecipazione in dir. Z
%Mx = Percentuale massa partecipante in dir. X
%My = Percentuale massa partecipante in dir. Y

%Mz = Percentuale massa partecipante in dir. Z
%Jpz = Percentuale momento d'inerzia polare partecipante intorno all'asse Z

Modo	C	Per.	Diff.	Φx	Φy	Φz	%Mx	%My	%Mz	%Jpz
1	*	0.13	337.47	135.65	-0.00	0.00	100.00	0.00	0.00	0.00
2	*	0.03	4.34	-0.00	0.00	0.00	0.00	0.00	0.00	100.00
3	*	0.03	4.34	-0.00	-135.65	0.00	0.00	100.00	0.00	0.00
Tot.cons.							100.00	100.00	0.00	100.00

Elenco coefficienti di risposta

Simbologia

Modo = Numero del modo di vibrare
Sx = Coefficiente di risposta (moltiplicato per 100) in dir. X
Sy = Coefficiente di risposta (moltiplicato per 100) in dir. Y

Stato limite di danno

Modo	Sx	Sy
1	13.38	13.38
2	7.04	7.04
3	6.97	6.97

Stato limite di salvaguardia della vita

Modo	Sx	Sy
1	16.12	16.12
2	11.25	11.25
3	11.19	11.19

Spostamenti dei nodi allo stato limite ultimo

Simbologia

Nodo = Numero del nodo
Sx = Spostamento in dir. X
CC = Numero della combinazione delle condizioni di carico elementari
Sy = Spostamento in dir. Y
Sz = Spostamento in dir. Z
Rx = Rotazione intorno all'asse X
Ry = Rotazione intorno all'asse Y
Rz = Rotazione intorno all'asse Z

Nodo		Sx <cm>	CC	Sy <cm>	CC	Sz <cm>	CC	Rx <rad>	CC	Ry <rad>	CC	Rz <rad>	CC
-502	Max	0.15	9	0.01	5	0.00	13	0.00	13	0.00	9	0.00	19
-502	Min.	-0.15	1	-0.01	13	-0.01	5	0.00	5	0.00	1	0.00	9
-501	Max	0.15	9	0.01	13	0.00	5	0.00	17	0.00	9	0.00	19
-501	Min.	-0.15	1	-0.01	18	-0.00	13	0.00	5	0.00	1	0.00	9
-500	Max	0.15	9	0.01	13	0.00	5	0.00	5	0.00	9	0.00	19
-500	Min.	-0.15	1	-0.01	19	-0.01	13	0.00	13	0.00	1	0.00	9
-499	Max	0.15	1	0.01	5	0.00	5	0.00	13	0.00	1	0.00	19
-499	Min.	-0.15	9	-0.01	13	-0.01	18	0.00	5	0.00	9	0.00	9
-498	Max	0.15	1	0.01	13	0.00	13	0.00	13	0.00	1	0.00	19
-498	Min.	-0.15	9	-0.01	18	-0.01	18	0.00	17	0.00	9	0.00	9
-497	Max	0.15	1	0.01	13	0.00	13	0.00	5	0.00	1	0.00	19
-497	Min.	-0.15	9	-0.01	19	-0.01	19	0.00	13	0.00	9	0.00	9
-496	Max	0.11	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00	1
-496	Min.	-0.12	1	-0.00	18	-0.01	5	0.00	5	0.00	1	0.00	9
-495	Max	0.12	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00	1
-495	Min.	-0.12	1	-0.00	18	-0.00	13	0.00	5	0.00	1	0.00	9
-494	Max	0.12	9	0.00	13	0.00	5	0.00	5	0.00	9	0.00	1
-494	Min.	-0.11	1	-0.01	19	-0.01	13	0.00	13	0.00	1	0.00	9
-493	Max	0.11	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00	1
-493	Min.	-0.12	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00	9
-492	Max	0.12	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00	1
-492	Min.	-0.12	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-491	Max	0.12	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	1
-491	Min.	-0.11	1	-0.01	19	-0.01	17	0.00	13	0.00	1	0.00	9
-490	Max	0.11	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	19
-490	Min.	-0.12	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00	9
-489	Max	0.12	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00	19
-489	Min.	-0.12	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-488	Max	0.12	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	19
-488	Min.	-0.11	1	-0.01	19	-0.01	17	0.00	13	0.00	1	0.00	9
-487	Max	0.11	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	19
-487	Min.	-0.12	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00	9
-486	Max	0.12	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	19
-486	Min.	-0.12	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9

-485	Max	0.12	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00 19
-485	Min.	-0.11	1	-0.01	19	-0.01	17	0.00	13	0.00	1	0.00 9
-484	Max	0.11	9	0.00	5	-0.00	9	0.00	13	0.00	1	0.00 19
-484	Min.	-0.12	1	-0.00	18	-0.01	17	0.00	5	0.00	9	0.00 13
-483	Max	0.12	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00 19
-483	Min.	-0.12	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00 9
-482	Max	0.12	9	0.00	13	-0.00	1	0.00	5	0.00	1	0.00 19
-482	Min.	-0.11	1	-0.01	19	-0.01	17	0.00	13	0.00	9	0.00 13
-481	Max	0.11	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00 19
-481	Min.	-0.12	9	-0.00	13	-0.01	17	0.00	5	0.00	9	0.00 9
-480	Max	0.12	1	0.00	5	-0.00	13	0.00	13	0.00	1	0.00 19
-480	Min.	-0.12	9	-0.00	18	-0.00	17	0.00	5	0.00	9	0.00 9
-479	Max	0.12	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00 19
-479	Min.	-0.11	9	-0.01	19	-0.01	17	0.00	13	0.00	9	0.00 9
-478	Max	0.11	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00 19
-478	Min.	-0.12	9	-0.00	13	-0.01	18	0.00	5	0.00	9	0.00 9
-477	Max	0.12	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00 19
-477	Min.	-0.12	9	-0.00	18	-0.00	17	0.00	5	0.00	9	0.00 9
-476	Max	0.12	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00 19
-476	Min.	-0.11	9	-0.01	19	-0.01	19	0.00	13	0.00	9	0.00 9
-475	Max	0.11	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00 1
-475	Min.	-0.12	9	-0.00	13	-0.01	18	0.00	5	0.00	9	0.00 9
-474	Max	0.12	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00 1
-474	Min.	-0.12	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00 9
-473	Max	0.12	1	0.00	13	0.00	13	0.00	5	0.00	1	0.00 1
-473	Min.	-0.11	9	-0.01	19	-0.01	19	0.00	13	0.00	9	0.00 9
-472	Max	0.11	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00 1
-472	Min.	-0.12	9	-0.00	13	-0.01	18	0.00	5	0.00	9	0.00 9
-471	Max	0.12	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00 1
-471	Min.	-0.12	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00 9
-470	Max	0.12	1	0.00	13	0.00	13	0.00	5	0.00	1	0.00 1
-470	Min.	-0.11	9	-0.01	19	-0.01	19	0.00	13	0.00	9	0.00 9
-469	Max	0.07	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00 1
-469	Min.	-0.09	1	-0.00	18	-0.01	5	0.00	5	0.00	1	0.00 9
-468	Max	0.08	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00 1
-468	Min.	-0.08	1	-0.00	18	-0.00	13	0.00	5	0.00	1	0.00 9
-467	Max	0.09	9	0.00	13	0.00	5	0.00	5	0.00	9	0.00 1
-467	Min.	-0.07	1	-0.01	19	-0.01	13	0.00	13	0.00	1	0.00 9
-466	Max	0.07	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00 1
-466	Min.	-0.09	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00 9
-465	Max	0.08	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00 1
-465	Min.	-0.08	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00 9
-464	Max	0.09	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00 1
-464	Min.	-0.07	1	-0.00	19	-0.01	17	0.00	13	0.00	1	0.00 9
-463	Max	0.07	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00 1
-463	Min.	-0.09	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00 9
-462	Max	0.08	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00 1
-462	Min.	-0.08	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00 9
-461	Max	0.09	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00 1
-461	Min.	-0.07	1	-0.00	19	-0.01	17	0.00	13	0.00	1	0.00 9
-460	Max	0.07	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00 19
-460	Min.	-0.09	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00 9
-459	Max	0.08	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00 1
-459	Min.	-0.08	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00 9
-458	Max	0.09	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00 19
-458	Min.	-0.07	1	-0.00	19	-0.01	17	0.00	13	0.00	1	0.00 9
-457	Max	0.07	9	0.00	5	-0.00	9	0.00	13	0.00	1	0.00 19
-457	Min.	-0.09	1	-0.00	18	-0.01	17	0.00	5	0.00	9	0.00 13
-456	Max	0.08	1	0.00	5	-0.00	13	0.00	13	0.00	9	0.00 19
-456	Min.	-0.08	9	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00 9
-455	Max	0.09	9	0.00	13	-0.00	1	0.00	5	0.00	1	0.00 19
-455	Min.	-0.07	1	-0.00	19	-0.01	17	0.00	13	0.00	9	0.00 13
-454	Max	0.07	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00 19
-454	Min.	-0.09	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00 9
-453	Max	0.08	1	0.00	5	-0.00	13	0.00	13	0.00	1	0.00 19
-453	Min.	-0.08	9	-0.00	18	-0.00	17	0.00	5	0.00	9	0.00 9
-452	Max	0.09	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00 19
-452	Min.	-0.07	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00 9
-451	Max	0.07	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00 1
-451	Min.	-0.09	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00 9
-450	Max	0.08	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00 1
-450	Min.	-0.08	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00 9
-449	Max	0.09	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00 1
-449	Min.	-0.07	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00 9
-448	Max	0.07	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00 1
-448	Min.	-0.09	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00 9
-447	Max	0.08	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00 1
-447	Min.	-0.08	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00 9
-446	Max	0.09	1	0.00	13	0.00	13	0.00	5	0.00	1	0.00 1
-446	Min.	-0.07	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00 9
-445	Max	0.07	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00 1
-445	Min.	-0.09	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00 9

-444	Max	0.08	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00	1
-444	Min.	-0.08	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-443	Max	0.09	1	0.00	13	0.00	13	0.00	5	0.00	1	0.00	1
-443	Min.	-0.07	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-442	Max	0.04	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00	1
-442	Min.	-0.06	1	-0.00	18	-0.01	5	0.00	5	0.00	1	0.00	9
-441	Max	0.05	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00	1
-441	Min.	-0.05	1	-0.00	18	-0.00	13	0.00	5	0.00	1	0.00	9
-440	Max	0.06	9	0.00	13	0.00	5	0.00	5	0.00	9	0.00	1
-440	Min.	-0.04	1	-0.00	19	-0.01	13	0.00	13	0.00	1	0.00	9
-439	Max	0.04	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-439	Min.	-0.06	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00	9
-438	Max	0.05	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00	1
-438	Min.	-0.05	1	-0.00	18	-0.00	13	0.00	5	0.00	1	0.00	9
-437	Max	0.06	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	1
-437	Min.	-0.04	1	-0.00	19	-0.01	17	0.00	13	0.00	1	0.00	9
-436	Max	0.04	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-436	Min.	-0.06	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00	9
-435	Max	0.05	9	0.00	5	0.00	5	0.00	13	0.00	9	0.00	1
-435	Min.	-0.05	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-434	Max	0.06	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	1
-434	Min.	-0.04	1	-0.00	19	-0.01	17	0.00	13	0.00	1	0.00	9
-433	Max	0.04	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-433	Min.	-0.06	1	-0.00	18	-0.01	17	0.00	5	0.00	1	0.00	9
-432	Max	0.05	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-432	Min.	-0.05	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-431	Max	0.06	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	1
-431	Min.	-0.04	1	-0.00	19	-0.01	17	0.00	13	0.00	1	0.00	9
-430	Max	0.04	9	0.00	5	-0.00	9	0.00	13	0.00	9	0.00	19
-430	Min.	-0.06	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	13
-429	Max	0.05	1	0.00	5	-0.00	13	0.00	18	0.00	9	0.00	19
-429	Min.	-0.05	9	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-428	Max	0.06	9	0.00	13	-0.00	1	0.00	5	0.00	9	0.00	19
-428	Min.	-0.04	1	-0.00	19	-0.00	17	0.00	13	0.00	1	0.00	13
-427	Max	0.04	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00	1
-427	Min.	-0.06	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-426	Max	0.05	1	0.00	5	-0.00	13	0.00	18	0.00	1	0.00	19
-426	Min.	-0.05	9	-0.00	18	-0.00	17	0.00	5	0.00	9	0.00	9
-425	Max	0.06	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00	1
-425	Min.	-0.04	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-424	Max	0.04	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00	1
-424	Min.	-0.06	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-423	Max	0.05	1	0.00	5	0.00	13	0.00	18	0.00	1	0.00	1
-423	Min.	-0.05	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-422	Max	0.06	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00	1
-422	Min.	-0.04	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-421	Max	0.04	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00	1
-421	Min.	-0.06	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-420	Max	0.05	1	0.00	5	0.00	13	0.00	18	0.00	1	0.00	1
-420	Min.	-0.05	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-419	Max	0.06	1	0.00	13	0.00	13	0.00	5	0.00	1	0.00	1
-419	Min.	-0.04	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-418	Max	0.04	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00	1
-418	Min.	-0.06	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-417	Max	0.05	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00	1
-417	Min.	-0.05	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-416	Max	0.06	1	0.00	13	0.00	13	0.00	5	0.00	1	0.00	1
-416	Min.	-0.04	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-415	Max	0.02	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00	1
-415	Min.	-0.03	1	-0.00	18	-0.00	5	0.00	5	0.00	1	0.00	9
-414	Max	0.03	9	0.00	5	0.00	13	0.00	17	0.00	9	0.00	1
-414	Min.	-0.03	1	-0.00	18	-0.00	5	0.00	5	0.00	1	0.00	9
-413	Max	0.03	9	0.00	13	0.00	5	0.00	5	0.00	9	0.00	1
-413	Min.	-0.02	1	-0.00	19	-0.00	13	0.00	13	0.00	1	0.00	9
-412	Max	0.02	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-412	Min.	-0.03	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-411	Max	0.03	9	0.00	5	0.00	13	0.00	18	0.00	9	0.00	1
-411	Min.	-0.03	1	-0.00	18	-0.00	5	0.00	5	0.00	1	0.00	9
-410	Max	0.03	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	1
-410	Min.	-0.02	1	-0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9
-409	Max	0.02	9	0.00	5	-0.00	13	0.00	18	0.00	9	0.00	1
-409	Min.	-0.03	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-408	Max	0.03	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00	1
-408	Min.	-0.03	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-407	Max	0.03	9	0.00	13	-0.00	5	0.00	19	0.00	9	0.00	1
-407	Min.	-0.02	1	-0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9
-406	Max	0.02	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-406	Min.	-0.03	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-405	Max	0.03	9	0.00	5	-0.00	13	0.00	18	0.00	9	0.00	1
-405	Min.	-0.03	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-404	Max	0.03	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	1
-404	Min.	-0.02	1	-0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9

-403	Max	0.02	9	0.00	5	-0.00	9	0.00	13	0.00	9	0.00	19
-403	Min.	-0.03	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	13
-402	Max	0.03	1	0.00	5	-0.00	13	0.00	13	0.00	1	0.00	19
-402	Min.	-0.03	9	-0.00	18	-0.00	17	0.00	5	0.00	9	0.00	9
-401	Max	0.03	9	0.00	13	-0.00	1	0.00	5	0.00	9	0.00	19
-401	Min.	-0.02	1	-0.00	19	-0.00	18	0.00	13	0.00	1	0.00	13
-400	Max	0.02	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00	1
-400	Min.	-0.03	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-399	Max	0.03	1	0.00	5	-0.00	13	0.00	13	0.00	1	0.00	19
-399	Min.	-0.03	9	-0.00	18	-0.00	17	0.00	5	0.00	9	0.00	9
-398	Max	0.03	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00	1
-398	Min.	-0.02	9	-0.00	19	-0.00	19	0.00	13	0.00	9	0.00	9
-397	Max	0.02	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00	1
-397	Min.	-0.03	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-396	Max	0.03	1	0.00	5	0.00	13	0.00	18	0.00	1	0.00	1
-396	Min.	-0.03	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-395	Max	0.03	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00	1
-395	Min.	-0.02	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-394	Max	0.02	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00	1
-394	Min.	-0.03	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-393	Max	0.03	1	0.00	5	0.00	13	0.00	18	0.00	1	0.00	1
-393	Min.	-0.03	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-392	Max	0.03	1	0.00	13	0.00	13	0.00	19	0.00	1	0.00	1
-392	Min.	-0.02	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-391	Max	0.02	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00	1
-391	Min.	-0.03	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-390	Max	0.03	1	0.00	5	0.00	13	0.00	18	0.00	1	0.00	1
-390	Min.	-0.03	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-389	Max	0.03	1	0.00	13	0.00	13	0.00	19	0.00	1	0.00	1
-389	Min.	-0.02	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-388	Max	0.00	9	0.00	5	0.00	13	0.00	18	0.00	9	0.00	1
-388	Min.	-0.01	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-387	Max	0.01	9	0.00	5	0.00	13	0.00	18	0.00	9	0.00	1
-387	Min.	-0.01	1	-0.00	18	-0.00	5	0.00	5	0.00	1	0.00	9
-386	Max	0.01	9	0.00	13	0.00	5	0.00	19	0.00	9	0.00	1
-386	Min.	-0.00	1	-0.00	19	-0.00	13	0.00	13	0.00	1	0.00	9
-385	Max	0.00	9	0.00	5	-0.00	13	0.00	18	0.00	9	0.00	1
-385	Min.	-0.01	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-384	Max	0.01	9	0.00	5	0.00	13	0.00	18	0.00	9	0.00	1
-384	Min.	-0.01	1	-0.00	18	-0.00	5	0.00	5	0.00	1	0.00	9
-383	Max	0.01	9	0.00	13	-0.00	5	0.00	19	0.00	9	0.00	1
-383	Min.	-0.00	1	-0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9
-382	Max	0.00	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-382	Min.	-0.01	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-381	Max	0.01	9	0.00	5	0.00	13	0.00	18	0.00	9	0.00	1
-381	Min.	-0.01	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-380	Max	0.01	9	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	1
-380	Min.	-0.00	1	-0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9
-379	Max	0.00	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	1
-379	Min.	-0.01	1	-0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-378	Max	0.01	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00	19
-378	Min.	-0.01	1	-0.00	18	-0.00	17	0.00	5	0.00	1	0.00	9
-377	Max	0.01	9	0.00	13	-0.00	5	0.00	19	0.00	9	0.00	1
-377	Min.	-0.00	1	-0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9
-376	Max	0.00	1	0.00	5	-0.00	9	0.00	13	0.00	9	0.00	19
-376	Min.	-0.01	9	-0.00	18	-0.00	18	0.00	5	0.00	1	0.00	9
-375	Max	0.01	1	0.00	5	-0.00	13	0.00	18	0.00	1	0.00	1
-375	Min.	-0.01	9	-0.00	18	-0.00	17	0.00	5	0.00	9	0.00	9
-374	Max	0.01	1	0.00	13	-0.00	1	0.00	5	0.00	9	0.00	19
-374	Min.	-0.00	9	-0.00	19	-0.00	19	0.00	13	0.00	1	0.00	9
-373	Max	0.00	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00	1
-373	Min.	-0.01	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-372	Max	0.01	1	0.00	5	0.00	5	0.00	18	0.00	1	0.00	19
-372	Min.	-0.01	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-371	Max	0.01	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00	1
-371	Min.	-0.00	9	-0.00	19	-0.00	19	0.00	13	0.00	9	0.00	9
-370	Max	0.00	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00	1
-370	Min.	-0.01	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-369	Max	0.01	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00	1
-369	Min.	-0.01	9	-0.00	18	-0.00	18	0.00	17	0.00	9	0.00	9
-368	Max	0.01	1	0.00	13	-0.00	13	0.00	5	0.00	1	0.00	1
-368	Min.	-0.00	9	-0.00	19	-0.00	19	0.00	13	0.00	9	0.00	9
-367	Max	0.00	1	0.00	5	0.00	5	0.00	18	0.00	1	0.00	1
-367	Min.	-0.01	9	-0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-366	Max	0.01	1	0.00	5	0.00	13	0.00	18	0.00	1	0.00	1
-366	Min.	-0.01	9	0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-365	Max	0.01	1	0.00	13	0.00	13	0.00	19	0.00	1	0.00	1
-365	Min.	-0.00	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-364	Max	0.00	1	0.00	5	0.00	5	0.00	18	0.00	1	0.00	1
-364	Min.	-0.01	9	-0.00	18	-0.01	18	0.00	5	0.00	9	0.00	9
-363	Max	0.01	1	0.00	5	0.00	13	0.00	18	0.00	1	0.00	1
-363	Min.	-0.01	9	0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9

-362	Max	0.01	1	0.00	13	0.00	13	0.00	19	0.00	1	0.00	1
-362	Min.	-0.00	9	-0.00	19	-0.01	19	0.00	13	0.00	9	0.00	9
-361	Max	0.00	17	0.00	1	0.00	5	0.00	1	0.00	18	0.00	18
-361	Min.	0.00	20	0.00	17	-0.00	18	0.00	18	0.00	1	0.00	5
-360	Max	0.00	5	0.00	5	0.00	5	0.00	5	0.00	13	0.00	1
-360	Min.	0.00	18	0.00	18	-0.00	18	0.00	18	0.00	19	0.00	9
-359	Max	0.00	9	0.00	5	0.00	5	0.00	5	0.00	9	0.00	5
-359	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	19	0.00	18
-358	Max	0.00	18	0.00	5	-0.00	5	0.00	5	0.00	5	0.00	1
-358	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	18	0.00	18
-357	Max	0.00	18	0.00	17	-0.00	5	0.00	17	0.00	1	0.00	1
-357	Min.	0.00	19	0.00	18	-0.00	18	0.00	13	0.00	18	0.00	18
-356	Max	0.00	20	0.00	17	-0.00	5	0.00	17	0.00	19	0.00	9
-356	Min.	0.00	19	0.00	18	-0.00	18	0.00	13	0.00	1	0.00	1
-355	Max	0.00	9	0.00	17	-0.00	5	0.00	5	0.00	18	0.00	19
-355	Min.	0.00	19	0.00	18	-0.00	18	0.00	18	0.00	1	0.00	9
-354	Max	0.00	9	0.00	13	-0.00	5	0.00	1	0.00	9	0.00	1
-354	Min.	0.00	18	0.00	18	-0.00	18	0.00	18	0.00	1	0.00	9
-353	Max	0.00	9	0.00	13	0.00	5	0.00	9	0.00	19	0.00	18
-353	Min.	0.00	19	0.00	18	-0.00	18	0.00	18	0.00	5	0.00	9
-352	Max	0.00	9	0.00	5	0.00	5	0.00	5	0.00	9	0.00	1
-352	Min.	0.00	19	0.00	18	-0.00	18	0.00	18	0.00	1	0.00	9
-351	Max	0.00	18	0.00	5	0.00	13	0.00	1	0.00	13	0.00	1
-351	Min.	0.00	1	0.00	18	-0.00	18	0.00	18	0.00	19	0.00	18
-350	Max	0.00	18	0.00	5	-0.00	13	0.00	9	0.00	9	0.00	1
-350	Min.	0.00	1	0.00	18	-0.00	18	0.00	18	0.00	1	0.00	9
-349	Max	0.00	17	0.00	17	-0.00	13	0.00	13	0.00	9	0.00	19
-349	Min.	0.00	21	0.00	19	-0.00	18	0.00	18	0.00	18	0.00	9
-348	Max	0.00	17	0.00	17	-0.00	13	0.00	17	0.00	9	0.00	9
-348	Min.	0.00	19	0.00	19	-0.00	18	0.00	5	0.00	19	0.00	1
-347	Max	0.00	17	0.00	17	-0.00	13	0.00	17	0.00	18	0.00	19
-347	Min.	0.00	19	0.00	19	-0.00	19	0.00	5	0.00	9	0.00	9
-346	Max	0.00	17	0.00	13	-0.00	13	0.00	13	0.00	19	0.00	19
-346	Min.	0.00	19	0.00	19	-0.00	19	0.00	19	0.00	13	0.00	9
-345	Max	0.00	17	0.00	13	0.00	13	0.00	13	0.00	18	0.00	19
-345	Min.	0.00	21	0.00	19	-0.00	19	0.00	19	0.00	1	0.00	13
-344	Max	0.00	19	0.00	13	0.00	13	0.00	13	0.00	18	0.00	1
-344	Min.	0.00	13	0.00	19	-0.00	19	0.00	19	0.00	5	0.00	9
-343	Max	0.00	21	0.00	9	0.00	13	0.00	9	0.00	9	0.00	13
-343	Min.	0.00	17	0.00	17	-0.00	19	0.00	19	0.00	19	0.00	19
-342	Max	0.00	20	0.00	5	0.00	13	0.00	5	0.00	5	0.00	1
-342	Min.	0.00	17	0.00	18	-0.00	19	0.00	18	0.00	18	0.00	9
-341	Max	0.00	17	0.00	13	0.00	5	0.00	13	0.00	19	0.00	1
-341	Min.	0.00	21	0.00	19	-0.00	18	0.00	19	0.00	13	0.00	9
-340	Max	0.00	18	0.00	5	0.00	13	0.00	5	0.00	5	0.00	1
-340	Min.	0.00	17	0.00	18	-0.00	19	0.00	18	0.00	13	0.00	18
-339	Max	0.00	17	0.00	13	0.00	5	0.00	13	0.00	19	0.00	19
-339	Min.	0.00	19	0.00	19	-0.00	18	0.00	19	0.00	13	0.00	9
-338	Max	0.00	9	0.00	13	0.00	1	0.00	1	0.00	9	0.00	18
-338	Min.	0.00	18	0.00	18	-0.00	19	0.00	18	0.00	19	0.00	9
-337	Max	0.00	18	0.00	5	0.00	9	0.00	9	0.00	19	0.00	1
-337	Min.	0.00	1	0.00	18	-0.00	19	0.00	18	0.00	1	0.00	18
-336	Max	0.00	9	0.00	13	0.00	1	0.00	9	0.00	18	0.00	1
-336	Min.	0.00	18	0.00	18	-0.00	19	0.00	18	0.00	5	0.00	18
-335	Max	0.00	18	0.00	5	0.00	9	0.00	1	0.00	13	0.00	18
-335	Min.	0.00	1	0.00	18	-0.00	19	0.00	18	0.00	18	0.00	9
-334	Max	0.00	9	0.00	17	-0.00	5	0.00	1	0.00	18	0.00	1
-334	Min.	0.00	19	0.00	18	-0.00	18	0.00	9	0.00	1	0.00	18
-333	Max	0.00	17	0.00	17	-0.00	13	0.00	9	0.00	9	0.00	18
-333	Min.	0.00	1	0.00	18	-0.00	18	0.00	1	0.00	18	0.00	9
-332	Max	0.00	9	0.00	17	-0.00	1	0.00	19	0.00	19	0.00	17
-332	Min.	0.00	17	0.00	18	-0.00	18	0.00	13	0.00	9	0.00	18
-331	Max	0.00	17	0.00	17	-0.00	9	0.00	19	0.00	1	0.00	19
-331	Min.	0.00	21	0.00	19	-0.00	18	0.00	5	0.00	18	0.00	17
-330	Max	0.00	20	0.00	17	-0.00	9	0.00	19	0.00	5	0.00	9
-330	Min.	0.00	17	0.00	18	-0.00	18	0.00	13	0.00	18	0.00	1
-329	Max	0.00	17	0.00	17	-0.00	1	0.00	17	0.00	18	0.00	9
-329	Min.	0.00	21	0.00	19	-0.00	18	0.00	5	0.00	13	0.00	1
-328	Max	0.00	1	0.00	5	0.00	13	0.00	5	0.00	9	0.00	1
-328	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	19	0.00	9
-327	Max	0.00	19	0.00	13	0.00	5	0.00	13	0.00	18	0.00	1
-327	Min.	0.00	9	0.00	19	-0.00	18	0.00	5	0.00	1	0.00	9
-319	Max	0.00	9	0.00	5	0.00	13	0.00	5	0.00	5	0.00	1
-319	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	13	0.00	9
-318	Max	0.00	17	0.00	13	0.00	5	0.00	13	0.00	5	0.00	1
-318	Min.	0.00	1	0.00	19	-0.00	18	0.00	5	0.00	13	0.00	9
-317	Max	0.00	20	0.00	5	0.00	13	0.00	19	0.00	19	0.00	1
-317	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	13	0.00	9
-316	Max	0.00	17	0.00	13	0.00	5	0.00	17	0.00	5	0.00	1
-316	Min.	0.00	21	0.00	19	-0.00	18	0.00	5	0.00	18	0.00	9
-315	Max	0.00	1	0.00	5	0.00	1	0.00	19	0.00	18	0.00	1
-315	Min.	0.00	18	0.00	18	-0.00	18	0.00	13	0.00	1	0.00	18

-314	Max	0.00	19	0.00	13	0.00	9	0.00	13	0.00	9	0.00	19
-314	Min.	0.00	9	0.00	19	-0.00	19	0.00	5	0.00	19	0.00	9
-313	Max	0.00	9	0.00	13	0.00	1	0.00	13	0.00	18	0.00	1
-313	Min.	0.00	18	0.00	18	-0.00	19	0.00	5	0.00	1	0.00	18
-312	Max	0.00	18	0.00	5	0.00	9	0.00	5	0.00	9	0.00	18
-312	Min.	0.00	1	0.00	18	-0.00	19	0.00	13	0.00	18	0.00	9
-311	Max	0.00	9	0.00	17	-0.00	5	0.00	19	0.00	18	0.00	19
-311	Min.	0.00	19	0.00	18	-0.00	18	0.00	9	0.00	1	0.00	9
-310	Max	0.00	17	0.00	17	-0.00	13	0.00	19	0.00	9	0.00	1
-310	Min.	0.00	1	0.00	18	-0.00	18	0.00	1	0.00	18	0.00	17
-309	Max	0.00	9	0.00	5	0.00	1	0.00	19	0.00	1	0.00	9
-309	Min.	0.00	19	0.00	18	-0.00	19	0.00	1	0.00	9	0.00	18
-308	Max	0.00	18	0.00	13	0.00	9	0.00	19	0.00	1	0.00	18
-308	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	9	0.00	1
-307	Max	0.00	9	0.00	13	0.00	1	0.00	9	0.00	18	0.00	18
-307	Min.	0.00	18	0.00	18	-0.00	19	0.00	1	0.00	5	0.00	9
-306	Max	0.00	18	0.00	5	0.00	9	0.00	1	0.00	13	0.00	1
-306	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	18
-305	Max	0.00	9	0.00	5	-0.00	1	0.00	19	0.00	18	0.00	1
-305	Min.	0.00	19	0.00	18	-0.00	18	0.00	9	0.00	1	0.00	18
-304	Max	0.00	18	0.00	13	-0.00	9	0.00	19	0.00	9	0.00	18
-304	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	18	0.00	9
-303	Max	0.00	9	0.00	5	0.00	1	0.00	19	0.00	18	0.00	1
-303	Min.	0.00	19	0.00	18	-0.00	19	0.00	1	0.00	1	0.00	9
-302	Max	0.00	18	0.00	13	0.00	9	0.00	19	0.00	9	0.00	1
-302	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	9
-301	Max	0.00	9	0.00	17	-0.00	1	0.00	19	0.00	19	0.00	1
-301	Min.	0.00	17	0.00	18	-0.00	18	0.00	13	0.00	9	0.00	9
-300	Max	0.00	17	0.00	17	-0.00	9	0.00	19	0.00	1	0.00	1
-300	Min.	0.00	1	0.00	19	-0.00	18	0.00	5	0.00	18	0.00	9
-299	Max	0.00	1	0.00	5	0.00	13	0.00	19	0.00	13	0.00	1
-299	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	19	0.00	9
-298	Max	0.00	17	0.00	13	0.00	5	0.00	17	0.00	17	0.00	1
-298	Min.	0.00	9	0.00	19	-0.00	18	0.00	5	0.00	5	0.00	9
-297	Max	0.00	9	0.00	17	-0.00	9	0.00	19	0.00	5	0.00	17
-297	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	18
-296	Max	0.00	17	0.00	17	-0.00	1	0.00	18	0.00	19	0.00	19
-296	Min.	0.00	21	0.00	19	-0.00	18	0.00	1	0.00	13	0.00	17
-295	Max	0.00	9	0.00	5	0.00	13	0.00	19	0.00	9	0.00	1
-295	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	19	0.00	9
-294	Max	0.00	17	0.00	13	0.00	5	0.00	13	0.00	18	0.00	1
-294	Min.	0.00	1	0.00	19	-0.00	18	0.00	5	0.00	1	0.00	9
-293	Max	0.00	20	0.00	17	-0.00	9	0.00	19	0.00	5	0.00	9
-293	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	1
-292	Max	0.00	17	0.00	17	-0.00	1	0.00	18	0.00	19	0.00	9
-292	Min.	0.00	21	0.00	19	-0.00	18	0.00	1	0.00	13	0.00	1
-291	Max	0.00	20	0.00	5	-0.00	13	0.00	19	0.00	1	0.00	1
-291	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	18	0.00	9
-290	Max	0.00	17	0.00	13	-0.00	5	0.00	17	0.00	19	0.00	1
-290	Min.	0.00	21	0.00	19	-0.00	18	0.00	5	0.00	9	0.00	9
-289	Max	0.00	9	0.00	5	0.00	13	0.00	19	0.00	5	0.00	1
-289	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	18	0.00	18
-288	Max	0.00	17	0.00	13	0.00	5	0.00	17	0.00	19	0.00	19
-288	Min.	0.00	1	0.00	19	-0.00	18	0.00	5	0.00	13	0.00	9
-287	Max	0.00	9	0.00	5	0.00	13	0.00	17	0.00	9	0.00	1
-287	Min.	0.00	1	0.00	18	-0.00	19	0.00	13	0.00	1	0.00	9
-286	Max	0.00	9	0.00	17	-0.00	1	0.00	19	0.00	18	0.00	19
-286	Min.	0.00	19	0.00	18	-0.00	18	0.00	9	0.00	9	0.00	9
-285	Max	0.00	17	0.00	17	-0.00	9	0.00	19	0.00	1	0.00	1
-285	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	18	0.00	9
-284	Max	0.00	9	0.00	13	0.00	5	0.00	13	0.00	9	0.00	1
-284	Min.	0.00	18	0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-283	Max	0.00	18	0.00	5	0.00	13	0.00	5	0.00	9	0.00	1
-283	Min.	0.00	1	0.00	18	-0.00	19	0.00	13	0.00	1	0.00	9
-282	Max	0.00	9	0.00	5	-0.00	1	0.00	19	0.00	18	0.00	1
-282	Min.	0.00	19	0.00	18	-0.00	19	0.00	9	0.00	9	0.00	18
-281	Max	0.00	18	0.00	13	-0.00	9	0.00	19	0.00	1	0.00	18
-281	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	18	0.00	9
-280	Max	0.00	9	0.00	5	-0.00	1	0.00	19	0.00	18	0.00	1
-280	Min.	0.00	19	0.00	18	-0.00	19	0.00	1	0.00	9	0.00	9
-279	Max	0.00	18	0.00	13	-0.00	9	0.00	19	0.00	1	0.00	1
-279	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	9
-278	Max	0.00	1	0.00	5	0.00	13	0.00	19	0.00	13	0.00	1
-278	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	5	0.00	9
-277	Max	0.00	17	0.00	13	0.00	5	0.00	18	0.00	13	0.00	1
-277	Min.	0.00	9	0.00	19	-0.00	18	0.00	5	0.00	5	0.00	9
-276	Max	0.00	9	0.00	5	0.00	1	0.00	9	0.00	18	0.00	1
-276	Min.	0.00	18	0.00	18	-0.00	19	0.00	1	0.00	9	0.00	18
-275	Max	0.00	18	0.00	13	0.00	9	0.00	1	0.00	1	0.00	18
-275	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	9
-274	Max	0.00	9	0.00	13	0.00	1	0.00	9	0.00	18	0.00	1
-274	Min.	0.00	18	0.00	18	-0.00	19	0.00	1	0.00	1	0.00	9

-273	Max	0.00	18	0.00	5	0.00	9	0.00	1	0.00	9	0.00	1
-273	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	9
-272	Max	0.00	1	0.00	5	0.00	13	0.00	17	0.00	9	0.00	18
-272	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	17	0.00	1
-271	Max	0.00	17	0.00	13	0.00	5	0.00	17	0.00	17	0.00	9
-271	Min.	0.00	9	0.00	19	-0.00	18	0.00	5	0.00	1	0.00	19
-270	Max	0.00	1	0.00	5	0.00	9	0.00	19	0.00	13	0.00	18
-270	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	5	0.00	5
-269	Max	0.00	17	0.00	13	0.00	1	0.00	18	0.00	13	0.00	13
-269	Min.	0.00	9	0.00	19	-0.00	18	0.00	1	0.00	5	0.00	19
-268	Max	0.00	9	0.00	17	-0.00	1	0.00	19	0.00	18	0.00	1
-268	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	9	0.00	9
-267	Max	0.00	17	0.00	17	-0.00	9	0.00	19	0.00	1	0.00	1
-267	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	18	0.00	9
-266	Max	0.00	9	0.00	13	0.00	1	0.00	5	0.00	9	0.00	18
-266	Min.	0.00	18	0.00	18	-0.00	19	0.00	18	0.00	1	0.00	9
-265	Max	0.00	18	0.00	5	0.00	9	0.00	13	0.00	9	0.00	1
-265	Min.	0.00	1	0.00	18	-0.00	19	0.00	18	0.00	1	0.00	18
-264	Max	0.00	9	0.00	17	-0.00	1	0.00	1	0.00	19	0.00	19
-264	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-263	Max	0.00	17	0.00	17	-0.00	9	0.00	9	0.00	1	0.00	1
-263	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	18	0.00	17
-262	Max	0.00	9	0.00	5	-0.00	13	0.00	17	0.00	5	0.00	1
-262	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	18	0.00	9
-261	Max	0.00	17	0.00	13	-0.00	5	0.00	17	0.00	19	0.00	1
-261	Min.	0.00	1	0.00	19	-0.00	18	0.00	5	0.00	13	0.00	9
-260	Max	0.00	9	0.00	5	-0.00	13	0.00	17	0.00	1	0.00	1
-260	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	18	0.00	18
-259	Max	0.00	17	0.00	13	-0.00	5	0.00	17	0.00	19	0.00	19
-259	Min.	0.00	1	0.00	19	-0.00	17	0.00	5	0.00	9	0.00	9
-258	Max	0.00	9	0.00	5	-0.00	13	0.00	17	0.00	9	0.00	1
-258	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	1	0.00	9
-257	Max	0.00	9	0.00	5	0.00	13	0.00	5	0.00	9	0.00	1
-257	Min.	0.00	1	0.00	18	-0.00	17	0.00	18	0.00	1	0.00	9
-256	Max	0.00	17	0.00	13	-0.00	5	0.00	17	0.00	9	0.00	1
-256	Min.	0.00	1	0.00	19	-0.00	17	0.00	5	0.00	1	0.00	9
-255	Max	0.00	9	0.00	5	-0.00	9	0.00	17	0.00	5	0.00	17
-255	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	18
-254	Max	0.00	17	0.00	13	-0.00	1	0.00	17	0.00	19	0.00	19
-254	Min.	0.00	1	0.00	19	-0.00	18	0.00	1	0.00	13	0.00	17
-253	Max	0.00	9	0.00	17	-0.00	9	0.00	1	0.00	1	0.00	1
-253	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	9
-252	Max	0.00	17	0.00	17	-0.00	1	0.00	9	0.00	19	0.00	1
-252	Min.	0.00	1	0.00	19	-0.00	18	0.00	1	0.00	9	0.00	9
-251	Max	0.00	9	0.00	5	0.00	9	0.00	1	0.00	13	0.00	1
-251	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	5	0.00	9
-250	Max	0.00	17	0.00	13	0.00	1	0.00	9	0.00	13	0.00	1
-250	Min.	0.00	1	0.00	19	-0.00	18	0.00	1	0.00	5	0.00	9
-249	Max	0.00	1	0.00	5	0.00	13	0.00	22	0.00	13	0.00	18
-249	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	17	0.00	1
-248	Max	0.00	17	0.00	13	0.00	5	0.00	22	0.00	17	0.00	9
-248	Min.	0.00	9	0.00	19	-0.00	18	0.00	18	0.00	5	0.00	19
-247	Max	0.00	9	0.00	5	-0.00	1	0.00	5	0.00	18	0.00	1
-247	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	9
-246	Max	0.00	9	0.00	13	-0.00	9	0.00	13	0.00	1	0.00	1
-246	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	9
-245	Max	0.00	9	0.00	5	-0.00	1	0.00	1	0.00	18	0.00	19
-245	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	9
-244	Max	0.00	17	0.00	13	-0.00	9	0.00	9	0.00	1	0.00	1
-244	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	9
-243	Max	0.00	9	0.00	5	0.00	1	0.00	1	0.00	18	0.00	1
-243	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	9
-242	Max	0.00	9	0.00	13	0.00	9	0.00	9	0.00	1	0.00	1
-242	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	9
-241	Max	0.00	9	0.00	5	0.00	1	0.00	9	0.00	18	0.00	1
-241	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	5	0.00	9
-240	Max	0.00	9	0.00	13	0.00	9	0.00	1	0.00	13	0.00	1
-240	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	18	0.00	9
-239	Max	0.00	1	0.00	5	0.00	13	0.00	9	0.00	9	0.00	1
-239	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	17	0.00	9
-238	Max	0.00	17	0.00	13	0.00	5	0.00	1	0.00	17	0.00	1
-238	Min.	0.00	9	0.00	19	-0.00	17	0.00	9	0.00	1	0.00	9
-237	Max	0.00	9	0.00	5	-0.00	13	0.00	18	0.00	9	0.00	1
-237	Min.	0.00	17	0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-236	Max	0.00	18	0.00	5	0.00	1	0.00	9	0.00	9	0.00	1
-236	Min.	0.00	1	0.00	18	-0.00	9	0.00	1	0.00	1	0.00	9
-235	Max	0.00	9	0.00	5	0.00	13	0.00	13	0.00	9	0.00	1
-235	Min.	0.00	1	0.00	18	-0.00	17	0.00	17	0.00	1	0.00	9
-234	Max	0.00	9	0.00	13	0.00	9	0.00	1	0.00	9	0.00	1
-234	Min.	0.00	18	0.00	18	-0.00	1	0.00	9	0.00	1	0.00	9
-233	Max	0.00	17	0.00	13	-0.00	5	0.00	19	0.00	9	0.00	1
-233	Min.	0.00	1	0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9

-232	Max	0.00	9	0.00	5	-0.00	9	0.00	13	0.00	5	0.00	17
-232	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	18
-231	Max	0.00	17	0.00	13	-0.00	1	0.00	5	0.00	19	0.00	19
-231	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	13	0.00	17
-230	Max	0.00	9	0.00	5	-0.00	13	0.00	13	0.00	1	0.00	1
-230	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	9
-229	Max	0.00	17	0.00	13	-0.00	5	0.00	5	0.00	1	0.00	1
-229	Min.	0.00	1	0.00	19	-0.00	17	0.00	13	0.00	9	0.00	9
-228	Max	0.00	9	0.00	5	-0.00	9	0.00	13	0.00	5	0.00	1
-228	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	18
-227	Max	0.00	17	0.00	13	-0.00	1	0.00	5	0.00	19	0.00	19
-227	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	13	0.00	9
-226	Max	0.00	9	0.00	5	0.00	9	0.00	13	0.00	13	0.00	1
-226	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	5	0.00	18
-225	Max	0.00	17	0.00	13	0.00	1	0.00	5	0.00	13	0.00	19
-225	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	5	0.00	9
-224	Max	0.00	9	0.00	17	-0.00	1	0.00	1	0.00	18	0.00	1
-224	Min.	0.00	17	0.00	18	-0.00	18	0.00	19	0.00	9	0.00	9
-223	Max	0.00	17	0.00	17	-0.00	9	0.00	9	0.00	1	0.00	1
-223	Min.	0.00	1	0.00	18	-0.00	18	0.00	19	0.00	18	0.00	9
-222	Max	0.00	9	0.00	5	-0.00	9	0.00	13	0.00	1	0.00	19
-222	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	9
-221	Max	0.00	17	0.00	13	-0.00	1	0.00	5	0.00	19	0.00	1
-221	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	9	0.00	9
-220	Max	0.00	1	0.00	5	0.00	9	0.00	9	0.00	13	0.00	17
-220	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	17	0.00	9
-219	Max	0.00	17	0.00	13	0.00	1	0.00	1	0.00	17	0.00	1
-219	Min.	0.00	9	0.00	19	-0.00	18	0.00	18	0.00	5	0.00	17
-218	Max	0.00	9	0.00	5	0.00	1	0.00	1	0.00	18	0.00	19
-218	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	9
-217	Max	0.00	9	0.00	13	0.00	9	0.00	9	0.00	1	0.00	1
-217	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	18
-216	Max	0.00	9	0.00	5	0.00	1	0.00	1	0.00	18	0.00	18
-216	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	5	0.00	9
-215	Max	0.00	9	0.00	13	0.00	9	0.00	9	0.00	13	0.00	1
-215	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	18	0.00	18
-214	Max	0.00	9	0.00	5	0.00	1	0.00	1	0.00	1	0.00	1
-214	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	18
-213	Max	0.00	9	0.00	13	0.00	9	0.00	9	0.00	1	0.00	18
-213	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	9
-212	Max	0.00	1	0.00	5	0.00	13	0.00	13	0.00	9	0.00	9
-212	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	1	0.00	1
-211	Max	0.00	17	0.00	13	0.00	5	0.00	5	0.00	9	0.00	9
-211	Min.	0.00	9	0.00	19	-0.00	17	0.00	13	0.00	1	0.00	1
-210	Max	0.00	9	0.00	5	0.00	9	0.00	13	0.00	18	0.00	17
-210	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	1	0.00	18
-209	Max	0.00	17	0.00	13	0.00	1	0.00	5	0.00	9	0.00	19
-209	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	19	0.00	17
-208	Max	0.00	9	0.00	5	0.00	9	0.00	13	0.00	5	0.00	1
-208	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	18
-207	Max	0.00	17	0.00	13	0.00	1	0.00	5	0.00	19	0.00	19
-207	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	13	0.00	9
-206	Max	0.00	9	0.00	5	0.00	9	0.00	13	0.00	5	0.00	18
-206	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	5
-205	Max	0.00	17	0.00	13	0.00	1	0.00	5	0.00	19	0.00	13
-205	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	13	0.00	19
-204	Max	0.00	9	0.00	5	0.00	1	0.00	5	0.00	9	0.00	1
-204	Min.	0.00	1	0.00	18	-0.00	19	0.00	13	0.00	1	0.00	18
-203	Max	0.00	9	0.00	13	0.00	9	0.00	13	0.00	9	0.00	18
-203	Min.	0.00	1	0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-202	Max	0.00	9	0.00	5	-0.00	9	0.00	13	0.00	19	0.00	1
-202	Min.	0.00	17	0.00	18	-0.00	19	0.00	5	0.00	13	0.00	18
-201	Max	0.00	17	0.00	13	-0.00	1	0.00	5	0.00	5	0.00	19
-201	Min.	0.00	1	0.00	19	-0.00	18	0.00	13	0.00	17	0.00	9
-199	Max	0.00	9	0.00	5	-0.00	13	0.00	18	0.00	9	0.00	1
-199	Min.	0.00	17	0.00	18	-0.00	19	0.00	5	0.00	1	0.00	9
-193	Max	0.00	17	0.00	13	-0.00	5	0.00	19	0.00	9	0.00	1
-193	Min.	0.00	1	0.00	19	-0.00	17	0.00	13	0.00	1	0.00	9
-191	Max	0.00	9	0.00	5	0.00	1	0.00	1	0.00	1	0.00	18
-191	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	9	0.00	9
-190	Max	0.00	9	0.00	13	0.00	9	0.00	9	0.00	1	0.00	1
-190	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	9	0.00	18
-189	Max	0.00	9	0.00	5	-0.00	1	0.00	13	0.00	19	0.00	1
-189	Min.	0.00	17	0.00	18	-0.00	18	0.00	19	0.00	9	0.00	9
-188	Max	0.00	17	0.00	13	-0.00	9	0.00	5	0.00	1	0.00	19
-188	Min.	0.00	1	0.00	18	-0.00	18	0.00	19	0.00	18	0.00	9
-187	Max	0.00	9	0.00	5	-0.00	9	0.00	9	0.00	1	0.00	1
-187	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	9
-186	Max	0.00	17	0.00	13	-0.00	1	0.00	1	0.00	19	0.00	1
-186	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	9	0.00	9
-185	Max	0.00	1	0.00	1	0.00	1	0.00	18	0.00	13	0.00	18
-185	Min.	0.00	17	0.00	18	0.00	18	0.00	9	0.00	17	0.00	1

-184	Max	0.00	17	0.00	9	0.00	9	0.00	19	0.00	17	0.00	9
-184	Min.	0.00	9	0.00	19	0.00	19	0.00	1	0.00	5	0.00	19
-183	Max	0.00	9	0.00	5	0.00	1	0.00	18	0.00	1	0.00	1
-183	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	9	0.00	18
-182	Max	0.00	9	0.00	13	0.00	9	0.00	18	0.00	1	0.00	18
-182	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	9	0.00	9
-181	Max	0.00	9	0.00	5	0.00	1	0.00	18	0.00	1	0.00	18
-181	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	9	0.00	9
-180	Max	0.00	9	0.00	13	0.00	9	0.00	18	0.00	1	0.00	1
-180	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	9	0.00	18
-179	Max	0.00	9	0.00	5	0.00	1	0.00	18	0.00	9	0.00	18
-179	Min.	0.00	1	0.00	18	-0.00	9	0.00	13	0.00	1	0.00	9
-178	Max	0.00	9	0.00	13	0.00	9	0.00	18	0.00	9	0.00	1
-178	Min.	0.00	1	0.00	18	-0.00	1	0.00	5	0.00	1	0.00	18
-177	Max	0.00	9	0.00	5	-0.00	9	0.00	18	0.00	5	0.00	1
-177	Min.	0.00	17	0.00	18	-0.00	19	0.00	1	0.00	18	0.00	17
-176	Max	0.00	17	0.00	13	-0.00	1	0.00	19	0.00	19	0.00	17
-176	Min.	0.00	1	0.00	19	-0.00	18	0.00	9	0.00	13	0.00	9
-175	Max	0.00	1	0.00	5	-0.00	9	0.00	18	0.00	1	0.00	18
-175	Min.	0.00	17	0.00	18	-0.00	19	0.00	5	0.00	9	0.00	1
-174	Max	0.00	17	0.00	13	-0.00	1	0.00	19	0.00	1	0.00	9
-174	Min.	0.00	9	0.00	19	-0.00	18	0.00	13	0.00	9	0.00	19
-173	Max	0.00	9	0.00	5	0.00	9	0.00	18	0.00	9	0.00	1
-173	Min.	0.00	17	0.00	18	-0.00	19	0.00	1	0.00	17	0.00	17
-172	Max	0.00	17	0.00	13	0.00	1	0.00	19	0.00	17	0.00	17
-172	Min.	0.00	1	0.00	19	-0.00	18	0.00	9	0.00	1	0.00	9
-171	Max	0.00	9	0.00	5	-0.00	13	0.00	13	0.00	9	0.00	17
-171	Min.	0.00	17	0.00	18	-0.00	19	0.00	5	0.00	1	0.00	20
-170	Max	0.00	9	0.00	5	0.00	13	0.00	18	0.00	9	0.00	1
-170	Min.	0.00	1	0.00	18	-0.00	19	0.00	13	0.00	1	0.00	9
-169	Max	0.00	17	0.00	13	-0.00	5	0.00	5	0.00	9	0.00	21
-169	Min.	0.00	1	0.00	19	-0.00	18	0.00	13	0.00	1	0.00	17
-168	Max	0.00	9	0.00	5	0.00	1	0.00	18	0.00	9	0.00	1
-168	Min.	0.00	1	0.00	18	-0.00	9	0.00	13	0.00	1	0.00	9
-167	Max	0.00	9	0.00	13	0.00	9	0.00	13	0.00	9	0.00	1
-167	Min.	0.00	1	0.00	18	-0.00	1	0.00	5	0.00	1	0.00	9
-166	Max	0.00	9	0.00	5	0.00	1	0.00	5	0.00	1	0.00	1
-166	Min.	0.00	1	0.00	18	-0.00	19	0.00	13	0.00	9	0.00	9
-165	Max	0.00	9	0.00	5	0.00	1	0.00	1	0.00	9	0.00	1
-165	Min.	0.00	1	0.00	18	-0.00	19	0.00	9	0.00	1	0.00	9
-164	Max	0.00	9	0.00	13	0.00	9	0.00	9	0.00	9	0.00	1
-164	Min.	0.00	1	0.00	18	-0.00	19	0.00	1	0.00	1	0.00	9
-163	Max	0.00	9	0.00	13	0.00	9	0.00	13	0.00	1	0.00	1
-163	Min.	0.00	1	0.00	18	-0.00	19	0.00	5	0.00	9	0.00	18
-162	Max	0.00	9	0.00	5	0.00	1	0.00	5	0.00	1	0.00	1
-162	Min.	0.00	1	0.00	18	-0.00	19	0.00	13	0.00	9	0.00	18
-161	Max	0.00	9	0.00	13	0.00	9	0.00	13	0.00	1	0.00	18
-161	Min.	0.00	1	0.00	18	-0.00	19	0.00	5	0.00	9	0.00	9
-160	Max	0.00	9	0.00	5	0.00	1	0.00	5	0.00	18	0.00	19
-160	Min.	0.00	1	0.00	18	-0.00	18	0.00	19	0.00	9	0.00	9
-159	Max	0.00	9	0.00	13	0.00	9	0.00	13	0.00	1	0.00	1
-159	Min.	0.00	1	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	9
-158	Max	0.00	9	0.00	5	-0.00	1	0.00	9	0.00	19	0.00	18
-158	Min.	0.00	17	0.00	18	-0.00	18	0.00	19	0.00	9	0.00	5
-157	Max	0.00	17	0.00	13	-0.00	9	0.00	1	0.00	1	0.00	13
-157	Min.	0.00	1	0.00	19	-0.00	18	0.00	18	0.00	18	0.00	18
-156	Max	0.00	1	0.00	5	-0.00	9	0.00	13	0.00	1	0.00	1
-156	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	18	0.00	18
-155	Max	0.00	17	0.00	13	-0.00	1	0.00	5	0.00	19	0.00	19
-155	Min.	0.00	9	0.00	19	-0.00	18	0.00	18	0.00	9	0.00	9
-154	Max	0.00	1	0.00	5	-0.00	9	0.00	9	0.00	17	0.00	18
-154	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	19	0.00	9
-153	Max	0.00	17	0.00	13	-0.00	1	0.00	1	0.00	18	0.00	1
-153	Min.	0.00	9	0.00	19	-0.00	19	0.00	18	0.00	17	0.00	18
-152	Max	0.00	9	0.00	5	-0.00	9	0.00	13	0.00	1	0.00	18
-152	Min.	0.00	17	0.00	18	-0.00	18	0.00	19	0.00	9	0.00	5
-151	Max	0.00	17	0.00	13	-0.00	1	0.00	5	0.00	1	0.00	13
-151	Min.	0.00	1	0.00	19	-0.00	19	0.00	13	0.00	9	0.00	19
-150	Max	0.00	9	0.00	5	0.00	9	0.00	9	0.00	1	0.00	17
-150	Min.	0.00	17	0.00	18	-0.00	18	0.00	19	0.00	17	0.00	9
-149	Max	0.00	17	0.00	13	0.00	1	0.00	1	0.00	17	0.00	1
-149	Min.	0.00	1	0.00	19	-0.00	19	0.00	18	0.00	9	0.00	17
-148	Max	0.00	1	0.00	5	-0.00	9	0.00	13	0.00	9	0.00	1
-148	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	1	0.00	18
-147	Max	0.00	1	0.00	5	-0.00	13	0.00	13	0.00	1	0.00	1
-147	Min.	0.00	9	0.00	18	-0.00	18	0.00	19	0.00	9	0.00	9
-146	Max	0.00	17	0.00	13	-0.00	1	0.00	5	0.00	9	0.00	19
-146	Min.	0.00	9	0.00	19	-0.00	19	0.00	13	0.00	1	0.00	9
-145	Max	0.00	9	0.00	17	0.00	9	0.00	9	0.00	13	0.00	20
-145	Min.	0.00	17	0.00	18	-0.00	19	0.00	19	0.00	17	0.00	17
-144	Max	0.00	17	0.00	17	0.00	1	0.00	1	0.00	17	0.00	17
-144	Min.	0.00	1	0.00	19	0.00	18	0.00	19	0.00	5	0.00	19

-143	Max	0.00	1	0.00	5	0.00	1	0.00	1	0.00	9	0.00 18
-143	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	1	0.00 9
-142	Max	0.00	1	0.00	13	0.00	9	0.00	9	0.00	9	0.00 1
-142	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	1	0.00 18
-141	Max	0.00	1	0.00	5	0.00	1	0.00	5	0.00	9	0.00 1
-141	Min.	0.00	9	0.00	18	-0.00	18	0.00	13	0.00	1	0.00 9
-140	Max	0.00	1	0.00	13	0.00	9	0.00	13	0.00	9	0.00 1
-140	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	1	0.00 9
-139	Max	0.00	1	0.00	5	0.00	1	0.00	5	0.00	19	0.00 1
-139	Min.	0.00	9	0.00	18	-0.00	18	0.00	13	0.00	17	0.00 9
-138	Max	0.00	1	0.00	13	0.00	9	0.00	13	0.00	17	0.00 1
-138	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	19	0.00 9
-137	Max	0.00	1	0.00	5	0.00	1	0.00	1	0.00	9	0.00 19
-137	Min.	0.00	9	0.00	18	-0.00	18	0.00	19	0.00	1	0.00 9
-136	Max	0.00	1	0.00	13	0.00	9	0.00	9	0.00	9	0.00 5
-136	Min.	0.00	9	0.00	18	-0.00	18	0.00	19	0.00	1	0.00 18
-135	Max	0.00	1	0.00	5	0.00	9	0.00	1	0.00	1	0.00 1
-135	Min.	0.00	9	0.00	18	-0.00	18	0.00	19	0.00	9	0.00 18
-134	Max	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1	0.00 18
-134	Min.	0.00	9	0.00	18	-0.00	18	0.00	19	0.00	9	0.00 9
-133	Max	0.00	1	0.00	5	0.00	9	0.00	5	0.00	1	0.00 1
-133	Min.	0.00	9	0.00	18	-0.00	18	0.00	13	0.00	9	0.00 9
-132	Max	0.00	1	0.00	13	0.00	1	0.00	13	0.00	1	0.00 1
-132	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	9	0.00 9
-131	Max	0.00	1	0.00	5	-0.00	9	0.00	1	0.00	18	0.00 1
-131	Min.	0.00	17	0.00	18	-0.00	19	0.00	18	0.00	1	0.00 18
-130	Max	0.00	17	0.00	13	-0.00	1	0.00	9	0.00	9	0.00 19
-130	Min.	0.00	9	0.00	18	-0.00	18	0.00	19	0.00	19	0.00 9
-129	Max	0.00	1	0.00	5	-0.00	1	0.00	9	0.00	9	0.00 18
-129	Min.	0.00	17	0.00	18	-0.00	18	0.00	19	0.00	19	0.00 5
-128	Max	0.00	17	0.00	13	-0.00	9	0.00	1	0.00	18	0.00 13
-128	Min.	0.00	9	0.00	19	-0.00	19	0.00	18	0.00	1	0.00 18
-127	Max	0.00	1	0.00	5	-0.00	1	0.00	13	0.00	18	0.00 5
-127	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	1	0.00 18
-126	Max	0.00	17	0.00	13	-0.00	9	0.00	5	0.00	9	0.00 19
-126	Min.	0.00	9	0.00	19	-0.00	19	0.00	13	0.00	19	0.00 13
-124	Max	0.00	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00 18
-124	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	9	0.00 9
-118	Max	0.00	17	0.00	13	-0.00	13	0.00	5	0.00	1	0.00 1
-118	Min.	0.00	9	0.00	19	-0.00	19	0.00	13	0.00	9	0.00 18
-116	Max	0.00	1	0.00	5	0.00	9	0.00	18	0.00	1	0.00 1
-116	Min.	0.00	9	0.00	18	-0.00	18	0.00	13	0.00	9	0.00 18
-115	Max	0.00	1	0.00	13	0.00	1	0.00	18	0.00	1	0.00 18
-115	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	9	0.00 9
-114	Max	0.00	1	0.00	5	0.00	1	0.00	18	0.00	19	0.00 5
-114	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	9	0.00 18
-113	Max	0.00	17	0.00	13	0.00	9	0.00	19	0.00	1	0.00 19
-113	Min.	0.00	9	0.00	19	-0.00	18	0.00	13	0.00	18	0.00 13
-112	Max	0.00	1	0.00	5	-0.00	9	0.00	19	0.00	19	0.00 5
-112	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	1	0.00 18
-111	Max	0.00	17	0.00	13	-0.00	1	0.00	18	0.00	9	0.00 18
-111	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	19	0.00 13
-110	Max	0.00	1	0.00	5	-0.00	9	0.00	19	0.00	18	0.00 18
-110	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	1	0.00 1
-109	Max	0.00	17	0.00	13	-0.00	1	0.00	18	0.00	9	0.00 9
-109	Min.	0.00	9	0.00	19	-0.00	18	0.00	1	0.00	19	0.00 18
-108	Max	0.00	1	0.00	5	-0.00	1	0.00	13	0.00	9	0.00 17
-108	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	19	0.00 9
-107	Max	0.00	17	0.00	13	-0.00	9	0.00	5	0.00	18	0.00 1
-107	Min.	0.00	9	0.00	19	-0.00	19	0.00	13	0.00	1	0.00 17
-106	Max	0.00	1	0.00	5	0.00	9	0.00	18	0.00	9	0.00 1
-106	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	1	0.00 18
-105	Max	0.00	1	0.00	13	0.00	1	0.00	18	0.00	9	0.00 18
-105	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	1	0.00 13
-104	Max	0.00	1	0.00	5	0.00	9	0.00	18	0.00	5	0.00 1
-104	Min.	0.00	9	0.00	18	-0.00	18	0.00	13	0.00	13	0.00 9
-103	Max	0.00	1	0.00	13	0.00	1	0.00	18	0.00	5	0.00 1
-103	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	13	0.00 9
-102	Max	0.00	1	0.00	5	-0.00	1	0.00	18	0.00	13	0.00 9
-102	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	5	0.00 1
-101	Max	0.00	17	0.00	13	-0.00	9	0.00	19	0.00	13	0.00 9
-101	Min.	0.00	9	0.00	19	-0.00	19	0.00	13	0.00	19	0.00 19
-100	Max	0.00	1	0.00	5	-0.00	5	0.00	13	0.00	1	0.00 1
-100	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	9	0.00 9
-99	Max	0.00	1	0.00	5	0.00	5	0.00	18	0.00	1	0.00 1
-99	Min.	0.00	9	0.00	18	-0.00	18	0.00	13	0.00	9	0.00 9
-98	Max	0.00	17	0.00	13	-0.00	13	0.00	5	0.00	1	0.00 1
-98	Min.	0.00	9	0.00	19	-0.00	19	0.00	13	0.00	9	0.00 9
-97	Max	0.00	1	0.00	5	-0.00	1	0.00	18	0.00	13	0.00 20
-97	Min.	0.00	17	0.00	18	-0.00	18	0.00	1	0.00	19	0.00 17
-96	Max	0.00	17	0.00	13	-0.00	9	0.00	19	0.00	18	0.00 17
-96	Min.	0.00	9	0.00	19	-0.00	19	0.00	9	0.00	5	0.00 20

-95	Max	0.00	1	0.00	5	-0.00	9	0.00	19	0.00	19	0.00	18
-95	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	1	0.00	17
-94	Max	0.00	17	0.00	13	-0.00	1	0.00	18	0.00	9	0.00	17
-94	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	19	0.00	18
-93	Max	0.00	1	0.00	5	-0.00	9	0.00	19	0.00	18	0.00	1
-93	Min.	0.00	17	0.00	18	-0.00	19	0.00	9	0.00	1	0.00	9
-92	Max	0.00	17	0.00	13	-0.00	1	0.00	19	0.00	9	0.00	1
-92	Min.	0.00	9	0.00	18	-0.00	19	0.00	1	0.00	19	0.00	9
-91	Max	0.00	1	0.00	5	-0.00	1	0.00	5	0.00	9	0.00	20
-91	Min.	0.00	17	0.00	18	-0.00	19	0.00	17	0.00	1	0.00	17
-90	Max	0.00	17	0.00	13	-0.00	9	0.00	13	0.00	9	0.00	17
-90	Min.	0.00	9	0.00	19	-0.00	19	0.00	17	0.00	1	0.00	20
-89	Max	0.00	1	0.00	5	-0.00	1	0.00	1	0.00	9	0.00	1
-89	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	19	0.00	9
-88	Max	0.00	17	0.00	13	-0.00	9	0.00	9	0.00	18	0.00	1
-88	Min.	0.00	9	0.00	19	-0.00	19	0.00	18	0.00	1	0.00	9
-87	Max	0.00	1	0.00	5	0.00	9	0.00	9	0.00	1	0.00	1
-87	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	9	0.00	9
-86	Max	0.00	1	0.00	5	0.00	1	0.00	18	0.00	5	0.00	1
-86	Min.	0.00	17	0.00	18	-0.00	18	0.00	5	0.00	18	0.00	9
-85	Max	0.00	1	0.00	5	-0.00	9	0.00	1	0.00	19	0.00	1
-85	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-84	Max	0.00	1	0.00	13	-0.00	1	0.00	9	0.00	9	0.00	1
-84	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	19	0.00	9
-83	Max	0.00	17	0.00	13	0.00	9	0.00	19	0.00	19	0.00	1
-83	Min.	0.00	9	0.00	19	-0.00	19	0.00	13	0.00	13	0.00	9
-82	Max	0.00	1	0.00	13	0.00	1	0.00	9	0.00	1	0.00	1
-82	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	9	0.00	9
-81	Max	0.00	1	0.00	17	0.00	9	0.00	1	0.00	5	0.00	18
-81	Min.	0.00	17	0.00	18	0.00	19	0.00	18	0.00	18	0.00	5
-80	Max	0.00	17	0.00	17	0.00	1	0.00	9	0.00	19	0.00	13
-80	Min.	0.00	9	0.00	19	0.00	18	0.00	19	0.00	13	0.00	19
-79	Max	0.00	1	0.00	5	0.00	9	0.00	1	0.00	9	0.00	1
-79	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	1	0.00	9
-78	Max	0.00	1	0.00	5	0.00	9	0.00	1	0.00	9	0.00	1
-78	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	1	0.00	9
-77	Max	0.00	1	0.00	13	0.00	1	0.00	9	0.00	9	0.00	1
-77	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	1	0.00	9
-76	Max	0.00	1	0.00	13	0.00	1	0.00	9	0.00	9	0.00	1
-76	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	1	0.00	9
-75	Max	0.00	1	0.00	5	-0.00	5	0.00	9	0.00	9	0.00	9
-75	Min.	0.00	17	0.00	18	-0.00	18	0.00	17	0.00	1	0.00	1
-74	Max	0.00	17	0.00	13	-0.00	13	0.00	1	0.00	9	0.00	9
-74	Min.	0.00	9	0.00	19	-0.00	19	0.00	17	0.00	1	0.00	1
-73	Max	0.00	1	0.00	5	-0.00	9	0.00	1	0.00	19	0.00	18
-73	Min.	0.00	17	0.00	18	-0.00	19	0.00	18	0.00	1	0.00	17
-72	Max	0.00	17	0.00	13	-0.00	1	0.00	9	0.00	9	0.00	17
-72	Min.	0.00	9	0.00	18	-0.00	19	0.00	18	0.00	19	0.00	18
-71	Max	0.00	1	0.00	5	0.00	9	0.00	1	0.00	1	0.00	1
-71	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-70	Max	0.00	1	0.00	5	-0.00	1	0.00	1	0.00	13	0.00	1
-70	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	19	0.00	9
-69	Max	0.00	17	0.00	13	-0.00	9	0.00	9	0.00	13	0.00	1
-69	Min.	0.00	9	0.00	19	-0.00	19	0.00	19	0.00	5	0.00	9
-68	Max	0.00	1	0.00	5	0.00	5	0.00	1	0.00	1	0.00	1
-68	Min.	0.00	17	0.00	18	-0.00	18	0.00	17	0.00	9	0.00	9
-67	Max	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00	1
-67	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-66	Max	0.00	17	0.00	13	0.00	13	0.00	9	0.00	1	0.00	1
-66	Min.	0.00	9	0.00	19	-0.00	19	0.00	17	0.00	9	0.00	9
-65	Max	0.00	1	0.00	5	0.00	5	0.00	13	0.00	1	0.00	1
-65	Min.	0.00	17	0.00	18	-0.00	18	0.00	17	0.00	18	0.00	9
-64	Max	0.00	17	0.00	13	0.00	13	0.00	5	0.00	19	0.00	1
-64	Min.	0.00	9	0.00	19	-0.00	19	0.00	17	0.00	9	0.00	9
-63	Max	0.00	1	0.00	5	0.00	1	0.00	13	0.00	1	0.00	1
-63	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-62	Max	0.00	1	0.00	5	-0.00	9	0.00	1	0.00	9	0.00	1
-62	Min.	0.00	17	0.00	18	-0.00	19	0.00	18	0.00	1	0.00	9
-61	Max	0.00	17	0.00	13	-0.00	1	0.00	9	0.00	9	0.00	1
-61	Min.	0.00	9	0.00	19	-0.00	19	0.00	18	0.00	1	0.00	9
-60	Max	0.00	1	0.00	5	-0.00	1	0.00	1	0.00	9	0.00	1
-60	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	19	0.00	17
-59	Max	0.00	17	0.00	13	-0.00	9	0.00	9	0.00	18	0.00	19
-59	Min.	0.00	9	0.00	19	-0.00	19	0.00	19	0.00	1	0.00	9
-58	Max	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1	0.00	1
-58	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-57	Max	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1	0.00	1
-57	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	18	0.00	9
-56	Max	0.00	17	0.00	13	0.00	13	0.00	13	0.00	19	0.00	1
-56	Min.	0.00	9	0.00	19	-0.00	19	0.00	19	0.00	9	0.00	9
-55	Max	0.00	1	0.00	13	0.00	9	0.00	9	0.00	5	0.00	1
-55	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	18	0.00	9

-54	Max	0.00	1	0.00	5	0.00	1	0.00	1	0.00	18	0.00	1
-54	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	1	0.00	9
-53	Max	0.00	1	0.00	5	0.00	9	0.00	9	0.00	9	0.00	1
-53	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	18	0.00	9
-52	Max	0.00	1	0.00	13	0.00	1	0.00	1	0.00	18	0.00	1
-52	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	1	0.00	9
-51	Max	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1	0.00	9
-51	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	1
-50	Max	0.00	1	0.00	5	0.00	13	0.00	13	0.00	1	0.00	1
-50	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-49	Max	0.00	17	0.00	13	0.00	13	0.00	13	0.00	1	0.00	9
-49	Min.	0.00	9	0.00	19	-0.00	19	0.00	19	0.00	9	0.00	1
-48	Max	0.00	1	0.00	5	0.00	1	0.00	13	0.00	1	0.00	1
-48	Min.	0.00	9	0.00	18	-0.00	18	0.00	18	0.00	9	0.00	9
-47	Max	0.00	1	0.00	13	0.00	9	0.00	13	0.00	1	0.00	1
-47	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-46	Max	0.00	1	0.00	5	0.00	1	0.00	1	0.00	1	0.00	1
-46	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	9	0.00	9
-45	Max	0.00	1	0.00	5	0.00	5	0.00	5	0.00	18	0.00	1
-45	Min.	0.00	17	0.00	18	-0.00	18	0.00	18	0.00	5	0.00	9
-44	Max	0.00	17	0.00	13	0.00	13	0.00	13	0.00	13	0.00	1
-44	Min.	0.00	9	0.00	19	-0.00	19	0.00	19	0.00	19	0.00	9
-43	Max	0.00	9	0.00	17	0.00	9	0.00	1	0.00	19	0.00	1
-43	Min.	0.00	17	0.00	20	-0.00	19	0.00	9	0.00	9	0.00	18
-42	Max	0.00	17	0.00	17	0.00	1	0.00	9	0.00	1	0.00	19
-42	Min.	0.00	1	0.00	21	-0.00	18	0.00	1	0.00	18	0.00	9
-34	Max	0.00	1	0.00	5	-0.00	13	0.00	5	0.00	19	0.00	1
-34	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	9	0.00	9
-33	Max	0.00	17	0.00	13	-0.00	5	0.00	13	0.00	1	0.00	1
-33	Min.	0.00	9	0.00	18	-0.00	19	0.00	5	0.00	19	0.00	9
-32	Max	0.00	1	0.00	5	-0.00	1	0.00	1	0.00	13	0.00	9
-32	Min.	0.00	17	0.00	18	-0.00	18	0.00	9	0.00	19	0.00	1
-31	Max	0.00	1	0.00	5	-0.00	9	0.00	5	0.00	18	0.00	1
-31	Min.	0.00	17	0.00	18	-0.00	19	0.00	18	0.00	1	0.00	17
-30	Max	0.00	19	0.00	13	-0.00	1	0.00	13	0.00	9	0.00	19
-30	Min.	0.00	9	0.00	19	-0.00	19	0.00	17	0.00	19	0.00	9
-29	Max	0.00	19	0.00	13	-0.00	9	0.00	9	0.00	18	0.00	9
-29	Min.	0.00	9	0.00	19	-0.00	19	0.00	1	0.00	5	0.00	1
-28	Max	0.00	1	0.00	5	0.00	1	0.00	5	0.00	1	0.00	1
-28	Min.	0.00	9	0.00	18	-0.00	18	0.00	13	0.00	9	0.00	9
-27	Max	0.00	9	0.00	5	0.00	5	0.00	5	0.00	1	0.00	9
-27	Min.	0.00	17	0.00	18	-0.00	18	0.00	13	0.00	18	0.00	1
-26	Max	0.00	17	0.00	13	0.00	13	0.00	13	0.00	19	0.00	9
-26	Min.	0.00	1	0.00	19	-0.00	19	0.00	19	0.00	9	0.00	1
-25	Max	0.00	1	0.00	13	0.00	9	0.00	9	0.00	5	0.00	1
-25	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	18	0.00	9
-24	Max	0.00	1	0.00	5	0.00	1	0.00	9	0.00	18	0.00	1
-24	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	13	0.00	9
-23	Max	0.00	1	0.00	13	0.00	9	0.00	19	0.00	1	0.00	20
-23	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	9	0.00	17
-22	Max	0.00	1	0.00	5	0.00	1	0.00	19	0.00	9	0.00	5
-22	Min.	0.00	9	0.00	18	-0.00	18	0.00	1	0.00	1	0.00	18
-21	Max	0.00	1	0.00	5	0.00	5	0.00	5	0.00	9	0.00	1
-21	Min.	0.00	17	0.00	18	-0.00	18	0.00	13	0.00	1	0.00	9
-20	Max	0.00	17	0.00	13	0.00	13	0.00	13	0.00	9	0.00	1
-20	Min.	0.00	9	0.00	19	-0.00	19	0.00	5	0.00	19	0.00	9
-19	Max	0.00	18	0.00	17	0.00	13	0.00	18	0.00	5	0.00	18
-19	Min.	0.00	5	0.00	1	-0.00	19	0.00	1	0.00	13	0.00	5
-18	Max	0.00	18	0.00	5	0.00	5	0.00	19	0.00	5	0.00	9
-18	Min.	0.00	5	0.00	18	-0.00	18	0.00	13	0.00	18	0.00	1
-17	Max	0.00	1	0.00	5	0.00	5	0.00	5	0.00	1	0.00	1
-17	Min.	0.00	17	0.00	18	-0.00	18	0.00	13	0.00	18	0.00	9
-16	Max	0.00	5	0.00	5	-0.00	1	0.00	19	0.00	13	0.00	5
-16	Min.	0.00	18	0.00	18	-0.00	18	0.00	13	0.00	5	0.00	18
-15	Max	0.00	1	0.00	5	-0.00	13	0.00	19	0.00	13	0.00	17
-15	Min.	0.00	18	0.00	18	-0.00	19	0.00	9	0.00	19	0.00	9
-14	Max	0.00	1	0.00	5	-0.00	13	0.00	19	0.00	18	0.00	9
-14	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	9	0.00	1
-13	Max	0.00	1	0.00	1	-0.00	13	0.00	19	0.00	19	0.00	19
-13	Min.	0.00	17	0.00	18	-0.00	19	0.00	13	0.00	9	0.00	17
-12	Max	0.00	1	0.00	13	0.00	9	0.00	19	0.00	1	0.00	1
-12	Min.	0.00	9	0.00	18	-0.00	19	0.00	13	0.00	9	0.00	9
-11	Max	0.00	1	0.00	13	0.00	9	0.00	9	0.00	18	0.00	18
-11	Min.	0.00	9	0.00	18	-0.00	19	0.00	1	0.00	9	0.00	1
-10	Max	0.00	1	0.00	5	0.00	5	0.00	19	0.00	1	0.00	1
-10	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-9	Max	0.00	1	0.00	5	0.00	1	0.00	1	0.00	1	0.00	1
-9	Min.	0.00	9	0.00	18	-0.00	18	0.00	9	0.00	19	0.00	18
-8	Max	0.00	1	0.00	5	0.00	1	0.00	19	0.00	1	0.00	1
-8	Min.	0.00	9	0.00	18	-0.00	18	0.00	5	0.00	9	0.00	9
-7	Max	0.00	19	0.00	9	-0.00	5	0.00	19	0.00	1	0.00	19
-7	Min.	0.00	9	0.00	19	-0.00	19	0.00	5	0.00	19	0.00	20

-6	Max	0.00	19	0.00	13	-0.00	5	0.00	19	0.00	1	0.00	9
-6	Min.	0.00	9	0.00	19	-0.00	19	0.00	5	0.00	18	0.00	1
-5	Max	0.00	19	0.00	13	-0.00	5	0.00	19	0.00	18	0.00	21
-5	Min.	0.00	9	0.00	19	-0.00	19	0.00	1	0.00	5	0.00	17
-4	Max	0.00	19	0.00	13	-0.00	9	0.00	18	0.00	13	0.00	19
-4	Min.	0.00	13	0.00	19	-0.00	19	0.00	5	0.00	5	0.00	13
-3	Max	0.00	17	0.00	13	0.00	13	0.00	13	0.00	19	0.00	1
-3	Min.	0.00	9	0.00	19	-0.00	19	0.00	19	0.00	9	0.00	9
-2	Max	0.00	13	0.00	13	0.00	13	0.00	18	0.00	19	0.00	9
-2	Min.	0.00	19	0.00	19	-0.00	19	0.00	5	0.00	13	0.00	1
-1	Max	0.00	13	0.00	17	0.00	5	0.00	19	0.00	5	0.00	13
-1	Min.	0.00	19	0.00	9	0.00	18	0.00	9	0.00	13	0.00	19
101	Max	0.15	1	0.01	13	0.00	13	0.00	5	0.00	1	0.00	19
101	Min.	-0.15	9	-0.01	19	-0.01	19	0.00	13	0.00	9	0.00	9
102	Max	0.15	1	0.01	13	-0.06	9	0.00	5	0.01	17	0.00	19
102	Min.	-0.15	9	-0.01	5	-0.53	17	0.00	13	0.00	1	0.00	9
103	Max	0.15	1	0.01	13	-0.15	9	0.00	5	0.00	17	0.00	19
103	Min.	-0.15	9	-0.01	5	-1.10	17	0.00	13	0.00	1	0.00	9
104	Max	0.15	1	0.01	13	-0.17	9	0.00	5	0.00	9	0.00	19
104	Min.	-0.15	9	-0.01	5	-1.29	17	0.00	13	0.00	17	0.00	9
105	Max	0.15	1	0.01	13	-0.13	9	0.00	5	0.00	9	0.00	19
105	Min.	-0.15	9	-0.01	5	-1.04	17	0.00	13	-0.00	17	0.00	9
106	Max	0.15	1	0.01	13	-0.04	9	0.00	5	0.00	9	0.00	19
106	Min.	-0.15	9	-0.01	18	-0.44	17	0.00	13	-0.01	17	0.00	9
107	Max	0.15	1	0.01	13	0.00	13	0.00	13	0.00	1	0.00	19
107	Min.	-0.15	9	-0.01	18	-0.00	18	0.00	5	0.00	9	0.00	9
108	Max	0.15	1	0.01	5	-0.04	1	0.00	13	0.01	17	0.00	19
108	Min.	-0.15	9	-0.01	18	-0.44	17	0.00	5	0.00	1	0.00	9
109	Max	0.15	1	0.01	5	-0.13	1	0.00	13	0.00	17	0.00	19
109	Min.	-0.15	9	-0.01	13	-1.04	17	0.00	5	0.00	1	0.00	9
110	Max	0.15	1	0.01	5	-0.17	1	0.00	13	0.00	17	0.00	19
110	Min.	-0.15	9	-0.01	13	-1.29	17	0.00	5	0.00	1	0.00	9
111	Max	0.15	1	0.01	5	-0.15	1	0.00	13	0.00	9	0.00	19
111	Min.	-0.15	9	-0.01	13	-1.10	17	0.00	5	-0.00	17	0.00	9
112	Max	0.15	1	0.01	5	-0.06	1	0.00	13	0.00	9	0.00	19
112	Min.	-0.15	9	-0.01	13	-0.53	17	0.00	5	-0.01	17	0.00	9
113	Max	0.15	1	0.01	5	0.00	5	0.00	13	0.00	1	0.00	19
113	Min.	-0.15	9	-0.01	13	-0.01	18	0.00	5	0.00	9	0.00	9
114	Max	0.15	1	0.01	13	-0.00	13	0.00	5	0.00	1	0.00	19
114	Min.	-0.15	9	-0.01	19	-0.01	19	0.00	13	0.00	9	0.00	9
115	Max	0.15	1	0.01	13	-0.08	9	0.00	5	0.01	17	0.00	19
115	Min.	-0.15	9	-0.01	5	-0.77	17	-0.00	17	0.00	1	0.00	9
116	Max	0.15	1	0.01	13	-0.17	9	0.00	5	0.00	17	0.00	19
116	Min.	-0.15	9	-0.01	5	-1.43	17	-0.00	17	0.00	1	0.00	9
117	Max	0.15	1	0.01	13	-0.19	9	0.00	5	0.00	9	0.00	19
117	Min.	-0.15	9	-0.01	5	-1.65	17	-0.00	17	0.00	17	0.00	9
118	Max	0.15	1	0.01	13	-0.15	9	0.00	5	0.00	9	0.00	19
118	Min.	-0.15	9	-0.01	5	-1.37	17	-0.00	17	-0.00	17	0.00	9
119	Max	0.15	1	0.01	13	-0.06	9	0.00	5	0.00	9	0.00	19
119	Min.	-0.15	9	-0.01	18	-0.66	17	-0.00	17	-0.01	17	0.00	9
120	Max	0.15	1	0.01	13	0.00	13	0.00	13	0.00	1	0.00	19
120	Min.	-0.15	9	-0.01	18	-0.00	17	0.00	5	0.00	9	0.00	9
121	Max	0.15	1	0.01	5	-0.06	1	0.00	13	0.01	17	0.00	19
121	Min.	-0.15	9	-0.01	18	-0.66	17	-0.00	17	0.00	1	0.00	9
122	Max	0.15	1	0.01	5	-0.15	1	0.00	13	0.00	17	0.00	19
122	Min.	-0.15	9	-0.01	13	-1.37	17	-0.00	17	0.00	1	0.00	9
123	Max	0.15	1	0.01	5	-0.19	1	0.00	13	0.00	17	0.00	19
123	Min.	-0.15	9	-0.01	13	-1.65	17	-0.00	17	0.00	1	0.00	9
124	Max	0.15	1	0.01	5	-0.17	1	0.00	13	0.00	9	0.00	19
124	Min.	-0.15	9	-0.01	13	-1.43	17	-0.00	17	-0.00	17	0.00	9
125	Max	0.15	1	0.01	5	-0.08	1	0.00	13	0.00	9	0.00	19
125	Min.	-0.15	9	-0.01	13	-0.77	17	-0.00	17	-0.01	17	0.00	9
126	Max	0.15	1	0.01	5	-0.00	5	0.00	13	0.00	1	0.00	19
126	Min.	-0.15	9	-0.01	13	-0.01	18	0.00	5	0.00	9	0.00	9
127	Max	0.15	1	0.01	13	-0.00	13	0.00	5	0.00	1	0.00	19
127	Min.	-0.15	9	-0.01	19	-0.01	17	0.00	13	0.00	9	0.00	9
128	Max	0.15	1	0.01	13	-0.08	9	0.00	17	0.01	17	0.00	19
128	Min.	-0.15	9	-0.01	5	-0.83	17	0.00	13	0.00	1	0.00	9
129	Max	0.15	1	0.01	13	-0.17	9	0.00	18	0.00	17	0.00	19
129	Min.	-0.15	9	-0.01	5	-1.56	17	0.00	17	0.00	1	0.00	9
130	Max	0.15	1	0.01	13	-0.20	9	0.00	18	0.00	9	0.00	19
130	Min.	-0.15	9	-0.01	5	-1.79	17	0.00	17	0.00	17	0.00	9
131	Max	0.15	1	0.01	13	-0.16	9	0.00	18	0.00	9	0.00	19
131	Min.	-0.15	9	-0.01	5	-1.49	17	0.00	22	-0.00	17	0.00	9
132	Max	0.15	1	0.01	13	-0.06	9	0.00	17	0.00	9	0.00	19
132	Min.	-0.15	9	-0.01	18	-0.71	17	0.00	13	-0.01	17	0.00	9
133	Max	0.15	1	0.01	13	-0.00	13	0.00	13	0.00	1	0.00	19
133	Min.	-0.15	9	-0.01	18	-0.00	17	0.00	5	0.00	9	0.00	9
134	Max	0.15	1	0.01	5	-0.06	1	0.00	17	0.01	17	0.00	19
134	Min.	-0.15	9	-0.01	18	-0.71	17	0.00	5	0.00	1	0.00	9
135	Max	0.15	1	0.01	5	-0.16	1	0.00	18	0.00	17	0.00	19
135	Min.	-0.15	9	-0.01	13	-1.49	17	0.00	22	0.00	1	0.00	9

136	Max	0.15	1	0.01	5	-0.20	1	0.00	18	0.00	17	0.00 19
136	Min.	-0.15	9	-0.01	13	-1.79	17	0.00	17	0.00	1	0.00 9
137	Max	0.15	1	0.01	5	-0.17	1	0.00	18	0.00	9	0.00 19
137	Min.	-0.15	9	-0.01	13	-1.56	17	0.00	17	-0.00	17	0.00 9
138	Max	0.15	1	0.01	5	-0.08	1	0.00	17	0.00	9	0.00 19
138	Min.	-0.15	9	-0.01	13	-0.83	17	0.00	5	-0.01	17	0.00 9
139	Max	0.15	1	0.01	5	-0.00	5	0.00	13	0.00	1	0.00 19
139	Min.	-0.15	9	-0.01	13	-0.01	17	0.00	5	0.00	9	0.00 9
140	Max	0.15	9	0.01	13	-0.00	1	0.00	5	0.00	1	0.00 19
140	Min.	-0.15	1	-0.01	19	-0.01	17	0.00	13	0.00	9	0.00 9
141	Max	0.15	9	0.01	13	-0.07	1	0.00	5	0.01	17	0.00 19
141	Min.	-0.15	1	-0.01	5	-0.71	17	0.00	13	0.00	9	0.00 9
142	Max	0.15	9	0.01	13	-0.15	1	0.00	5	0.00	17	0.00 19
142	Min.	-0.15	1	-0.01	5	-1.47	17	0.00	13	0.00	9	0.00 9
143	Max	0.15	9	0.01	13	-0.18	1	0.00	5	0.00	1	0.00 19
143	Min.	-0.15	1	-0.01	5	-1.73	17	0.00	13	0.00	17	0.00 9
144	Max	0.15	9	0.01	13	-0.14	1	0.00	5	0.00	1	0.00 19
144	Min.	-0.15	1	-0.01	5	-1.40	17	0.00	13	-0.01	17	0.00 9
145	Max	0.15	9	0.01	13	-0.05	1	0.00	5	0.00	1	0.00 19
145	Min.	-0.15	1	-0.01	18	-0.59	17	0.00	13	-0.01	17	0.00 9
146	Max	0.15	9	0.01	13	-0.00	13	0.00	13	0.00	9	0.00 19
146	Min.	-0.15	1	-0.01	18	-0.01	17	0.00	5	0.00	1	0.00 9
147	Max	0.15	9	0.01	5	-0.05	9	0.00	13	0.01	17	0.00 19
147	Min.	-0.15	1	-0.01	18	-0.59	17	0.00	5	0.00	9	0.00 9
148	Max	0.15	9	0.01	5	-0.14	9	0.00	13	0.01	17	0.00 19
148	Min.	-0.15	1	-0.01	13	-1.40	17	0.00	5	0.00	9	0.00 9
149	Max	0.15	9	0.01	5	-0.18	9	0.00	13	0.00	17	0.00 19
149	Min.	-0.15	1	-0.01	13	-1.73	17	0.00	5	0.00	9	0.00 9
150	Max	0.15	9	0.01	5	-0.15	9	0.00	13	0.00	1	0.00 19
150	Min.	-0.15	1	-0.01	13	-1.47	17	0.00	5	-0.00	17	0.00 9
151	Max	0.15	9	0.01	5	-0.07	9	0.00	13	0.00	1	0.00 19
151	Min.	-0.15	1	-0.01	13	-0.71	17	0.00	5	-0.01	17	0.00 9
152	Max	0.15	9	0.01	5	-0.00	9	0.00	13	0.00	1	0.00 19
152	Min.	-0.15	1	-0.01	13	-0.01	17	0.00	5	0.00	9	0.00 9
153	Max	0.15	9	0.01	13	-0.00	5	0.00	5	0.00	9	0.00 19
153	Min.	-0.15	1	-0.01	19	-0.01	17	0.00	13	0.00	1	0.00 9
154	Max	0.15	9	0.01	13	-0.08	1	0.00	5	0.01	17	0.00 19
154	Min.	-0.15	1	-0.01	5	-0.83	17	0.00	17	0.00	9	0.00 9
155	Max	0.15	9	0.01	13	-0.17	1	0.00	17	0.00	17	0.00 19
155	Min.	-0.15	1	-0.01	5	-1.56	17	0.00	19	0.00	9	0.00 9
156	Max	0.15	9	0.01	13	-0.20	1	0.00	17	0.00	1	0.00 19
156	Min.	-0.15	1	-0.01	5	-1.79	17	0.00	19	0.00	17	0.00 9
157	Max	0.15	9	0.01	13	-0.16	1	0.00	22	0.00	1	0.00 19
157	Min.	-0.15	1	-0.01	5	-1.49	17	0.00	19	-0.00	17	0.00 9
158	Max	0.15	9	0.01	13	-0.06	1	0.00	5	0.00	1	0.00 19
158	Min.	-0.15	1	-0.01	18	-0.71	17	0.00	17	-0.01	17	0.00 9
159	Max	0.15	9	0.01	13	-0.00	13	0.00	13	0.00	9	0.00 19
159	Min.	-0.15	1	-0.01	18	-0.00	17	0.00	5	0.00	1	0.00 9
160	Max	0.15	9	0.01	5	-0.06	9	0.00	13	0.01	17	0.00 19
160	Min.	-0.15	1	-0.01	18	-0.71	17	0.00	17	0.00	9	0.00 9
161	Max	0.15	9	0.01	5	-0.16	9	0.00	22	0.00	17	0.00 19
161	Min.	-0.15	1	-0.01	13	-1.49	17	0.00	19	0.00	9	0.00 9
162	Max	0.15	9	0.01	5	-0.20	9	0.00	17	0.00	17	0.00 19
162	Min.	-0.15	1	-0.01	13	-1.79	17	0.00	19	0.00	9	0.00 9
163	Max	0.15	9	0.01	5	-0.17	9	0.00	17	0.00	1	0.00 19
163	Min.	-0.15	1	-0.01	13	-1.56	17	0.00	19	-0.00	17	0.00 9
164	Max	0.15	9	0.01	5	-0.08	9	0.00	13	0.00	1	0.00 19
164	Min.	-0.15	1	-0.01	13	-0.83	17	0.00	17	-0.01	17	0.00 9
165	Max	0.15	9	0.01	5	-0.00	13	0.00	13	0.00	9	0.00 19
165	Min.	-0.15	1	-0.01	13	-0.01	17	0.00	5	0.00	1	0.00 9
166	Max	0.15	9	0.01	13	-0.00	5	0.00	5	0.00	9	0.00 19
166	Min.	-0.15	1	-0.01	19	-0.01	17	0.00	13	0.00	1	0.00 9
167	Max	0.15	9	0.01	13	-0.08	1	0.00	17	0.01	17	0.00 19
167	Min.	-0.15	1	-0.01	5	-0.77	17	0.00	13	0.00	9	0.00 9
168	Max	0.15	9	0.01	13	-0.17	1	0.00	17	0.00	17	0.00 19
168	Min.	-0.15	1	-0.01	5	-1.43	17	0.00	13	0.00	9	0.00 9
169	Max	0.15	9	0.01	13	-0.19	1	0.00	17	0.00	1	0.00 19
169	Min.	-0.15	1	-0.01	5	-1.65	17	0.00	13	0.00	17	0.00 9
170	Max	0.15	9	0.01	13	-0.15	1	0.00	17	0.00	1	0.00 19
170	Min.	-0.15	1	-0.01	5	-1.37	17	0.00	13	-0.00	17	0.00 9
171	Max	0.15	9	0.01	13	-0.06	1	0.00	17	0.00	1	0.00 19
171	Min.	-0.15	1	-0.01	18	-0.66	17	0.00	13	-0.01	17	0.00 9
172	Max	0.15	9	0.01	13	0.00	5	0.00	13	0.00	9	0.00 19
172	Min.	-0.15	1	-0.01	18	-0.00	17	0.00	5	0.00	1	0.00 9
173	Max	0.15	9	0.01	5	-0.06	9	0.00	17	0.01	17	0.00 19
173	Min.	-0.15	1	-0.01	18	-0.66	17	0.00	5	0.00	9	0.00 9
174	Max	0.15	9	0.01	5	-0.15	9	0.00	17	0.00	17	0.00 19
174	Min.	-0.15	1	-0.01	13	-1.37	17	0.00	5	0.00	9	0.00 9
175	Max	0.15	9	0.01	5	-0.19	9	0.00	17	0.00	17	0.00 19
175	Min.	-0.15	1	-0.01	13	-1.65	17	0.00	5	0.00	9	0.00 9
176	Max	0.15	9	0.01	5	-0.17	9	0.00	17	0.00	1	0.00 19
176	Min.	-0.15	1	-0.01	13	-1.43	17	0.00	5	-0.00	17	0.00 9

177	Max	0.15	9	0.01	5	-0.08	9	0.00	17	0.00	1	0.00 19
177	Min.	-0.15	1	-0.01	13	-0.77	17	0.00	5	-0.01	17	0.00 9
178	Max	0.15	9	0.01	5	-0.00	13	0.00	13	0.00	9	0.00 19
178	Min.	-0.15	1	-0.01	13	-0.01	17	0.00	5	0.00	1	0.00 9
179	Max	0.15	9	0.01	13	-0.00	5	0.00	5	0.00	9	0.00 19
179	Min.	-0.15	1	-0.01	19	-0.01	17	0.00	13	0.00	1	0.00 9
180	Max	0.15	9	0.01	13	-0.06	1	0.00	5	0.01	17	0.00 19
180	Min.	-0.15	1	-0.01	5	-0.53	17	0.00	13	0.00	9	0.00 9
181	Max	0.15	9	0.01	13	-0.15	1	0.00	5	0.00	17	0.00 19
181	Min.	-0.15	1	-0.01	5	-1.10	17	0.00	13	0.00	9	0.00 9
182	Max	0.15	9	0.01	13	-0.17	1	0.00	5	0.00	1	0.00 19
182	Min.	-0.15	1	-0.01	5	-1.29	17	0.00	13	0.00	17	0.00 9
183	Max	0.15	9	0.01	13	-0.13	1	0.00	5	0.00	1	0.00 19
183	Min.	-0.15	1	-0.01	5	-1.04	17	0.00	13	-0.00	17	0.00 9
184	Max	0.15	9	0.01	13	-0.04	1	0.00	5	0.00	1	0.00 19
184	Min.	-0.15	1	-0.01	18	-0.44	17	0.00	13	-0.01	17	0.00 9
185	Max	0.15	9	0.01	13	0.00	5	0.00	13	0.00	9	0.00 19
185	Min.	-0.15	1	-0.01	18	-0.00	17	0.00	5	0.00	1	0.00 9
186	Max	0.15	9	0.01	5	-0.04	9	0.00	13	0.01	17	0.00 19
186	Min.	-0.15	1	-0.01	18	-0.44	17	0.00	5	0.00	9	0.00 9
187	Max	0.15	9	0.01	5	-0.13	9	0.00	13	0.00	17	0.00 19
187	Min.	-0.15	1	-0.01	13	-1.04	17	0.00	5	0.00	9	0.00 9
188	Max	0.15	9	0.01	5	-0.17	9	0.00	13	0.00	17	0.00 19
188	Min.	-0.15	1	-0.01	13	-1.29	17	0.00	5	0.00	9	0.00 9
189	Max	0.15	9	0.01	5	-0.15	9	0.00	13	0.00	1	0.00 19
189	Min.	-0.15	1	-0.01	13	-1.10	17	0.00	5	-0.00	17	0.00 9
190	Max	0.15	9	0.01	5	-0.06	9	0.00	13	0.00	1	0.00 19
190	Min.	-0.15	1	-0.01	13	-0.53	17	0.00	5	-0.01	17	0.00 9
191	Max	0.15	9	0.01	5	-0.00	13	0.00	13	0.00	9	0.00 19
191	Min.	-0.15	1	-0.01	13	-0.01	17	0.00	5	0.00	1	0.00 9

Min = -1.79
Max = 0.83

Reazioni vincolari

Simbologia

Nodo = Numero del nodo
Rx = Reazione vincolare (forza) in dir. X
CC = Numero della combinazione delle condizioni di carico elementari
Ry = Reazione vincolare (forza) in dir. Y
Rz = Reazione vincolare (forza) in dir. Z
Mx = Reazione vincolare (momento) intorno all'asse X
My = Reazione vincolare (momento) intorno all'asse Y
Mz = Reazione vincolare (momento) intorno all'asse Z

Nodo		Rx <daN>	CC	Ry <daN>	CC	Rz <daN>	CC	Mx <daNm>	CC	My <daNm>	CC	Mz <daNm>	CC
-326	Max	3540.11	18	7701.91	18	49153.80	19	-1044.03	13	4197.34	19	30.83	17
-326	Min.	1229.37	1	-33.21	5	20794.90	13	-3055.65	19	1781.04	13	-24.96	18
-325	Max	3057.35	17	4574.15	18	74888.00	19	-1230.38	13	5963.20	18	32.02	18
-325	Min.	616.53	20	-1970.14	17	32610.40	9	-3134.52	17	1582.30	5	3.87	1
-324	Max	1529.51	19	2481.49	18	69488.60	19	-246.60	9	-1483.75	1	-1.00	9
-324	Min.	357.53	9	-408.19	17	29724.70	1	-1037.32	17	-5083.59	18	-37.17	18
-323	Max	215.39	19	11050.30	18	52061.40	19	1131.77	18	892.71	1	39.53	9
-323	Min.	-149.36	9	134.26	5	24430.70	13	-2306.67	17	-892.45	9	-39.47	1
-322	Max	-357.64	1	2480.70	18	69774.50	19	-246.67	1	5083.41	18	37.35	18
-322	Min.	-1379.17	18	-408.58	17	29724.80	9	-1037.51	17	1483.59	9	0.99	1
-321	Max	-340.58	21	5558.17	19	71791.20	18	-1161.97	21	-1582.13	13	-3.80	9
-321	Min.	-3057.17	17	-1970.66	17	32611.70	1	-3134.63	17	-6060.19	19	-36.64	19
-320	Max	-1229.21	9	8851.65	19	45669.80	18	-972.82	21	-1781.30	5	32.28	19
-320	Min.	-3712.51	19	-33.57	13	20795.20	5	-2766.86	17	-3856.02	17	-30.82	17
-200	Max	14362.90	17	11108.70	18	62108.30	19	1471.27	19	9808.17	17	94.61	17
-200	Min.	5557.60	1	-739.38	5	24369.90	9	121.44	20	4537.69	13	18.81	1
-198	Max	9814.36	17	6630.83	18	97327.40	19	224.85	5	2697.97	18	68.12	17
-198	Min.	3722.93	9	-1488.95	5	42363.60	9	-904.53	18	-1014.56	17	15.78	9
-197	Max	1512.85	17	3005.24	18	81182.80	19	533.07	9	-1527.76	9	74.36	18
-197	Min.	150.46	9	-365.65	5	32452.50	1	-160.74	1	-7871.85	18	-21.15	1
-196	Max	6151.01	1	43859.50	18	103596.00	17	1102.94	5	17639.10	1	345.27	9
-196	Min.	-6149.91	9	-3750.25	5	52994.20	13	-2280.27	18	-17633.40	9	-344.01	1
-195	Max	-150.18	1	2999.57	18	81368.90	19	532.23	1	7871.22	18	21.29	9
-195	Min.	-1511.74	17	-366.23	13	32455.30	9	-159.57	9	1527.94	1	-74.05	18
-194	Max	-3722.32	1	7859.98	19	92309.00	18	225.26	13	1014.95	17	-15.74	1
-194	Min.	-9813.42	17	-1488.89	13	42364.90	1	-1035.54	19	-2815.81	19	-68.10	17
-192	Max	-5557.07	9	12887.10	19	56088.90	18	1259.82	13	-4538.34	5	-18.78	9
-192	Min.	-14362.10	17	-740.01	13	24369.40	1	-36.14	19	-9808.65	17	-94.58	17
-125	Max	16519.70	17	8104.07	18	65325.30	18	498.24	5	10663.80	18	58.65	17
-125	Min.	6333.51	1	-1347.91	5	24141.80	1	-1572.43	18	5351.45	1	20.36	21
-123	Max	11916.90	17	7663.96	18	102458.00	18	1419.16	19	2804.84	19	-2.81	9
-123	Min.	4469.93	1	-618.10	5	43499.70	1	230.53	13	-1143.73	17	-32.64	17

-122	Max	1865.22	17	2829.08	18	78197.90	18	209.21	13	-490.75	1	3.91	9
-122	Min.	84.44	1	-234.49	5	29754.60	9	-125.65	18	-6168.92	19	-8.65	1
-121	Max	6948.73	9	25525.80	18	126569.00	18	762.44	13	19245.70	9	49.03	9
-121	Min.	-6926.12	1	-4238.11	5	56703.30	13	-2387.20	18	-19193.90	1	-72.92	19
-120	Max	-79.09	9	2800.03	18	78129.40	18	221.86	5	6190.25	19	9.68	9
-120	Min.	-1852.63	17	-230.03	13	29736.10	1	-87.24	18	494.22	9	-4.29	1
-119	Max	-4468.81	9	8742.60	19	102912.00	19	1381.15	13	1146.20	17	33.25	17
-119	Min.	-11914.10	17	-618.09	13	43487.80	9	231.97	5	-1944.09	18	3.72	1
-117	Max	-6332.70	9	9469.50	19	65779.40	19	498.65	13	-5350.64	9	-21.84	20
-117	Min.	-16518.60	17	-1347.88	13	24144.10	9	-1695.58	19	-10827.40	19	-58.64	17
-41	Max	7222.04	17	3785.52	18	56561.90	18	2995.49	18	9047.89	18	-16.95	1
-41	Min.	2827.08	20	-1516.58	5	20210.40	5	667.33	5	2701.15	5	-132.09	18
-40	Max	5965.65	17	6112.10	18	81932.00	18	2372.75	17	3320.09	19	6.59	9
-40	Min.	2325.53	1	428.22	5	33113.30	1	728.33	1	60.81	13	-51.90	1
-39	Max	1409.79	17	1837.97	18	68940.20	18	1492.72	18	-1084.94	9	18.80	17
-39	Min.	188.76	1	-88.64	5	27600.90	9	105.11	1	-4686.79	19	2.33	1
-38	Max	531.00	9	7757.23	18	79127.80	18	2633.89	18	3118.83	9	11.91	9
-38	Min.	-611.50	1	-654.95	13	26373.40	13	-125.83	5	-3233.88	1	-22.59	18
-37	Max	-165.75	9	1797.07	18	69101.20	18	1361.07	18	4566.42	19	-0.09	9
-37	Min.	-1376.93	17	-87.53	13	27552.20	1	82.76	9	977.46	1	-18.42	1
-36	Max	-2323.94	9	6732.64	19	82622.60	19	2370.21	17	-60.70	5	51.85	9
-36	Min.	-5962.47	17	427.81	13	33099.60	9	726.25	9	-1780.38	18	-6.58	1
-35	Max	-2791.10	21	4516.00	19	57253.60	19	3117.20	19	-2700.40	13	138.62	19
-35	Min.	-7221.34	17	-1516.53	13	20210.80	13	667.35	13	-9359.45	19	16.94	9

Sollecitazioni aste

Simbologia

Asta = Numero dell'asta
N1 = Nodo1
N2 = Nodo2
X = Coordinata progressiva rispetto al nodo iniziale
N = Sforzo normale
CC = Numero della combinazione delle condizioni di carico elementari
Ty = Taglio in dir. Y
Mz = Momento flettente intorno all'asse Z
Tz = Taglio in dir. Z
My = Momento flettente intorno all'asse Y
Mx = Momento torcente intorno all'asse X

Asta	N1	N2		X	N	CC	Ty	CC	Mz	CC	Tz	CC	My	CC	Mx	CC
				<cm>	<daN>		<daN>		<daNm>		<daN>		<daNm>		<daNm>	
101	101	102	Max	35.00	0.00	1	0.00	19	0.00	13	5638.62	17	0.00	1	0.00	13
101	101	102	Max	117.00	0.00	1	0.00	19	0.00	5	5011.54	17	4366.56	17	0.00	13
101	101	102	Min.	35.00	-91917.70	17	0.00	13	0.00	19	794.45	21	0.00	1	-0.00	19
101	101	102	Min.	117.00	-91917.70	17	0.00	13	0.00	13	661.65	21	597.00	21	-0.00	19
101	102	103	Max	0.00	0.00	1	0.00	19	0.00	18	3788.93	17	4366.86	17	0.00	13
101	102	103	Max	117.00	0.00	1	0.00	19	0.00	19	2894.20	17	8276.49	17	0.00	13
101	102	103	Min.	0.00	-91917.70	17	0.00	18	0.00	13	549.92	21	597.00	1	-0.00	19
101	102	103	Min.	117.00	-91917.70	17	0.00	18	0.00	5	360.43	21	1129.56	21	-0.00	19
101	103	104	Max	0.00	0.00	1	0.00	5	0.00	13	1461.84	17	8276.65	17	0.00	13
101	103	104	Max	117.00	0.00	1	0.00	5	0.00	5	567.11	17	9463.59	17	0.00	13
101	103	104	Min.	0.00	-91917.70	17	0.00	19	0.00	18	232.97	21	1129.56	1	-0.00	19
101	103	104	Min.	117.00	-91917.70	17	0.00	19	0.00	18	43.49	21	1291.29	21	-0.00	19
101	104	105	Max	0.00	0.00	1	0.00	5	0.00	18	-83.97	9	9463.58	17	0.00	13
101	104	105	Max	117.00	0.00	1	0.00	5	0.00	18	-273.46	9	7927.83	17	0.00	13
101	104	105	Min.	0.00	-91917.70	17	0.00	19	0.00	19	-865.24	17	1291.29	1	-0.00	19
101	104	105	Min.	117.00	-91917.70	17	0.00	19	0.00	19	-1759.97	17	1082.19	21	-0.00	19
101	105	106	Max	0.00	0.00	1	0.00	18	0.00	13	-400.92	9	7927.64	17	0.00	13
101	105	106	Max	117.00	0.00	1	0.00	18	0.00	18	-590.40	9	3669.20	17	0.00	13
101	105	106	Min.	0.00	-91917.70	17	0.00	5	0.00	18	-3192.33	17	1082.19	1	-0.00	19
101	105	106	Min.	117.00	-91917.70	17	0.00	5	0.00	5	-4087.06	17	502.26	21	-0.00	19
101	106	107	Max	0.00	0.00	1	0.00	13	0.00	18	-695.39	9	3668.90	17	0.00	13
101	106	107	Max	67.00	0.00	1	0.00	13	0.00	18	-803.90	9	0.00	9	0.00	13
101	106	107	Min.	0.00	-91917.70	17	0.00	19	0.00	19	-5219.78	17	502.26	9	-0.00	19
101	106	107	Min.	67.00	-91917.70	17	0.00	19	0.00	19	-5732.15	17	0.00	17	-0.00	19
101	107	108	Max	50.00	0.00	1	0.00	18	0.00	18	5732.15	17	0.00	1	0.00	13
101	107	108	Max	117.00	0.00	1	0.00	18	0.00	18	5219.78	17	3668.89	17	0.00	13
101	107	108	Min.	50.00	-91917.70	17	0.00	13	0.00	5	803.90	21	0.00	1	-0.00	19
101	107	108	Min.	117.00	-91917.70	17	0.00	13	0.00	13	695.39	21	502.26	21	-0.00	19
101	108	109	Max	0.00	0.00	1	0.00	18	0.00	13	4087.06	17	3669.20	17	0.00	13
101	108	109	Max	117.00	0.00	1	0.00	18	0.00	18	3192.33	17	7927.64	17	0.00	13
101	108	109	Min.	0.00	-91917.70	17	0.00	5	0.00	18	590.40	21	502.26	9	-0.00	19
101	108	109	Min.	117.00	-91917.70	17	0.00	5	0.00	5	400.92	21	1082.19	21	-0.00	19
101	109	110	Max	0.00	0.00	1	0.00	5	0.00	18	1759.97	17	7927.83	17	0.00	13
101	109	110	Max	117.00	0.00	1	0.00	5	0.00	18	865.24	17	9463.58	17	0.00	13
101	109	110	Min.	0.00	-91917.70	17	0.00	19	0.00	13	273.46	21	1082.19	1	-0.00	19
101	109	110	Min.	117.00	-91917.70	17	0.00	19	0.00	19	83.97	21	1291.29	21	-0.00	19
101	110	111	Max	0.00	0.00	1	0.00	5	0.00	13	-43.49	9	9463.59	17	0.00	13
101	110	111	Max	117.00	0.00	1	0.00	5	0.00	13	-232.97	9	8276.66	17	0.00	13

101	110	111	Min.	0.00	-91917.70	17	0.00	18	0.00	5	-567.11	17	1291.29	1	-0.00	19
101	110	111	Min.	117.00	-91917.70	17	0.00	18	0.00	18	-1461.84	17	1129.56	21	-0.00	19
101	111	112	Max	0.00	0.00	1	0.00	13	0.00	18	-360.43	9	8276.49	17	0.00	13
101	111	112	Max	117.00	0.00	1	0.00	13	0.00	18	-549.92	9	4366.86	17	0.00	13
101	111	112	Min.	0.00	-91917.70	17	0.00	18	0.00	19	-2894.20	17	1129.56	1	-0.00	19
101	111	112	Min.	117.00	-91917.70	17	0.00	18	0.00	5	-3788.93	17	597.00	21	-0.00	19
101	112	113	Max	0.00	0.00	1	0.00	18	0.00	5	-661.65	9	4366.56	17	0.00	13
101	112	113	Max	82.00	0.00	1	0.00	18	0.00	18	-794.45	9	0.00	17	0.00	13
101	112	113	Min.	0.00	-91917.70	17	0.00	19	0.00	18	-5011.54	17	597.00	9	-0.00	19
101	112	113	Min.	82.00	-91917.70	17	0.00	19	0.00	13	-5638.62	17	0.00	21	-0.00	19
102	114	115	Max	35.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00	1
102	114	115	Max	76.00									100.74	17		
102	114	115	Max	117.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00	1
102	114	115	Min.	35.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00	1
102	114	115	Min.	76.00									7.56	1		
102	114	115	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00	1
102	115	116	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	115	116	Max	57.80									205.05	17		
102	115	116	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00	1
102	115	116	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	115	116	Min.	58.02									15.38	1		
102	115	116	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00	1
102	116	117	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	116	117	Max	57.80									205.05	17		
102	116	117	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
102	116	117	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	116	117	Min.	58.50									15.38	1		
102	116	117	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
102	117	118	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	117	118	Max	58.50									205.08	17		
102	117	118	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00	1
102	117	118	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	117	118	Min.	58.50									15.38	1		
102	117	118	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00	1
102	118	119	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	118	119	Max	57.80									205.05	17		
102	118	119	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
102	118	119	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	118	119	Min.	58.50									15.38	1		
102	118	119	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
102	119	120	Max	0.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00	1
102	119	120	Max	33.10									67.24	17		
102	119	120	Max	67.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	18	0.00	1
102	119	120	Min.	0.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00	1
102	119	120	Min.	33.23									5.04	1		
102	119	120	Min.	67.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	17	0.00	1
102	120	121	Max	50.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00	1
102	120	121	Max	83.50									67.25	17		
102	120	121	Max	117.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	17	0.00	1
102	120	121	Min.	50.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00	1
102	120	121	Min.	83.50									5.04	1		
102	120	121	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	1	0.00	1
102	121	122	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	121	122	Max	57.80									205.05	17		
102	121	122	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
102	121	122	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	121	122	Min.	58.50									15.38	1		
102	121	122	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
102	122	123	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	122	123	Max	57.80									205.05	17		
102	122	123	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
102	122	123	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	122	123	Min.	58.50									15.38	1		
102	122	123	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
102	123	124	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	123	124	Max	57.80									205.05	17		
102	123	124	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
102	123	124	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	123	124	Min.	58.50									15.38	1		
102	123	124	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
102	124	125	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
102	124	125	Max	57.80									205.05	17		
102	124	125	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
102	124	125	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
102	124	125	Min.	58.50									15.38	1		
102	124	125	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
102	125	126	Max	0.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00	1
102	125	126	Max	41.00									100.74	17		
102	125	126	Max	82.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00	1
102	125	126	Min.	0.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00	1
102	125	126	Min.	41.00									7.56	1		
102	125	126	Min.	82.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00	1

103	127	128	Max	35.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00	1
103	127	128	Max	76.00									100.74	17		
103	127	128	Max	117.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00	1
103	127	128	Min.	35.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00	1
103	127	128	Min.	76.00									7.56	1		
103	127	128	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00	1
103	128	129	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	128	129	Max	57.80									205.05	17		
103	128	129	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00	1
103	128	129	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	128	129	Min.	58.02									15.38	1		
103	128	129	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00	1
103	129	130	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	129	130	Max	57.80									205.05	17		
103	129	130	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
103	129	130	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	129	130	Min.	58.50									15.38	1		
103	129	130	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
103	130	131	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	130	131	Max	58.50									205.08	17		
103	130	131	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00	1
103	130	131	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	130	131	Min.	58.50									15.38	1		
103	130	131	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00	1
103	131	132	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	131	132	Max	57.80									205.05	17		
103	131	132	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
103	131	132	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	131	132	Min.	58.50									15.38	1		
103	131	132	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
103	132	133	Max	0.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00	1
103	132	133	Max	33.10									67.24	17		
103	132	133	Max	67.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	18	0.00	1
103	132	133	Min.	0.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00	1
103	132	133	Min.	33.23									5.04	1		
103	132	133	Min.	67.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	17	0.00	1
103	133	134	Max	50.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00	1
103	133	134	Max	83.50									67.25	17		
103	133	134	Max	117.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	17	0.00	1
103	133	134	Min.	50.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00	1
103	133	134	Min.	83.50									5.04	1		
103	133	134	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	1	0.00	1
103	134	135	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	134	135	Max	57.80									205.05	17		
103	134	135	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
103	134	135	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	134	135	Min.	58.50									15.38	1		
103	134	135	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
103	135	136	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	135	136	Max	57.80									205.05	17		
103	135	136	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
103	135	136	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	135	136	Min.	58.50									15.38	1		
103	135	136	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
103	136	137	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	136	137	Max	57.80									205.05	17		
103	136	137	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
103	136	137	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	136	137	Min.	58.50									15.38	1		
103	136	137	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
103	137	138	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
103	137	138	Max	57.80									205.05	17		
103	137	138	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
103	137	138	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
103	137	138	Min.	58.50									15.38	1		
103	137	138	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
103	138	139	Max	0.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00	1
103	138	139	Max	41.00									100.74	17		
103	138	139	Max	82.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00	1
103	138	139	Min.	0.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00	1
103	138	139	Min.	41.00									7.56	1		
103	138	139	Min.	82.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00	1
104	140	141	Max	35.00	0.00	1	0.00	19	0.00	13	10607.50	17	0.00	1	0.00	13
104	140	141	Max	117.00	0.00	1	0.00	19	0.00	19	9531.34	17	8256.92	17	0.00	13
104	140	141	Min.	35.00	-124143.00	17	0.00	13	0.00	18	1127.12	1	0.00	1	-0.00	19
104	140	141	Min.	117.00	-124143.00	17	0.00	13	0.00	13	984.25	1	865.66	1	-0.00	19
104	141	142	Max	0.00	0.00	1	0.00	18	0.00	19	7086.12	17	8256.33	17	0.00	13
104	141	142	Max	117.00	0.00	1	0.00	18	0.00	18	5550.65	17	15648.80	17	0.00	13
104	141	142	Min.	0.00	-124143.00	17	0.00	19	0.00	13	760.80	1	865.66	1	-0.00	19
104	141	142	Min.	117.00	-124143.00	17	0.00	19	0.00	19	556.96	1	1636.55	1	-0.00	19
104	142	143	Max	0.00	0.00	1	0.00	19	0.00	18	2685.95	17	15648.50	17	0.00	13
104	142	143	Max	117.00	0.00	1	0.00	19	0.00	19	1150.48	17	17892.80	17	0.00	13

104	142	143	Min.	0.00	-124143.00	17	0.00	18	0.00	5	302.04	1	1636.54	1	-0.00 19
104	142	143	Min.	117.00	-124143.00	17	0.00	18	0.00	13	98.20	1	1870.68	1	-0.00 19
104	143	144	Max	0.00	0.00	1	0.00	13	0.00	19	-156.72	1	17892.80	17	0.00 13
104	143	144	Max	117.00	0.00	1	0.00	13	0.00	13	-360.56	1	14988.90	17	0.00 13
104	143	144	Min.	0.00	-124143.00	17	0.00	19	0.00	13	-1714.23	17	1870.68	1	-0.00 19
104	143	144	Min.	117.00	-124143.00	17	0.00	19	0.00	19	-3249.70	17	1568.07	1	-0.00 19
104	144	145	Max	0.00	0.00	1	0.00	19	0.00	19	-615.48	1	14989.30	17	0.00 13
104	144	145	Max	117.00	0.00	1	0.00	19	0.00	19	-819.32	1	6937.21	17	0.00 13
104	144	145	Min.	0.00	-124143.00	17	0.00	5	0.00	18	-6114.40	17	1568.08	1	-0.00 19
104	144	145	Min.	117.00	-124143.00	17	0.00	5	0.00	13	-7649.87	17	728.72	1	-0.00 19
104	145	146	Max	0.00	0.00	1	0.00	5	0.00	13	-1029.29	1	6937.82	17	0.00 13
104	145	146	Max	67.00	0.00	1	0.00	5	0.00	5	-1146.02	1	0.00	18	0.00 13
104	145	146	Min.	0.00	-124143.00	17	0.00	13	0.00	19	-9915.31	17	728.73	1	-0.00 19
104	145	146	Min.	67.00	-124143.00	17	0.00	13	0.00	13	-10794.60	17	0.00	17	-0.00 19
104	146	147	Max	50.00	0.00	1	0.00	19	0.00	13	10794.60	17	0.00	1	0.00 13
104	146	147	Max	117.00	0.00	1	0.00	19	0.00	19	9915.31	17	6937.82	17	0.00 13
104	146	147	Min.	50.00	-124143.00	17	0.00	18	0.00	19	1146.02	1	0.00	1	-0.01 19
104	146	147	Min.	117.00	-124143.00	17	0.00	18	0.00	18	1029.29	1	728.73	1	-0.01 19
104	147	148	Max	0.00	0.00	1	0.00	18	0.00	13	7649.87	17	6937.21	17	0.00 13
104	147	148	Max	117.00	0.00	1	0.00	18	0.00	19	6114.40	17	14989.30	17	0.00 13
104	147	148	Min.	0.00	-124143.00	17	0.00	5	0.00	18	819.32	1	728.72	1	-0.01 19
104	147	148	Min.	117.00	-124143.00	17	0.00	5	0.00	5	615.48	1	1568.08	1	-0.01 19
104	148	149	Max	0.00	0.00	1	0.00	13	0.00	19	3249.70	17	14988.90	17	0.00 13
104	148	149	Max	117.00	0.00	1	0.00	13	0.00	13	1714.23	17	17892.80	17	0.00 13
104	148	149	Min.	0.00	-124143.00	17	0.00	18	0.00	13	360.56	1	1568.07	1	-0.01 19
104	148	149	Min.	117.00	-124143.00	17	0.00	18	0.00	18	156.72	1	1870.68	1	-0.01 19
104	149	150	Max	0.00	0.00	1	0.00	5	0.00	18	-98.20	1	17892.80	17	0.00 13
104	149	150	Max	117.00	0.00	1	0.00	5	0.00	18	-302.04	1	15648.50	17	0.00 13
104	149	150	Min.	0.00	-124143.00	17	0.00	18	0.00	13	-1150.48	17	1870.68	1	-0.01 19
104	149	150	Min.	117.00	-124143.00	17	0.00	18	0.00	13	-2685.95	17	1636.54	1	-0.01 19
104	150	151	Max	0.00	0.00	1	0.00	13	0.00	18	-556.96	1	15648.80	17	0.00 13
104	150	151	Max	117.00	0.00	1	0.00	13	0.00	19	-760.80	1	8256.33	17	0.00 13
104	150	151	Min.	0.00	-124143.00	17	0.00	18	0.00	13	-5550.65	17	1636.54	1	-0.01 19
104	150	151	Min.	117.00	-124143.00	17	0.00	18	0.00	18	-7086.12	17	865.66	1	-0.01 19
104	151	152	Max	0.00	0.00	1	0.00	18	0.00	19	-984.25	1	8256.92	17	0.00 13
104	151	152	Max	82.00	0.00	1	0.00	18	0.00	18	-1127.12	1	0.00	17	0.00 13
104	151	152	Min.	0.00	-124143.00	17	0.00	19	0.00	18	-9531.34	17	865.66	1	-0.01 19
104	151	152	Min.	82.00	-124143.00	17	0.00	19	0.00	13	-10607.50	17	0.00	1	-0.01 19
105	153	154	Max	35.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00 1
105	153	154	Max	76.00									100.74	17	
105	153	154	Max	117.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00 1
105	153	154	Min.	35.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00 1
105	153	154	Min.	76.00									7.56	1	
105	153	154	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00 1
105	154	155	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00 1
105	154	155	Max	57.80									205.05	17	
105	154	155	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00 1
105	154	155	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00 1
105	154	155	Min.	58.02									15.38	1	
105	154	155	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00 1
105	155	156	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00 1
105	155	156	Max	57.80									205.05	17	
105	155	156	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00 1
105	155	156	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00 1
105	155	156	Min.	58.50									15.38	1	
105	155	156	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00 1
105	156	157	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00 1
105	156	157	Max	58.50									205.08	17	
105	156	157	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00 1
105	156	157	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00 1
105	156	157	Min.	58.50									15.38	1	
105	156	157	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00 1
105	157	158	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00 1
105	157	158	Max	57.80									205.05	17	
105	157	158	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00 1
105	157	158	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00 1
105	157	158	Min.	58.50									15.38	1	
105	157	158	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00 1
105	158	159	Max	0.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00 1
105	158	159	Max	33.10									67.24	17	
105	158	159	Max	67.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	18	0.00 1
105	158	159	Min.	0.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00 1
105	158	159	Min.	33.23									5.04	1	
105	158	159	Min.	67.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	17	0.00 1
105	159	160	Max	50.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00 1
105	159	160	Max	83.50									67.25	17	
105	159	160	Max	117.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	17	0.00 1
105	159	160	Min.	50.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00 1
105	159	160	Min.	83.50									5.04	1	
105	159	160	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	1	0.00 1
105	160	161	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00 1
105	160	161	Max	57.80									205.05	17	

105	160	161	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
105	160	161	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
105	160	161	Min.	58.50									15.38	1		
105	160	161	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
105	161	162	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
105	161	162	Max	57.80									205.05	17		
105	161	162	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
105	161	162	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
105	161	162	Min.	58.50									15.38	1		
105	161	162	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
105	162	163	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
105	162	163	Max	57.80									205.05	17		
105	162	163	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
105	162	163	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
105	162	163	Min.	58.50									15.38	1		
105	162	163	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
105	163	164	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
105	163	164	Max	57.80									205.05	17		
105	163	164	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
105	163	164	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
105	163	164	Min.	58.50									15.38	1		
105	163	164	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
105	164	165	Max	0.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00	1
105	164	165	Max	41.00									100.74	17		
105	164	165	Max	82.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00	1
105	164	165	Min.	0.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00	1
105	164	165	Min.	41.00									7.56	1		
105	164	165	Min.	82.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00	1
106	166	167	Max	35.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00	1
106	166	167	Max	76.00									100.74	17		
106	166	167	Max	117.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00	1
106	166	167	Min.	35.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00	1
106	166	167	Min.	76.00									7.56	1		
106	166	167	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00	1
106	167	168	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
106	167	168	Max	57.80									205.05	17		
106	167	168	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00	1
106	167	168	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
106	167	168	Min.	58.02									15.38	1		
106	167	168	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00	1
106	168	169	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
106	168	169	Max	57.80									205.05	17		
106	168	169	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
106	168	169	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
106	168	169	Min.	58.50									15.38	1		
106	168	169	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
106	169	170	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
106	169	170	Max	58.50									205.08	17		
106	169	170	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	17	0.00	1
106	169	170	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
106	169	170	Min.	58.50									15.38	1		
106	169	170	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	1	0.00	1
106	170	171	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
106	170	171	Max	57.80									205.05	17		
106	170	171	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
106	170	171	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
106	170	171	Min.	58.50									15.38	1		
106	170	171	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
106	171	172	Max	0.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00	1
106	171	172	Max	33.10									67.24	17		
106	171	172	Max	67.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	18	0.00	1
106	171	172	Min.	0.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00	1
106	171	172	Min.	33.23									5.04	1		
106	171	172	Min.	67.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	17	0.00	1
106	172	173	Max	50.00	0.00	1	0.00	1	0.00	1	401.51	17	0.00	1	0.00	1
106	172	173	Max	83.50									67.25	17		
106	172	173	Max	117.00	0.00	1	0.00	1	0.00	1	-30.12	1	0.00	17	0.00	1
106	172	173	Min.	50.00	-22630.70	17	0.00	1	0.00	1	30.12	1	0.00	1	0.00	1
106	172	173	Min.	83.50									5.04	1		
106	172	173	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-401.51	17	0.00	1	0.00	1
106	173	174	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
106	173	174	Max	57.80									205.05	17		
106	173	174	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
106	173	174	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
106	173	174	Min.	58.50									15.38	1		
106	173	174	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1
106	174	175	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00	1
106	174	175	Max	57.80									205.05	17		
106	174	175	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00	1
106	174	175	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00	1
106	174	175	Min.	58.50									15.38	1		
106	174	175	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00	1

106	175	176	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00 1
106	175	176	Max	57.80									205.05	17	
106	175	176	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00 1
106	175	176	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00 1
106	175	176	Min.	58.50									15.38	1	
106	175	176	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00 1
106	176	177	Max	0.00	0.00	1	0.00	1	0.00	1	701.14	17	0.00	1	0.00 1
106	176	177	Max	57.80									205.05	17	
106	176	177	Max	117.00	0.00	1	0.00	1	0.00	1	-52.59	1	0.00	1	0.00 1
106	176	177	Min.	0.00	-22630.70	17	0.00	1	0.00	1	52.59	1	0.00	17	0.00 1
106	176	177	Min.	58.50									15.38	1	
106	176	177	Min.	117.00	-22630.70	17	0.00	1	0.00	1	-701.14	17	0.00	17	0.00 1
106	177	178	Max	0.00	0.00	1	0.00	1	0.00	1	491.40	17	0.00	1	0.00 1
106	177	178	Max	41.00									100.74	17	
106	177	178	Max	82.00	0.00	1	0.00	1	0.00	1	-36.86	1	0.00	17	0.00 1
106	177	178	Min.	0.00	-22630.70	17	0.00	1	0.00	1	36.86	1	0.00	1	0.00 1
106	177	178	Min.	41.00									7.56	1	
106	177	178	Min.	82.00	-22630.70	17	0.00	1	0.00	1	-491.40	17	0.00	1	0.00 1
107	179	180	Max	35.00	0.00	1	0.00	19	0.00	13	5638.62	17	0.00	1	0.00 13
107	179	180	Max	117.00	0.00	1	0.00	19	0.00	5	5011.54	17	4366.56	17	0.00 13
107	179	180	Min.	35.00	-91917.70	17	0.00	13	0.00	19	794.45	9	0.00	1	0.00 19
107	179	180	Min.	117.00	-91917.70	17	0.00	13	0.00	13	661.65	9	597.00	9	0.00 19
107	180	181	Max	0.00	0.00	1	0.00	19	0.00	18	3788.93	17	4366.86	17	0.00 13
107	180	181	Max	117.00	0.00	1	0.00	19	0.00	19	2894.20	17	8276.49	17	0.00 13
107	180	181	Min.	0.00	-91917.70	17	0.00	18	0.00	13	549.92	9	597.00	21	0.00 19
107	180	181	Min.	117.00	-91917.70	17	0.00	18	0.00	5	360.43	9	1129.56	1	0.00 19
107	181	182	Max	0.00	0.00	1	0.00	5	0.00	13	1461.84	17	8276.65	17	0.00 13
107	181	182	Max	117.00	0.00	1	0.00	5	0.00	5	567.11	17	9463.59	17	0.00 13
107	181	182	Min.	0.00	-91917.70	17	0.00	19	0.00	18	232.97	9	1129.56	21	0.00 19
107	181	182	Min.	117.00	-91917.70	17	0.00	19	0.00	18	43.49	9	1291.29	1	0.00 19
107	182	183	Max	0.00	0.00	1	0.00	5	0.00	18	-83.97	21	9463.58	17	0.00 13
107	182	183	Max	117.00	0.00	1	0.00	5	0.00	18	-273.46	21	7927.83	17	0.00 13
107	182	183	Min.	0.00	-91917.70	17	0.00	19	0.00	19	-865.24	17	1291.29	21	0.00 19
107	182	183	Min.	117.00	-91917.70	17	0.00	19	0.00	19	-1759.97	17	1082.19	1	0.00 19
107	183	184	Max	0.00	0.00	1	0.00	18	0.00	13	-400.92	21	7927.64	17	0.00 13
107	183	184	Max	117.00	0.00	1	0.00	18	0.00	18	-590.40	1	3669.20	17	0.00 13
107	183	184	Min.	0.00	-91917.70	17	0.00	5	0.00	18	-3192.33	17	1082.19	21	0.00 19
107	183	184	Min.	117.00	-91917.70	17	0.00	5	0.00	5	-4087.06	17	502.26	9	0.00 19
107	184	185	Max	0.00	0.00	1	0.00	13	0.00	18	-695.39	1	3668.90	17	0.00 13
107	184	185	Max	67.00	0.00	1	0.00	13	0.00	18	-803.90	1	0.00	1	0.00 13
107	184	185	Min.	0.00	-91917.70	17	0.00	19	0.00	19	-5219.78	17	502.26	21	0.00 19
107	184	185	Min.	67.00	-91917.70	17	0.00	19	0.00	19	-5732.15	17	0.00	17	0.00 19
107	185	186	Max	50.00	0.00	1	0.00	18	0.00	18	5732.15	17	0.00	1	0.00 13
107	185	186	Max	117.00	0.00	1	0.00	18	0.00	18	5219.78	17	3668.89	17	0.00 13
107	185	186	Min.	50.00	-91917.70	17	0.00	13	0.00	5	803.90	9	0.00	1	-0.00 19
107	185	186	Min.	117.00	-91917.70	17	0.00	13	0.00	13	695.39	9	502.26	9	-0.00 19
107	186	187	Max	0.00	0.00	1	0.00	18	0.00	13	4087.06	17	3669.20	17	0.00 13
107	186	187	Max	117.00	0.00	1	0.00	18	0.00	18	3192.33	17	7927.64	17	0.00 13
107	186	187	Min.	0.00	-91917.70	17	0.00	5	0.00	18	590.40	9	502.26	1	-0.00 19
107	186	187	Min.	117.00	-91917.70	17	0.00	5	0.00	5	400.92	9	1082.19	1	-0.00 19
107	187	188	Max	0.00	0.00	1	0.00	5	0.00	18	1759.97	17	7927.83	17	0.00 13
107	187	188	Max	117.00	0.00	1	0.00	5	0.00	18	865.24	17	9463.58	17	0.00 13
107	187	188	Min.	0.00	-91917.70	17	0.00	19	0.00	13	273.46	9	1082.19	21	-0.00 19
107	187	188	Min.	117.00	-91917.70	17	0.00	19	0.00	19	83.97	9	1291.29	1	-0.00 19
107	188	189	Max	0.00	0.00	1	0.00	5	0.00	13	-43.49	21	9463.59	17	0.00 13
107	188	189	Max	117.00	0.00	1	0.00	5	0.00	13	-232.97	21	8276.66	17	0.00 13
107	188	189	Min.	0.00	-91917.70	17	0.00	18	0.00	5	-567.11	17	1291.29	21	-0.00 19
107	188	189	Min.	117.00	-91917.70	17	0.00	18	0.00	18	-1461.84	17	1129.56	1	-0.00 19
107	189	190	Max	0.00	0.00	1	0.00	13	0.00	18	-360.43	1	8276.49	17	0.00 13
107	189	190	Max	117.00	0.00	1	0.00	13	0.00	18	-549.92	1	4366.86	17	0.00 13
107	189	190	Min.	0.00	-91917.70	17	0.00	18	0.00	19	-2894.20	17	1129.56	21	-0.00 19
107	189	190	Min.	117.00	-91917.70	17	0.00	18	0.00	5	-3788.93	17	597.00	1	-0.00 19
107	190	191	Max	0.00	0.00	1	0.00	18	0.00	5	-661.65	1	4366.56	17	0.00 13
107	190	191	Max	82.00	0.00	1	0.00	18	0.00	18	-794.45	1	0.00	17	0.00 13
107	190	191	Min.	0.00	-91917.70	17	0.00	19	0.00	18	-5011.54	17	597.00	1	-0.00 19
107	190	191	Min.	82.00	-91917.70	17	0.00	19	0.00	13	-5638.62	17	0.00	21	-0.00 19
108	101	114	Max	0.00	0.00	1	0.00	1	0.00	1	8.75	13	5.01	17	0.00 9
108	101	114	Max	10.33									2.10	19	
108	101	114	Max	79.00	0.00	1	0.00	1	0.00	1	-6.10	13	-0.10	13	0.00 9
108	101	114	Min.	0.00	-22630.70	17	0.00	1	0.00	1	-1.48	17	-1.15	13	-0.01 17
108	101	114	Min.	14.63									0.23	5	
108	101	114	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-21.53	17	-4.08	17	-0.01 17
108	114	127	Max	0.00	0.00	1	0.00	1	0.00	1	10.13	17	-0.77	21	0.00 9
108	114	127	Max	29.34									0.12	19	
108	114	127	Max	79.00	0.00	1	0.00	1	0.00	1	-6.88	9	-1.28	1	0.00 9
108	114	127	Min.	0.00	-22630.70	17	0.00	1	0.00	1	5.71	21	-4.88	17	0.00 1
108	114	127	Min.	39.93									-2.85	17	
108	114	127	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-12.60	19	-4.79	17	0.00 1
108	127	140	Max	0.00	0.00	1	0.00	1	0.00	1	36.10	17	-1.31	13	0.01 17
108	127	140	Max	62.45									1.25	5	
108	127	140	Max	79.00	0.00	1	0.00	1	0.00	1	16.05	17	11.07	17	0.01 17
108	127	140	Min.	0.00	-22630.70	17	0.00	1	0.00	1	9.04	21	-9.53	17	0.00 21

108	127	140	Min.	47.40									0.68	21		
108	127	140	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-7.82	19	-0.30	19	0.00	21
108	140	153	Max	0.00	0.00	1	0.00	1	0.00	1	6.06	5	10.36	17	-0.00	9
108	140	153	Max	12.16									1.44	19		
108	140	153	Max	79.00	0.00	1	0.00	1	0.00	1	-8.79	5	-1.36	5	-0.00	9
108	140	153	Min.	0.00	-22630.70	17	0.00	1	0.00	1	-15.19	17	-0.28	5	-0.01	17
108	140	153	Min.	15.80									0.56	15		
108	140	153	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-35.24	17	-9.55	17	-0.01	17
108	153	166	Max	0.00	0.00	1	0.00	1	0.00	1	10.54	17	-0.23	19	0.00	9
108	153	166	Max	40.62									0.29	13		
108	153	166	Max	79.00	0.00	1	0.00	1	0.00	1	-7.20	13	-1.09	13	0.00	9
108	153	166	Min.	0.00	-22630.70	17	0.00	1	0.00	1	3.94	21	-4.67	17	0.00	19
108	153	166	Min.	41.53									-2.48	17		
108	153	166	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-15.24	19	-4.35	19	0.00	19
108	166	179	Max	0.00	0.00	1	0.00	1	0.00	1	21.66	17	-0.32	19	0.01	17
108	166	179	Max	63.20									1.46	22		
108	166	179	Max	79.00	0.00	1	0.00	1	0.00	1	1.61	17	4.70	17	0.01	17
108	166	179	Min.	0.00	-22630.70	17	0.00	1	0.00	1	5.88	21	-4.49	17	0.00	1
108	166	179	Min.	64.27									0.02	13		
108	166	179	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-12.42	19	-2.21	19	0.00	1
109	102	115	Max	0.00	0.00	1	0.00	1	0.00	9	1222.61	17	0.00	1	0.30	17
109	102	115	Max	79.00	0.00	1	0.00	1	0.00	9	1202.56	17	957.94	17	0.30	17
109	102	115	Min.	0.00	-22630.70	17	0.00	1	0.00	1	111.73	1	0.00	1	0.00	9
109	102	115	Min.	79.00	-22630.70	17	0.00	1	0.00	1	96.88	1	82.40	1	0.00	9
109	115	128	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	957.94	17	0.30	17
109	115	128	Max	38.76									959.92	17		
109	115	128	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	957.94	17	0.30	17
109	115	128	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	82.40	1	0.00	9
109	115	128	Min.	38.76									83.86	1		
109	115	128	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	82.40	1	0.00	9
109	128	141	Max	0.00	0.00	1	0.00	1	0.00	1	-96.88	1	957.94	17	0.30	17
109	128	141	Max	79.00	0.00	1	0.00	1	0.00	1	-111.73	1	0.00	17	0.30	17
109	128	141	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1202.56	17	82.40	1	0.00	9
109	128	141	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1222.61	17	0.00	1	0.00	9
109	141	154	Max	0.00	0.00	1	0.00	1	0.00	1	1222.61	17	0.00	1	-0.00	21
109	141	154	Max	79.00	0.00	1	0.00	1	0.00	1	1202.56	17	957.94	17	-0.00	21
109	141	154	Min.	0.00	-22630.70	17	0.00	1	0.00	9	111.73	1	0.00	1	-0.30	17
109	141	154	Min.	79.00	-22630.70	17	0.00	1	0.00	9	96.88	1	82.40	1	-0.30	17
109	154	167	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	957.94	17	-0.00	21
109	154	167	Max	38.76									959.92	17		
109	154	167	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	957.94	17	-0.00	21
109	154	167	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	82.40	1	-0.30	17
109	154	167	Min.	38.76									83.86	1		
109	154	167	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	82.40	1	-0.30	17
109	167	180	Max	0.00	0.00	1	0.00	1	0.00	1	-96.88	1	957.94	17	-0.00	21
109	167	180	Max	79.00	0.00	1	0.00	1	0.00	1	-111.73	1	0.00	17	-0.00	21
109	167	180	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1202.56	17	82.40	1	-0.30	17
109	167	180	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1222.61	17	0.00	1	-0.30	17
110	103	116	Max	0.00	0.00	1	0.00	1	0.00	9	1432.35	17	0.00	1	0.17	17
110	103	116	Max	79.00	0.00	1	0.00	1	0.00	9	1412.30	17	1123.64	17	0.17	17
110	103	116	Min.	0.00	-22630.70	17	0.00	1	0.00	1	127.46	1	0.00	1	0.00	9
110	103	116	Min.	79.00	-22630.70	17	0.00	1	0.00	1	112.61	1	94.83	1	0.00	9
110	116	129	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	1123.64	17	0.17	17
110	116	129	Max	38.76									1125.62	17		
110	116	129	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	1123.64	17	0.17	17
110	116	129	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	94.83	1	0.00	9
110	116	129	Min.	38.76									96.29	1		
110	116	129	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	94.83	1	0.00	9
110	129	142	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.17	17
110	129	142	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.17	17
110	129	142	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	0.00	9
110	129	142	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	0.00	9
110	142	155	Max	0.00	0.00	1	0.00	1	0.00	1	1432.35	17	0.00	1	-0.00	21
110	142	155	Max	79.00	0.00	1	0.00	1	0.00	1	1412.30	17	1123.64	17	-0.00	21
110	142	155	Min.	0.00	-22630.70	17	0.00	1	0.00	9	127.46	1	0.00	1	-0.17	17
110	142	155	Min.	79.00	-22630.70	17	0.00	1	0.00	9	112.61	1	94.83	1	-0.17	17
110	155	168	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	1123.64	17	-0.00	21
110	155	168	Max	38.76									1125.62	17		
110	155	168	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	1123.64	17	-0.00	21
110	155	168	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	94.83	1	-0.17	17
110	155	168	Min.	38.76									96.29	1		
110	155	168	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	94.83	1	-0.17	17
110	168	181	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	-0.00	21
110	168	181	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	-0.00	21
110	168	181	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	-0.17	17
110	168	181	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	-0.17	17
111	104	117	Max	0.00	0.00	1	0.00	1	0.00	9	1432.35	17	0.00	1	0.00	19
111	104	117	Max	79.00	0.00	1	0.00	1	0.00	9	1412.30	17	1123.64	17	0.00	19
111	104	117	Min.	0.00	-22630.70	17	0.00	1	0.00	1	127.46	1	0.00	1	-0.01	17
111	104	117	Min.	79.00	-22630.70	17	0.00	1	0.00	1	112.61	1	94.83	1	-0.01	17
111	117	130	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	1123.64	17	0.00	19
111	117	130	Max	38.76									1125.62	17		

111	117	130	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	1123.64	17	0.00	19
111	117	130	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	94.83	1	-0.01	17
111	117	130	Min.	38.76									96.29	1		
111	117	130	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	94.83	1	-0.01	17
111	130	143	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.00	19
111	130	143	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.00	19
111	130	143	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	-0.01	17
111	130	143	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	-0.01	17
111	143	156	Max	0.00	0.00	1	0.00	1	0.00	1	1432.35	17	0.00	1	0.01	17
111	143	156	Max	79.00	0.00	1	0.00	1	0.00	1	1412.30	17	1123.64	17	0.01	17
111	143	156	Min.	0.00	-22630.70	17	0.00	1	0.00	9	127.46	1	0.00	1	0.00	9
111	143	156	Min.	79.00	-22630.70	17	0.00	1	0.00	9	112.61	1	94.83	1	0.00	9
111	156	169	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	1123.64	17	0.01	17
111	156	169	Max	38.76									1125.62	17		
111	156	169	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	1123.64	17	0.01	17
111	156	169	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	94.83	1	0.00	9
111	156	169	Min.	38.76									96.29	1		
111	156	169	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	94.83	1	0.00	9
111	169	182	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.01	17
111	169	182	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.01	17
111	169	182	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	0.00	9
111	169	182	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	0.00	9
112	105	118	Max	0.00	0.00	1	0.00	1	0.00	9	1432.35	17	0.00	1	-0.00	21
112	105	118	Max	79.00	0.00	1	0.00	1	0.00	9	1412.30	17	1123.64	17	-0.00	21
112	105	118	Min.	0.00	-22630.70	17	0.00	1	0.00	1	127.46	1	0.00	1	-0.19	17
112	105	118	Min.	79.00	-22630.70	17	0.00	1	0.00	1	112.61	1	94.83	1	-0.19	17
112	118	131	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	1123.64	17	-0.00	21
112	118	131	Max	38.76									1125.62	17		
112	118	131	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	1123.64	17	-0.00	21
112	118	131	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	94.83	1	-0.19	17
112	118	131	Min.	38.76									96.29	1		
112	118	131	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	94.83	1	-0.19	17
112	131	144	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	-0.00	21
112	131	144	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	-0.00	21
112	131	144	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	-0.19	17
112	131	144	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	-0.19	17
112	144	157	Max	0.00	0.00	1	0.00	1	0.00	1	1432.35	17	0.00	1	0.19	17
112	144	157	Max	79.00	0.00	1	0.00	1	0.00	1	1412.30	17	1123.64	17	0.19	17
112	144	157	Min.	0.00	-22630.70	17	0.00	1	0.00	9	127.46	1	0.00	1	0.00	9
112	144	157	Min.	79.00	-22630.70	17	0.00	1	0.00	9	112.61	1	94.83	1	0.00	9
112	157	170	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	1123.64	17	0.19	17
112	157	170	Max	38.76									1125.62	17		
112	157	170	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	1123.64	17	0.19	17
112	157	170	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	94.83	1	0.00	9
112	157	170	Min.	38.76									96.29	1		
112	157	170	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	94.83	1	0.00	9
112	170	183	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.19	17
112	170	183	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.19	17
112	170	183	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	0.00	9
112	170	183	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	0.00	9
113	106	119	Max	0.00	0.00	1	0.00	1	0.00	9	1132.72	17	0.00	1	-0.00	21
113	106	119	Max	79.00	0.00	1	0.00	1	0.00	9	1112.67	17	886.93	17	-0.00	21
113	106	119	Min.	0.00	-22630.70	17	0.00	1	0.00	1	104.98	1	0.00	1	-0.31	17
113	106	119	Min.	79.00	-22630.70	17	0.00	1	0.00	1	90.13	1	77.07	1	-0.31	17
113	119	132	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	886.93	17	-0.00	21
113	119	132	Max	38.76									888.91	17		
113	119	132	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	886.93	17	-0.00	21
113	119	132	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	77.07	1	-0.31	17
113	119	132	Min.	38.76									78.54	1		
113	119	132	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	77.07	1	-0.31	17
113	132	145	Max	0.00	0.00	1	0.00	1	0.00	1	-90.13	1	886.93	17	-0.00	21
113	132	145	Max	79.00	0.00	1	0.00	1	0.00	1	-104.98	1	0.00	17	-0.00	21
113	132	145	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1112.67	17	77.07	1	-0.31	17
113	132	145	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1132.72	17	0.00	1	-0.31	17
113	145	158	Max	0.00	0.00	1	0.00	1	0.00	1	1132.72	17	0.00	1	0.31	17
113	145	158	Max	79.00	0.00	1	0.00	1	0.00	1	1112.67	17	886.93	17	0.31	17
113	145	158	Min.	0.00	-22630.70	17	0.00	1	0.00	9	104.98	1	0.00	1	0.00	9
113	145	158	Min.	79.00	-22630.70	17	0.00	1	0.00	9	90.13	1	77.07	1	0.00	9
113	158	171	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	886.93	17	0.31	17
113	158	171	Max	38.76									888.91	17		
113	158	171	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	886.93	17	0.31	17
113	158	171	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	77.07	1	0.00	9
113	158	171	Min.	38.76									78.54	1		
113	158	171	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	77.07	1	0.00	9
113	171	184	Max	0.00	0.00	1	0.00	1	0.00	1	-90.13	1	886.93	17	0.31	17
113	171	184	Max	79.00	0.00	1	0.00	1	0.00	1	-104.98	1	0.00	17	0.31	17
113	171	184	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1112.67	17	77.07	1	0.00	9
113	171	184	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1132.72	17	0.00	1	0.00	9
114	107	120	Max	0.00	0.00	1	0.00	1	0.00	9	10.56	13	6.78	17	0.00	9
114	107	120	Max	18.53									2.06	22		
114	107	120	Max	79.00	0.00	1	0.00	1	0.00	1	-4.29	13	0.75	13	0.00	9
114	107	120	Min.	0.00	-22630.70	17	0.00	9	0.00	1	-3.13	17	-1.73	13	0.00	1

114	107	120	Min.	22.20									0.15	5		
114	107	120	Min.	79.00	-22630.70	17	0.00	9	0.00	9	-23.18	17	-3.61	17	0.00	1
114	120	133	Max	0.00	0.00	1	0.00	9	0.00	1	13.38	17	-1.76	20	0.00	9
114	120	133	Max	55.84									-0.03	13		
114	120	133	Max	79.00	0.00	1	0.00	9	0.00	9	-4.35	13	-0.53	13	0.00	9
114	120	133	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.61	20	-7.91	17	0.00	19
114	120	133	Min.	52.04									-4.38	17		
114	120	133	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-9.98	18	-5.26	17	0.00	19
114	133	146	Max	0.00	0.00	1	0.00	9	0.00	1	51.25	17	-2.32	20	0.00	9
114	133	146	Max	78.21									2.55	15		
114	133	146	Max	79.00	0.00	1	0.00	9	0.00	9	31.20	17	18.28	17	0.00	9
114	133	146	Min.	0.00	-22630.70	17	0.00	1	0.00	9	11.19	20	-14.29	17	0.00	19
114	133	146	Min.	59.50									1.01	20		
114	133	146	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-4.95	18	0.66	20	0.00	19
114	146	159	Max	0.00	0.00	1	0.00	9	0.00	1	7.48	13	13.52	17	0.00	9
114	146	159	Max	15.80									1.67	18		
114	146	159	Max	79.00	0.00	1	0.00	9	0.00	9	-7.37	13	-0.86	13	0.00	9
114	146	159	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-21.53	17	-0.91	13	0.00	19
114	146	159	Min.	31.60									0.52	1		
114	146	159	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-41.58	17	-11.41	17	0.00	19
114	159	172	Max	0.00	0.00	1	0.00	1	0.00	9	16.99	17	-1.58	20	0.00	9
114	159	172	Max	65.29									0.99	13		
114	159	172	Max	79.00	0.00	1	0.00	1	0.00	9	-2.46	13	0.83	13	0.00	9
114	159	172	Min.	0.00	-22630.70	17	0.00	1	0.00	1	5.71	20	-8.36	17	0.00	1
114	159	172	Min.	63.20									-2.69	17		
114	159	172	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-12.99	18	-4.40	18	0.00	1
114	172	185	Max	0.00	0.00	1	0.00	1	0.00	1	34.53	17	-1.45	20	0.00	9
114	172	185	Max	67.70									2.18	19		
114	172	185	Max	79.00	0.00	1	0.00	1	0.00	1	14.48	17	10.32	17	0.00	9
114	172	185	Min.	0.00	-22630.70	17	0.00	9	0.00	9	10.18	20	-9.04	17	0.00	1
114	172	185	Min.	53.46									1.30	20		
114	172	185	Min.	79.00	-22630.70	17	0.00	9	0.00	9	-6.50	18	0.55	5	0.00	1
115	108	121	Max	0.00	0.00	1	0.00	1	0.00	9	1132.72	17	0.00	1	0.31	17
115	108	121	Max	79.00	0.00	1	0.00	1	0.00	9	1112.67	17	886.93	17	0.31	17
115	108	121	Min.	0.00	-22630.70	17	0.00	1	0.00	1	104.98	1	0.00	1	0.00	9
115	108	121	Min.	79.00	-22630.70	17	0.00	1	0.00	1	90.13	1	77.07	1	0.00	9
115	121	134	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	886.93	17	0.31	17
115	121	134	Max	38.76									888.91	17		
115	121	134	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	886.93	17	0.31	17
115	121	134	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	77.07	1	0.00	9
115	121	134	Min.	38.76									78.54	1		
115	121	134	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	77.07	1	0.00	9
115	134	147	Max	0.00	0.00	1	0.00	1	0.00	1	-90.13	1	886.93	17	0.31	17
115	134	147	Max	79.00	0.00	1	0.00	1	0.00	1	-104.98	1	0.00	17	0.31	17
115	134	147	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1112.67	17	77.07	1	0.00	9
115	134	147	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1132.72	17	0.00	1	0.00	9
115	147	160	Max	0.00	0.00	1	0.00	1	0.00	1	1132.72	17	0.00	1	-0.00	21
115	147	160	Max	79.00	0.00	1	0.00	1	0.00	1	1112.67	17	886.93	17	-0.00	21
115	147	160	Min.	0.00	-22630.70	17	0.00	1	0.00	9	104.98	1	0.00	1	-0.31	17
115	147	160	Min.	79.00	-22630.70	17	0.00	1	0.00	9	90.13	1	77.07	1	-0.31	17
115	160	173	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	886.93	17	-0.00	21
115	160	173	Max	38.76									888.91	17		
115	160	173	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	886.93	17	-0.00	21
115	160	173	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	77.07	1	-0.31	17
115	160	173	Min.	38.76									78.54	1		
115	160	173	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	77.07	1	-0.31	17
115	173	186	Max	0.00	0.00	1	0.00	1	0.00	1	-90.13	1	886.93	17	-0.00	21
115	173	186	Max	79.00	0.00	1	0.00	1	0.00	1	-104.98	1	0.00	17	-0.00	21
115	173	186	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1112.67	17	77.07	1	-0.31	17
115	173	186	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1132.72	17	0.00	1	-0.31	17
116	109	122	Max	0.00	0.00	1	0.00	1	0.00	9	1432.35	17	0.00	1	0.19	17
116	109	122	Max	79.00	0.00	1	0.00	1	0.00	9	1412.30	17	1123.64	17	0.19	17
116	109	122	Min.	0.00	-22630.70	17	0.00	1	0.00	1	127.46	1	0.00	1	0.00	9
116	109	122	Min.	79.00	-22630.70	17	0.00	1	0.00	1	112.61	1	94.83	1	0.00	9
116	122	135	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	1123.64	17	0.19	17
116	122	135	Max	38.76									1125.62	17		
116	122	135	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	1123.64	17	0.19	17
116	122	135	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	94.83	1	0.00	9
116	122	135	Min.	38.76									96.29	1		
116	122	135	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	94.83	1	0.00	9
116	135	148	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.19	17
116	135	148	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.19	17
116	135	148	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	0.00	9
116	135	148	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	0.00	9
116	148	161	Max	0.00	0.00	1	0.00	1	0.00	1	1432.35	17	0.00	1	-0.00	21
116	148	161	Max	79.00	0.00	1	0.00	1	0.00	1	1412.30	17	1123.64	17	-0.00	21
116	148	161	Min.	0.00	-22630.70	17	0.00	1	0.00	9	127.46	1	0.00	1	-0.19	17
116	148	161	Min.	79.00	-22630.70	17	0.00	1	0.00	9	112.61	1	94.83	1	-0.19	17
116	161	174	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	1123.64	17	-0.00	21
116	161	174	Max	38.76									1125.62	17		
116	161	174	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	1123.64	17	-0.00	21
116	161	174	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	94.83	1	-0.19	17

116	161	174	Min.	38.76									96.29	1	
116	161	174	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	94.83	1	-0.19 17
116	174	187	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	-0.00 21
116	174	187	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	-0.00 21
116	174	187	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	-0.19 17
116	174	187	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	-0.19 17
117	110	123	Max	0.00	0.00	1	0.00	1	0.00	9	1432.35	17	0.00	1	0.01 17
117	110	123	Max	79.00	0.00	1	0.00	1	0.00	9	1412.30	17	1123.64	17	0.01 17
117	110	123	Min.	0.00	-22630.70	17	0.00	1	0.00	1	127.46	1	0.00	1	0.00 9
117	110	123	Min.	79.00	-22630.70	17	0.00	1	0.00	1	112.61	1	94.83	1	0.00 9
117	123	136	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	1123.64	17	0.01 17
117	123	136	Max	38.76									1125.62	17	
117	123	136	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	1123.64	17	0.01 17
117	123	136	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	94.83	1	0.00 9
117	123	136	Min.	38.76									96.29	1	
117	123	136	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	94.83	1	0.00 9
117	136	149	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.01 17
117	136	149	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.01 17
117	136	149	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	0.00 9
117	136	149	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	0.00 9
117	149	162	Max	0.00	0.00	1	0.00	1	0.00	1	1432.35	17	0.00	1	0.00 19
117	149	162	Max	79.00	0.00	1	0.00	1	0.00	1	1412.30	17	1123.64	17	0.00 19
117	149	162	Min.	0.00	-22630.70	17	0.00	1	0.00	9	127.46	1	0.00	1	-0.01 17
117	149	162	Min.	79.00	-22630.70	17	0.00	1	0.00	9	112.61	1	94.83	1	-0.01 17
117	162	175	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	1123.64	17	0.00 19
117	162	175	Max	38.76									1125.62	17	
117	162	175	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	1123.64	17	0.00 19
117	162	175	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	94.83	1	-0.01 17
117	162	175	Min.	38.76									96.29	1	
117	162	175	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	94.83	1	-0.01 17
117	175	188	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.00 19
117	175	188	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.00 19
117	175	188	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	-0.01 17
117	175	188	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	-0.01 17
118	111	124	Max	0.00	0.00	1	0.00	1	0.00	9	1432.35	17	0.00	1	-0.00 21
118	111	124	Max	79.00	0.00	1	0.00	1	0.00	9	1412.30	17	1123.64	17	-0.00 21
118	111	124	Min.	0.00	-22630.70	17	0.00	1	0.00	1	127.46	1	0.00	1	-0.17 17
118	111	124	Min.	79.00	-22630.70	17	0.00	1	0.00	1	112.61	1	94.83	1	-0.17 17
118	124	137	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	1123.64	17	-0.00 21
118	124	137	Max	38.76									1125.62	17	
118	124	137	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	1123.64	17	-0.00 21
118	124	137	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	94.83	1	-0.17 17
118	124	137	Min.	38.76									96.29	1	
118	124	137	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	94.83	1	-0.17 17
118	137	150	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	-0.00 21
118	137	150	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	-0.00 21
118	137	150	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	-0.17 17
118	137	150	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	-0.17 17
118	150	163	Max	0.00	0.00	1	0.00	1	0.00	1	1432.35	17	0.00	1	0.17 17
118	150	163	Max	79.00	0.00	1	0.00	1	0.00	1	1412.30	17	1123.64	17	0.17 17
118	150	163	Min.	0.00	-22630.70	17	0.00	1	0.00	9	127.46	1	0.00	1	0.00 9
118	150	163	Min.	79.00	-22630.70	17	0.00	1	0.00	9	112.61	1	94.83	1	0.00 9
118	163	176	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	1123.64	17	0.17 17
118	163	176	Max	38.76									1125.62	17	
118	163	176	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	1123.64	17	0.17 17
118	163	176	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	94.83	1	0.00 9
118	163	176	Min.	38.76									96.29	1	
118	163	176	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	94.83	1	0.00 9
118	176	189	Max	0.00	0.00	1	0.00	1	0.00	1	-112.61	1	1123.64	17	0.17 17
118	176	189	Max	79.00	0.00	1	0.00	1	0.00	1	-127.46	1	0.00	17	0.17 17
118	176	189	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1412.30	17	94.83	1	0.00 9
118	176	189	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1432.35	17	0.00	1	0.00 9
119	112	125	Max	0.00	0.00	1	0.00	1	0.00	9	1222.61	17	0.00	1	-0.00 21
119	112	125	Max	79.00	0.00	1	0.00	1	0.00	9	1202.56	17	957.94	17	-0.00 21
119	112	125	Min.	0.00	-22630.70	17	0.00	1	0.00	1	111.73	1	0.00	1	-0.30 17
119	112	125	Min.	79.00	-22630.70	17	0.00	1	0.00	1	96.88	1	82.40	1	-0.30 17
119	125	138	Max	0.00	0.00	1	0.00	1	0.00	1	10.02	17	957.94	17	-0.00 21
119	125	138	Max	38.76									959.92	17	
119	125	138	Max	79.00	0.00	1	0.00	1	0.00	1	-7.43	1	957.94	17	-0.00 21
119	125	138	Min.	0.00	-22630.70	17	0.00	1	0.00	9	7.43	1	82.40	1	-0.30 17
119	125	138	Min.	38.76									83.86	1	
119	125	138	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-10.02	17	82.40	1	-0.30 17
119	138	151	Max	0.00	0.00	1	0.00	1	0.00	1	-96.88	1	957.94	17	-0.00 21
119	138	151	Max	79.00	0.00	1	0.00	1	0.00	1	-111.73	1	0.00	17	-0.00 21
119	138	151	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1202.56	17	82.40	1	-0.30 17
119	138	151	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1222.61	17	0.00	1	-0.30 17
119	151	164	Max	0.00	0.00	1	0.00	1	0.00	1	1222.61	17	0.00	1	0.30 17
119	151	164	Max	79.00	0.00	1	0.00	1	0.00	1	1202.56	17	957.94	17	0.30 17
119	151	164	Min.	0.00	-22630.70	17	0.00	1	0.00	9	111.73	1	0.00	1	0.00 9
119	151	164	Min.	79.00	-22630.70	17	0.00	1	0.00	9	96.88	1	82.40	1	0.00 9
119	164	177	Max	0.00	0.00	1	0.00	1	0.00	9	10.02	17	957.94	17	0.30 17
119	164	177	Max	38.76									959.92	17	

119	164	177	Max	79.00	0.00	1	0.00	1	0.00	9	-7.43	1	957.94	17	0.30	17	
119	164	177	Min.	0.00	-22630.70	17	0.00	1	0.00	1	7.43	1	82.40	1	0.00	9	
119	164	177	Min.	38.76									83.86	1			
119	164	177	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-10.02	17	82.40	1	0.00	9	
119	177	190	Max	0.00	0.00	1	0.00	1	0.00	1	-96.88	1	957.94	17	0.30	17	
119	177	190	Max	79.00	0.00	1	0.00	1	0.00	1	-111.73	1	0.00	17	0.30	17	
119	177	190	Min.	0.00	-22630.70	17	0.00	1	0.00	9	-1202.56	17	82.40	1	0.00	9	
119	177	190	Min.	79.00	-22630.70	17	0.00	1	0.00	9	-1222.61	17	0.00	1	0.00	9	
120	113	126	Max	0.00	0.00	1	0.00	1	0.00	1	8.75	5	5.01	17	0.01	17	
120	113	126	Max	12.04									1.98	18			
120	113	126	Max	79.00	0.00	1	0.00	1	0.00	1	-6.10	5	-0.10	5	0.01	17	
120	113	126	Min.	0.00	-22630.70	17	0.00	1	0.00	1	-1.48	17	-1.15	5	0.00	1	
120	113	126	Min.	14.62									0.23	13			
120	113	126	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-21.53	17	-4.08	17	0.00	1	
120	126	139	Max	0.00	0.00	1	0.00	1	0.00	1	10.54	19	-0.90	20	0.00	9	
120	126	139	Max	30.99									0.07	18			
120	126	139	Max	79.00	0.00	1	0.00	1	0.00	1	-6.88	1	-1.28	9	0.00	9	
120	126	139	Min.	0.00	-22630.70	17	0.00	1	0.00	1	6.03	20	-4.88	17	0.00	19	
120	126	139	Min.	39.93									-2.85	17			
120	126	139	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-12.14	18	-4.79	17	0.00	19	
120	139	152	Max	0.00	0.00	1	0.00	1	0.00	1	36.10	17	-1.31	5	-0.00	9	
120	139	152	Max	58.30									1.63	19			
120	139	152	Max	79.00	0.00	1	0.00	1	0.00	1	16.05	17	11.07	17	-0.00	9	
120	139	152	Min.	0.00	-22630.70	17	0.00	1	0.00	1	9.27	5	-9.53	17	-0.01	17	
120	139	152	Min.	49.23									0.74	20			
120	139	152	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-7.31	18	-0.05	20	-0.01	17	
120	152	165	Max	0.00	0.00	1	0.00	1	0.00	1	6.73	19	10.36	17	0.01	17	
120	152	165	Max	14.85									1.31	18			
120	152	165	Max	79.00	0.00	1	0.00	1	0.00	1	-8.79	13	-1.36	13	0.01	17	
120	152	165	Min.	0.00	-22630.70	17	0.00	1	0.00	1	-15.19	17	-0.28	13	0.00	21	
120	152	165	Min.	15.80									0.56	7			
120	152	165	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-35.24	17	-9.55	17	0.00	21	
120	165	178	Max	0.00	0.00	1	0.00	1	0.00	1	10.54	17	-0.41	20	0.00	9	
120	165	178	Max	40.92									0.37	19			
120	165	178	Max	79.00	0.00	1	0.00	1	0.00	1	-7.20	21	-1.09	21	0.00	9	
120	165	178	Min.	0.00	-22630.70	17	0.00	1	0.00	1	4.50	20	-4.67	17	0.00	1	
120	165	178	Min.	41.53									-2.48	17			
120	165	178	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-14.39	18	-4.27	17	0.00	1	
120	178	191	Max	0.00	0.00	1	0.00	1	0.00	1	21.66	17	-0.38	13	0.00	9	
120	178	191	Max	63.20									1.46	22			
120	178	191	Max	79.00	0.00	1	0.00	1	0.00	1	1.61	17	4.70	17	0.00	9	
120	178	191	Min.	0.00	-22630.70	17	0.00	1	0.00	1	6.18	20	-4.49	17	-0.01	17	
120	178	191	Min.	64.27									0.02	5			
120	178	191	Min.	79.00	-22630.70	17	0.00	1	0.00	1	-11.97	18	-2.04	18	-0.01	17	

Sollecitazioni elementi bidimensionali

Simbologia

Bid. = Numero del muro/elemento bidimensionale
Nodo = Numero del nodo
σ_{xx} = Tensione normale sulle facce perp. all'asse X
CC = Numero della combinazione delle condizioni di carico elementari
σ_{zz} = Tensione normale sulle facce perp. all'asse Z
τ_{xz} = Tensione in dir. Z sulle facce perp. all'asse X
Mxx = Momento che provoca variazione di tensione sulle facce perp. all'asse X
Mzz = Momento che provoca variazione di tensione sulle facce perp. all'asse Z
Mxz = Momento che provoca variazione di tensione tangenziale sulle facce perp. all'asse X
τ_{zy} = Tensione in dir. Y sulle facce perp. all'asse Z
τ_{xy} = Tensione in dir. Y sulle facce perp. all'asse X

Bid.	Nodo	σ_{xx} <daN/mq>	CC	σ_{zz} <daN/mq>	CC	τ_{xz} <daN/mq>	CC	Mxx <daNm/m>	CC	Mzz <daNm/m>	CC	Mxz <daNm/m>	CC	τ_{zy} <daN/mq>	CC	τ_{xy} <daN/mq>	CC
102	Max	-196	-68.02	13	-15883.50	20	4175.43	18	1574.96	1	15328.40	1	1292.11	9	4693.02	9	668.43	9
102	Max	-170	-68.02	13	-15883.50	20	4175.43	18	1574.96	1	15328.40	1	1292.11	9	4693.02	9	668.43	9
102	Max	-378	-68.02	13	-15883.50	20	4175.43	18	1574.96	1	15328.40	1	1292.11	9	4693.02	9	668.43	9
102	Max	-381	-68.02	13	-15883.50	20	4175.43	18	1574.96	1	15328.40	1	1292.11	9	4693.02	9	668.43	9
102	Min.	-196	-2819.66	18	-37676.10	17	-17875.60	17	-1573.10	9	-15322.10	9	-1290.73	1	-4695.08	1	-666.46	1
102	Min.	-170	-2819.66	18	-37676.10	17	-17875.60	17	-1573.10	9	-15322.10	9	-1290.73	1	-4695.08	1	-666.46	1
102	Min.	-378	-2819.66	18	-37676.10	17	-17875.60	17	-1573.10	9	-15322.10	9	-1290.73	1	-4695.08	1	-666.46	1
102	Min.	-381	-2819.66	18	-37676.10	17	-17875.60	17	-1573.10	9	-15322.10	9	-1290.73	1	-4695.08	1	-666.46	1
102	Max	-235	-300.29	5	-14064.30	20	35170.40	18	1108.25	1	15165.10	1	821.75	9	4292.31	9	1455.72	9
102	Max	-196	-300.29	5	-14064.30	20	35170.40	18	1108.25	1	15165.10	1	821.75	9	4292.31	9	1455.72	9
102	Max	-381	-300.29	5	-14064.30	20	35170.40	18	1108.25	1	15165.10	1	821.75	9	4292.31	9	1455.72	9
102	Max	-384	-300.29	5	-14064.30	20	35170.40	18	1108.25	1	15165.10	1	821.75	9	4292.31	9	1455.72	9
102	Min.	-235	-21690.00	18	-36867.20	17	8535.49	5	-1107.89	9	-15160.20	9	-821.27	1	-4292.85	1	-1454.34	1
102	Min.	-196	-21690.00	18	-36867.20	17	8535.49	5	-1107.89	9	-15160.20	9	-821.27	1	-4292.85	1	-1454.34	1
102	Min.	-381	-21690.00	18	-36867.20	17	8535.49	5	-1107.89	9	-15160.20	9	-821.27	1	-4292.85	1	-1454.34	1
102	Min.	-384	-21690.00	18	-36867.20	17	8535.49	5	-1107.89	9	-15160.20	9	-821.27	1	-4292.85	1	-1454.34	1
102	Max	-257	375.81	13	21492.60	18	20183.50	18	220.30	1	13390.70	1	860.74	9	208.13	9	1026.26	9
102	Max	-235	375.81	13	21492.60	18	20183.50	18	220.30	1	13390.70	1	860.74	9	208.13	9	1026.26	9
102	Max	-384	375.81	13	21492.60	18	20183.50	18	220.30	1	13390.70	1	860.74	9	208.13	9	1026.26	9
102	Max	-387	375.81	13	21492.60	18	20183.50	18	220.30	1	13390.70	1	860.74	9	208.13	9	1026.26	9
102	Min.	-257	-23345.90	18	-9540.96	5	-1290.01	5	-220.17	9	-13386.80	9	-860.16	1	-358.33	19	-1025.19	1
102	Min.	-235	-23345.90	18	-9540.96	5	-1290.01	5	-220.17	9	-13386.80	9	-860.16	1	-358.33	19	-1025.19	1
102	Min.	-384	-23345.90	18	-9540.96	5	-1290.01	5	-220.17	9	-13386.80	9	-860.16	1	-358.33	19	-1025.19	1
102	Min.	-387	-23345.90	18	-9540.96	5	-1290.01	5	-220.17	9	-13386.80	9	-860.16	1	-358.33	19	-1025.19	1

102	Max	-170	-741.08	13	4084.62	18	14354.50	18	894.60	1	12411.90	1	113.20	9	240.78	9	194.96	9
102	Max	-147	-741.08	13	4084.62	18	14354.50	18	894.60	1	12411.90	1	113.20	9	240.78	9	194.96	9
102	Max	-375	-741.08	13	4084.62	18	14354.50	18	894.60	1	12411.90	1	113.20	9	240.78	9	194.96	9
102	Max	-378	-741.08	13	4084.62	18	14354.50	18	894.60	1	12411.90	1	113.20	9	240.78	9	194.96	9
102	Min.	-170	-6208.45	18	-6328.89	17	-2653.12	5	-892.20	9	-12404.60	9	-111.46	1	-243.46	1	-190.99	1
102	Min.	-147	-6208.45	18	-6328.89	17	-2653.12	5	-892.20	9	-12404.60	9	-111.46	1	-243.46	1	-190.99	1
102	Min.	-375	-6208.45	18	-6328.89	17	-2653.12	5	-892.20	9	-12404.60	9	-111.46	1	-243.46	1	-190.99	1
102	Min.	-378	-6208.45	18	-6328.89	17	-2653.12	5	-892.20	9	-12404.60	9	-111.46	1	-243.46	1	-190.99	1
102	Max	-147	-234.99	13	-17437.10	5	32141.80	18	1630.48	1	15414.50	9	1162.77	9	4878.68	1	982.53	9
102	Max	-121	-234.99	13	-17437.10	5	32141.80	18	1630.48	1	15414.50	9	1162.77	9	4878.68	1	982.53	9
102	Max	-372	-234.99	13	-17437.10	5	32141.80	18	1630.48	1	15414.50	9	1162.77	9	4878.68	1	982.53	9
102	Max	-375	-234.99	13	-17437.10	5	32141.80	18	1630.48	1	15414.50	9	1162.77	9	4878.68	1	982.53	9
102	Min.	-147	-10332.30	18	-36340.90	17	6819.92	5	-1627.97	9	-15402.30	1	-1159.38	1	-4891.84	9	-978.36	1
102	Min.	-121	-10332.30	18	-36340.90	17	6819.92	5	-1627.97	9	-15402.30	1	-1159.38	1	-4891.84	9	-978.36	1
102	Min.	-372	-10332.30	18	-36340.90	17	6819.92	5	-1627.97	9	-15402.30	1	-1159.38	1	-4891.84	9	-978.36	1
102	Min.	-375	-10332.30	18	-36340.90	17	6819.92	5	-1627.97	9	-15402.30	1	-1159.38	1	-4891.84	9	-978.36	1
102	Max	-121	-1260.61	13	-17164.40	13	-5808.90	20	1560.40	9	15389.10	9	1199.79	9	5053.37	1	1281.84	9
102	Max	-99	-1260.61	13	-17164.40	13	-5808.90	20	1560.40	9	15389.10	9	1199.79	9	5053.37	1	1281.84	9
102	Max	-369	-1260.61	13	-17164.40	13	-5808.90	20	1560.40	9	15389.10	9	1199.79	9	5053.37	1	1281.84	9
102	Max	-372	-1260.61	13	-17164.40	13	-5808.90	20	1560.40	9	15389.10	9	1199.79	9	5053.37	1	1281.84	9
102	Min.	-121	-2314.51	17	-37909.00	17	-15569.90	17	-1550.64	1	-15381.80	1	-1189.83	1	-5071.37	9	-1276.84	1
102	Min.	-99	-2314.51	17	-37909.00	17	-15569.90	17	-1550.64	1	-15381.80	1	-1189.83	1	-5071.37	9	-1276.84	1
102	Min.	-369	-2314.51	17	-37909.00	17	-15569.90	17	-1550.64	1	-15381.80	1	-1189.83	1	-5071.37	9	-1276.84	1
102	Min.	-372	-2314.51	17	-37909.00	17	-15569.90	17	-1550.64	1	-15381.80	1	-1189.83	1	-5071.37	9	-1276.84	1
102	Max	-99	-691.22	13	-438.35	5	6651.06	18	590.55	9	12584.50	9	274.81	9	868.22	1	774.89	9
102	Max	-67	-691.22	13	-438.35	5	6651.06	18	590.55	9	12584.50	9	274.81	9	868.22	1	774.89	9
102	Max	-366	-691.22	13	-438.35	5	6651.06	18	590.55	9	12584.50	9	274.81	9	868.22	1	774.89	9
102	Max	-369	-691.22	13	-438.35	5	6651.06	18	590.55	9	12584.50	9	274.81	9	868.22	1	774.89	9
102	Min.	-99	-4591.03	18	-10453.40	17	-1979.21	13	-585.01	1	-12605.20	1	-263.59	1	-866.50	9	-763.01	1
102	Min.	-67	-4591.03	18	-10453.40	17	-1979.21	13	-585.01	1	-12605.20	1	-263.59	1	-866.50	9	-763.01	1
102	Min.	-366	-4591.03	18	-10453.40	17	-1979.21	13	-585.01	1	-12605.20	1	-263.59	1	-866.50	9	-763.01	1
102	Min.	-369	-4591.03	18	-10453.40	17	-1979.21	13	-585.01	1	-12605.20	1	-263.59	1	-866.50	9	-763.01	1
102	Max	-67	-237.31	13	-5055.59	13	16143.90	18	231.57	9	13842.40	9	681.48	9	2126.95	1	1051.65	9
102	Max	-50	-237.31	13	-5055.59	13	16143.90	18	231.57	9	13842.40	9	681.48	9	2126.95	1	1051.65	9
102	Max	-363	-237.31	13	-5055.59	13	16143.90	18	231.57	9	13842.40	9	681.48	9	2126.95	1	1051.65	9
102	Max	-366	-237.31	13	-5055.59	13	16143.90	18	231.57	9	13842.40	9	681.48	9	2126.95	1	1051.65	9
102	Min.	-67	-5635.09	18	-44036.40	18	2151.31	13	-233.69	1	-13908.30	1	-667.18	1	-2067.24	9	-1053.89	1
102	Min.	-50	-5635.09	18	-44036.40	18	2151.31	13	-233.69	1	-13908.30	1	-667.18	1	-2067.24	9	-1053.89	1
102	Min.	-363	-5635.09	18	-44036.40	18	2151.31	13	-233.69	1	-13908.30	1	-667.18	1	-2067.24	9	-1053.89	1
102	Min.	-366	-5635.09	18	-44036.40	18	2151.31	13	-233.69	1	-13908.30	1	-667.18	1	-2067.24	9	-1053.89	1
102	Max	-468	735.47	17	-2674.40	5	742.74	17	19.00	1	3946.91	1	210.86	9	3611.41	9	49.67	1
102	Max	-465	735.47	17	-2674.40	5	742.74	17	19.00	1	3946.91	1	210.86	9	3611.41	9	49.67	1
102	Max	-492	735.47	17	-2674.40	5	742.74	17	19.00	1	3946.91	1	210.86	9	3611.41	9	49.67	1
102	Max	-495	735.47	17	-2674.40	5	742.74	17	19.00	1	3946.91	1	210.86	9	3611.41	9	49.67	1
102	Min.	-468	-4789.97	18	-14515.40	17	-1035.97	18	-18.89	9	-3946.38	9	-211.31	1	-3613.52	1	-49.49	9
102	Min.	-465	-4789.97	18	-14515.40	17	-1035.97	18	-18.89	9	-3946.38	9	-211.31	1	-3613.52	1	-49.49	9
102	Min.	-492	-4789.97	18	-14515.40	17	-1035.97	18	-18.89	9	-3946.38	9	-211.31	1	-3613.52	1	-49.49	9
102	Min.	-495	-4789.97	18	-14515.40	17	-1035.97	18	-18.89	9	-3946.38	9	-211.31	1	-3613.52	1	-49.49	9
102	Max	-495	686.17	17	-1814.79	5	-86.15	5	7.42	1	1314.64	1	234.78	9	3687.09	9	11.74	1
102	Max	-492	686.17	17	-1814.79	5	-86.15	5	7.42	1	1314.64	1	234.78	9	3687.09	9	11.74	1
102	Max	185	686.17	17	-1814.79	5	-86.15	5	7.42	1	1314.64	1	234.78	9	3687.09	9	11.74	1
102	Max	-501	686.17	17	-1814.79	5	-86.15	5	7.42	1	1314.64	1	234.78	9	3687.09	9	11.74	1
102	Min.	-495	73.37	20	-11019.00	17	-3300.30	17	-7.38	9	-1314.51	9	-235.42	1	-3689.49	1	-11.68	9
102	Min.	-492	73.37	20	-11019.00	17	-3300.30	17	-7.38	9	-1314.51	9	-235.42	1	-3689.49	1	-11.68	9
102	Min.	185	73.37	20	-11019.00	17	-3300.30	17	-7.38	9	-1314.51	9	-235.42	1	-3689.49	1	-11.68	9
102	Min.	-501	73.37	20	-11019.00	17	-3300.30	17	-7.38	9	-1314.51	9	-235.42	1	-3689.49	1	-11.68	9
102	Max	-384	3972.53	17	-7029.69	20	11085.50	18	585.47	1	11858.70	1	351.49	9	3210.51	9	981.26	9
102	Max	-381	3972.53	17	-7029.69	20	11085.50	18	585.47	1	11858.70	1	351.49	9	3210.51	9	981.26	9
102	Max	-408	3972.53	17	-7029.69	20	11085.50	18	585.47	1	11858.70	1	351.49	9	3210.51	9	981.26	9
102	Max	-411	3972.53	17	-7029.69	20	11085.50	18	585.47	1	11858.70	1	351.49	9	3210.51	9	981.26	9
102	Min.	-384	-21151.80	18	-25694.90	17	138.63	5	-584.66	9	-11854.90	9	-350.46	1	-3211.71	1	-979.97	1
102	Min.	-381	-21151.80	18	-25694.90	17	138.63	5	-584.66	9	-11854.90	9	-350.46	1	-3211.71	1	-979.97	1
102	Min.	-408	-21151.80	18	-25694.90	17	138.63	5	-584.66	9	-11854.90	9	-350.46	1	-3211.71	1	-979.97	1
102	Min.	-411	-21151.80	18	-25694.90	17	138.63	5	-584.66	9	-11854.90	9	-350.46	1	-3211.71	1	-979.97	1
102	Max	-411	1163.63	17	-5017.71	5	1838.06	5	326.72	1	9161.39	1	54.16	9	2886.92	9	88.83	9
102	Max	-408	1163.63	17	-5017.71	5	1838.06	5	326.72	1	9161.39	1	54.16	9	2886.92	9	88.83	9
102	Max	-435	1163.63	17	-5017.71	5	1838.06	5	326.72	1	9161.39	1	54.16	9	2886.92	9	88.83	9
102	Max	-438	1163.63	17	-5017.71	5	1838.06	5	326.72	1	9161.39	1	54.16	9	2886.92	9	88.83	9
102	Min.	-411	-22425.10	18	-19478.40	17	-440.58	13	-325.85	9	-9159.16	9	-169.47	19	-2888.38	1	-88.32	1
102	Min.	-408	-22425.10	18	-19478.40	17	-440.58	13	-325.85	9	-9159.16	9	-169.47	19	-2888.38	1	-88.32	1
102	Min.	-435	-22425.10	18	-19478.40	17	-440.58	13	-325.85	9	-9159.16	9	-169.47	19	-2888.38	1	-88.32	1
102	Min.	-438	-22425.10	18	-19478.40	17	-440.58	13	-325.85	9	-9159.16	9	-169.47	19	-2888.38	1	-88.32	1
102	Max	-438	3.47	13	-4142.71	5	1466.63	5	184.95	1	6555.25	1	202.13	9	2904.15	9	130.89	9
102	Max	-435	3.47	13	-4142.71	5	1466.63	5	184.95	1	6555.25	1	202.13	9	2904.15	9	130.89	9
102	Max	-462	3.47	13	-4142.71	5	1466.63	5	184.95	1	6555.25	1	202.13	9	2904.15	9	130.89	9
102	Max	-465	3.47	13	-4142.71	5	1466.63	5	184.95	1	6555.25	1	202.13	9	2904.15	9	130.89	9
102	Min.	-438	-14031.90	18	-16841.00	17	-1211.54	18	-184.14	9	-6554.27	9	-202.37	1	-2905.42	1	-130.60	1
102	Min.	-435	-14031.90	18	-16841.00	17	-1211.54	18	-184.14	9	-6554.27	9	-202.37	1	-2905.42	1	-130.60	1
102	Min.	-462	-14031.90	18	-16841.00	17	-1211.54	18	-184.14	9	-6554.27	9	-202.37	1	-2905.42	1	-130.60	1
102	Min.	-465	-14031.90	18	-16841.00	17	-1211.54	18	-184.14	9	-6554.27	9	-202.37	1	-2905.42	1	-130.60	1
102	Max	-465	211.76	17	-2866.35	5	1342.38	5	99.10	1	3923.71	1	290.43	9	2891.19	9	64.32	9
102	Max	-462	211.76	17	-2866.35	5	1342.38	5	99.10	1	3923.71	1	290.43	9	2891.19	9	64.32	9
102	Max	-489	211.76	17	-2866.35	5	1342.38	5	99.10	1	3923.71	1	290.43	9	2891.19	9	64.32	9
102	Max	-492	211.76	17	-2866.35	5	1342.38	5	99.10	1	3923.71	1	290.43	9	2891.19	9	64.32	9
102	Min.	-465	-5699.96	18	-12696.00	17	-1575.06	18	-98.56	9	-3923.41	9	-291.36	1	-2892.15	1	-64.18	1
102	Min.	-462	-5699.96	18	-12696.00	17	-1575.06	18	-98.56	9	-3923.41	9	-291.36	1	-2892.15	1	-64.18	1
102	Min.	-489	-5699.96	18	-12696.00	17	-1575.06	18	-98.56	9	-3923.41	9	-291.36	1	-2892.15	1	-64.18	1
102	Min.	-492	-5699.96	18	-12696.00	17	-1575.06	18	-98.56	9	-3923.41	9	-291.36	1	-2892.15	1	-64.18	1
102	Max	-492	24.91	5	-2099.87	5	4349.63	17	31.64	1	1306.06	1	336.20	9	2881.96	9	19.84	9
102	Max	-489	24.91	5	-2099.87	5	4349.63	17	31.64	1	1306.06	1	336.20	9	2881.96	9	19.84	9
102	Max	172	24.91	5	-2099.87	5	4349.63	17	31.64	1	1306.06	1	336.20	9	2881.96	9	19.84	9
102	Max	185	24.91	5	-2099.87	5	4349.63	17	31.64	1	1306.06	1	336.20	9	2881.96	9	19.84	9
102	Min.	-492	-1082.55	18	-12498.70	17	-552.50	13	-31.45	9	-1306.01	9	-337.50	1	-2882.73	1	-19.80	1
102	Min.	-489	-1082.55	18	-12498.70	17	-552.50	13	-31.45	9	-1306.01	9	-337.50	1	-2882.73	1	-19.80	1
102	Min.	172	-1082.55	18	-12498.70	17	-552.50	13	-31.45	9	-1306.01	9	-337.50	1	-2882.73	1	-19.80	1
102	Min.	185	-1082.55	18	-12498.70	17	-552.50	13	-31.45	9	-1306.01	9	-337.50	1	-2882.73	1	-19.80	1
102	Max	-381	2598.98	17	-6603.09	20	9460.94	18	806.04	1	11631.50	1	97.36	9	3142.74	9	652.32	9
102	Max	-378	2598.98	17	-6603.09	20	9460.94	18	806.04	1	11631.50	1	97.36	9	3142.74	9	652.32	9
102	Max	-405	2598.98	17	-6603.09	20	9460.94	18	806.04	1	11631.50	1	97.36	9	3142.74	9	652.32	9
102	Max	-408	2598.98	17	-6603.09	20	9460.94	18	806.04	1	11631.50	1	97.36	9	3142.74	9	652.32	9
102	Min.	-381	-16266.00	18	-24971.50	17	-3763.46	5	-804.27	9	-11627.80	9	-147.28	19	-3145.08	1	-651.11	1
102	Min.	-378	-16266.00	18	-24971.50	17	-3763.46	5	-804.27	9	-11627.80	9	-147.28	19	-3145.08	1	-651.11	1
102	Min.	-405	-16266.00	18	-24971.50	17	-3763.46	5	-804.27	9	-11627.80	9	-147.28	19	-3145.08	1	-651.11	1
102	Min.	-408	-16266.00	18	-24971.50	17	-3763.46	5	-804.27	9	-11627.80	9	-147.28	19	-3145.08	1	-651.11	1
102	Max	-408	618.75	17	-5947.33	20	5522.30	18	618.42	1	9064.50	1	44.76	9	2915.91	9	259.67	9
102	Max	-405	618.75	17	-5947.33	20	5522.30	18	618.42	1	9064.50	1	44.76	9	2915.91	9	259.67	9
102	Max	-432	618.75	17	-5947.33	20	5522.30	18	618.42	1	9064.50	1	44.76	9	2915.91	9	259.67	9
102	Max	-435	618.75	17	-5947.33	20	5522.30	18	618.42	1	9064.50	1	44.76	9	2915.91	9	259.67	9
102	Min.	-408	-17059.90	18	-21260.60	17	-1724.16	13	-616.36	9	-9063.12	9	-182.75	19	-2917.95	1	-259.33	1

102	Min.	-405	-17059.90	18	-21260.60	17	-1724.16	13	-616.36	9	-9063.12	9	-182.75	19	-2917.95	1	-259.33	1
102	Min.	-432	-17059.90	18	-21260.60	17	-1724.16	13	-616.36	9	-9063.12	9	-182.75	19	-2917.95	1	-259.33	1
102	Min.	-435	-17059.90	18	-21260.60	17	-1724.16	13	-616.36	9	-9063.12	9	-182.75	19	-2917.95	1	-259.33	1
102	Max	-435	950.96	17	-5327.29	13	2142.16	5	354.39	1	6468.09	1	116.48	9	2862.54	9	80.95	9
102	Max	-432	950.96	17	-5327.29	13	2142.16	5	354.39	1	6468.09	1	116.48	9	2862.54	9	80.95	9
102	Max	-459	950.96	17	-5327.29	13	2142.16	5	354.39	1	6468.09	1	116.48	9	2862.54	9	80.95	9
102	Max	-462	950.96	17	-5327.29	13	2142.16	5	354.39	1	6468.09	1	116.48	9	2862.54	9	80.95	9
102	Min.	-435	-11804.00	18	-17412.20	17	-1756.12	13	-352.69	9	-6467.98	9	-200.14	19	-2863.87	1	-81.13	1
102	Min.	-432	-11804.00	18	-17412.20	17	-1756.12	13	-352.69	9	-6467.98	9	-200.14	19	-2863.87	1	-81.13	1
102	Min.	-459	-11804.00	18	-17412.20	17	-1756.12	13	-352.69	9	-6467.98	9	-200.14	19	-2863.87	1	-81.13	1
102	Min.	-462	-11804.00	18	-17412.20	17	-1756.12	13	-352.69	9	-6467.98	9	-200.14	19	-2863.87	1	-81.13	1
102	Max	-462	-63.85	5	-3638.85	13	1946.01	5	197.02	1	3873.57	1	198.37	9	2803.26	9	39.29	9
102	Max	-459	-63.85	5	-3638.85	13	1946.01	5	197.02	1	3873.57	1	198.37	9	2803.26	9	39.29	9
102	Max	-486	-63.85	5	-3638.85	13	1946.01	5	197.02	1	3873.57	1	198.37	9	2803.26	9	39.29	9
102	Max	-489	-63.85	5	-3638.85	13	1946.01	5	197.02	1	3873.57	1	198.37	9	2803.26	9	39.29	9
102	Min.	-462	-6375.03	18	-14295.20	17	-1970.11	13	-195.97	9	-3873.79	9	-208.87	19	-2803.99	1	-39.49	1
102	Min.	-459	-6375.03	18	-14295.20	17	-1970.11	13	-195.97	9	-3873.79	9	-208.87	19	-2803.99	1	-39.49	1
102	Min.	-486	-6375.03	18	-14295.20	17	-1970.11	13	-195.97	9	-3873.79	9	-208.87	19	-2803.99	1	-39.49	1
102	Min.	-489	-6375.03	18	-14295.20	17	-1970.11	13	-195.97	9	-3873.79	9	-208.87	19	-2803.99	1	-39.49	1
102	Max	-489	-144.09	5	-1036.33	13	1898.11	5	61.86	1	1290.73	1	234.03	9	2779.20	9	12.80	9
102	Max	-486	-144.09	5	-1036.33	13	1898.11	5	61.86	1	1290.73	1	234.03	9	2779.20	9	12.80	9
102	Max	159	-144.09	5	-1036.33	13	1898.11	5	61.86	1	1290.73	1	234.03	9	2779.20	9	12.80	9
102	Max	172	-144.09	5	-1036.33	13	1898.11	5	61.86	1	1290.73	1	234.03	9	2779.20	9	12.80	9
102	Min.	-489	-1955.06	18	-3997.53	17	-2019.62	13	-61.52	9	-1290.85	9	-235.84	1	-2779.66	1	-12.87	1
102	Min.	-486	-1955.06	18	-3997.53	17	-2019.62	13	-61.52	9	-1290.85	9	-235.84	1	-2779.66	1	-12.87	1
102	Min.	159	-1955.06	18	-3997.53	17	-2019.62	13	-61.52	9	-1290.85	9	-235.84	1	-2779.66	1	-12.87	1
102	Min.	172	-1955.06	18	-3997.53	17	-2019.62	13	-61.52	9	-1290.85	9	-235.84	1	-2779.66	1	-12.87	1
102	Max	-378	-2314.79	13	-8336.22	20	13675.60	18	1161.48	1	11740.40	1	110.19	9	2894.79	9	77.56	9
102	Max	-375	-2314.79	13	-8336.22	20	13675.60	18	1161.48	1	11740.40	1	110.19	9	2894.79	9	77.56	9
102	Max	-402	-2314.79	13	-8336.22	20	13675.60	18	1161.48	1	11740.40	1	110.19	9	2894.79	9	77.56	9
102	Max	-405	-2314.79	13	-8336.22	20	13675.60	18	1161.48	1	11740.40	1	110.19	9	2894.79	9	77.56	9
102	Min.	-378	-15222.30	18	-23117.20	17	-3104.14	5	-1158.14	9	-11737.30	9	-145.73	19	-2899.06	1	-80.59	19
102	Min.	-375	-15222.30	18	-23117.20	17	-3104.14	5	-1158.14	9	-11737.30	9	-145.73	19	-2899.06	1	-80.59	19
102	Min.	-402	-15222.30	18	-23117.20	17	-3104.14	5	-1158.14	9	-11737.30	9	-145.73	19	-2899.06	1	-80.59	19
102	Min.	-405	-15222.30	18	-23117.20	17	-3104.14	5	-1158.14	9	-11737.30	9	-145.73	19	-2899.06	1	-80.59	19
102	Max	-405	1430.19	17	-7203.36	20	6971.93	18	662.12	1	9026.43	1	60.25	9	3069.87	9	42.39	9
102	Max	-402	1430.19	17	-7203.36	20	6971.93	18	662.12	1	9026.43	1	60.25	9	3069.87	9	42.39	9
102	Max	-429	1430.19	17	-7203.36	20	6971.93	18	662.12	1	9026.43	1	60.25	9	3069.87	9	42.39	9
102	Max	-432	1430.19	17	-7203.36	20	6971.93	18	662.12	1	9026.43	1	60.25	9	3069.87	9	42.39	9
102	Min.	-405	-10948.50	18	-21448.30	17	-2476.37	13	-658.88	9	-9026.58	9	-184.57	19	-3072.56	1	-47.23	19
102	Min.	-402	-10948.50	18	-21448.30	17	-2476.37	13	-658.88	9	-9026.58	9	-184.57	19	-3072.56	1	-47.23	19
102	Min.	-429	-10948.50	18	-21448.30	17	-2476.37	13	-658.88	9	-9026.58	9	-184.57	19	-3072.56	1	-47.23	19
102	Min.	-432	-10948.50	18	-21448.30	17	-2476.37	13	-658.88	9	-9026.58	9	-184.57	19	-3072.56	1	-47.23	19
102	Max	-432	675.73	17	-5679.46	20	2457.99	18	469.26	1	6394.32	1	83.30	9	2870.25	9	11.73	9
102	Max	-429	675.73	17	-5679.46	20	2457.99	18	469.26	1	6394.32	1	83.30	9	2870.25	9	11.73	9
102	Max	-456	675.73	17	-5679.46	20	2457.99	18	469.26	1	6394.32	1	83.30	9	2870.25	9	11.73	9
102	Max	-459	675.73	17	-5679.46	20	2457.99	18	469.26	1	6394.32	1	83.30	9	2870.25	9	11.73	9
102	Min.	-432	-9040.84	18	-18353.90	17	-2366.20	13	-466.90	9	-6395.38	9	-203.27	19	-2871.38	1	-23.64	19
102	Min.	-429	-9040.84	18	-18353.90	17	-2366.20	13	-466.90	9	-6395.38	9	-203.27	19	-2871.38	1	-23.64	19
102	Min.	-456	-9040.84	18	-18353.90	17	-2366.20	13	-466.90	9	-6395.38	9	-203.27	19	-2871.38	1	-23.64	19
102	Min.	-459	-9040.84	18	-18353.90	17	-2366.20	13	-466.90	9	-6395.38	9	-203.27	19	-2871.38	1	-23.64	19
102	Max	-459	1394.32	17	-4257.87	20	2137.00	5	248.19	1	3839.44	1	121.94	9	2816.66	9	6.40	9
102	Max	-456	1394.32	17	-4257.87	20	2137.00	5	248.19	1	3839.44	1	121.94	9	2816.66	9	6.40	9
102	Max	-483	1394.32	17	-4257.87	20	2137.00	5	248.19	1	3839.44	1	121.94	9	2816.66	9	6.40	9
102	Max	-486	1394.32	17	-4257.87	20	2137.00	5	248.19	1	3839.44	1	121.94	9	2816.66	9	6.40	9
102	Min.	-459	-5032.18	18	-15702.80	17	-2495.38	13	-246.87	9	-3840.24	9	-211.36	19	-2817.14	1	-11.03	19
102	Min.	-456	-5032.18	18	-15702.80	17	-2495.38	13	-246.87	9	-3840.24	9	-211.36	19	-2817.14	1	-11.03	19
102	Min.	-483	-5032.18	18	-15702.80	17	-2495.38	13	-246.87	9	-3840.24	9	-211.36	19	-2817.14	1	-11.03	19
102	Min.	-486	-5032.18	18	-15702.80	17	-2495.38	13	-246.87	9	-3840.24	9	-211.36	19	-2817.14	1	-11.03	19
102	Max	-486	110.23	17	-2748.99	13	1381.35	5	78.53	1	1279.93	1	138.41	9	2791.12	9	2.03	9
102	Max	-483	110.23	17	-2748.99	13	1381.35	5	78.53	1	1279.93	1	138.41	9	2791.12	9	2.03	9
102	Max	146	110.23	17	-2748.99	13	1381.35	5	78.53	1	1279.93	1	138.41	9	2791.12	9	2.03	9
102	Max	159	110.23	17	-2748.99	13	1381.35	5	78.53	1	1279.93	1	138.41	9	2791.12	9	2.03	9
102	Min.	-486	-1621.31	18	-17247.30	17	-7478.54	17	-78.11	9	-1280.21	9	-214.43	19	-2791.37	1	-3.18	19
102	Min.	-483	-1621.31	18	-17247.30	17	-7478.54	17	-78.11	9	-1280.21	9	-214.43	19	-2791.37	1	-3.18	19
102	Min.	146	-1621.31	18	-17247.30	17	-7478.54	17	-78.11	9	-1280.21	9	-214.43	19	-2791.37	1	-3.18	19
102	Min.	159	-1621.31	18	-17247.30	17	-7478.54	17	-78.11	9	-1280.21	9	-214.43	19	-2791.37	1	-3.18	19
102	Max	-375	1380.82	17	-10753.50	13	13326.30	18	1012.23	9	11533.90	9	128.85	9	3262.49	1	809.21	9
102	Max	-372	1380.82	17	-10753.50	13	13326.30	18	1012.23	9	11533.90	9	128.85	9	3262.49	1	809.21	9
102	Max	-399	1380.82	17	-10753.50	13	13326.30	18	1012.23	9	11533.90	9	128.85	9	3262.49	1	809.21	9
102	Max	-402	1380.82	17	-10753.50	13	13326.30	18	1012.23	9	11533.90	9	128.85	9	3262.49	1	809.21	9
102	Min.	-375	-4119.72	18	-24741.10	17	-964.26	13	-1007.21	1	-11533.10	1	-143.82	19	-3269.64	9	-810.13	1
102	Min.	-372	-4119.72	18	-24741.10	17	-964.26	13	-1007.21	1	-11533.10	1	-143.82	19	-3269.64	9	-810.13	1
102	Min.	-399	-4119.72	18	-24741.10	17	-964.26	13	-1007.21	1	-11533.10	1	-143.82	19	-3269.64	9	-810.13	1
102	Min.	-402	-4119.72	18	-24741.10	17	-964.26	13	-1007.21	1	-11533.10	1	-143.82	19	-3269.64	9	-810.13	1
102	Max	-402	376.71	17	-8795.75	13	6952.01	18	766.01	9	8926.06	9	62.15	9	2932.53	1	247.73	9
102	Max	-399	376.71	17	-8795.75	13	6952.01	18	766.01	9	8926.06	9	62.15	9	2932.53	1	247.73	9
102	Max	-426	376.71	17	-8795.75	13	6952.01	18	766.01	9	8926.06	9	62.15	9	2932.53	1	247.73	9
102	Max	-429	376.71	17	-8795.75	13	6952.01	18	766.01	9	8926.06	9	62.15	9	2932.53	1	247.73	9
102	Min.	-402	-7507.69	18	-21381.50	17	-2686.15	13	-762.12	1	-8928.69	1	-185.09	19	-2934.57	9	-250.99	1
102	Min.	-399	-7507.69	18	-21381.50	17	-2686.15	13	-762.12	1	-8928.69	1	-185.09	19	-2934.57	9	-250.99	1
102	Min.	-426	-7507.69	18	-21381.50	17	-2686.15	13	-762.12	1	-8928.69	1	-185.09	19	-2934.57	9	-250.99	1
102	Min.	-429	-7507.69	18	-21381.50	17	-2686.15	13	-762.12	1	-8928.69	1	-185.09	19	-2934.57	9	-250.99	1
102	Max	-429	870.39	17	-6538.65	13	3056.85	18	452.60	9	6382.45	9	76.34	9	2866.89	1	64.71	9
102	Max	-426	870.39	17	-6538.65	13	3056.85	18	452.60	9	6382.45	9	76.34	9	2866.89	1	64.71	9
102	Max	-453	870.39	17	-6538.65	13	3056.85	18	452.60	9	6382.45	9	76.34	9	2866.89	1	64.71	9
102	Max	-456	870.39	17	-6538.65	13	3056.85	18	452.60	9	6382.45	9	76.34	9	2866.89	1	64.71	9
102	Min.	-429	-5697.65	18	-18328.20	17	-2579.66	13	-450.21	1	-6384.68	1	-204.11	19	-2867.21	9	-66.56	1
102	Min.	-426	-5697.65	18	-18328.20	17	-2579.66	13	-450.21	1	-6384.68	1	-204.11	19	-2867.21	9	-66.56	1
102	Min.	-453	-5697.65	18	-18328.20	17	-2579.66	13	-450.21	1	-6384.68	1	-204.11	19	-2867.21	9	-66.56	1
102	Min.	-456	-5697.65	18	-18328.20	17	-2579.66	13	-450.21	1	-6384.68	1	-204.11	19	-2867.21	9	-66.56	1
102	Max	-456	1393.71	17	-4370.56	13	2144.76	13	246.99	9	3830.03	9	61.61	9	2807.58	1	31.02	9
102	Max	-453	1393.71	17	-4370.56	13	2144.76	13	246.99	9	3830.03	9	61.61	9	2807.58	1	31.02	9
102	Max	-480	1393.71	17	-4370.56	13	2144.76	13	246.99	9	3830.03	9	61.61	9	2807.58	1	31.02	9
102	Max	-483	1393.71	17	-4370.56	13	2144.76	13	246.99	9	3830.03	9	61.61	9	2807.58	1	31.02	9
102	Min.	-456	-3372.14	18	-15696.30	17	-2468.84	5	-245.77	1	-3831.29	1	-212.18	19	-2807.57	9	-31.83	1
102	Min.	-453	-3372.14	18	-15696.30	17	-2468.84	5	-245.77	1	-3831.29	1	-212.18	19	-2807.57	9	-31.83	1
102	Min.	-480	-3372.14	18	-15696.30	17	-2468.84	5	-245.77	1	-3831.29	1	-212.18	19	-2807.57	9	-31.83	1
102	Min.	-483	-3372.14	18	-15696.30	17	-2468.84	5	-245.77	1	-3831.29	1	-212.18	19	-2807.57	9	-31.83	1
102	Max	-483	145.51	17	-2719.36	13	6835.33	17	77.43	9	1277.49	9	56.42	9	2784.44	1	9.99	9
102	Max	-480	145.51	17	-2719.36	13	6835.33	17	77.43	9	1277.49	9	56.42	9	2784.44	1	9.99	9
102	Max	133	145.51	17	-2719.36	13	6835.33	17	77.43	9	1277.49	9	56.42	9	2784.44	1	9.99	9
102	Max	146	145.51	17	-2719.36	13	6835.33	17	77.43	9	1277.49	9	56.42	9	2784.44	1	9.99	9
102	Min.	-483	-1195.02	18	-17220.40	17	-1749.83	5	-77.06	1	-1277.90	1	-215.09	19	-2784.36	9	-10.22	1
102	Min.	-480	-1195.02	18	-17220.40	17	-1749.83	5	-77.06	1	-1277.90	1	-215.09	19	-2784.36	9	-10.22	1
102	Min.	133	-1195.02	18	-17220.40	17	-1749.83	5	-77.06	1	-1277.90	1	-215.09	19	-2784.36	9	-10.22	1
102	Min.	146	-1195.02	18	-17220.40	17	-1749.83	5	-77.06	1	-1277.90	1	-215.09	19	-2784.36	9	-10.22	1
102	Max	-372	1928.87	17	-9844.02	13	6091.63	18	894.40	9	11522.80	9	193.26	9	3286.10	1	1158.03	9
102	Max	-369	1928.87	17	-9844.02	13	6091.63	18	894.40	9	11522.80	9	193.26	9	3286.10	1	1158.03	9

102	Max	-396	1928.87	17	-9844.02	13	6091.63	18	894.40	9	11522.80	9	193.26	9	3286.10	1	1158.03	9
102	Max	-399	1928.87	17	-9844.02	13	6091.63	18	894.40	9	11522.80	9	193.26	9	3286.10	1	1158.03	9
102	Min.	-372	-3094.33	18	-25194.00	17	-3080.28	13	-890.57	1	-11527.60	1	-190.19	1	-3291.69	9	-1170.21	1
102	Min.	-369	-3094.33	18	-25194.00	17	-3080.28	13	-890.57	1	-11527.60	1	-190.19	1	-3291.69	9	-1170.21	1
102	Min.	-396	-3094.33	18	-25194.00	17	-3080.28	13	-890.57	1	-11527.60	1	-190.19	1	-3291.69	9	-1170.21	1
102	Min.	-399	-3094.33	18	-25194.00	17	-3080.28	13	-890.57	1	-11527.60	1	-190.19	1	-3291.69	9	-1170.21	1
102	Max	-399	350.38	17	-7026.33	13	5845.43	18	623.57	9	8919.97	9	123.20	9	2852.13	1	98.23	9
102	Max	-396	350.38	17	-7026.33	13	5845.43	18	623.57	9	8919.97	9	123.20	9	2852.13	1	98.23	9
102	Max	-423	350.38	17	-7026.33	13	5845.43	18	623.57	9	8919.97	9	123.20	9	2852.13	1	98.23	9
102	Max	-426	350.38	17	-7026.33	13	5845.43	18	623.57	9	8919.97	9	123.20	9	2852.13	1	98.23	9
102	Min.	-399	-3939.62	18	-20761.90	17	-2386.23	13	-620.36	1	-8925.43	1	-184.64	19	-2851.03	9	-103.61	1
102	Min.	-396	-3939.62	18	-20761.90	17	-2386.23	13	-620.36	1	-8925.43	1	-184.64	19	-2851.03	9	-103.61	1
102	Min.	-423	-3939.62	18	-20761.90	17	-2386.23	13	-620.36	1	-8925.43	1	-184.64	19	-2851.03	9	-103.61	1
102	Min.	-426	-3939.62	18	-20761.90	17	-2386.23	13	-620.36	1	-8925.43	1	-184.64	19	-2851.03	9	-103.61	1
102	Max	-426	931.85	17	-5263.25	13	2322.22	18	353.21	9	6409.58	9	57.30	9	2816.15	1	130.07	9
102	Max	-423	931.85	17	-5263.25	13	2322.22	18	353.21	9	6409.58	9	57.30	9	2816.15	1	130.07	9
102	Max	-450	931.85	17	-5263.25	13	2322.22	18	353.21	9	6409.58	9	57.30	9	2816.15	1	130.07	9
102	Max	-453	931.85	17	-5263.25	13	2322.22	18	353.21	9	6409.58	9	57.30	9	2816.15	1	130.07	9
102	Min.	-426	-2681.52	18	-17338.90	17	-2452.13	5	-351.56	1	-6412.58	1	-202.91	19	-2815.32	9	-132.04	1
102	Min.	-423	-2681.52	18	-17338.90	17	-2452.13	5	-351.56	1	-6412.58	1	-202.91	19	-2815.32	9	-132.04	1
102	Min.	-450	-2681.52	18	-17338.90	17	-2452.13	5	-351.56	1	-6412.58	1	-202.91	19	-2815.32	9	-132.04	1
102	Min.	-453	-2681.52	18	-17338.90	17	-2452.13	5	-351.56	1	-6412.58	1	-202.91	19	-2815.32	9	-132.04	1
102	Max	-453	15.31	5	-3510.10	13	1599.88	13	189.28	9	3849.97	9	103.46	9	2779.01	1	60.59	9
102	Max	-450	15.31	5	-3510.10	13	1599.88	13	189.28	9	3849.97	9	103.46	9	2779.01	1	60.59	9
102	Max	-477	15.31	5	-3510.10	13	1599.88	13	189.28	9	3849.97	9	103.46	9	2779.01	1	60.59	9
102	Max	-480	15.31	5	-3510.10	13	1599.88	13	189.28	9	3849.97	9	103.46	9	2779.01	1	60.59	9
102	Min.	-453	-2157.15	18	-14114.10	17	-2262.91	5	-188.47	1	-3851.51	1	-211.01	19	-2778.46	9	-61.39	1
102	Min.	-450	-2157.15	18	-14114.10	17	-2262.91	5	-188.47	1	-3851.51	1	-211.01	19	-2778.46	9	-61.39	1
102	Min.	-477	-2157.15	18	-14114.10	17	-2262.91	5	-188.47	1	-3851.51	1	-211.01	19	-2778.46	9	-61.39	1
102	Min.	-480	-2157.15	18	-14114.10	17	-2262.91	5	-188.47	1	-3851.51	1	-211.01	19	-2778.46	9	-61.39	1
102	Max	-480	-130.75	5	-995.10	13	1657.85	13	59.70	9	1284.17	9	131.66	9	2762.25	1	17.26	9
102	Max	-477	-130.75	5	-995.10	13	1657.85	13	59.70	9	1284.17	9	131.66	9	2762.25	1	17.26	9
102	Max	120	-130.75	5	-995.10	13	1657.85	13	59.70	9	1284.17	9	131.66	9	2762.25	1	17.26	9
102	Max	133	-130.75	5	-995.10	13	1657.85	13	59.70	9	1284.17	9	131.66	9	2762.25	1	17.26	9
102	Min.	-480	-1433.16	17	-3928.43	17	-2206.70	5	-59.45	1	-1284.65	1	-214.20	19	-2761.76	9	-17.50	1
102	Min.	-477	-1433.16	17	-3928.43	17	-2206.70	5	-59.45	1	-1284.65	1	-214.20	19	-2761.76	9	-17.50	1
102	Min.	120	-1433.16	17	-3928.43	17	-2206.70	5	-59.45	1	-1284.65	1	-214.20	19	-2761.76	9	-17.50	1
102	Min.	133	-1433.16	17	-3928.43	17	-2206.70	5	-59.45	1	-1284.65	1	-214.20	19	-2761.76	9	-17.50	1
102	Max	-369	-1364.72	13	-5851.74	13	5523.40	18	615.48	9	11578.10	9	126.50	9	2646.99	1	710.44	9
102	Max	-366	-1364.72	13	-5851.74	13	5523.40	18	615.48	9	11578.10	9	126.50	9	2646.99	1	710.44	9
102	Max	-393	-1364.72	13	-5851.74	13	5523.40	18	615.48	9	11578.10	9	126.50	9	2646.99	1	710.44	9
102	Max	-396	-1364.72	13	-5851.74	13	5523.40	18	615.48	9	11578.10	9	126.50	9	2646.99	1	710.44	9
102	Min.	-369	-6836.97	18	-21768.90	17	-2738.21	13	-614.20	1	-11592.60	1	-141.85	19	-2637.07	9	-733.56	1
102	Min.	-366	-6836.97	18	-21768.90	17	-2738.21	13	-614.20	1	-11592.60	1	-141.85	19	-2637.07	9	-733.56	1
102	Min.	-393	-6836.97	18	-21768.90	17	-2738.21	13	-614.20	1	-11592.60	1	-141.85	19	-2637.07	9	-733.56	1
102	Min.	-396	-6836.97	18	-21768.90	17	-2738.21	13	-614.20	1	-11592.60	1	-141.85	19	-2637.07	9	-733.56	1
102	Max	-396	1234.38	17	-4915.12	5	2831.72	18	263.69	9	9050.90	9	91.06	9	2870.71	1	306.90	9
102	Max	-393	1234.38	17	-4915.12	5	2831.72	18	263.69	9	9050.90	9	91.06	9	2870.71	1	306.90	9
102	Max	-420	1234.38	17	-4915.12	5	2831.72	18	263.69	9	9050.90	9	91.06	9	2870.71	1	306.90	9
102	Max	-423	1234.38	17	-4915.12	5	2831.72	18	263.69	9	9050.90	9	91.06	9	2870.71	1	306.90	9
102	Min.	-396	-327.42	18	-19219.00	17	-1979.65	5	-262.32	1	-9057.65	1	-174.16	19	-2865.60	9	-310.44	1
102	Min.	-393	-327.42	18	-19219.00	17	-1979.65	5	-262.32	1	-9057.65	1	-174.16	19	-2865.60	9	-310.44	1
102	Min.	-420	-327.42	18	-19219.00	17	-1979.65	5	-262.32	1	-9057.65	1	-174.16	19	-2865.60	9	-310.44	1
102	Min.	-423	-327.42	18	-19219.00	17	-1979.65	5	-262.32	1	-9057.65	1	-174.16	19	-2865.60	9	-310.44	1
102	Max	-423	106.49	5	-3696.16	5	981.01	18	184.84	9	6463.86	9	120.40	9	2818.48	1	128.05	9
102	Max	-420	106.49	5	-3696.16	5	981.01	18	184.84	9	6463.86	9	120.40	9	2818.48	1	128.05	9
102	Max	-447	106.49	5	-3696.16	5	981.01	18	184.84	9	6463.86	9	120.40	9	2818.48	1	128.05	9
102	Max	-450	106.49	5	-3696.16	5	981.01	18	184.84	9	6463.86	9	120.40	9	2818.48	1	128.05	9
102	Min.	-423	-1050.71	18	-16066.20	17	-1774.81	5	-184.20	1	-6467.17	1	-189.52	19	-2815.84	9	-129.16	1
102	Min.	-420	-1050.71	18	-16066.20	17	-1774.81	5	-184.20	1	-6467.17	1	-189.52	19	-2815.84	9	-129.16	1
102	Min.	-447	-1050.71	18	-16066.20	17	-1774.81	5	-184.20	1	-6467.17	1	-189.52	19	-2815.84	9	-129.16	1
102	Min.	-450	-1050.71	18	-16066.20	17	-1774.81	5	-184.20	1	-6467.17	1	-189.52	19	-2815.84	9	-129.16	1
102	Max	-450	232.81	17	-2633.48	5	855.99	13	94.50	9	3888.60	9	203.45	9	2837.92	1	68.29	9
102	Max	-447	232.81	17	-2633.48	5	855.99	13	94.50	9	3888.60	9	203.45	9	2837.92	1	68.29	9
102	Max	-474	232.81	17	-2633.48	5	855.99	13	94.50	9	3888.60	9	203.45	9	2837.92	1	68.29	9
102	Max	-477	232.81	17	-2633.48	5	855.99	13	94.50	9	3888.60	9	203.45	9	2837.92	1	68.29	9
102	Min.	-450	-599.96	18	-12261.40	17	-1567.73	5	-94.16	1	-3890.27	1	-207.31	1	-2835.90	9	-68.89	1
102	Min.	-447	-599.96	18	-12261.40	17	-1567.73	5	-94.16	1	-3890.27	1	-207.31	1	-2835.90	9	-68.89	1
102	Min.	-474	-599.96	18	-12261.40	17	-1567.73	5	-94.16	1	-3890.27	1	-207.31	1	-2835.90	9	-68.89	1
102	Min.	-477	-599.96	18	-12261.40	17	-1567.73	5	-94.16	1	-3890.27	1	-207.31	1	-2835.90	9	-68.89	1
102	Max	-477	28.30	5	-2020.71	5	304.09	13	29.51	9	1296.18	9	241.28	9	2837.62	1	22.12	9
102	Max	-474	28.30	5	-2020.71	5	304.09	13	29.51	9	1296.18	9	241.28	9	2837.62	1	22.12	9
102	Max	107	28.30	5	-2020.71	5	304.09	13	29.51	9	1296.18	9	241.28	9	2837.62	1	22.12	9
102	Max	120	28.30	5	-2020.71	5	304.09	13	29.51	9	1296.18	9	241.28	9	2837.62	1	22.12	9
102	Min.	-477	-245.33	18	-12358.40	17	-4725.49	17	-29.40	1	-1296.68	1	-245.15	1	-2835.85	9	-22.28	1
102	Min.	-474	-245.33	18	-12358.40	17	-4725.49	17	-29.40	1	-1296.68	1	-245.15	1	-2835.85	9	-22.28	1
102	Min.	107	-245.33	18	-12358.40	17	-4725.49	17	-29.40	1	-1296.68	1	-245.15	1	-2835.85	9	-22.28	1
102	Min.	120	-245.33	18	-12358.40	17	-4725.49	17	-29.40	1	-1296.68	1	-245.15	1	-2835.85	9	-22.28	1
102	Max	-366	-611.39	5	-1888.87	5	2657.41	18	108.87	9	11393.70	9	90.06	9	2314.08	1	197.54	1
102	Max	-363	-611.39	5	-1888.87	5	2657.41	18	108.87	9	11393.70	9	90.06	9	2314.08	1	197.54	1
102	Max	-390	-611.39	5	-1888.87	5	2657.41	18	108.87	9	11393.70	9	90.06	9	2314.08	1	197.54	1
102	Max	-393	-611.39	5	-1888.87	5	2657.41	18	108.87	9	11393.70	9	90.06	9	2314.08	1	197.54	1
102	Min.	-366	-1779.10	18	-19716.60	18	-475.75	5	-108.20	1	-11413.10	1	-89.91	1	-2290.62	9	-210.24	9
102	Min.	-363	-1779.10	18	-19716.60	18	-475.75	5	-108.20	1	-11413.10	1	-89.91	1	-2290.62	9	-210.24	9
102	Min.	-390	-1779.10	18	-19716.60	18	-475.75	5	-108.20	1	-11413.10	1	-89.91	1	-2290.62	9	-210.24	9
102	Min.	-393	-1779.10	18	-19716.60	18	-475.75	5	-108.20	1	-11413.10	1	-89.91	1	-2290.62	9	-210.24	9
102	Max	-393	347.81	17	-2472.05	5	405.96	18	60.22	9	9079.51	9	56.67	9	2919.64	1	272.59	1
102	Max	-390	347.81	17	-2472.05	5	405.96	18	60.22	9	9079.51	9	56.67	9	2919.64	1	272.59	1
102	Max	-417	347.81	17	-2472.05	5	405.96	18	60.22	9	9079.51	9	56.67	9	2919.64	1	272.59	1
102	Max	-420	347.81	17	-2472.05	5	405.96	18	60.22	9	9079.51	9	56.67	9	2919.64	1	272.59	1
102	Min.	-393	86.54	20	-16604.70	17	-951.84	5	-60.10	1	-9085.94	1	-95.62	19	-2908.66	9	-271.90	9
102	Min.	-390	86.54	20	-16604.70	17	-951.84	5	-60.10	1	-9085.94	1	-95.62	19	-2908.66	9	-271.90	9
102	Min.	-417	86.54	20	-16604.70	17	-951.84	5	-60.10	1	-9085.94	1	-95.62	19	-2908.66	9	-271.90	9
102	Min.	-420	86.54	20	-16604.70	17	-951.84	5	-60.10	1	-9085.94	1	-95.62	19	-2908.66	9	-271.90	9
102	Max	-420	18.11	5	-2632.01	5	318.95	18	37.05	9	6514.99	9	101.21	9	3280.81	1	58.53	1
102	Max	-417	18.11	5	-2632.01	5	318.95	18	37.05	9	6514.99	9	101.21	9	3280.81	1	58.53	1
102	Max	-444	18.11	5	-2632.01	5	318.95	18	37.05	9	6514.99	9	101.21	9	3280.81	1	58.53	1
102	Max	-447	18.11	5	-2632.01	5	318.95	18	37.05	9	6514.99	9	101.21	9	3280.81	1	58.53	1
102	Min.	-420	-267.34	17	-15247.30	17	-523.45	5	-36.95	1	-6518.50	1	-103.38	1	-3271.26	9	-59.09	9
102	Min.	-417	-267.34	17	-15247.30	17	-523.45	5	-36.95	1	-6518.50	1	-103.38	1	-3271.26	9	-59.09	9
102	Min.	-444	-267.34	17	-15247.30	17	-523.45	5	-36.95	1	-6518.50	1	-103.38	1	-3271.26	9	-59.09	9
102	Min.	-447	-267.34	17	-15247.30	17	-523.45	5	-36.95	1	-6518.50	1	-103.38	1	-3271.26	9	-59.09	9
102	Max	-447	626.44	17	-2338.59	5	160.16	13	21.33	9	3904.90	9	161.86	9	3426.33	1	40.38	1
102	Max	-444	626.44	17	-2338.59	5	160.16	13	21.33	9	3904.90	9	161.86	9	3426.33	1	40.38	1
102	Max	-471	626.44	17	-2338.59	5	160.16	13	21.33	9	3904.90	9	161.86	9	3426.33	1	40.38	1
102	Max	-474	626.44	17	-2338.59	5	160.16	13	21.33	9	3904.90	9	161.86	9	3426.33	1	40.38	1
102	Min.	-447	11.84	20	-13863.90	17	-856.51	17	-21.27	1	-3906.60	1	-164.06	1	-3417.81	9	-40.56	9
102	Min.	-444	11.84	20	-13863.90	17	-856.51	17	-21.27	1	-3906.60	1	-164.06	1	-3417.81	9	-40.56	9
102	Min.	-471	11.84	20	-13863.90	17	-856.51	17	-21.27	1	-3906.60	1	-164.06	1	-3417.81	9	-40.56	9

102	Min.	-474	11.84	20	-13863.90	17	-856.51	17	-21.27	1	-3906.60	1	-164.06	1	-3417.81	9	-40.56	9
102	Max	-474	727.67	17	-1707.95	5	3192.38	17	6.02	9	1302.31	9	183.58	9	3501.77	1	13.86	1
102	Max	-471	727.67	17	-1707.95	5	3192.38	17	6.02	9	1302.31	9	183.58	9	3501.77	1	13.86	1
102	Max	-498	727.67	17	-1707.95	5	3192.38	17	6.02	9	1302.31	9	183.58	9	3501.77	1	13.86	1
102	Max	107	727.67	17	-1707.95	5	3192.38	17	6.02	9	1302.31	9	183.58	9	3501.77	1	13.86	1
102	Min.	-474	103.46	20	-10809.20	17	27.98	5	-6.00	1	-1302.82	1	-185.76	1	-3493.66	9	-13.91	9
102	Min.	-471	103.46	20	-10809.20	17	27.98	5	-6.00	1	-1302.82	1	-185.76	1	-3493.66	9	-13.91	9
102	Min.	-498	103.46	20	-10809.20	17	27.98	5	-6.00	1	-1302.82	1	-185.76	1	-3493.66	9	-13.91	9
102	Min.	107	103.46	20	-10809.20	17	27.98	5	-6.00	1	-1302.82	1	-185.76	1	-3493.66	9	-13.91	9
102	Max	-441	-188.10	13	-3228.96	5	469.09	5	52.96	1	6587.52	1	152.18	9	3449.70	9	47.83	1
102	Max	-438	-188.10	13	-3228.96	5	469.09	5	52.96	1	6587.52	1	152.18	9	3449.70	9	47.83	1
102	Max	-465	-188.10	13	-3228.96	5	469.09	5	52.96	1	6587.52	1	152.18	9	3449.70	9	47.83	1
102	Max	-468	-188.10	13	-3228.96	5	469.09	5	52.96	1	6587.52	1	152.18	9	3449.70	9	47.83	1
102	Min.	-441	-15205.10	18	-16428.70	17	-1044.32	18	-52.79	9	-6586.20	9	-152.29	1	-3451.24	1	-47.57	9
102	Min.	-438	-15205.10	18	-16428.70	17	-1044.32	18	-52.79	9	-6586.20	9	-152.29	1	-3451.24	1	-47.57	9
102	Min.	-465	-15205.10	18	-16428.70	17	-1044.32	18	-52.79	9	-6586.20	9	-152.29	1	-3451.24	1	-47.57	9
102	Min.	-468	-15205.10	18	-16428.70	17	-1044.32	18	-52.79	9	-6586.20	9	-152.29	1	-3451.24	1	-47.57	9
102	Max	-387	-85.06	13	-2108.90	5	4069.24	19	287.05	1	11916.20	1	32.38	9	2433.18	9	310.32	1
102	Max	-384	-85.06	13	-2108.90	5	4069.24	19	287.05	1	11916.20	1	32.38	9	2433.18	9	310.32	1
102	Max	-411	-85.06	13	-2108.90	5	4069.24	19	287.05	1	11916.20	1	32.38	9	2433.18	9	310.32	1
102	Max	-414	-85.06	13	-2108.90	5	4069.24	19	287.05	1	11916.20	1	32.38	9	2433.18	9	310.32	1
102	Min.	-387	-36551.70	18	-17463.40	17	2183.44	5	-286.88	9	-11912.40	9	-80.98	19	-2432.79	1	-310.03	9
102	Min.	-384	-36551.70	18	-17463.40	17	2183.44	5	-286.88	9	-11912.40	9	-80.98	19	-2432.79	1	-310.03	9
102	Min.	-411	-36551.70	18	-17463.40	17	2183.44	5	-286.88	9	-11912.40	9	-80.98	19	-2432.79	1	-310.03	9
102	Min.	-414	-36551.70	18	-17463.40	17	2183.44	5	-286.88	9	-11912.40	9	-80.98	19	-2432.79	1	-310.03	9
102	Max	-414	1015.79	17	-3763.90	5	497.84	5	26.06	1	9288.70	1	29.80	9	3222.93	9	202.24	1
102	Max	-411	1015.79	17	-3763.90	5	497.84	5	26.06	1	9288.70	1	29.80	9	3222.93	9	202.24	1
102	Max	-438	1015.79	17	-3763.90	5	497.84	5	26.06	1	9288.70	1	29.80	9	3222.93	9	202.24	1
102	Max	-441	1015.79	17	-3763.90	5	497.84	5	26.06	1	9288.70	1	29.80	9	3222.93	9	202.24	1
102	Min.	-414	-23423.10	18	-18945.40	17	-278.33	18	-25.89	9	-9286.16	9	-91.31	19	-3223.67	1	-201.87	9
102	Min.	-411	-23423.10	18	-18945.40	17	-278.33	18	-25.89	9	-9286.16	9	-91.31	19	-3223.67	1	-201.87	9
102	Min.	-438	-23423.10	18	-18945.40	17	-278.33	18	-25.89	9	-9286.16	9	-91.31	19	-3223.67	1	-201.87	9
102	Min.	-441	-23423.10	18	-18945.40	17	-278.33	18	-25.89	9	-9286.16	9	-91.31	19	-3223.67	1	-201.87	9
103	Max	-413	53.91	17	-3109.44	5	405.00	5	111.92	17	5859.08	1	137.59	17	4327.27	17	197.78	1
103	Max	-410	53.91	17	-3109.44	5	405.00	5	111.92	17	5859.08	1	137.59	17	4327.27	17	197.78	1
103	Max	-437	53.91	17	-3109.44	5	405.00	5	111.92	17	5859.08	1	137.59	17	4327.27	17	197.78	1
103	Max	-440	53.91	17	-3109.44	5	405.00	5	111.92	17	5859.08	1	137.59	17	4327.27	17	197.78	1
103	Min.	-413	-20664.30	19	-16803.30	17	-554.90	13	21.76	9	-881.69	9	31.40	1	69.21	1	-27.85	9
103	Min.	-410	-20664.30	19	-16803.30	17	-554.90	13	21.76	9	-881.69	9	31.40	1	69.21	1	-27.85	9
103	Min.	-437	-20664.30	19	-16803.30	17	-554.90	13	21.76	9	-881.69	9	31.40	1	69.21	1	-27.85	9
103	Min.	-440	-20664.30	19	-16803.30	17	-554.90	13	21.76	9	-881.69	9	31.40	1	69.21	1	-27.85	9
103	Max	-494	480.68	17	-1231.99	5	161.96	19	6.67	1	1058.03	1	-28.13	9	-987.06	9	-26.61	1
103	Max	-491	480.68	17	-1231.99	5	161.96	19	6.67	1	1058.03	1	-28.13	9	-987.06	9	-26.61	1
103	Max	179	480.68	17	-1231.99	5	161.96	19	6.67	1	1058.03	1	-28.13	9	-987.06	9	-26.61	1
103	Max	-500	480.68	17	-1231.99	5	161.96	19	6.67	1	1058.03	1	-28.13	9	-987.06	9	-26.61	1
103	Min.	-494	46.05	21	-7955.53	17	-2209.66	17	-15.15	17	97.38	9	-543.47	17	-8299.95	17	-360.07	17
103	Min.	-491	46.05	21	-7955.53	17	-2209.66	17	-15.15	17	97.38	9	-543.47	17	-8299.95	17	-360.07	17
103	Min.	179	46.05	21	-7955.53	17	-2209.66	17	-15.15	17	97.38	9	-543.47	17	-8299.95	17	-360.07	17
103	Min.	-500	46.05	21	-7955.53	17	-2209.66	17	-15.15	17	97.38	9	-543.47	17	-8299.95	17	-360.07	17
103	Max	-440	-46.69	5	-2366.87	5	464.56	5	109.74	17	6403.07	17	58.53	9	1267.11	9	431.45	17
103	Max	-437	-46.69	5	-2366.87	5	464.56	5	109.74	17	6403.07	17	58.53	9	1267.11	9	431.45	17
103	Max	-464	-46.69	5	-2366.87	5	464.56	5	109.74	17	6403.07	17	58.53	9	1267.11	9	431.45	17
103	Max	-467	-46.69	5	-2366.87	5	464.56	5	109.74	17	6403.07	17	58.53	9	1267.11	9	431.45	17
103	Min.	-440	-12594.10	19	-13469.50	17	-785.35	19	29.45	9	377.39	9	-72.83	1	-2381.09	1	97.19	9
103	Min.	-437	-12594.10	19	-13469.50	17	-785.35	19	29.45	9	377.39	9	-72.83	1	-2381.09	1	97.19	9
103	Min.	-464	-12594.10	19	-13469.50	17	-785.35	19	29.45	9	377.39	9	-72.83	1	-2381.09	1	97.19	9
103	Min.	-467	-12594.10	19	-13469.50	17	-785.35	19	29.45	9	377.39	9	-72.83	1	-2381.09	1	97.19	9
103	Max	-467	443.88	17	-1837.21	5	553.96	5	112.78	17	4585.45	17	44.20	9	-265.84	9	72.00	1
103	Max	-464	443.88	17	-1837.21	5	553.96	5	112.78	17	4585.45	17	44.20	9	-265.84	9	72.00	1
103	Max	-491	443.88	17	-1837.21	5	553.96	5	112.78	17	4585.45	17	44.20	9	-265.84	9	72.00	1
103	Max	-494	443.88	17	-1837.21	5	553.96	5	112.78	17	4585.45	17	44.20	9	-265.84	9	72.00	1
103	Min.	-467	-4147.13	19	-11131.40	17	-785.46	19	25.72	9	568.88	9	-133.60	1	-5574.98	17	-14.94	17
103	Min.	-464	-4147.13	19	-11131.40	17	-785.46	19	25.72	9	568.88	9	-133.60	1	-5574.98	17	-14.94	17
103	Min.	-491	-4147.13	19	-11131.40	17	-785.46	19	25.72	9	568.88	9	-133.60	1	-5574.98	17	-14.94	17
103	Min.	-494	-4147.13	19	-11131.40	17	-785.46	19	25.72	9	568.88	9	-133.60	1	-5574.98	17	-14.94	17
103	Max	-386	-10.05	5	-4055.37	5	339.82	5	101.46	17	5045.31	1	256.70	17	10523.00	17	246.35	17
103	Max	-383	-10.05	5	-4055.37	5	339.82	5	101.46	17	5045.31	1	256.70	17	10523.00	17	246.35	17
103	Max	-410	-10.05	5	-4055.37	5	339.82	5	101.46	17	5045.31	1	256.70	17	10523.00	17	246.35	17
103	Max	-413	-10.05	5	-4055.37	5	339.82	5	101.46	17	5045.31	1	256.70	17	10523.00	17	246.35	17
103	Min.	-386	-31113.60	19	-20914.00	17	-770.60	13	10.36	9	-3606.56	9	74.32	1	3254.96	1	103.37	9
103	Min.	-383	-31113.60	19	-20914.00	17	-770.60	13	10.36	9	-3606.56	9	74.32	1	3254.96	1	103.37	9
103	Min.	-410	-31113.60	19	-20914.00	17	-770.60	13	10.36	9	-3606.56	9	74.32	1	3254.96	1	103.37	9
103	Min.	-413	-31113.60	19	-20914.00	17	-770.60	13	10.36	9	-3606.56	9	74.32	1	3254.96	1	103.37	9
103	Max	-464	-3.66	17	-2235.28	5	1516.15	5	322.86	17	4616.63	17	42.01	9	-338.67	9	661.49	17
103	Max	-461	-3.66	17	-2235.28	5	1516.15	5	322.86	17	4616.63	17	42.01	9	-338.67	9	661.49	17
103	Max	-488	-3.66	17	-2235.28	5	1516.15	5	322.86	17	4616.63	17	42.01	9	-338.67	9	661.49	17
103	Max	-491	-3.66	17	-2235.28	5	1516.15	5	322.86	17	4616.63	17	42.01	9	-338.67	9	661.49	17
103	Min.	-464	-4988.05	19	-9946.70	17	-1285.98	13	69.99	9	574.01	9	-187.19	17	-4233.51	17	126.22	1
103	Min.	-461	-4988.05	19	-9946.70	17	-1285.98	13	69.99	9	574.01	9	-187.19	17	-4233.51	17	126.22	1
103	Min.	-488	-4988.05	19	-9946.70	17	-1285.98	13	69.99	9	574.01	9	-187.19	17	-4233.51	17	126.22	1
103	Min.	-491	-4988.05	19	-9946.70	17	-1285.98	13	69.99	9	574.01	9	-187.19	17	-4233.51	17	126.22	1
103	Max	-491	-6.54	9	-1530.22	5	3207.29	17	63.91	17	1062.40	1	166.69	17	-1145.78	9	659.96	17
103	Max	-488	-6.54	9	-1530.22	5	3207.29	17	63.91	17	1062.40	1	166.69	17	-1145.78	9	659.96	17
103	Max	166	-6.54	9	-1530.22	5	3207.29	17	63.91	17	1062.40	1	166.69	17	-1145.78	9	659.96	17
103	Max	179	-6.54	9	-1530.22	5	3207.29	17	63.91	17	1062.40	1	166.69	17	-1145.78	9	659.96	17
103	Min.	-491	-928.51	19	-8985.36	17	-818.84	13	18.02	9	108.56	9	-132.39	1	-7918.97	17	110.09	1
103	Min.	-488	-928.51	19	-8985.36	17	-818.84	13	18.02	9	108.56	9	-132.39	1	-7918.97	17	110.09	1
103	Min.	166	-928.51	19	-8985.36	17	-818.84	13	18.02	9	108.56	9	-132.39	1	-7918.97	17	110.09	1
103	Min.	179	-928.51	19	-8985.36	17	-818.84	13	18.02	9	108.56	9	-132.39	1	-7918.97	17	110.09	1
103	Max	-380	-354.78	5	-5988.17	21	10797.90	19	395.15	1	4960.21	1	69.69	9	9224.33	17	70.00	9
103	Max	-377	-354.78	5	-5988.17	21	10797.90	19	395.15	1	4960.21	1	69.69	9	9224.33	17	70.00	9
103	Max	-404	-354.78	5	-5988.17	21	10797.90	19	395.15	1	4960.21	1	69.69	9	9224.33	17	70.00	9
103	Max	-407	-354.78	5	-5988.17	21	10797.90	19	395.15	1	4960.21	1	69.69	9	9224.33	17	70.00	9
103	Min.	-380	-15192.30	19	-19014.30	17	-2458.70	13	-264.19	9	-3522.49	9	-39.86	1	2475.00	1	-217.94	1
103	Min.	-377	-15192.30	19	-19014.30	17	-2458.70	13	-264.19	9	-3522.49	9	-39.86	1	2475.00	1	-217.94	1
103	Min.	-404	-15192.30	19	-19014.30	17	-2458.70	13	-264.19	9	-3522.49	9	-39.86	1	2475.00	1	-217.94	1
103	Min.	-407	-15192.30	19	-19014.30	17	-2458.70	13	-264.19	9	-3522.49	9	-39.86	1	2475.00	1	-217.94	1
103	Max	-407	-280.64	5	-4913.66	21	4569.29	19	465.16	17	5748.39	1	48.71	9	3613.04	17	171.21	9
103	Max	-404	-280.64	5	-4913.66	21	4569.29	19	465.16	17	5748.39	1	48.71	9	3613.04	17	171.21	9
103	Max	-431	-280.64	5	-4913.66	21	4569.29	19	465.16	17	5748.39	1	48.71	9	3613.04	17	171.21	9
103	Max	-434	-280.64	5	-4913.66	21	4569.29	19	465.16	17	5748.39	1	48.71	9	3613.04	17	171.21	9
103	Min.	-407	-15455.50	19	-16801.90	17	-2448.88	13	4.30	9	-857.45	9	-36.41	19	-102.12	1	-11.66	1
103	Min.	-404	-15455.50	19	-16801.90	17	-2448.88	13	4.30	9	-857.45	9	-36.41	19	-102.12	1	-11.66	1
103	Min.	-431	-15455.50	19	-16801.90	17	-2448.88	13	4.30	9	-857.45	9	-36.41	19	-102.12	1	-11.66	1
103	Min.	-434	-15455.50	19	-16801.90	17	-2448.88	13	4.30	9	-857.45	9	-36.41	19	-102.12	1	-11.66	1
103	Max	-434	-165.32	22	-4506.39	5	2215.64	5	541.62	17	6250.67	17	37.84	9	924.20	9	101.46	9
103	Max	-431	-165.32	22	-4506.39	5	2215.64	5	541.62	17	6250.67	17	37.84	9	924.20	9	101.46	9
103	Max	-458	-165.32	22	-4506.39	5	2215.64	5	541.62	17	6250.67	17	37.84	9	924.20	9	101.46	9
103	Max	-461	-165.32	22	-4506.39	5	2215.64	5	541.62	17	6250.67	17	37.84	9	924.20	9	101.46	9

103	Min.	-434	-10788.10	19	-13909.90	17	-2213.43	13	98.84	9	367.56	9	-61.88	19	-2040.90	1	8.56	1
103	Min.	-431	-10788.10	19	-13909.90	17	-2213.43	13	98.84	9	367.56	9	-61.88	19	-2040.90	1	8.56	1
103	Min.	-458	-10788.10	19	-13909.90	17	-2213.43	13	98.84	9	367.56	9	-61.88	19	-2040.90	1	8.56	1
103	Min.	-461	-10788.10	19	-13909.90	17	-2213.43	13	98.84	9	367.56	9	-61.88	19	-2040.90	1	8.56	1
103	Max	-461	-218.87	1	-3012.89	5	2297.80	5	402.32	17	4387.58	17	40.58	9	-382.44	9	51.51	9
103	Max	-458	-218.87	1	-3012.89	5	2297.80	5	402.32	17	4387.58	17	40.58	9	-382.44	9	51.51	9
103	Max	-485	-218.87	1	-3012.89	5	2297.80	5	402.32	17	4387.58	17	40.58	9	-382.44	9	51.51	9
103	Max	-488	-218.87	1	-3012.89	5	2297.80	5	402.32	17	4387.58	17	40.58	9	-382.44	9	51.51	9
103	Min.	-461	-5591.29	19	-11009.70	17	-2143.62	13	92.99	9	549.14	9	-95.84	19	-4601.78	17	-178.99	17
103	Min.	-458	-5591.29	19	-11009.70	17	-2143.62	13	92.99	9	549.14	9	-95.84	19	-4601.78	17	-178.99	17
103	Min.	-485	-5591.29	19	-11009.70	17	-2143.62	13	92.99	9	549.14	9	-95.84	19	-4601.78	17	-178.99	17
103	Min.	-488	-5591.29	19	-11009.70	17	-2143.62	13	92.99	9	549.14	9	-95.84	19	-4601.78	17	-178.99	17
103	Max	-488	-158.59	9	-890.86	5	2356.99	5	146.33	17	1605.22	17	38.34	9	-710.71	9	11.61	9
103	Max	-485	-158.59	9	-890.86	5	2356.99	5	146.33	17	1605.22	17	38.34	9	-710.71	9	11.61	9
103	Max	153	-158.59	9	-890.86	5	2356.99	5	146.33	17	1605.22	17	38.34	9	-710.71	9	11.61	9
103	Max	166	-158.59	9	-890.86	5	2356.99	5	146.33	17	1605.22	17	38.34	9	-710.71	9	11.61	9
103	Min.	-488	-1735.94	19	-3084.19	17	-2088.49	13	36.64	9	244.89	9	-116.86	19	-4605.21	17	-165.79	17
103	Min.	-485	-1735.94	19	-3084.19	17	-2088.49	13	36.64	9	244.89	9	-116.86	19	-4605.21	17	-165.79	17
103	Min.	153	-1735.94	19	-3084.19	17	-2088.49	13	36.64	9	244.89	9	-116.86	19	-4605.21	17	-165.79	17
103	Min.	166	-1735.94	19	-3084.19	17	-2088.49	13	36.64	9	244.89	9	-116.86	19	-4605.21	17	-165.79	17
103	Max	-377	-658.59	5	-8006.62	21	10688.90	19	466.13	1	4983.64	1	29.79	9	9300.73	17	64.75	9
103	Max	-374	-658.59	5	-8006.62	21	10688.90	19	466.13	1	4983.64	1	29.79	9	9300.73	17	64.75	9
103	Max	-401	-658.59	5	-8006.62	21	10688.90	19	466.13	1	4983.64	1	29.79	9	9300.73	17	64.75	9
103	Max	-404	-658.59	5	-8006.62	21	10688.90	19	466.13	1	4983.64	1	29.79	9	9300.73	17	64.75	9
103	Min.	-377	-10776.60	19	-18938.30	17	-2153.84	13	-301.31	9	-3499.50	9	-43.99	19	2449.39	1	-67.64	1
103	Min.	-374	-10776.60	19	-18938.30	17	-2153.84	13	-301.31	9	-3499.50	9	-43.99	19	2449.39	1	-67.64	1
103	Min.	-401	-10776.60	19	-18938.30	17	-2153.84	13	-301.31	9	-3499.50	9	-43.99	19	2449.39	1	-67.64	1
103	Min.	-404	-10776.60	19	-18938.30	17	-2153.84	13	-301.31	9	-3499.50	9	-43.99	19	2449.39	1	-67.64	1
103	Max	-404	-481.67	5	-6095.39	21	6500.71	19	512.04	17	5720.80	1	27.09	9	3588.32	17	53.03	9
103	Max	-401	-481.67	5	-6095.39	21	6500.71	19	512.04	17	5720.80	1	27.09	9	3588.32	17	53.03	9
103	Max	-428	-481.67	5	-6095.39	21	6500.71	19	512.04	17	5720.80	1	27.09	9	3588.32	17	53.03	9
103	Max	-431	-481.67	5	-6095.39	21	6500.71	19	512.04	17	5720.80	1	27.09	9	3588.32	17	53.03	9
103	Min.	-404	-11137.10	19	-16618.40	17	-2456.30	13	-27.67	9	-839.00	9	-54.53	19	-141.09	1	-27.33	1
103	Min.	-401	-11137.10	19	-16618.40	17	-2456.30	13	-27.67	9	-839.00	9	-54.53	19	-141.09	1	-27.33	1
103	Min.	-428	-11137.10	19	-16618.40	17	-2456.30	13	-27.67	9	-839.00	9	-54.53	19	-141.09	1	-27.33	1
103	Min.	-431	-11137.10	19	-16618.40	17	-2456.30	13	-27.67	9	-839.00	9	-54.53	19	-141.09	1	-27.33	1
103	Max	-431	-297.31	1	-4909.15	21	2911.27	19	551.30	17	6255.35	17	18.25	9	950.89	9	247.95	17
103	Max	-428	-297.31	1	-4909.15	21	2911.27	19	551.30	17	6255.35	17	18.25	9	950.89	9	247.95	17
103	Max	-455	-297.31	1	-4909.15	21	2911.27	19	551.30	17	6255.35	17	18.25	9	950.89	9	247.95	17
103	Max	-458	-297.31	1	-4909.15	21	2911.27	19	551.30	17	6255.35	17	18.25	9	950.89	9	247.95	17
103	Min.	-431	-8575.04	19	-14251.50	17	-2523.65	13	92.32	9	374.99	9	-70.53	19	-2042.87	1	20.24	1
103	Min.	-428	-8575.04	19	-14251.50	17	-2523.65	13	92.32	9	374.99	9	-70.53	19	-2042.87	1	20.24	1
103	Min.	-455	-8575.04	19	-14251.50	17	-2523.65	13	92.32	9	374.99	9	-70.53	19	-2042.87	1	20.24	1
103	Min.	-458	-8575.04	19	-14251.50	17	-2523.65	13	92.32	9	374.99	9	-70.53	19	-2042.87	1	20.24	1
103	Max	-458	422.66	17	-3702.80	21	2699.62	5	335.06	17	4527.91	17	111.90	17	-396.71	9	-83.38	9
103	Max	-455	422.66	17	-3702.80	21	2699.62	5	335.06	17	4527.91	17	111.90	17	-396.71	9	-83.38	9
103	Max	-482	422.66	17	-3702.80	21	2699.62	5	335.06	17	4527.91	17	111.90	17	-396.71	9	-83.38	9
103	Max	-485	422.66	17	-3702.80	21	2699.62	5	335.06	17	4527.91	17	111.90	17	-396.71	9	-83.38	9
103	Min.	-458	-4813.33	19	-11922.80	17	-2565.62	13	88.62	9	571.67	9	-64.52	19	-4818.23	17	-960.21	17
103	Min.	-455	-4813.33	19	-11922.80	17	-2565.62	13	88.62	9	571.67	9	-64.52	19	-4818.23	17	-960.21	17
103	Min.	-482	-4813.33	19	-11922.80	17	-2565.62	13	88.62	9	571.67	9	-64.52	19	-4818.23	17	-960.21	17
103	Min.	-485	-4813.33	19	-11922.80	17	-2565.62	13	88.62	9	571.67	9	-64.52	19	-4818.23	17	-960.21	17
103	Max	-383	-137.12	5	-4576.44	21	8301.46	19	252.81	1	4996.77	1	174.01	17	9182.55	17	381.04	9
103	Max	-380	-137.12	5	-4576.44	21	8301.46	19	252.81	1	4996.77	1	174.01	17	9182.55	17	381.04	9
103	Max	-407	-137.12	5	-4576.44	21	8301.46	19	252.81	1	4996.77	1	174.01	17	9182.55	17	381.04	9
103	Max	-410	-137.12	5	-4576.44	21	8301.46	19	252.81	1	4996.77	1	174.01	17	9182.55	17	381.04	9
103	Min.	-383	-22856.50	19	-20364.90	17	-2628.63	13	-132.57	9	-3587.77	9	-12.67	1	2514.32	1	-70.01	1
103	Min.	-380	-22856.50	19	-20364.90	17	-2628.63	13	-132.57	9	-3587.77	9	-12.67	1	2514.32	1	-70.01	1
103	Min.	-407	-22856.50	19	-20364.90	17	-2628.63	13	-132.57	9	-3587.77	9	-12.67	1	2514.32	1	-70.01	1
103	Min.	-410	-22856.50	19	-20364.90	17	-2628.63	13	-132.57	9	-3587.77	9	-12.67	1	2514.32	1	-70.01	1
103	Max	-410	-99.51	5	-4497.24	5	1284.32	5	323.05	17	5811.90	1	136.98	17	3565.98	17	224.57	17
103	Max	-407	-99.51	5	-4497.24	5	1284.32	5	323.05	17	5811.90	1	136.98	17	3565.98	17	224.57	17
103	Max	-434	-99.51	5	-4497.24	5	1284.32	5	323.05	17	5811.90	1	136.98	17	3565.98	17	224.57	17
103	Max	-437	-99.51	5	-4497.24	5	1284.32	5	323.05	17	5811.90	1	136.98	17	3565.98	17	224.57	17
103	Min.	-410	-19853.80	19	-16972.10	17	-1669.10	13	34.07	9	-874.13	9	16.13	21	-83.59	1	-10.46	1
103	Min.	-407	-19853.80	19	-16972.10	17	-1669.10	13	34.07	9	-874.13	9	16.13	21	-83.59	1	-10.46	1
103	Min.	-434	-19853.80	19	-16972.10	17	-1669.10	13	34.07	9	-874.13	9	16.13	21	-83.59	1	-10.46	1
103	Min.	-437	-19853.80	19	-16972.10	17	-1669.10	13	34.07	9	-874.13	9	16.13	21	-83.59	1	-10.46	1
103	Max	-437	-113.28	5	-3373.72	5	1422.00	5	346.87	17	6310.95	17	66.26	9	925.90	9	174.52	9
103	Max	-434	-113.28	5	-3373.72	5	1422.00	5	346.87	17	6310.95	17	66.26	9	925.90	9	174.52	9
103	Max	-461	-113.28	5	-3373.72	5	1422.00	5	346.87	17	6310.95	17	66.26	9	925.90	9	174.52	9
103	Max	-464	-113.28	5	-3373.72	5	1422.00	5	346.87	17	6310.95	17	66.26	9	925.90	9	174.52	9
103	Min.	-437	-11909.00	19	-13785.60	17	-1403.45	13	73.33	9	369.51	9	-69.47	19	-2008.68	1	41.45	1
103	Min.	-434	-11909.00	19	-13785.60	17	-1403.45	13	73.33	9	369.51	9	-69.47	19	-2008.68	1	41.45	1
103	Min.	-461	-11909.00	19	-13785.60	17	-1403.45	13	73.33	9	369.51	9	-69.47	19	-2008.68	1	41.45	1
103	Min.	-464	-11909.00	19	-13785.60	17	-1403.45	13	73.33	9	369.51	9	-69.47	19	-2008.68	1	41.45	1
103	Max	-256	14.50	5	4069.41	19	17954.90	19	15.03	1	2102.31	1	179.06	9	17648.50	17	605.34	9
103	Max	-233	14.50	5	4069.41	19	17954.90	19	15.03	1	2102.31	1	179.06	9	17648.50	17	605.34	9
103	Max	-383	14.50	5	4069.41	19	17954.90	19	15.03	1	2102.31	1	179.06	9	17648.50	17	605.34	9
103	Max	-386	14.50	5	4069.41	19	17954.90	19	15.03	1	2102.31	1	179.06	9	17648.50	17	605.34	9
103	Min.	-256	-17483.40	19	-28138.50	17	-3725.19	13	-346.72	17	-8366.22	9	-247.26	1	7387.86	1	-836.92	1
103	Min.	-233	-17483.40	19	-28138.50	17	-3725.19	13	-346.72	17	-8366.22	9	-247.26	1	7387.86	1	-836.92	1
103	Min.	-383	-17483.40	19	-28138.50	17	-3725.19	13	-346.72	17	-8366.22	9	-247.26	1	7387.86	1	-836.92	1
103	Min.	-386	-17483.40	19	-28138.50	17	-3725.19	13	-346.72	17	-8366.22	9	-247.26	1	7387.86	1	-836.92	1
103	Max	-233	-233.33	5	-6372.32	21	17541.20	19	147.92	1	2318.11	1	69.96	9	15767.60	17	498.47	9
103	Max	-193	-233.33	5	-6372.32	21	17541.20	19	147.92	1	2318.11	1	69.96	9	15767.60	17	498.47	9
103	Max	-380	-233.33	5	-6372.32	21	17541.20	19	147.92	1	2318.11	1	69.96	9	15767.60	17	498.47	9
103	Max	-383	-233.33	5	-6372.32	21	17541.20	19	147.92	1	2318.11	1	69.96	9	15767.60	17	498.47	9
103	Min.	-233	-11563.70	19	-21835.30	17	-2802.83	13	-587.66	9	-8024.44	9	-121.32	1	5706.70	1	-493.58	1
103	Min.	-193	-11563.70	19	-21835.30	17	-2802.83	13	-587.66	9	-8024.44	9	-121.32	1	5706.70	1	-493.58	1
103	Min.	-380	-11563.70	19	-21835.30	17	-2802.83	13	-587.66	9	-8024.44	9	-121.32	1	5706.70	1	-493.58	1
103	Min.	-383	-11563.70	19	-21835.30	17	-2802.83	13	-587.66	9	-8024.44	9	-121.32	1	5706.70	1	-493.58	1
103	Max	-193	-607.58	5	-8500.55	21	15934.70	19	226.20	9	2448.18	1	83.64	9	15735.90	17	230.01	9
103	Max	-169	-607.58	5	-8500.55	21	15934.70	19	226.20	9	2448.18	1	83.64	9	15735.90	17	230.01	9
103	Max	-377	-607.58	5	-8500.55	21	15934.70	19	226.20	9	2448.18	1	83.64	9	15735.90	17	230.01	9
103	Max	-380	-607.58	5	-8500.55	21	15934.70	19	226.20	9	2448.18	1	83.64	9	15735.90	17	230.01	9
103	Min.	-193	-9027.75	19	-21020.00	17	-1701.53	13	-706.28	1	-8024.40	9	-13.66	1	5464.46	9	-114.94	1
103	Min.	-169	-9027.75	19	-21020.00	17	-1701.53	13	-706.28	1	-8024.40	9	-13.66	1	5464.46	9	-114.94	1
103	Min.	-377	-9027.75	19	-21020.00	17	-1701.53	13	-706.28	1	-8024.40	9	-13.66	1	5464.46	9	-114.94	1
103	Min.	-380	-9027.75	19	-21020.00	17	-1701.53	13	-706.28	1	-8024.40	9	-13.66	1	5464.46	9	-114.94	1
103	Max	-169	-564.29	5	-11286.80	21	13792.60	19	182.44	1	2310.29	1	31.63	18	16444.90	17	83.06	9
103	Max	-146	-564.29	5	-11286.80	21	13792.60	19	182.44	1	2310.29	1	31.63	18	16444.90	17	83.06	9
103	Max	-374	-564.29	5	-11286.80	21	13792.60	19	182.44	1	2310.29	1	31.63	18	16444.90	17	83.06	9
103	Max	-377	-564.29	5	-11286.80	21	13792.60	19	182.44	1	2310.29	1	31.63	18	16444.90	17	83.06	9
103	Min.	-169	-6520.11	19	-21500.70	17	-1864.76	13	-852.18	9	-8164.16	9	3.83	1	6058.14	1	-43.35	1
103	Min.	-146	-6520.11	19	-21500.70	17	-1864.76	13	-852.18	9	-8164.16	9	3.83	1	6058.14	1	-43.35	1
103	Min.	-374	-6520.11	19	-21500.70	17	-1864.76	13	-852.18	9	-8164.16	9	3.83	1	6058.14	1	-43.35	1
103	Min.	-377	-6520.11	19	-21500.70	17	-1864.76	13	-852.18	9	-8164.16	9	3.83	1	6058.14	1	-43.35	1
103	Max	-146	-908.02	13	-11195.90	13	11240.20	19	273.21	1	2509.65	1	-21.38	9	15705.70	17	84.48	18

103	Max	-118	-908.02	13	-11195.90	13	11240.20	19	273.21	1	2509.65	1	-21.38	9	15705.70	17	84.48	18
103	Max	-371	-908.02	13	-11195.90	13	11240.20	19	273.21	1	2509.65	1	-21.38	9	15705.70	17	84.48	18
103	Max	-374	-908.02	13	-11195.90	13	11240.20	19	273.21	1	2509.65	1	-21.38	9	15705.70	17	84.48	18
103	Min.	-146	-5549.34	19	-21583.50	17	-1644.21	13	-749.63	9	-8047.57	9	-147.42	19	5423.95	1	-25.43	17
103	Min.	-118	-5549.34	19	-21583.50	17	-1644.21	13	-749.63	9	-8047.57	9	-147.42	19	5423.95	1	-25.43	17
103	Min.	-371	-5549.34	19	-21583.50	17	-1644.21	13	-749.63	9	-8047.57	9	-147.42	19	5423.95	1	-25.43	17
103	Min.	-374	-5549.34	19	-21583.50	17	-1644.21	13	-749.63	9	-8047.57	9	-147.42	19	5423.95	1	-25.43	17
103	Max	-118	-549.89	13	-9997.07	13	10947.20	19	219.15	9	2460.85	9	148.54	18	15819.60	17	198.26	9
103	Max	-98	-549.89	13	-9997.07	13	10947.20	19	219.15	9	2460.85	9	148.54	18	15819.60	17	198.26	9
103	Max	-368	-549.89	13	-9997.07	13	10947.20	19	219.15	9	2460.85	9	148.54	18	15819.60	17	198.26	9
103	Max	-371	-549.89	13	-9997.07	13	10947.20	19	219.15	9	2460.85	9	148.54	18	15819.60	17	198.26	9
103	Min.	-118	-5931.57	19	-22165.80	17	-985.07	13	-753.55	1	-8067.40	1	50.07	1	5431.61	9	-271.17	1
103	Min.	-98	-5931.57	19	-22165.80	17	-985.07	13	-753.55	1	-8067.40	1	50.07	1	5431.61	9	-271.17	1
103	Min.	-368	-5931.57	19	-22165.80	17	-985.07	13	-753.55	1	-8067.40	1	50.07	1	5431.61	9	-271.17	1
103	Min.	-371	-5931.57	19	-22165.80	17	-985.07	13	-753.55	1	-8067.40	1	50.07	1	5431.61	9	-271.17	1
103	Max	-98	-191.17	13	-7574.88	13	9259.14	19	100.48	9	2146.34	9	88.53	9	16233.60	17	674.69	9
103	Max	-66	-191.17	13	-7574.88	13	9259.14	19	100.48	9	2146.34	9	88.53	9	16233.60	17	674.69	9
103	Max	-365	-191.17	13	-7574.88	13	9259.14	19	100.48	9	2146.34	9	88.53	9	16233.60	17	674.69	9
103	Max	-368	-191.17	13	-7574.88	13	9259.14	19	100.48	9	2146.34	9	88.53	9	16233.60	17	674.69	9
103	Min.	-98	-5089.26	19	-26828.90	19	-1308.72	13	-634.61	1	-8164.15	1	-111.96	1	6079.62	9	-298.03	1
103	Min.	-66	-5089.26	19	-26828.90	19	-1308.72	13	-634.61	1	-8164.15	1	-111.96	1	6079.62	9	-298.03	1
103	Min.	-365	-5089.26	19	-26828.90	19	-1308.72	13	-634.61	1	-8164.15	1	-111.96	1	6079.62	9	-298.03	1
103	Min.	-368	-5089.26	19	-26828.90	19	-1308.72	13	-634.61	1	-8164.15	1	-111.96	1	6079.62	9	-298.03	1
103	Max	-66	-242.43	13	-5893.43	13	11427.40	19	53.76	9	2074.35	9	278.14	9	17399.40	17	632.25	9
103	Max	-49	-242.43	13	-5893.43	13	11427.40	19	53.76	9	2074.35	9	278.14	9	17399.40	17	632.25	9
103	Max	-362	-242.43	13	-5893.43	13	11427.40	19	53.76	9	2074.35	9	278.14	9	17399.40	17	632.25	9
103	Max	-365	-242.43	13	-5893.43	13	11427.40	19	53.76	9	2074.35	9	278.14	9	17399.40	17	632.25	9
103	Min.	-66	-4905.35	19	-47189.90	19	248.17	13	-314.35	1	-8391.39	1	-155.34	1	7238.14	9	-645.95	1
103	Min.	-49	-4905.35	19	-47189.90	19	248.17	13	-314.35	1	-8391.39	1	-155.34	1	7238.14	9	-645.95	1
103	Min.	-362	-4905.35	19	-47189.90	19	248.17	13	-314.35	1	-8391.39	1	-155.34	1	7238.14	9	-645.95	1
103	Min.	-365	-4905.35	19	-47189.90	19	248.17	13	-314.35	1	-8391.39	1	-155.34	1	7238.14	9	-645.95	1
103	Max	-395	-35.15	13	-4895.24	13	4583.41	19	311.16	17	5799.52	9	-48.76	13	3575.55	17	-17.53	9
103	Max	-392	-35.15	13	-4895.24	13	4583.41	19	311.16	17	5799.52	9	-48.76	13	3575.55	17	-17.53	9
103	Max	-419	-35.15	13	-4895.24	13	4583.41	19	311.16	17	5799.52	9	-48.76	13	3575.55	17	-17.53	9
103	Max	-422	-35.15	13	-4895.24	13	4583.41	19	311.16	17	5799.52	9	-48.76	13	3575.55	17	-17.53	9
103	Min.	-395	-1516.25	19	-17716.60	17	-1191.62	13	25.85	1	-887.35	1	-163.87	19	-82.20	9	-276.17	17
103	Min.	-392	-1516.25	19	-17716.60	17	-1191.62	13	25.85	1	-887.35	1	-163.87	19	-82.20	9	-276.17	17
103	Min.	-419	-1516.25	19	-17716.60	17	-1191.62	13	25.85	1	-887.35	1	-163.87	19	-82.20	9	-276.17	17
103	Min.	-422	-1516.25	19	-17716.60	17	-1191.62	13	25.85	1	-887.35	1	-163.87	19	-82.20	9	-276.17	17
103	Max	-422	-105.65	13	-3661.40	13	2258.47	19	344.28	17	6297.22	17	59.72	9	940.07	1	-38.35	9
103	Max	-419	-105.65	13	-3661.40	13	2258.47	19	344.28	17	6297.22	17	59.72	9	940.07	1	-38.35	9
103	Max	-446	-105.65	13	-3661.40	13	2258.47	19	344.28	17	6297.22	17	59.72	9	940.07	1	-38.35	9
103	Max	-449	-105.65	13	-3661.40	13	2258.47	19	344.28	17	6297.22	17	59.72	9	940.07	1	-38.35	9
103	Min.	-422	-1317.36	19	-14299.10	17	-1296.99	13	70.77	1	360.83	1	-81.48	19	-1997.12	9	-169.99	1
103	Min.	-419	-1317.36	19	-14299.10	17	-1296.99	13	70.77	1	360.83	1	-81.48	19	-1997.12	9	-169.99	1
103	Min.	-446	-1317.36	19	-14299.10	17	-1296.99	13	70.77	1	360.83	1	-81.48	19	-1997.12	9	-169.99	1
103	Min.	-449	-1317.36	19	-14299.10	17	-1296.99	13	70.77	1	360.83	1	-81.48	19	-1997.12	9	-169.99	1
103	Max	-449	-1.57	17	-2413.01	13	1442.88	5	320.76	17	4611.74	17	172.01	17	-332.30	1	-126.90	9
103	Max	-446	-1.57	17	-2413.01	13	1442.88	5	320.76	17	4611.74	17	172.01	17	-332.30	1	-126.90	9
103	Max	-473	-1.57	17	-2413.01	13	1442.88	5	320.76	17	4611.74	17	172.01	17	-332.30	1	-126.90	9
103	Max	-476	-1.57	17	-2413.01	13	1442.88	5	320.76	17	4611.74	17	172.01	17	-332.30	1	-126.90	9
103	Min.	-449	-709.20	19	-10257.40	17	-1375.56	13	68.39	1	570.85	1	-51.21	1	-4224.13	17	-662.89	17
103	Min.	-446	-709.20	19	-10257.40	17	-1375.56	13	68.39	1	570.85	1	-51.21	1	-4224.13	17	-662.89	17
103	Min.	-473	-709.20	19	-10257.40	17	-1375.56	13	68.39	1	570.85	1	-51.21	1	-4224.13	17	-662.89	17
103	Min.	-476	-709.20	19	-10257.40	17	-1375.56	13	68.39	1	570.85	1	-51.21	1	-4224.13	17	-662.89	17
103	Max	-476	-7.22	1	-1589.96	13	971.38	5	63.27	17	1061.46	9	121.84	9	-1141.14	1	-110.36	9
103	Max	-473	-7.22	1	-1589.96	13	971.38	5	63.27	17	1061.46	9	121.84	9	-1141.14	1	-110.36	9
103	Max	101	-7.22	1	-1589.96	13	971.38	5	63.27	17	1061.46	9	121.84	9	-1141.14	1	-110.36	9
103	Max	114	-7.22	1	-1589.96	13	971.38	5	63.27	17	1061.46	9	121.84	9	-1141.14	1	-110.36	9
103	Min.	-476	-237.64	19	-9088.71	17	-2953.18	17	17.53	1	107.61	1	-183.65	17	-7911.92	17	-660.50	17
103	Min.	-473	-237.64	19	-9088.71	17	-2953.18	17	17.53	1	107.61	1	-183.65	17	-7911.92	17	-660.50	17
103	Min.	101	-237.64	19	-9088.71	17	-2953.18	17	17.53	1	107.61	1	-183.65	17	-7911.92	17	-660.50	17
103	Min.	114	-237.64	19	-9088.71	17	-2953.18	17	17.53	1	107.61	1	-183.65	17	-7911.92	17	-660.50	17
103	Max	-365	-69.28	13	-4533.58	13	2596.05	19	74.24	9	4990.27	9	-72.54	9	10548.90	17	-29.93	1
103	Max	-362	-69.28	13	-4533.58	13	2596.05	19	74.24	9	4990.27	9	-72.54	9	10548.90	17	-29.93	1
103	Max	-389	-69.28	13	-4533.58	13	2596.05	19	74.24	9	4990.27	9	-72.54	9	10548.90	17	-29.93	1
103	Max	-392	-69.28	13	-4533.58	13	2596.05	19	74.24	9	4990.27	9	-72.54	9	10548.90	17	-29.93	1
103	Min.	-365	-703.47	19	-26960.70	19	-402.55	13	-2.34	1	-3656.79	1	-252.56	17	3297.99	9	-137.79	17
103	Min.	-362	-703.47	19	-26960.70	19	-402.55	13	-2.34	1	-3656.79	1	-252.56	17	3297.99	9	-137.79	17
103	Min.	-389	-703.47	19	-26960.70	19	-402.55	13	-2.34	1	-3656.79	1	-252.56	17	3297.99	9	-137.79	17
103	Min.	-392	-703.47	19	-26960.70	19	-402.55	13	-2.34	1	-3656.79	1	-252.56	17	3297.99	9	-137.79	17
103	Max	-392	102.05	17	-3593.73	13	1488.97	19	112.79	17	5842.41	9	-31.88	9	4390.54	17	24.96	1
103	Max	-389	102.05	17	-3593.73	13	1488.97	19	112.79	17	5842.41	9	-31.88	9	4390.54	17	24.96	1
103	Max	-416	102.05	17	-3593.73	13	1488.97	19	112.79	17	5842.41	9	-31.88	9	4390.54	17	24.96	1
103	Max	-419	102.05	17	-3593.73	13	1488.97	19	112.79	17	5842.41	9	-31.88	9	4390.54	17	24.96	1
103	Min.	-392	-76.73	19	-17710.20	17	-380.02	13	21.00	1	-902.89	1	-133.90	17	112.85	9	-200.84	9
103	Min.	-389	-76.73	19	-17710.20	17	-380.02	13	21.00	1	-902.89	1	-133.90	17	112.85	9	-200.84	9
103	Min.	-416	-76.73	19	-17710.20	17	-380.02	13	21.00	1	-902.89	1	-133.90	17	112.85	9	-200.84	9
103	Min.	-419	-76.73	19	-17710.20	17	-380.02	13	21.00	1	-902.89	1	-133.90	17	112.85	9	-200.84	9
103	Max	-419	-54.57	13	-2743.89	13	647.40	19	107.35	17	6390.75	17	66.25	9	1292.95	1	-97.33	1
103	Max	-416	-54.57	13	-2743.89	13	647.40	19	107.35	17	6390.75	17	66.25	9	1292.95	1	-97.33	1
103	Max	-443	-54.57	13	-2743.89	13	647.40	19	107.35	17	6390.75	17	66.25	9	1292.95	1	-97.33	1
103	Max	-446	-54.57	13	-2743.89	13	647.40	19	107.35	17	6390.75	17	66.25	9	1292.95	1	-97.33	1
103	Min.	-419	-310.31	17	-14146.40	17	-420.86	13	27.97	1	369.14	1	-63.73	1	-2351.78	9	-432.42	17
103	Min.	-416	-310.31	17	-14146.40	17	-420.86	13	27.97	1	369.14	1	-63.73	1	-2351.78	9	-432.42	17
103	Min.	-443	-310.31	17	-14146.40	17	-420.86	13	27.97	1	369.14	1	-63.73	1	-2351.78	9	-432.42	17
103	Min.	-446	-310.31	17	-14146.40	17	-420.86	13	27.97	1	369.14	1	-63.73	1	-2351.78	9	-432.42	17
103	Max	-446	446.95	17	-2072.27	13	381.77	5	112.59	17	4578.63	17	127.42	9	-234.24	1	18.34	17
103	Max	-443	446.95	17	-2072.27	13	381.77	5	112.59	17	4578.63	17	127.42	9	-234.24	1	18.34	17
103	Max	-470	446.95	17	-2072.27	13	381.77	5	112.59	17	4578.63	17	127.42	9	-234.24	1	18.34	17
103	Max	-473	446.95	17	-2072.27	13	381.77	5	112.59	17	4578.63	17	127.42	9	-234.24	1	18.34	17
103	Min.	-446	11.78	21	-11540.30	17	-509.53	13	25.45	1	564.50	1	-49.86	1	-5522.97	17	-70.37	9
103	Min.	-443	11.78	21	-11540.30	17	-509.53	13	25.45	1	564.50	1	-49.86	1	-5522.97	17	-70.37	9
103	Min.	-470	11.78	21	-11540.30	17	-509.53	13	25.45	1	564.50	1	-49.86	1	-5522.97	17	-70.37	9
103	Min.	-473	11.78	21	-11540.30	17	-509.53	13	25.45	1	564.50	1	-49.86	1	-5522.97	17	-70.37	9
103	Max	-473	479.89	17	-1312.02	13	2290.50	17	6.51	9	1056.90	9	532.83	17	-954.85	1	359.44	17
103	Max	-470	479.89	17	-1312.02	13	2290.50	17	6.51	9	1056.90	9	532.83	17	-954.85	1	359.44	17
103	Max	-497	479.89	17	-1312.02	13	2290.50	17	6.51	9	1056.90	9	532.83	17	-954.85	1	359.44	17
103	Max	101	479.89	17	-1312.02	13	2290.50	17	6.51	9	1056.90	9	532.83	17	-954.85	1	359.44	17
103	Min.	-473	44.89	21	-8092.70	17	-106.87	13	-15.45	17	96.20	1	21.64	1	-8247.54	17	26.09	9
103	Min.	-470	44.89	21	-8092.70	17	-106.87	13	-15.45	17	96.20	1	21.64	1	-8247.54	17	26.09	9
103	Min.	-497	44.89	21	-8092.70	17	-106.87	13	-15.45	17	96.20	1	21.64	1	-8247.54	17	26.09	9
103	Min.	101	44.89	21	-8092.70	17	-106.87	13	-15.45	17	96.20	1	21.64	1	-8247.54	17	26.09	9
103	Max	-455	430.85	17	-3822.52	13	2853.00	5	334.43	17	4526.60	17	11.34	9	-394.65	1	953.54	17
103	Max	-452	430.85	17	-3822.52	13	2853.00	5	334.43	17	4526.60	17	11.34	9	-394.65	1	953.54	17
103	Max	-479	430.85	17	-3822.52	13	2853.00	5	334.43	17	4526.60	17	11.34	9	-394.65	1	953.54	17
103	Max	-482	430.85	17	-3822.52	13	2853.00	5	334.43	17	4526.60	17	11.34	9	-394.65	1	953.54	17
103	Min.	-455	-3444.58	19	-11985.40	17	-2421.16	13	88.08	1	570.69	1	-129.33	17	-4815.10	17	79.87	1
103	Min.	-452	-3444.58	19	-11985.40	17	-2421.16	13	88.08	1	570.69	1	-129.33	17	-4815.10	17	79.87	1

103	Min.	-479	-3444.58	19	-11985.40	17	-2421.16	13	88.08	1	570.69	1	-129.33	17	-4815.10	17	79.87	1
103	Min.	-482	-3444.58	19	-11985.40	17	-2421.16	13	88.08	1	570.69	1	-129.33	17	-4815.10	17	79.87	1
103	Max	-482	-40.40	9	-2169.93	13	5245.05	17	73.92	9	1014.30	9	578.36	17	-1247.83	1	1223.66	17
103	Max	-479	-40.40	9	-2169.93	13	5245.05	17	73.92	9	1014.30	9	578.36	17	-1247.83	1	1223.66	17
103	Max	127	-40.40	9	-2169.93	13	5245.05	17	73.92	9	1014.30	9	578.36	17	-1247.83	1	1223.66	17
103	Max	140	-40.40	9	-2169.93	13	5245.05	17	73.92	9	1014.30	9	578.36	17	-1247.83	1	1223.66	17
103	Min.	-482	-1175.72	19	-12284.80	17	-1959.19	13	-52.39	17	68.32	17	10.18	21	-9256.73	17	125.47	1
103	Min.	-479	-1175.72	19	-12284.80	17	-1959.19	13	-52.39	17	68.32	17	10.18	21	-9256.73	17	125.47	1
103	Min.	127	-1175.72	19	-12284.80	17	-1959.19	13	-52.39	17	68.32	17	10.18	21	-9256.73	17	125.47	1
103	Min.	140	-1175.72	19	-12284.80	17	-1959.19	13	-52.39	17	68.32	17	10.18	21	-9256.73	17	125.47	1
103	Max	-371	-279.42	13	-7968.99	13	9615.37	19	405.65	9	4948.54	9	35.67	9	9206.07	17	-8.51	9
103	Max	-368	-279.42	13	-7968.99	13	9615.37	19	405.65	9	4948.54	9	35.67	9	9206.07	17	-8.51	9
103	Max	-395	-279.42	13	-7968.99	13	9615.37	19	405.65	9	4948.54	9	35.67	9	9206.07	17	-8.51	9
103	Max	-398	-279.42	13	-7968.99	13	9615.37	19	405.65	9	4948.54	9	35.67	9	9206.07	17	-8.51	9
103	Min.	-371	-6049.94	19	-19571.40	17	-1590.51	13	-264.67	1	-3537.38	1	-99.21	19	2442.52	9	-412.19	19
103	Min.	-368	-6049.94	19	-19571.40	17	-1590.51	13	-264.67	1	-3537.38	1	-99.21	19	2442.52	9	-412.19	19
103	Min.	-395	-6049.94	19	-19571.40	17	-1590.51	13	-264.67	1	-3537.38	1	-99.21	19	2442.52	9	-412.19	19
103	Min.	-398	-6049.94	19	-19571.40	17	-1590.51	13	-264.67	1	-3537.38	1	-99.21	19	2442.52	9	-412.19	19
103	Max	-398	-255.34	13	-6330.94	13	6925.25	19	457.82	17	5734.11	9	7.49	9	3637.37	17	40.10	9
103	Max	-395	-255.34	13	-6330.94	13	6925.25	19	457.82	17	5734.11	9	7.49	9	3637.37	17	40.10	9
103	Max	-422	-255.34	13	-6330.94	13	6925.25	19	457.82	17	5734.11	9	7.49	9	3637.37	17	40.10	9
103	Max	-425	-255.34	13	-6330.94	13	6925.25	19	457.82	17	5734.11	9	7.49	9	3637.37	17	40.10	9
103	Min.	-398	-4862.22	19	-17284.10	17	-1829.27	13	-2.98	1	-869.60	1	-103.37	19	-90.39	9	-124.29	1
103	Min.	-395	-4862.22	19	-17284.10	17	-1829.27	13	-2.98	1	-869.60	1	-103.37	19	-90.39	9	-124.29	1
103	Min.	-422	-4862.22	19	-17284.10	17	-1829.27	13	-2.98	1	-869.60	1	-103.37	19	-90.39	9	-124.29	1
103	Min.	-425	-4862.22	19	-17284.10	17	-1829.27	13	-2.98	1	-869.60	1	-103.37	19	-90.39	9	-124.29	1
103	Max	-425	-135.29	13	-4702.91	13	3623.04	19	537.67	17	6243.29	17	22.31	9	933.05	1	-20.58	9
103	Max	-422	-135.29	13	-4702.91	13	3623.04	19	537.67	17	6243.29	17	22.31	9	933.05	1	-20.58	9
103	Max	-449	-135.29	13	-4702.91	13	3623.04	19	537.67	17	6243.29	17	22.31	9	933.05	1	-20.58	9
103	Max	-452	-135.29	13	-4702.91	13	3623.04	19	537.67	17	6243.29	17	22.31	9	933.05	1	-20.58	9
103	Min.	-425	-3253.34	19	-14235.20	17	-2003.85	13	95.45	1	362.85	1	-88.08	19	-2034.21	9	-114.04	1
103	Min.	-422	-3253.34	19	-14235.20	17	-2003.85	13	95.45	1	362.85	1	-88.08	19	-2034.21	9	-114.04	1
103	Min.	-449	-3253.34	19	-14235.20	17	-2003.85	13	95.45	1	362.85	1	-88.08	19	-2034.21	9	-114.04	1
103	Min.	-452	-3253.34	19	-14235.20	17	-2003.85	13	95.45	1	362.85	1	-88.08	19	-2034.21	9	-114.04	1
103	Max	-452	-213.92	9	-3126.65	13	2390.37	5	399.69	17	4384.55	17	61.62	9	-378.05	1	173.98	17
103	Max	-449	-213.92	9	-3126.65	13	2390.37	5	399.69	17	4384.55	17	61.62	9	-378.05	1	173.98	17
103	Max	-476	-213.92	9	-3126.65	13	2390.37	5	399.69	17	4384.55	17	61.62	9	-378.05	1	173.98	17
103	Max	-479	-213.92	9	-3126.65	13	2390.37	5	399.69	17	4384.55	17	61.62	9	-378.05	1	173.98	17
103	Min.	-452	-2201.02	19	-11200.10	17	-2071.33	13	90.95	1	547.13	1	-65.62	19	-4595.44	17	-54.25	1
103	Min.	-449	-2201.02	19	-11200.10	17	-2071.33	13	90.95	1	547.13	1	-65.62	19	-4595.44	17	-54.25	1
103	Min.	-476	-2201.02	19	-11200.10	17	-2071.33	13	90.95	1	547.13	1	-65.62	19	-4595.44	17	-54.25	1
103	Min.	-479	-2201.02	19	-11200.10	17	-2071.33	13	90.95	1	547.13	1	-65.62	19	-4595.44	17	-54.25	1
103	Max	-479	-157.10	9	-927.66	13	2329.44	5	145.63	17	1604.37	17	85.06	9	-707.75	1	164.87	17
103	Max	-476	-157.10	9	-927.66	13	2329.44	5	145.63	17	1604.37	17	85.06	9	-707.75	1	164.87	17
103	Max	114	-157.10	9	-927.66	13	2329.44	5	145.63	17	1604.37	17	85.06	9	-707.75	1	164.87	17
103	Max	127	-157.10	9	-927.66	13	2329.44	5	145.63	17	1604.37	17	85.06	9	-707.75	1	164.87	17
103	Min.	-479	-1103.24	17	-3146.56	17	-2123.71	13	36.09	1	244.32	1	-49.54	1	-4600.81	17	-12.07	1
103	Min.	-476	-1103.24	17	-3146.56	17	-2123.71	13	36.09	1	244.32	1	-49.54	1	-4600.81	17	-12.07	1
103	Min.	114	-1103.24	17	-3146.56	17	-2123.71	13	36.09	1	244.32	1	-49.54	1	-4600.81	17	-12.07	1
103	Min.	127	-1103.24	17	-3146.56	17	-2123.71	13	36.09	1	244.32	1	-49.54	1	-4600.81	17	-12.07	1
103	Max	-368	-179.61	13	-6310.49	13	8729.39	19	244.80	9	4976.23	9	33.52	9	9306.84	17	98.74	9
103	Max	-365	-179.61	13	-6310.49	13	8729.39	19	244.80	9	4976.23	9	33.52	9	9306.84	17	98.74	9
103	Max	-392	-179.61	13	-6310.49	13	8729.39	19	244.80	9	4976.23	9	33.52	9	9306.84	17	98.74	9
103	Max	-395	-179.61	13	-6310.49	13	8729.39	19	244.80	9	4976.23	9	33.52	9	9306.84	17	98.74	9
103	Min.	-368	-4253.24	19	-24156.50	19	-988.80	13	-147.74	1	-3618.47	1	-150.28	1	2580.24	9	-367.24	1
103	Min.	-365	-4253.24	19	-24156.50	19	-988.80	13	-147.74	1	-3618.47	1	-150.28	1	2580.24	9	-367.24	1
103	Min.	-392	-4253.24	19	-24156.50	19	-988.80	13	-147.74	1	-3618.47	1	-150.28	1	2580.24	9	-367.24	1
103	Min.	-395	-4253.24	19	-24156.50	19	-988.80	13	-147.74	1	-3618.47	1	-150.28	1	2580.24	9	-367.24	1
103	Max	-374	-636.28	13	-9486.01	13	10212.10	19	465.44	1	4957.41	9	33.11	9	9279.28	17	207.71	18
103	Max	-371	-636.28	13	-9486.01	13	10212.10	19	465.44	1	4957.41	9	33.11	9	9279.28	17	207.71	18
103	Max	-398	-636.28	13	-9486.01	13	10212.10	19	465.44	1	4957.41	9	33.11	9	9279.28	17	207.71	18
103	Max	-401	-636.28	13	-9486.01	13	10212.10	19	465.44	1	4957.41	9	33.11	9	9279.28	17	207.71	18
103	Min.	-374	-7997.76	19	-19206.40	17	-1888.29	13	-317.16	9	-3519.78	1	-23.34	19	2427.67	1	76.79	1
103	Min.	-371	-7997.76	19	-19206.40	17	-1888.29	13	-317.16	9	-3519.78	1	-23.34	19	2427.67	1	76.79	1
103	Min.	-398	-7997.76	19	-19206.40	17	-1888.29	13	-317.16	9	-3519.78	1	-23.34	19	2427.67	1	76.79	1
103	Min.	-401	-7997.76	19	-19206.40	17	-1888.29	13	-317.16	9	-3519.78	1	-23.34	19	2427.67	1	76.79	1
103	Max	-401	-444.20	13	-7595.13	13	7159.85	19	520.49	17	5713.92	9	16.88	9	3620.61	17	-12.33	9
103	Max	-398	-444.20	13	-7595.13	13	7159.85	19	520.49	17	5713.92	9	16.88	9	3620.61	17	-12.33	9
103	Max	-425	-444.20	13	-7595.13	13	7159.85	19	520.49	17	5713.92	9	16.88	9	3620.61	17	-12.33	9
103	Max	-428	-444.20	13	-7595.13	13	7159.85	19	520.49	17	5713.92	9	16.88	9	3620.61	17	-12.33	9
103	Min.	-401	-7811.96	19	-16756.50	17	-2235.77	13	-24.06	1	-845.33	1	-70.32	19	-119.83	9	-115.17	19
103	Min.	-398	-7811.96	19	-16756.50	17	-2235.77	13	-24.06	1	-845.33	1	-70.32	19	-119.83	9	-115.17	19
103	Min.	-425	-7811.96	19	-16756.50	17	-2235.77	13	-24.06	1	-845.33	1	-70.32	19	-119.83	9	-115.17	19
103	Min.	-428	-7811.96	19	-16756.50	17	-2235.77	13	-24.06	1	-845.33	1	-70.32	19	-119.83	9	-115.17	19
103	Max	-485	-39.29	9	-2156.11	5	2238.31	5	74.08	1	1014.41	1	-40.01	9	-1249.03	9	-126.71	9
103	Max	-482	-39.29	9	-2156.11	5	2238.31	5	74.08	1	1014.41	1	-40.01	9	-1249.03	9	-126.71	9
103	Max	140	-39.29	9	-2156.11	5	2238.31	5	74.08	1	1014.41	1	-40.01	9	-1249.03	9	-126.71	9
103	Max	153	-39.29	9	-2156.11	5	2238.31	5	74.08	1	1014.41	1	-40.01	9	-1249.03	9	-126.71	9
103	Min.	-485	-1499.05	19	-12263.20	17	-4768.82	17	-52.02	17	68.57	17	-597.14	17	-9258.41	17	-1225.89	17
103	Min.	-482	-1499.05	19	-12263.20	17	-4768.82	17	-52.02	17	68.57	17	-597.14	17	-9258.41	17	-1225.89	17
103	Min.	140	-1499.05	19	-12263.20	17	-4768.82	17	-52.02	17	68.57	17	-597.14	17	-9258.41	17	-1225.89	17
103	Min.	153	-1499.05	19	-12263.20	17	-4768.82	17	-52.02	17	68.57	17	-597.14	17	-9258.41	17	-1225.89	17
103	Max	-428	-284.04	13	-5733.61	13	3895.24	19	546.91	17	6254.37	17	10.89	9	951.09	1	-29.20	9
103	Max	-425	-284.04	13	-5733.61	13	3895.24	19	546.91	17	6254.37	17	10.89	9	951.09	1	-29.20	9
103	Max	-452	-284.04	13	-5733.61	13	3895.24	19	546.91	17	6254.37	17	10.89	9	951.09	1	-29.20	9
103	Max	-455	-284.04	13	-5733.61	13	3895.24	19	546.91	17	6254.37	17	10.89	9	951.09	1	-29.20	9
103	Min.	-428	-5966.40	19	-14372.70	17	-2420.95	13	89.34	1	373.99	1	-83.62	19	-2044.70	9	-260.20	17
103	Min.	-425	-5966.40	19	-14372.70	17	-2420.95	13	89.34	1	373.99	1	-83.62	19	-2044.70	9	-260.20	17
103	Min.	-452	-5966.40	19	-14372.70	17	-2420.95	13	89.34	1	373.99	1	-83.62	19	-2044.70	9	-260.20	17
103	Min.	-455	-5966.40	19	-14372.70	17	-2420.95	13	89.34	1	373.99	1	-83.62	19	-2044.70	9	-260.20	17
104	Max	-493	-6.54	1	-1530.18	13	3207.91	17	-18.02	1	-108.42	1	132.38	9	7918.42	17	-110.09	9
104	Max	-490	-6.54	1	-1530.18	13	3207.91	17	-18.02	1	-108.42	1	132.38	9	7918.42	17	-110.09	9
104	Max	178	-6.54	1	-1530.18	13	3207.91	17	-18.02	1	-108.42	1	132.38	9	7918.42	17	-110.09	9
104	Max	191	-6.54	1	-1530.18	13	3207.91	17	-18.02	1	-108.42	1	132.38	9	7918.42	17	-110.09	9
104	Min.	-493	-787.88	18	-8985.11	17	-818.03	5	-63.91	17	-1062.26	9	-166.70	17	1145.36	1	-659.95	17
104	Min.	-490	-787.88	18	-8985.11	17	-818.03	5	-63.91	17	-1062.26	9	-166.70	17	1145.36	1	-659.95	17
104	Min.	178	-787.88	18	-8985.11	17	-818.03	5	-63.91	17	-1062.26	9	-166.70	17	1145.36	1	-659.95	17
104	Min.	191	-787.88	18	-8985.11	17	-818.03	5	-63.91	17	-1062.26	9	-166.70	17	1145.36	1	-659.95	17
104	Max	-382	-354.47	13	-6438.46	20	9322.06	18	264.28	1	3523.70	1	39.89	9	-2475.46	9	218.01	9
104	Max	-379	-354.47	13	-6438.46	20	9322.06	18	264.28	1	3523.70	1	39.89	9	-2475.46	9	218.01	9
104	Max	-406	-354.47	13	-6438.46	20	9322.06	18	264.28	1	3523.70	1	39.89	9	-2475.46	9	218.01	9
104	Max	-409	-354.47	13	-6438.46	20	9322.06	18	264.28	1	3523.70	1	39.89	9	-2475.46	9	218.01	9
104	Min.	-382	-12937.50	18	-19013.10	17	-2458.58	5	-395.06	9	-4958.99	9	-71.99	19	-9224.93	17	-69.98	1
104	Min.	-379	-12937.50	18	-19013.10	17	-2458.58	5	-395.06	9	-4958.99	9	-71.99	19	-9224.93	17	-69.98	1
104	Min.	-406	-12937.50	18	-19013.10	17	-2458.58	5	-395.06	9	-4958.99	9	-71.99	19	-9224.93	17	-69.98	1
104	Min.	-409	-12937.50	18	-19013.10	17	-2458.58	5	-395.06	9	-4958.99	9	-71.99	19	-9224.93	17	-69.98	1
104	Max	-415	53.91	17	-3106.29	13	405.28	13	-21.75	1	882.65	1	-31.39	9	-69.62	9	27.88	1
104	Max	-412	53.91	17	-3106.29	13	405.28	13	-21.75	1	882.65	1	-31.39	9	-69.62	9	27.88	1
104	Max	-439	53.91	17	-3106.29	13	405.28	13	-21.75	1	882.65	1	-31.39	9	-69.62	9	27.88	1

104	Max	-442	53.91	17	-3106.29	13	405.28	13	-21.75	1	882.65	1	-31.39	9	-69.62	9	27.88	1
104	Min.	-415	-17449.60	18	-16800.90	17	-554.87	5	-111.91	17	-5858.12	9	-137.58	17	-4327.81	17	-197.74	9
104	Min.	-412	-17449.60	18	-16800.90	17	-554.87	5	-111.91	17	-5858.12	9	-137.58	17	-4327.81	17	-197.74	9
104	Min.	-439	-17449.60	18	-16800.90	17	-554.87	5	-111.91	17	-5858.12	9	-137.58	17	-4327.81	17	-197.74	9
104	Min.	-442	-17449.60	18	-16800.90	17	-554.87	5	-111.91	17	-5858.12	9	-137.58	17	-4327.81	17	-197.74	9
104	Max	-442	-46.69	13	-2366.41	13	464.83	13	-29.44	1	-376.70	1	72.83	9	2380.63	9	-97.18	1
104	Max	-439	-46.69	13	-2366.41	13	464.83	13	-29.44	1	-376.70	1	72.83	9	2380.63	9	-97.18	1
104	Max	-466	-46.69	13	-2366.41	13	464.83	13	-29.44	1	-376.70	1	72.83	9	2380.63	9	-97.18	1
104	Max	-469	-46.69	13	-2366.41	13	464.83	13	-29.44	1	-376.70	1	72.83	9	2380.63	9	-97.18	1
104	Min.	-442	-10644.50	18	-13467.90	17	-603.46	18	-109.74	17	-6402.16	17	-58.54	1	-1267.55	1	-431.44	17
104	Min.	-439	-10644.50	18	-13467.90	17	-603.46	18	-109.74	17	-6402.16	17	-58.54	1	-1267.55	1	-431.44	17
104	Min.	-466	-10644.50	18	-13467.90	17	-603.46	18	-109.74	17	-6402.16	17	-58.54	1	-1267.55	1	-431.44	17
104	Min.	-469	-10644.50	18	-13467.90	17	-603.46	18	-109.74	17	-6402.16	17	-58.54	1	-1267.55	1	-431.44	17
104	Max	-469	443.88	17	-1837.04	13	553.99	13	-25.72	1	-568.46	1	133.59	9	5574.35	17	14.95	17
104	Max	-466	443.88	17	-1837.04	13	553.99	13	-25.72	1	-568.46	1	133.59	9	5574.35	17	14.95	17
104	Max	-493	443.88	17	-1837.04	13	553.99	13	-25.72	1	-568.46	1	133.59	9	5574.35	17	14.95	17
104	Max	-496	443.88	17	-1837.04	13	553.99	13	-25.72	1	-568.46	1	133.59	9	5574.35	17	14.95	17
104	Min.	-469	-3491.07	18	-11130.40	17	-582.30	18	-112.78	17	-4584.90	17	-44.21	1	265.38	1	-71.99	9
104	Min.	-466	-3491.07	18	-11130.40	17	-582.30	18	-112.78	17	-4584.90	17	-44.21	1	265.38	1	-71.99	9
104	Min.	-493	-3491.07	18	-11130.40	17	-582.30	18	-112.78	17	-4584.90	17	-44.21	1	265.38	1	-71.99	9
104	Min.	-496	-3491.07	18	-11130.40	17	-582.30	18	-112.78	17	-4584.90	17	-44.21	1	265.38	1	-71.99	9
104	Max	-496	480.68	17	-1231.93	13	154.26	13	15.15	17	-97.24	1	543.45	17	8299.30	17	360.08	17
104	Max	-493	480.68	17	-1231.93	13	154.26	13	15.15	17	-97.24	1	543.45	17	8299.30	17	360.08	17
104	Max	191	480.68	17	-1231.93	13	154.26	13	15.15	17	-97.24	1	543.45	17	8299.30	17	360.08	17
104	Max	-502	480.68	17	-1231.93	13	154.26	13	15.15	17	-97.24	1	543.45	17	8299.30	17	360.08	17
104	Min.	-496	46.92	20	-7955.20	17	-2209.47	17	-6.67	9	-1057.89	9	28.12	1	986.58	1	26.62	9
104	Min.	-493	46.92	20	-7955.20	17	-2209.47	17	-6.67	9	-1057.89	9	28.12	1	986.58	1	26.62	9
104	Min.	191	46.92	20	-7955.20	17	-2209.47	17	-6.67	9	-1057.89	9	28.12	1	986.58	1	26.62	9
104	Min.	-502	46.92	20	-7955.20	17	-2209.47	17	-6.67	9	-1057.89	9	28.12	1	986.58	1	26.62	9
104	Max	-385	-136.80	13	-5130.62	20	7089.47	18	132.62	1	3588.99	1	12.70	9	-2514.74	9	70.07	9
104	Max	-382	-136.80	13	-5130.62	20	7089.47	18	132.62	1	3588.99	1	12.70	9	-2514.74	9	70.07	9
104	Max	-409	-136.80	13	-5130.62	20	7089.47	18	132.62	1	3588.99	1	12.70	9	-2514.74	9	70.07	9
104	Max	-412	-136.80	13	-5130.62	20	7089.47	18	132.62	1	3588.99	1	12.70	9	-2514.74	9	70.07	9
104	Min.	-385	-19376.60	18	-20362.60	17	-2628.52	5	-252.75	9	-4995.54	9	-176.40	19	-9183.11	17	-380.97	1
104	Min.	-382	-19376.60	18	-20362.60	17	-2628.52	5	-252.75	9	-4995.54	9	-176.40	19	-9183.11	17	-380.97	1
104	Min.	-409	-19376.60	18	-20362.60	17	-2628.52	5	-252.75	9	-4995.54	9	-176.40	19	-9183.11	17	-380.97	1
104	Min.	-412	-19376.60	18	-20362.60	17	-2628.52	5	-252.75	9	-4995.54	9	-176.40	19	-9183.11	17	-380.97	1
104	Max	-412	-99.48	13	-4496.06	13	1285.19	13	-34.04	1	875.08	1	-41.45	9	83.17	9	10.50	9
104	Max	-409	-99.48	13	-4496.06	13	1285.19	13	-34.04	1	875.08	1	-41.45	9	83.17	9	10.50	9
104	Max	-436	-99.48	13	-4496.06	13	1285.19	13	-34.04	1	875.08	1	-41.45	9	83.17	9	10.50	9
104	Max	-439	-99.48	13	-4496.06	13	1285.19	13	-34.04	1	875.08	1	-41.45	9	83.17	9	10.50	9
104	Min.	-412	-16786.40	18	-16970.40	17	-1669.01	5	-323.01	17	-5810.94	9	-151.86	19	-3566.54	17	-224.53	17
104	Min.	-409	-16786.40	18	-16970.40	17	-1669.01	5	-323.01	17	-5810.94	9	-151.86	19	-3566.54	17	-224.53	17
104	Min.	-436	-16786.40	18	-16970.40	17	-1669.01	5	-323.01	17	-5810.94	9	-151.86	19	-3566.54	17	-224.53	17
104	Min.	-439	-16786.40	18	-16970.40	17	-1669.01	5	-323.01	17	-5810.94	9	-151.86	19	-3566.54	17	-224.53	17
104	Max	-439	-113.26	13	-3373.49	13	1422.83	13	-73.31	1	-368.83	1	68.57	9	2008.26	9	-41.43	9
104	Max	-436	-113.26	13	-3373.49	13	1422.83	13	-73.31	1	-368.83	1	68.57	9	2008.26	9	-41.43	9
104	Max	-463	-113.26	13	-3373.49	13	1422.83	13	-73.31	1	-368.83	1	68.57	9	2008.26	9	-41.43	9
104	Max	-466	-113.26	13	-3373.49	13	1422.83	13	-73.31	1	-368.83	1	68.57	9	2008.26	9	-41.43	9
104	Min.	-439	-10080.90	18	-13784.40	17	-1403.37	5	-346.85	17	-6310.04	17	-66.83	19	-926.31	1	-174.50	1
104	Min.	-436	-10080.90	18	-13784.40	17	-1403.37	5	-346.85	17	-6310.04	17	-66.83	19	-926.31	1	-174.50	1
104	Min.	-463	-10080.90	18	-13784.40	17	-1403.37	5	-346.85	17	-6310.04	17	-66.83	19	-926.31	1	-174.50	1
104	Min.	-466	-10080.90	18	-13784.40	17	-1403.37	5	-346.85	17	-6310.04	17	-66.83	19	-926.31	1	-174.50	1
104	Max	-466	-3.65	17	-2235.15	13	1516.27	13	-69.98	1	-573.59	1	187.19	17	4232.95	17	-126.21	9
104	Max	-463	-3.65	17	-2235.15	13	1516.27	13	-69.98	1	-573.59	1	187.19	17	4232.95	17	-126.21	9
104	Max	-490	-3.65	17	-2235.15	13	1516.27	13	-69.98	1	-573.59	1	187.19	17	4232.95	17	-126.21	9
104	Max	-493	-3.65	17	-2235.15	13	1516.27	13	-69.98	1	-573.59	1	187.19	17	4232.95	17	-126.21	9
104	Min.	-466	-4218.08	18	-9945.94	17	-1285.19	5	-322.85	17	-4616.08	17	-42.01	1	338.26	1	-661.48	17
104	Min.	-463	-4218.08	18	-9945.94	17	-1285.19	5	-322.85	17	-4616.08	17	-42.01	1	338.26	1	-661.48	17
104	Min.	-490	-4218.08	18	-9945.94	17	-1285.19	5	-322.85	17	-4616.08	17	-42.01	1	338.26	1	-661.48	17
104	Min.	-493	-4218.08	18	-9945.94	17	-1285.19	5	-322.85	17	-4616.08	17	-42.01	1	338.26	1	-661.48	17
104	Max	-457	430.85	17	-3822.54	5	2853.20	13	-88.05	9	-570.28	9	129.37	17	4814.54	17	-79.87	9
104	Max	-454	430.85	17	-3822.54	5	2853.20	13	-88.05	9	-570.28	9	129.37	17	4814.54	17	-79.87	9
104	Max	-481	430.85	17	-3822.54	5	2853.20	13	-88.05	9	-570.28	9	129.37	17	4814.54	17	-79.87	9
104	Max	-484	430.85	17	-3822.54	5	2853.20	13	-88.05	9	-570.28	9	129.37	17	4814.54	17	-79.87	9
104	Min.	-457	-2922.20	18	-11985.50	17	-2419.65	5	-334.39	17	-4526.06	17	-48.25	19	394.23	9	-953.54	17
104	Min.	-454	-2922.20	18	-11985.50	17	-2419.65	5	-334.39	17	-4526.06	17	-48.25	19	394.23	9	-953.54	17
104	Min.	-481	-2922.20	18	-11985.50	17	-2419.65	5	-334.39	17	-4526.06	17	-48.25	19	394.23	9	-953.54	17
104	Min.	-484	-2922.20	18	-11985.50	17	-2419.65	5	-334.39	17	-4526.06	17	-48.25	19	394.23	9	-953.54	17
104	Max	-484	-40.40	1	-2169.94	5	5246.22	17	52.40	17	-68.14	17	-28.15	9	9256.17	17	-125.47	9
104	Max	-481	-40.40	1	-2169.94	5	5246.22	17	52.40	17	-68.14	17	-28.15	9	9256.17	17	-125.47	9
104	Max	139	-40.40	1	-2169.94	5	5246.22	17	52.40	17	-68.14	17	-28.15	9	9256.17	17	-125.47	9
104	Max	152	-40.40	1	-2169.94	5	5246.22	17	52.40	17	-68.14	17	-28.15	9	9256.17	17	-125.47	9
104	Min.	-484	-1002.18	18	-12284.80	17	-1957.68	5	-73.92	1	-1014.17	1	-578.32	17	1247.40	9	-1223.66	17
104	Min.	-481	-1002.18	18	-12284.80	17	-1957.68	5	-73.92	1	-1014.17	1	-578.32	17	1247.40	9	-1223.66	17
104	Min.	139	-1002.18	18	-12284.80	17	-1957.68	5	-73.92	1	-1014.17	1	-578.32	17	1247.40	9	-1223.66	17
104	Min.	152	-1002.18	18	-12284.80	17	-1957.68	5	-73.92	1	-1014.17	1	-578.32	17	1247.40	9	-1223.66	17
104	Max	-373	-279.76	5	-7969.12	5	8472.69	18	264.77	9	3538.62	9	86.54	9	-2442.97	1	370.20	9
104	Max	-370	-279.76	5	-7969.12	5	8472.69	18	264.77	9	3538.62	9	86.54	9	-2442.97	1	370.20	9
104	Max	-397	-279.76	5	-7969.12	5	8472.69	18	264.77	9	3538.62	9	86.54	9	-2442.97	1	370.20	9
104	Max	-400	-279.76	5	-7969.12	5	8472.69	18	264.77	9	3538.62	9	86.54	9	-2442.97	1	370.20	9
104	Min.	-373	-5345.88	18	-19572.50	17	-1589.32	5	-405.55	1	-4947.33	1	-35.67	1	-9206.69	17	8.47	1
104	Min.	-370	-5345.88	18	-19572.50	17	-1589.32	5	-405.55	1	-4947.33	1	-35.67	1	-9206.69	17	8.47	1
104	Min.	-397	-5345.88	18	-19572.50	17	-1589.32	5	-405.55	1	-4947.33	1	-35.67	1	-9206.69	17	8.47	1
104	Min.	-400	-5345.88	18	-19572.50	17	-1589.32	5	-405.55	1	-4947.33	1	-35.67	1	-9206.69	17	8.47	1
104	Max	-400	-255.48	5	-6331.07	5	6210.14	18	3.05	9	870.55	9	56.09	17	89.96	1	124.27	9
104	Max	-397	-255.48	5	-6331.07	5	6210.14	18	3.05	9	870.55	9	56.09	17	89.96	1	124.27	9
104	Max	-424	-255.48	5	-6331.07	5	6210.14	18	3.05	9	870.55	9	56.09	17	89.96	1	124.27	9
104	Max	-427	-255.48	5	-6331.07	5	6210.14	18	3.05	9	870.55	9	56.09	17	89.96	1	124.27	9
104	Min.	-400	-4233.41	18	-17285.20	17	-1827.97	5	-457.74	17	-5733.17	1	-26.24	19	-3637.96	17	-40.11	1
104	Min.	-397	-4233.41	18	-17285.20	17	-1827.97	5	-457.74	17	-5733.17	1	-26.24	19	-3637.96	17	-40.11	1
104	Min.	-424	-4233.41	18	-17285.20	17	-1827.97	5	-457.74	17	-5733.17	1	-26.24	19	-3637.96	17	-40.11	1
104	Min.	-427	-4233.41	18	-17285.20	17	-1827.97	5	-457.74	17	-5733.17	1	-26.24	19	-3637.96	17	-40.11	1
104	Max	-427	-135.31	5	-4703.89	5	3373.65	18	-95.42	9	-362.17	9	45.31	17	2033.79	1	114.03	9
104	Max	-424	-135.31	5	-4703.89	5	3373.65	18	-95.42	9	-362.17	9	45.31	17	2033.79	1	114.03	9
104	Max	-451	-135.31	5	-4703.89	5	3373.65	18	-95.42	9	-362.17	9	45.31	17	2033.79	1	114.03	9
104	Max	-454	-135.31	5	-4703.89	5	3373.65	18	-95.42	9	-362.17	9	45.31	17	2033.79	1	114.03	9
104	Min.	-427	-2783.36	18	-14236.00	17	-2002.58	5	-537.62	17	-6242.39	17	-51.77	19	-933.48	9	20.57	1
104	Min.	-424	-2783.36	18	-14236.00	17	-2002.58	5	-537.62	17	-6242.39	17	-51.77	19	-933.48	9	20.57	1
104	Min.	-451	-2783.36	18	-14236.00	17	-2002.58	5	-537.62	17	-6242.39	17	-51.77	19	-933.48	9	20.57	1
104	Min.	-454	-2783.36	18	-14236.00	17	-2002.58	5	-537.62	17	-6242.39	17	-51.77	19	-933.48	9	20.57	1
104	Max	-454	-213.93	1	-3127.24	5	2390.54	13	-90.93	9	-546.72	9	51.19	9	4594.88	17	54.24	9
104	Max	-451	-213.93	1	-3127.24	5	2390.54	13	-90.93	9	-546.72	9	51.19	9	4594.88	17	54.24	9
104	Max	-478	-213.93	1	-3127.24	5	2390.54	13	-90.93	9	-546.72	9	51.19	9	4594.88	17	54.24	9
104	Max	-481	-213.93	1	-3127.24	5	2390.54	13	-90.93	9	-546.72	9	51.19	9	4594.88	17	54.24	9
104	Min.	-454	-1906.79	18	-11200.50	17	-2070.05	5	-399.66	17	-4384.01	17	-79.50	19	377.62	9	-173.99	17
104	Min.	-451	-1906.79	18	-11200.50	17	-2070.05	5	-399.66	17	-4384.01	17	-79.50	19	377.62	9	-173.99	17
104	Min.	-478	-1906.79	18	-11200.50	17	-2070.05	5	-399.66	17	-4384.01	17	-79.50	19	377.62	9	-173.99	17
104	Min.	-481	-1906.79	18	-11200.50	17	-2070.05	5	-399.66	17	-4384.01	17	-79.50	19	377.62	9	-173.99	17

104	Max	-481	-156.08	21	-927.86	5	2329.61	13	-36.09	9	-244.18	9	49.58	9	4600.26	17	12.07	9
104	Max	-478	-156.08	21	-927.86	5	2329.61	13	-36.09	9	-244.18	9	49.58	9	4600.26	17	12.07	9
104	Max	126	-156.08	21	-927.86	5	2329.61	13	-36.09	9	-244.18	9	49.58	9	4600.26	17	12.07	9
104	Max	139	-156.08	21	-927.86	5	2329.61	13	-36.09	9	-244.18	9	49.58	9	4600.26	17	12.07	9
104	Min.	-481	-1103.24	17	-3146.72	17	-2122.43	5	-145.62	17	-1604.19	17	-99.54	19	707.33	9	-164.88	17
104	Min.	-478	-1103.24	17	-3146.72	17	-2122.43	5	-145.62	17	-1604.19	17	-99.54	19	707.33	9	-164.88	17
104	Min.	126	-1103.24	17	-3146.72	17	-2122.43	5	-145.62	17	-1604.19	17	-99.54	19	707.33	9	-164.88	17
104	Min.	139	-1103.24	17	-3146.72	17	-2122.43	5	-145.62	17	-1604.19	17	-99.54	19	707.33	9	-164.88	17
104	Max	-370	-180.01	5	-6313.47	5	7799.57	18	147.80	9	3619.72	9	150.28	9	-2580.70	1	367.11	9
104	Max	-367	-180.01	5	-6313.47	5	7799.57	18	147.80	9	3619.72	9	150.28	9	-2580.70	1	367.11	9
104	Max	-394	-180.01	5	-6313.47	5	7799.57	18	147.80	9	3619.72	9	150.28	9	-2580.70	1	367.11	9
104	Max	-397	-180.01	5	-6313.47	5	7799.57	18	147.80	9	3619.72	9	150.28	9	-2580.70	1	367.11	9
104	Min.	-370	-3842.64	18	-23452.60	18	-987.66	5	-244.76	1	-4975.01	1	-33.52	1	-9307.45	17	-98.78	1
104	Min.	-367	-3842.64	18	-23452.60	18	-987.66	5	-244.76	1	-4975.01	1	-33.52	1	-9307.45	17	-98.78	1
104	Min.	-394	-3842.64	18	-23452.60	18	-987.66	5	-244.76	1	-4975.01	1	-33.52	1	-9307.45	17	-98.78	1
104	Min.	-397	-3842.64	18	-23452.60	18	-987.66	5	-244.76	1	-4975.01	1	-33.52	1	-9307.45	17	-98.78	1
104	Max	-397	-35.19	5	-4897.55	5	4112.22	18	-25.82	9	888.32	9	144.34	17	81.79	1	276.12	17
104	Max	-394	-35.19	5	-4897.55	5	4112.22	18	-25.82	9	888.32	9	144.34	17	81.79	1	276.12	17
104	Max	-421	-35.19	5	-4897.55	5	4112.22	18	-25.82	9	888.32	9	144.34	17	81.79	1	276.12	17
104	Max	-424	-35.19	5	-4897.55	5	4112.22	18	-25.82	9	888.32	9	144.34	17	81.79	1	276.12	17
104	Min.	-397	-1305.30	18	-17718.30	17	-1190.75	5	-311.11	17	-5798.57	1	24.94	21	-3576.12	17	17.50	1
104	Min.	-394	-1305.30	18	-17718.30	17	-1190.75	5	-311.11	17	-5798.57	1	24.94	21	-3576.12	17	17.50	1
104	Min.	-421	-1305.30	18	-17718.30	17	-1190.75	5	-311.11	17	-5798.57	1	24.94	21	-3576.12	17	17.50	1
104	Min.	-424	-1305.30	18	-17718.30	17	-1190.75	5	-311.11	17	-5798.57	1	24.94	21	-3576.12	17	17.50	1
104	Max	-424	-105.67	5	-3663.05	5	2102.72	18	-70.75	9	-360.13	9	73.55	9	1996.70	1	169.97	9
104	Max	-421	-105.67	5	-3663.05	5	2102.72	18	-70.75	9	-360.13	9	73.55	9	1996.70	1	169.97	9
104	Max	-448	-105.67	5	-3663.05	5	2102.72	18	-70.75	9	-360.13	9	73.55	9	1996.70	1	169.97	9
104	Max	-451	-105.67	5	-3663.05	5	2102.72	18	-70.75	9	-360.13	9	73.55	9	1996.70	1	169.97	9
104	Min.	-424	-1143.67	18	-14300.40	17	-1296.17	5	-344.25	17	-6296.31	17	-59.68	1	-940.50	9	38.33	1
104	Min.	-421	-1143.67	18	-14300.40	17	-1296.17	5	-344.25	17	-6296.31	17	-59.68	1	-940.50	9	38.33	1
104	Min.	-448	-1143.67	18	-14300.40	17	-1296.17	5	-344.25	17	-6296.31	17	-59.68	1	-940.50	9	38.33	1
104	Min.	-451	-1143.67	18	-14300.40	17	-1296.17	5	-344.25	17	-6296.31	17	-59.68	1	-940.50	9	38.33	1
104	Max	-451	-1.57	17	-2414.00	5	1442.99	13	-68.38	9	-570.43	9	51.26	9	4223.57	17	662.87	17
104	Max	-448	-1.57	17	-2414.00	5	1442.99	13	-68.38	9	-570.43	9	51.26	9	4223.57	17	662.87	17
104	Max	-475	-1.57	17	-2414.00	5	1442.99	13	-68.38	9	-570.43	9	51.26	9	4223.57	17	662.87	17
104	Max	-478	-1.57	17	-2414.00	5	1442.99	13	-68.38	9	-570.43	9	51.26	9	4223.57	17	662.87	17
104	Min.	-451	-602.46	18	-10258.10	17	-1374.76	5	-320.74	17	-4611.19	17	-171.95	17	331.88	9	126.89	1
104	Min.	-448	-602.46	18	-10258.10	17	-1374.76	5	-320.74	17	-4611.19	17	-171.95	17	331.88	9	126.89	1
104	Min.	-475	-602.46	18	-10258.10	17	-1374.76	5	-320.74	17	-4611.19	17	-171.95	17	331.88	9	126.89	1
104	Min.	-478	-602.46	18	-10258.10	17	-1374.76	5	-320.74	17	-4611.19	17	-171.95	17	331.88	9	126.89	1
104	Max	-478	-7.22	9	-1590.29	5	971.49	13	-17.53	9	-107.47	9	183.72	17	7911.36	17	660.50	17
104	Max	-475	-7.22	9	-1590.29	5	971.49	13	-17.53	9	-107.47	9	183.72	17	7911.36	17	660.50	17
104	Max	113	-7.22	9	-1590.29	5	971.49	13	-17.53	9	-107.47	9	183.72	17	7911.36	17	660.50	17
104	Max	126	-7.22	9	-1590.29	5	971.49	13	-17.53	9	-107.47	9	183.72	17	7911.36	17	660.50	17
104	Min.	-478	-202.22	18	-9088.97	17	-2952.56	17	-63.26	17	-1061.33	1	-121.80	1	1140.72	9	110.36	1
104	Min.	-475	-202.22	18	-9088.97	17	-2952.56	17	-63.26	17	-1061.33	1	-121.80	1	1140.72	9	110.36	1
104	Min.	113	-202.22	18	-9088.97	17	-2952.56	17	-63.26	17	-1061.33	1	-121.80	1	1140.72	9	110.36	1
104	Min.	126	-202.22	18	-9088.97	17	-2952.56	17	-63.26	17	-1061.33	1	-121.80	1	1140.72	9	110.36	1
104	Max	-367	-69.36	5	-4537.77	5	2302.98	18	2.35	9	3658.06	9	252.58	17	-3298.36	1	137.69	17
104	Max	-364	-69.36	5	-4537.77	5	2302.98	18	2.35	9	3658.06	9	252.58	17	-3298.36	1	137.69	17
104	Max	-391	-69.36	5	-4537.77	5	2302.98	18	2.35	9	3658.06	9	252.58	17	-3298.36	1	137.69	17
104	Max	-394	-69.36	5	-4537.77	5	2302.98	18	2.35	9	3658.06	9	252.58	17	-3298.36	1	137.69	17
104	Min.	-367	-651.84	18	-26115.70	18	-402.18	5	-74.21	1	-4989.06	1	72.55	1	-10549.40	17	29.93	9
104	Min.	-364	-651.84	18	-26115.70	18	-402.18	5	-74.21	1	-4989.06	1	72.55	1	-10549.40	17	29.93	9
104	Min.	-391	-651.84	18	-26115.70	18	-402.18	5	-74.21	1	-4989.06	1	72.55	1	-10549.40	17	29.93	9
104	Min.	-394	-651.84	18	-26115.70	18	-402.18	5	-74.21	1	-4989.06	1	72.55	1	-10549.40	17	29.93	9
104	Max	-394	102.06	17	-3596.81	5	1336.82	18	-20.99	9	903.88	9	133.91	17	-113.36	1	200.82	1
104	Max	-391	102.06	17	-3596.81	5	1336.82	18	-20.99	9	903.88	9	133.91	17	-113.36	1	200.82	1
104	Max	-418	102.06	17	-3596.81	5	1336.82	18	-20.99	9	903.88	9	133.91	17	-113.36	1	200.82	1
104	Max	-421	102.06	17	-3596.81	5	1336.82	18	-20.99	9	903.88	9	133.91	17	-113.36	1	200.82	1
104	Min.	-394	-51.85	18	-17712.60	17	-379.74	5	-112.78	17	-5841.45	1	31.89	1	-4391.24	17	-25.00	9
104	Min.	-391	-51.85	18	-17712.60	17	-379.74	5	-112.78	17	-5841.45	1	31.89	1	-4391.24	17	-25.00	9
104	Min.	-418	-51.85	18	-17712.60	17	-379.74	5	-112.78	17	-5841.45	1	31.89	1	-4391.24	17	-25.00	9
104	Min.	-421	-51.85	18	-17712.60	17	-379.74	5	-112.78	17	-5841.45	1	31.89	1	-4391.24	17	-25.00	9
104	Max	-421	-54.57	5	-2746.06	5	606.92	18	-27.96	9	-368.44	9	63.76	9	2351.23	1	432.40	17
104	Max	-418	-54.57	5	-2746.06	5	606.92	18	-27.96	9	-368.44	9	63.76	9	2351.23	1	432.40	17
104	Max	-445	-54.57	5	-2746.06	5	606.92	18	-27.96	9	-368.44	9	63.76	9	2351.23	1	432.40	17
104	Max	-448	-54.57	5	-2746.06	5	606.92	18	-27.96	9	-368.44	9	63.76	9	2351.23	1	432.40	17
104	Min.	-421	-310.32	17	-14148.10	17	-420.60	5	-107.35	17	-6389.83	17	-66.22	1	-1293.53	9	97.32	9
104	Min.	-418	-310.32	17	-14148.10	17	-420.60	5	-107.35	17	-6389.83	17	-66.22	1	-1293.53	9	97.32	9
104	Min.	-445	-310.32	17	-14148.10	17	-420.60	5	-107.35	17	-6389.83	17	-66.22	1	-1293.53	9	97.32	9
104	Min.	-448	-310.32	17	-14148.10	17	-420.60	5	-107.35	17	-6389.83	17	-66.22	1	-1293.53	9	97.32	9
104	Max	-448	446.95	17	-2073.57	5	381.81	13	-25.44	9	-564.08	9	49.90	9	5522.18	17	70.36	1
104	Max	-445	446.95	17	-2073.57	5	381.81	13	-25.44	9	-564.08	9	49.90	9	5522.18	17	70.36	1
104	Max	-472	446.95	17	-2073.57	5	381.81	13	-25.44	9	-564.08	9	49.90	9	5522.18	17	70.36	1
104	Max	-475	446.95	17	-2073.57	5	381.81	13	-25.44	9	-564.08	9	49.90	9	5522.18	17	70.36	1
104	Min.	-448	20.81	20	-11541.30	17	-509.27	5	-112.59	17	-4578.07	17	-127.38	1	233.63	9	-18.36	17
104	Min.	-445	20.81	20	-11541.30	17	-509.27	5	-112.59	17	-4578.07	17	-127.38	1	233.63	9	-18.36	17
104	Min.	-472	20.81	20	-11541.30	17	-509.27	5	-112.59	17	-4578.07	17	-127.38	1	233.63	9	-18.36	17
104	Min.	-475	20.81	20	-11541.30	17	-509.27	5	-112.59	17	-4578.07	17	-127.38	1	233.63	9	-18.36	17
104	Max	-475	479.89	17	-1312.45	5	2290.70	17	15.45	17	-96.06	9	-21.60	9	8246.73	17	-26.09	1
104	Max	-472	479.89	17	-1312.45	5	2290.70	17	15.45	17	-96.06	9	-21.60	9	8246.73	17	-26.09	1
104	Max	-499	479.89	17	-1312.45	5	2290.70	17	15.45	17	-96.06	9	-21.60	9	8246.73	17	-26.09	1
104	Max	113	479.89	17	-1312.45	5	2290.70	17	15.45	17	-96.06	9	-21.60	9	8246.73	17	-26.09	1
104	Min.	-475	48.59	20	-8093.04	17	-106.61	5	-6.51	1	-1056.76	1	-532.77	17	954.22	9	-359.44	17
104	Min.	-472	48.59	20	-8093.04	17	-106.61	5	-6.51	1	-1056.76	1	-532.77	17	954.22	9	-359.44	17
104	Min.	-499	48.59	20	-8093.04	17	-106.61	5	-6.51	1	-1056.76	1	-532.77	17	954.22	9	-359.44	17
104	Min.	113	48.59	20	-8093.04	17	-106.61	5	-6.51	1	-1056.76	1	-532.77	17	954.22	9	-359.44	17
104	Max	-409	-280.52	13	-5265.49	20	4098.81	18	-4.24	1	858.39	1	13.29	9	101.69	9	11.69	9
104	Max	-406	-280.52	13	-5265.49	20	4098.81	18	-4.24	1	858.39	1	13.29	9	101.69	9	11.69	9
104	Max	-433	-280.52	13	-5265.49	20	4098.81	18	-4.24	1	858.39	1	13.29	9	101.69	9	11.69	9
104	Max	-436	-280.52	13	-5265.49	20	4098.81	18	-4.24	1	858.39	1	13.29	9	101.69	9	11.69	9
104	Min.	-409	-13121.00	18	-16800.90	17	-2448.75	5	-465.08	17	-5747.45	9	-91.05	19	-3613.61	17	-171.18	1
104	Min.	-406	-13121.00	18	-16800.90	17	-2448.75	5	-465.08	17	-5747.45	9	-91.05	19	-3613.61	17	-171.18	1
104	Min.	-433	-13121.00	18	-16800.90	17	-2448.75	5	-465.08	17	-5747.45	9	-91.05	19	-3613.61	17	-171.18	1
104	Min.	-436	-13121.00	18	-16800.90	17	-2448.75	5	-465.08	17	-5747.45	9	-91.05	19	-3613.61	17	-171.18	1
104	Max	-436	-165.31	22	-4506.26	13	2216.95	13	-98.80	1	-366.88	1	28.92	9	2040.47	9	-8.54	9
104	Max	-433	-165.31	22	-4506.26	13	2216.95	13	-98.80	1	-366.88	1	28.92	9	2040.47	9	-8.54	9
104	Max	-460	-165.31	22	-4506.26	13	2216.95	13	-98.80	1	-366.88	1	28.92	9	2040.47	9	-8.54	9
104	Max	-463	-165.31	22	-4506.26	13	2216.95	13	-98.80	1	-366.88	1	28.92	9	2040.47	9	-8.54	9
104	Min.	-436	-9143.01	18	-13909.10	17	-2213.29	5	-541.57	17	-6249.77	17	-76.90	19	-924.63	1	-101.45	1
104	Min.	-433	-9143.01	18	-13909.10	17	-2213.29	5	-541.57	17	-6249.77	17	-76.90	19	-924.63	1	-101.45	1
104	Min.	-460	-9143.01	18	-13909.10	17	-2213.29	5	-541.57	17	-6249.77	17	-76.90	19	-924.63	1	-101.45	1
104	Min.	-463	-9143.01	18	-13909.10	17	-2213.29	5	-541.57	17	-6249.77	17	-76.90	19	-924.63	1	-101.45	1
104	Max	-463	-216.75	21	-3012.81	13	2297.97	13	-92.97	1	-548.73	1	71.94	9	4601.22	17	179.00	17
104	Max	-460	-216.75	21	-3012.81	13	2297.97	13	-92.97	1	-548.73	1	71.94	9	4601.22	17	179.00	17
104	Max	-487	-216.75	21	-3012.81	13	2297.97	13	-92.97	1	-548.73	1	71.94	9	4601.22	17	179.00	17
104	Max	-490	-216.75	21	-3012.81	13	2297.97	13	-92.97	1	-548.73	1	71.94	9	4601.22	17	179.00	17
104	Min.	-463	-4769.77	18	-11009.30	17	-2142.35	5	-402.30	17	-4387.04	17	-48.54	19	382.02	1	-51.50	1

104	Min.	-460	-4769.77	18	-11009.30	17	-2142.35	5	-402.30	17	-4387.04	17	-48.54	19	382.02	1	-51.50	1
104	Min.	-487	-4769.77	18	-11009.30	17	-2142.35	5	-402.30	17	-4387.04	17	-48.54	19	382.02	1	-51.50	1
104	Min.	-490	-4769.77	18	-11009.30	17	-2142.35	5	-402.30	17	-4387.04	17	-48.54	19	382.02	1	-51.50	1
104	Max	-490	-158.60	1	-890.83	13	2357.16	13	-36.63	1	-244.75	1	95.90	9	4604.65	17	165.79	17
104	Max	-487	-158.60	1	-890.83	13	2357.16	13	-36.63	1	-244.75	1	95.90	9	4604.65	17	165.79	17
104	Max	165	-158.60	1	-890.83	13	2357.16	13	-36.63	1	-244.75	1	95.90	9	4604.65	17	165.79	17
104	Max	178	-158.60	1	-890.83	13	2357.16	13	-36.63	1	-244.75	1	95.90	9	4604.65	17	165.79	17
104	Min.	-490	-1502.08	18	-3084.04	17	-2087.21	5	-146.32	17	-1605.04	17	-38.33	1	710.29	1	-11.61	1
104	Min.	-487	-1502.08	18	-3084.04	17	-2087.21	5	-146.32	17	-1605.04	17	-38.33	1	710.29	1	-11.61	1
104	Min.	165	-1502.08	18	-3084.04	17	-2087.21	5	-146.32	17	-1605.04	17	-38.33	1	710.29	1	-11.61	1
104	Min.	178	-1502.08	18	-3084.04	17	-2087.21	5	-146.32	17	-1605.04	17	-38.33	1	710.29	1	-11.61	1
104	Max	-379	-658.49	13	-8291.73	20	9296.71	18	301.42	1	3500.72	1	20.92	9	-2449.86	9	67.68	9
104	Max	-376	-658.49	13	-8291.73	20	9296.71	18	301.42	1	3500.72	1	20.92	9	-2449.86	9	67.68	9
104	Max	-403	-658.49	13	-8291.73	20	9296.71	18	301.42	1	3500.72	1	20.92	9	-2449.86	9	67.68	9
104	Max	-406	-658.49	13	-8291.73	20	9296.71	18	301.42	1	3500.72	1	20.92	9	-2449.86	9	67.68	9
104	Min.	-379	-9241.36	18	-18938.00	17	-2153.72	5	-466.01	9	-4982.42	9	-57.62	19	-9301.36	17	-64.77	1
104	Min.	-376	-9241.36	18	-18938.00	17	-2153.72	5	-466.01	9	-4982.42	9	-57.62	19	-9301.36	17	-64.77	1
104	Min.	-403	-9241.36	18	-18938.00	17	-2153.72	5	-466.01	9	-4982.42	9	-57.62	19	-9301.36	17	-64.77	1
104	Min.	-406	-9241.36	18	-18938.00	17	-2153.72	5	-466.01	9	-4982.42	9	-57.62	19	-9301.36	17	-64.77	1
104	Max	-406	-481.62	13	-6376.26	20	5799.96	18	27.74	1	839.94	1	19.84	9	140.64	9	27.35	9
104	Max	-403	-481.62	13	-6376.26	20	5799.96	18	27.74	1	839.94	1	19.84	9	140.64	9	27.35	9
104	Max	-430	-481.62	13	-6376.26	20	5799.96	18	27.74	1	839.94	1	19.84	9	140.64	9	27.35	9
104	Max	-433	-481.62	13	-6376.26	20	5799.96	18	27.74	1	839.94	1	19.84	9	140.64	9	27.35	9
104	Min.	-406	-9504.83	18	-16618.10	17	-2455.75	5	-511.94	17	-5719.87	9	-70.94	19	-3588.91	17	-53.02	1
104	Min.	-403	-9504.83	18	-16618.10	17	-2455.75	5	-511.94	17	-5719.87	9	-70.94	19	-3588.91	17	-53.02	1
104	Min.	-430	-9504.83	18	-16618.10	17	-2455.75	5	-511.94	17	-5719.87	9	-70.94	19	-3588.91	17	-53.02	1
104	Min.	-433	-9504.83	18	-16618.10	17	-2455.75	5	-511.94	17	-5719.87	9	-70.94	19	-3588.91	17	-53.02	1
104	Max	-433	-296.33	21	-5072.50	20	2796.03	18	-92.27	1	-374.32	1	19.12	9	2042.44	9	-20.23	9
104	Max	-430	-296.33	21	-5072.50	20	2796.03	18	-92.27	1	-374.32	1	19.12	9	2042.44	9	-20.23	9
104	Max	-457	-296.33	21	-5072.50	20	2796.03	18	-92.27	1	-374.32	1	19.12	9	2042.44	9	-20.23	9
104	Max	-460	-296.33	21	-5072.50	20	2796.03	18	-92.27	1	-374.32	1	19.12	9	2042.44	9	-20.23	9
104	Min.	-433	-7302.22	18	-14251.30	17	-2522.15	5	-551.24	17	-6254.46	17	-69.88	19	-951.32	1	-247.94	17
104	Min.	-430	-7302.22	18	-14251.30	17	-2522.15	5	-551.24	17	-6254.46	17	-69.88	19	-951.32	1	-247.94	17
104	Min.	-457	-7302.22	18	-14251.30	17	-2522.15	5	-551.24	17	-6254.46	17	-69.88	19	-951.32	1	-247.94	17
104	Min.	-460	-7302.22	18	-14251.30	17	-2522.15	5	-551.24	17	-6254.46	17	-69.88	19	-951.32	1	-247.94	17
104	Max	-460	422.65	17	-3742.64	20	2699.83	13	-88.60	1	-571.27	1	21.40	9	4817.67	17	960.22	17
104	Max	-457	422.65	17	-3742.64	20	2699.83	13	-88.60	1	-571.27	1	21.40	9	4817.67	17	960.22	17
104	Max	-484	422.65	17	-3742.64	20	2699.83	13	-88.60	1	-571.27	1	21.40	9	4817.67	17	960.22	17
104	Max	-487	422.65	17	-3742.64	20	2699.83	13	-88.60	1	-571.27	1	21.40	9	4817.67	17	960.22	17
104	Min.	-460	-4080.17	18	-11922.60	17	-2564.11	5	-335.02	17	-4527.37	17	-111.88	17	396.29	1	83.38	1
104	Min.	-457	-4080.17	18	-11922.60	17	-2564.11	5	-335.02	17	-4527.37	17	-111.88	17	396.29	1	83.38	1
104	Min.	-484	-4080.17	18	-11922.60	17	-2564.11	5	-335.02	17	-4527.37	17	-111.88	17	396.29	1	83.38	1
104	Min.	-487	-4080.17	18	-11922.60	17	-2564.11	5	-335.02	17	-4527.37	17	-111.88	17	396.29	1	83.38	1
104	Max	-487	-38.01	21	-2156.11	13	2238.51	13	52.03	17	-68.39	17	597.16	17	9257.85	17	1225.89	17
104	Max	-484	-38.01	21	-2156.11	13	2238.51	13	52.03	17	-68.39	17	597.16	17	9257.85	17	1225.89	17
104	Max	152	-38.01	21	-2156.11	13	2238.51	13	52.03	17	-68.39	17	597.16	17	9257.85	17	1225.89	17
104	Max	165	-38.01	21	-2156.11	13	2238.51	13	52.03	17	-68.39	17	597.16	17	9257.85	17	1225.89	17
104	Min.	-487	-1274.27	18	-12263.10	17	-4767.65	17	-74.07	9	-1014.28	9	22.98	21	1248.61	1	126.71	1
104	Min.	-484	-1274.27	18	-12263.10	17	-4767.65	17	-74.07	9	-1014.28	9	22.98	21	1248.61	1	126.71	1
104	Min.	152	-1274.27	18	-12263.10	17	-4767.65	17	-74.07	9	-1014.28	9	22.98	21	1248.61	1	126.71	1
104	Min.	165	-1274.27	18	-12263.10	17	-4767.65	17	-74.07	9	-1014.28	9	22.98	21	1248.61	1	126.71	1
104	Max	-376	-636.38	5	-9486.06	5	8934.53	18	317.27	1	3521.00	9	9.16	9	-2428.14	9	-76.83	9
104	Max	-373	-636.38	5	-9486.06	5	8934.53	18	317.27	1	3521.00	9	9.16	9	-2428.14	9	-76.83	9
104	Max	-400	-636.38	5	-9486.06	5	8934.53	18	317.27	1	3521.00	9	9.16	9	-2428.14	9	-76.83	9
104	Max	-403	-636.38	5	-9486.06	5	8934.53	18	317.27	1	3521.00	9	9.16	9	-2428.14	9	-76.83	9
104	Min.	-376	-6942.66	18	-19206.70	17	-1887.07	5	-465.33	9	-4956.20	1	-74.99	19	-9279.92	17	-232.50	19
104	Min.	-373	-6942.66	18	-19206.70	17	-1887.07	5	-465.33	9	-4956.20	1	-74.99	19	-9279.92	17	-232.50	19
104	Min.	-400	-6942.66	18	-19206.70	17	-1887.07	5	-465.33	9	-4956.20	1	-74.99	19	-9279.92	17	-232.50	19
104	Min.	-403	-6942.66	18	-19206.70	17	-1887.07	5	-465.33	9	-4956.20	1	-74.99	19	-9279.92	17	-232.50	19
104	Max	-403	-444.28	5	-7595.17	5	6398.40	18	24.13	9	846.28	9	25.64	9	119.38	1	94.68	9
104	Max	-400	-444.28	5	-7595.17	5	6398.40	18	24.13	9	846.28	9	25.64	9	119.38	1	94.68	9
104	Max	-427	-444.28	5	-7595.17	5	6398.40	18	24.13	9	846.28	9	25.64	9	119.38	1	94.68	9
104	Max	-430	-444.28	5	-7595.17	5	6398.40	18	24.13	9	846.28	9	25.64	9	119.38	1	94.68	9
104	Min.	-403	-6723.49	18	-16756.80	17	-2234.35	5	-520.38	17	-5712.99	1	-58.08	19	-3621.21	17	12.32	1
104	Min.	-400	-6723.49	18	-16756.80	17	-2234.35	5	-520.38	17	-5712.99	1	-58.08	19	-3621.21	17	12.32	1
104	Min.	-427	-6723.49	18	-16756.80	17	-2234.35	5	-520.38	17	-5712.99	1	-58.08	19	-3621.21	17	12.32	1
104	Min.	-430	-6723.49	18	-16756.80	17	-2234.35	5	-520.38	17	-5712.99	1	-58.08	19	-3621.21	17	12.32	1
104	Max	-430	-284.06	5	-5733.64	5	3647.04	18	-89.30	9	-373.31	9	29.79	17	2044.27	1	260.19	17
104	Max	-427	-284.06	5	-5733.64	5	3647.04	18	-89.30	9	-373.31	9	29.79	17	2044.27	1	260.19	17
104	Max	-454	-284.06	5	-5733.64	5	3647.04	18	-89.30	9	-373.31	9	29.79	17	2044.27	1	260.19	17
104	Max	-457	-284.06	5	-5733.64	5	3647.04	18	-89.30	9	-373.31	9	29.79	17	2044.27	1	260.19	17
104	Min.	-430	-5105.72	18	-14372.90	17	-2419.45	5	-546.85	17	-6253.47	17	-57.03	19	-951.52	9	29.21	1
104	Min.	-427	-5105.72	18	-14372.90	17	-2419.45	5	-546.85	17	-6253.47	17	-57.03	19	-951.52	9	29.21	1
104	Min.	-454	-5105.72	18	-14372.90	17	-2419.45	5	-546.85	17	-6253.47	17	-57.03	19	-951.52	9	29.21	1
104	Min.	-457	-5105.72	18	-14372.90	17	-2419.45	5	-546.85	17	-6253.47	17	-57.03	19	-951.52	9	29.21	1
104	Max	-258	15.03	13	1433.11	18	15078.40	18	346.79	17	8367.68	1	247.32	9	-7387.97	9	837.15	9
104	Max	-237	15.03	13	1433.11	18	15078.40	18	346.79	17	8367.68	1	247.32	9	-7387.97	9	837.15	9
104	Max	-385	15.03	13	1433.11	18	15078.40	18	346.79	17	8367.68	1	247.32	9	-7387.97	9	837.15	9
104	Max	-388	15.03	13	1433.11	18	15078.40	18	346.79	17	8367.68	1	247.32	9	-7387.97	9	837.15	9
104	Min.	-258	-14835.20	18	-28133.80	17	-3725.06	5	-14.98	9	-2100.84	9	-179.00	1	-17648.70	17	-605.03	1
104	Min.	-237	-14835.20	18	-28133.80	17	-3725.06	5	-14.98	9	-2100.84	9	-179.00	1	-17648.70	17	-605.03	1
104	Min.	-385	-14835.20	18	-28133.80	17	-3725.06	5	-14.98	9	-2100.84	9	-179.00	1	-17648.70	17	-605.03	1
104	Min.	-388	-14835.20	18	-28133.80	17	-3725.06	5	-14.98	9	-2100.84	9	-179.00	1	-17648.70	17	-605.03	1
104	Max	-237	-232.74	13	-6848.71	20	14783.20	18	587.76	1	8025.89	1	121.36	9	-5707.14	9	493.71	9
104	Max	-199	-232.74	13	-6848.71	20	14783.20	18	587.76	1	8025.89	1	121.36	9	-5707.14	9	493.71	9
104	Max	-382	-232.74	13	-6848.71	20	14783.20	18	587.76	1	8025.89	1	121.36	9	-5707.14	9	493.71	9
104	Max	-385	-232.74	13	-6848.71	20	14783.20	18	587.76	1	8025.89	1	121.36	9	-5707.14	9	493.71	9
104	Min.	-237	-9890.88	18	-21833.10	17	-2802.70	5	-147.83	9	-2316.64	9	-69.93	1	-15768.20	17	-498.24	1
104	Min.	-199	-9890.88	18	-21833.10	17	-2802.70	5	-147.83	9	-2316.64	9	-69.93	1	-15768.20	17	-498.24	1
104	Min.	-382	-9890.88	18	-21833.10	17	-2802.70	5	-147.83	9	-2316.64	9	-69.93	1	-15768.20	17	-498.24	1
104	Min.	-385	-9890.88	18	-21833.10	17	-2802.70	5	-147.83	9	-2316.64	9	-69.93	1	-15768.20	17	-498.24	1
104	Max	-199	-607.39	13	-8805.17	20	13702.70	18	706.41	9	8025.88	1	13.67	9	-5465.00	1	114.99	9
104	Max	-171	-607.39	13	-8805.17	20	13702.70	18	706.41	9	8025.88	1	13.67	9	-5465.00	1	114.99	9
104	Max	-379	-607.39	13	-8805.17	20	13702.70	18	706.41	9	8025.88	1	13.67	9	-5465.00	1	114.99	9
104	Max	-382	-607.39	13	-8805.17	20	13702.70	18	706.41	9	8025.88	1	13.67	9	-5465.00	1	114.99	9
104	Min.	-199	-7792.65	18	-21018.80	17	-1701.49	5	-226.05	1	-2446.67	9	-90.60	19	-15736.60	17	-229.85	1
104	Min.	-171	-7792.65	18	-21018.80	17	-1701.49	5	-226.05	1	-2446.67	9	-90.60	19	-15736.60	17	-229.85	1
104	Min.	-379	-7792.65	18	-21018.80	17	-1701.49	5	-226.05	1	-2446.67	9	-90.60	19	-15736.60	17	-229.85	1
104	Min.	-382	-7792.65	18	-21018.80	17	-1701.49	5	-226.05	1	-2446.67	9	-90.60	19	-15736.60	17	-229.85	1
104	Max	-171	-564.23	13	-11347.80	13	11875.00	18	852.33	1	8165.67	1	-3.82	9	-6058.62	9	43.36	9
104	Max	-148	-564.23	13	-11347.80	13	11875.00	18	852.33	1	8165.67	1	-3.82	9	-6058.62	9	43.36	9
104	Max	-376	-564.23	13	-11347.80	13	11875.00	18	852.33	1	8165.67	1	-3.82	9	-6058.62	9	43.36	9
104	Max	-379	-564.23	13	-11347.80	13	11875.00	18	852.33	1	8165.67	1	-3.82	9	-6058.62	9	43.36	9
104	Min.	-171	-5636.54	18	-21500.40	17	-1864.60	5	-182.30	9	-2308.80	9	-49.79	19	-16445.60	17	-99.71	19
104	Min.	-148	-5636.54	18	-21500.40	17	-1864.60	5	-182.30	9	-2308.80	9	-49.79	19	-16445.60	17	-99.71	19
104	Min.	-376	-5636.54	18	-21500.40	17	-1864.60	5	-182.30	9	-2308.80	9	-49.79	19	-16445.60	17	-99.71	19
104	Min.	-379	-5636.54	18	-21500.40	17	-1864.60	5	-182.30	9	-2308.80	9	-49.79	19	-16445.60	17	-99.71	19
104	Max	-148	-908.10	5	-11196.00	5	9666.23	18	749.78	1	8049.11	1	121.64	18	-5424.42	9	25.59	17
104	Max	-124	-908.10	5	-11196.00	5	9666.23	18	749.78	1	8049.11	1	121.64	18	-5424.42	9	25.59	17

104	Max	-373	-908.10	5	-11196.00	5	9666.23	18	749.78	1	8049.11	1	121.64	18	-5424.42	9	25.59	17
104	Max	-376	-908.10	5	-11196.00	5	9666.23	18	749.78	1	8049.11	1	121.64	18	-5424.42	9	25.59	17
104	Min.	-148	-4921.46	18	-21584.00	17	-1643.30	5	-273.04	9	-2508.15	9	21.37	1	-15706.40	17	-132.94	19
104	Min.	-124	-4921.46	18	-21584.00	17	-1643.30	5	-273.04	9	-2508.15	9	21.37	1	-15706.40	17	-132.94	19
104	Min.	-373	-4921.46	18	-21584.00	17	-1643.30	5	-273.04	9	-2508.15	9	21.37	1	-15706.40	17	-132.94	19
104	Min.	-376	-4921.46	18	-21584.00	17	-1643.30	5	-273.04	9	-2508.15	9	21.37	1	-15706.40	17	-132.94	19
104	Max	-124	-550.19	5	-9997.16	5	9619.51	18	753.69	9	8068.95	9	-50.08	9	-5432.11	1	271.40	9
104	Max	-100	-550.19	5	-9997.16	5	9619.51	18	753.69	9	8068.95	9	-50.08	9	-5432.11	1	271.40	9
104	Max	-370	-550.19	5	-9997.16	5	9619.51	18	753.69	9	8068.95	9	-50.08	9	-5432.11	1	271.40	9
104	Max	-373	-550.19	5	-9997.16	5	9619.51	18	753.69	9	8068.95	9	-50.08	9	-5432.11	1	271.40	9
104	Min.	-124	-5305.01	18	-22166.80	17	-984.99	5	-219.04	1	-2459.37	1	-160.85	19	-15820.30	17	-198.36	1
104	Min.	-100	-5305.01	18	-22166.80	17	-984.99	5	-219.04	1	-2459.37	1	-160.85	19	-15820.30	17	-198.36	1
104	Min.	-370	-5305.01	18	-22166.80	17	-984.99	5	-219.04	1	-2459.37	1	-160.85	19	-15820.30	17	-198.36	1
104	Min.	-373	-5305.01	18	-22166.80	17	-984.99	5	-219.04	1	-2459.37	1	-160.85	19	-15820.30	17	-198.36	1
104	Max	-100	-191.40	5	-7575.12	5	8096.67	18	634.71	9	8165.65	9	111.91	9	-6080.06	1	298.30	9
104	Max	-68	-191.40	5	-7575.12	5	8096.67	18	634.71	9	8165.65	9	111.91	9	-6080.06	1	298.30	9
104	Max	-367	-191.40	5	-7575.12	5	8096.67	18	634.71	9	8165.65	9	111.91	9	-6080.06	1	298.30	9
104	Max	-370	-191.40	5	-7575.12	5	8096.67	18	634.71	9	8165.65	9	111.91	9	-6080.06	1	298.30	9
104	Min.	-100	-4605.40	18	-25910.80	18	-1307.65	5	-100.30	1	-2144.87	1	-88.55	1	-16234.20	17	-674.88	1
104	Min.	-68	-4605.40	18	-25910.80	18	-1307.65	5	-100.30	1	-2144.87	1	-88.55	1	-16234.20	17	-674.88	1
104	Min.	-367	-4605.40	18	-25910.80	18	-1307.65	5	-100.30	1	-2144.87	1	-88.55	1	-16234.20	17	-674.88	1
104	Min.	-370	-4605.40	18	-25910.80	18	-1307.65	5	-100.30	1	-2144.87	1	-88.55	1	-16234.20	17	-674.88	1
104	Max	-68	-242.96	5	-5899.75	5	10455.40	18	314.42	9	8392.94	9	155.25	9	-7238.50	1	646.38	9
104	Max	-51	-242.96	5	-5899.75	5	10455.40	18	314.42	9	8392.94	9	155.25	9	-7238.50	1	646.38	9
104	Max	-364	-242.96	5	-5899.75	5	10455.40	18	314.42	9	8392.94	9	155.25	9	-7238.50	1	646.38	9
104	Max	-367	-242.96	5	-5899.75	5	10455.40	18	314.42	9	8392.94	9	155.25	9	-7238.50	1	646.38	9
104	Min.	-68	-4496.40	18	-44654.40	18	249.49	5	-53.79	1	-2072.85	1	-278.20	1	-17399.80	17	-632.49	1
104	Min.	-51	-4496.40	18	-44654.40	18	249.49	5	-53.79	1	-2072.85	1	-278.20	1	-17399.80	17	-632.49	1
104	Min.	-364	-4496.40	18	-44654.40	18	249.49	5	-53.79	1	-2072.85	1	-278.20	1	-17399.80	17	-632.49	1
104	Min.	-367	-4496.40	18	-44654.40	18	249.49	5	-53.79	1	-2072.85	1	-278.20	1	-17399.80	17	-632.49	1
104	Max	-388	-9.99	13	-4051.15	13	340.15	13	-10.35	1	3607.78	1	-74.30	9	-3255.29	9	-103.37	1
104	Max	-385	-9.99	13	-4051.15	13	340.15	13	-10.35	1	3607.78	1	-74.30	9	-3255.29	9	-103.37	1
104	Max	-412	-9.99	13	-4051.15	13	340.15	13	-10.35	1	3607.78	1	-74.30	9	-3255.29	9	-103.37	1
104	Max	-415	-9.99	13	-4051.15	13	340.15	13	-10.35	1	3607.78	1	-74.30	9	-3255.29	9	-103.37	1
104	Min.	-388	-26281.10	18	-20910.90	17	-770.55	5	-101.45	17	-5044.08	9	-256.67	17	-10523.40	17	-246.37	17
104	Min.	-385	-26281.10	18	-20910.90	17	-770.55	5	-101.45	17	-5044.08	9	-256.67	17	-10523.40	17	-246.37	17
104	Min.	-412	-26281.10	18	-20910.90	17	-770.55	5	-101.45	17	-5044.08	9	-256.67	17	-10523.40	17	-246.37	17
104	Min.	-415	-26281.10	18	-20910.90	17	-770.55	5	-101.45	17	-5044.08	9	-256.67	17	-10523.40	17	-246.37	17
401	Max	-126	-2538.54	1	189.83	13	3097.13	19	9570.50	17	537.92	17	488.79	17	2206.93	19	14813.00	19
401	Max	-118	-2538.54	1	189.83	13	3097.13	19	9570.50	17	537.92	17	488.79	17	2206.93	19	14813.00	19
401	Max	-98	-2538.54	1	189.83	13	3097.13	19	9570.50	17	537.92	17	488.79	17	2206.93	19	14813.00	19
401	Max	-101	-2538.54	1	189.83	13	3097.13	19	9570.50	17	537.92	17	488.79	17	2206.93	19	14813.00	19
401	Min.	-126	-6812.91	17	-2619.31	19	-519.84	13	2938.77	9	-35.18	13	183.36	5	165.95	13	5520.46	9
401	Min.	-118	-6812.91	17	-2619.31	19	-519.84	13	2938.77	9	-35.18	13	183.36	5	165.95	13	5520.46	9
401	Min.	-98	-6812.91	17	-2619.31	19	-519.84	13	2938.77	9	-35.18	13	183.36	5	165.95	13	5520.46	9
401	Min.	-101	-6812.91	17	-2619.31	19	-519.84	13	2938.77	9	-35.18	13	183.36	5	165.95	13	5520.46	9
401	Max	-126	1839.33	19	-2747.77	1	1139.45	17	-1123.52	9	-1759.01	9	-426.65	5	-10915.20	9	25510.70	19
401	Max	-101	1839.33	19	-2747.77	1	1139.45	17	-1123.52	9	-1759.01	9	-426.65	5	-10915.20	9	25510.70	19
401	Max	-96	1839.33	19	-2747.77	1	1139.45	17	-1123.52	9	-1759.01	9	-426.65	5	-10915.20	9	25510.70	19
401	Max	-119	1839.33	19	-2747.77	1	1139.45	17	-1123.52	9	-1759.01	9	-426.65	5	-10915.20	9	25510.70	19
401	Min.	-126	48.29	13	-7259.93	17	-2387.83	19	-2620.76	19	-4832.42	19	-1169.84	18	-27131.10	19	10322.20	9
401	Min.	-101	48.29	13	-7259.93	17	-2387.83	19	-2620.76	19	-4832.42	19	-1169.84	18	-27131.10	19	10322.20	9
401	Min.	-96	48.29	13	-7259.93	17	-2387.83	19	-2620.76	19	-4832.42	19	-1169.84	18	-27131.10	19	10322.20	9
401	Min.	-119	48.29	13	-7259.93	17	-2387.83	19	-2620.76	19	-4832.42	19	-1169.84	18	-27131.10	19	10322.20	9
401	Max	-101	-2398.07	1	61.35	13	3311.91	19	7046.75	17	2954.69	19	289.59	9	2327.08	19	14080.90	19
401	Max	-98	-2398.07	1	61.35	13	3311.91	19	7046.75	17	2954.69	19	289.59	9	2327.08	19	14080.90	19
401	Max	-66	-2398.07	1	61.35	13	3311.91	19	7046.75	17	2954.69	19	289.59	9	2327.08	19	14080.90	19
401	Max	-74	-2398.07	1	61.35	13	3311.91	19	7046.75	17	2954.69	19	289.59	9	2327.08	19	14080.90	19
401	Min.	-101	-6215.89	17	-1688.29	19	-134.59	13	1290.34	9	818.71	9	2.86	1	-60.27	13	4007.89	9
401	Min.	-98	-6215.89	17	-1688.29	19	-134.59	13	1290.34	9	818.71	9	2.86	1	-60.27	13	4007.89	9
401	Min.	-66	-6215.89	17	-1688.29	19	-134.59	13	1290.34	9	818.71	9	2.86	1	-60.27	13	4007.89	9
401	Min.	-74	-6215.89	17	-1688.29	19	-134.59	13	1290.34	9	818.71	9	2.86	1	-60.27	13	4007.89	9
401	Max	-101	19.87	9	-1225.34	9	-26.23	13	4856.24	19	-524.04	9	485.75	19	-81.94	9	473.66	19
401	Max	-74	19.87	9	-1225.34	9	-26.23	13	4856.24	19	-524.04	9	485.75	19	-81.94	9	473.66	19
401	Max	-69	19.87	9	-1225.34	9	-26.23	13	4856.24	19	-524.04	9	485.75	19	-81.94	9	473.66	19
401	Max	-96	19.87	9	-1225.34	9	-26.23	13	4856.24	19	-524.04	9	485.75	19	-81.94	9	473.66	19
401	Min.	-101	-507.52	19	-3120.64	17	-2286.09	19	1828.07	9	-2648.48	19	-87.06	13	-3256.96	17	22.93	13
401	Min.	-74	-507.52	19	-3120.64	17	-2286.09	19	1828.07	9	-2648.48	19	-87.06	13	-3256.96	17	22.93	13
401	Min.	-69	-507.52	19	-3120.64	17	-2286.09	19	1828.07	9	-2648.48	19	-87.06	13	-3256.96	17	22.93	13
401	Min.	-96	-507.52	19	-3120.64	17	-2286.09	19	1828.07	9	-2648.48	19	-87.06	13	-3256.96	17	22.93	13
401	Max	-74	-1834.34	21	24.47	13	4934.73	19	7112.54	19	3261.53	19	-419.65	9	-1813.77	9	12194.40	19
401	Max	-66	-1834.34	21	24.47	13	4934.73	19	7112.54	19	3261.53	19	-419.65	9	-1813.77	9	12194.40	19
401	Max	-49	-1834.34	21	24.47	13	4934.73	19	7112.54	19	3261.53	19	-419.65	9	-1813.77	9	12194.40	19
401	Max	-44	-1834.34	21	24.47	13	4934.73	19	7112.54	19	3261.53	19	-419.65	9	-1813.77	9	12194.40	19
401	Min.	-74	-4263.33	17	-2268.00	19	1310.10	9	1671.30	9	628.16	13	-1961.68	19	-5184.77	19	2726.90	9
401	Min.	-66	-4263.33	17	-2268.00	19	1310.10	9	1671.30	9	628.16	13	-1961.68	19	-5184.77	19	2726.90	9
401	Min.	-49	-4263.33	17	-2268.00	19	1310.10	9	1671.30	9	628.16	13	-1961.68	19	-5184.77	19	2726.90	9
401	Min.	-44	-4263.33	17	-2268.00	19	1310.10	9	1671.30	9	628.16	13	-1961.68	19	-5184.77	19	2726.90	9
401	Max	-74	257.83	13	-2006.70	9	-820.87	13	-791.18	5	-950.29	9	937.23	18	-7938.09	9	-8513.93	9
401	Max	-44	257.83	13	-2006.70	9	-820.87	13	-791.18	5	-950.29	9	937.23	18	-7938.09	9	-8513.93	9
401	Max	-36	257.83	13	-2006.70	9	-820.87	13	-791.18	5	-950.29	9	937.23	18	-7938.09	9	-8513.93	9
401	Max	-69	257.83	13	-2006.70	9	-820.87	13	-791.18	5	-950.29	9	937.23	18	-7938.09	9	-8513.93	9
401	Min.	-74	-1688.73	19	-5002.78	17	-4699.86	19	-1880.64	18	-3828.94	19	159.71	5	-22606.90	19	-22006.10	19
401	Min.	-44	-1688.73	19	-5002.78	17	-4699.86	19	-1880.64	18	-3828.94	19	159.71	5	-22606.90	19	-22006.10	19
401	Min.	-36	-1688.73	19	-5002.78	17	-4699.86	19	-1880.64	18	-3828.94	19	159.71	5	-22606.90	19	-22006.10	19
401	Min.	-69	-1688.73	19	-5002.78	17	-4699.86	19	-1880.64	18	-3828.94	19	159.71	5	-22606.90	19	-22006.10	19
401	Max	-36	-1496.14	9	1895.55	19	1834.20	19	-1112.20	13	-1343.48	5	2671.46	19	11822.40	19	25065.60	19
401	Max	-44	-1496.14	9	1895.55	19	1834.20	19	-1112.20	13	-1343.48	5	2671.46	19	11822.40	19	25065.60	19
401	Max	-20	-1496.14	9	1895.55	19	1834.20	19	-1112.20	13	-1343.48	5	2671.46	19	11822.40	19	25065.60	19
401	Max	-4	-1496.14	9	1895.55	19	1834.20	19	-1112.20	13	-1343.48	5	2671.46	19	11822.40	19	25065.60	19
401	Min.	-36	-3694.15	17	144.83	13	-212.23	13	-3524.54	19	-3238.25	18	1101.55	13	4578.27	13	9195.78	13
401	Min.	-44	-3694.15	17	144.83	13	-212.23	13	-3524.54	19	-3238.25	18	1101.55	13	4578.27	13	9195.78	13
401	Min.	-20	-3694.15	17	144.83	13	-212.23	13	-3524.54	19	-3238.25	18	1101.55	13	4578.27	13	9195.78	13
401	Min.	-4	-3694.15	17	144.83	13	-212.23	13	-3524.54	19	-3238.25	18	1101.55	13	4578.27	13	9195.78	13
401	Max	-44	-792.33	21	62.33	13	3461.13	19	6612.05	19	-407.43	5	1498.12	19	-1936.04	13	9413.13	19
401	Max	-49	-792.33	21	62.33	13	3461.13	19	6612.05	19	-407.43	5	1498.12	19	-1936.04	13	9413.13	19
401	Max	-26	-792.33	21	62.33	13	3461.13	19	6612.05	19	-407.43	5	1498.12	19	-1936.04	13	9413.13	19
401	Max	-20	-792.33	21	62.33	13	3461.13	19	6612.05	19	-407.43	5	1498.12	19	-1936.04	13	9413.13	19
401	Min.	-44	-2072.48	17	-2788.47	19	772.37	13	2025.64	9	-1102.16	18	-3.27	9	-8651.97	19	2420.14	13
401	Min.	-49	-2072.48	17	-2788.47	19	772.37	13	2025.64	9	-1102.16	18	-3.27	9	-8651.97	19	2420.14	13
401	Min.	-26	-2072.48	17	-2788.47	19	772.37	13	2025.64	9	-1102.16	18	-3.27	9	-8651.97	19	2420.14	13
401	Min.	-20	-2072.48	17	-2788.47	19	772.37	13	2025.64	9	-1102.16	18	-3.27	9	-8651.97	19	2420.14	13
401	Max	-20	1835.22	19	-22.57	13	1477.44	19	1922.12	19	-286.83	1	2430.17	19	2801.08	18	3340.23	19
401	Max	-26	1835.22	19	-22.57	13	1477.44	19	1922.12	19	-286.83	1	2430.17	19	2801.08	18	3340.23	19
401	Max	-3	1835.22	19	-22.57	13	1477.44	19	1922.12	19	-286.83	1	2430.17	19	2801.08	18	3340.23	19
401	Max	-4	1835.22	19	-22.57	13	1477.44	19	1922.12	19	-286.83	1	2430.17	19	2801.08	18	3340.23	19
401	Min.	-20	84.07	13	-604.65	19	-24.03	13	371.61	13	-734.72	18	841.86	13	1280.06	5	1060.11	13
401	Min.	-26	84.07	13	-604.65	19	-24.03	13	371.61	13	-734.72	18	841.86	13	1280.06	5	1060.11	13
401	Min.	-3	84.07	13	-604.65	19	-24.03	13	371.61	13	-734.72	18	841.86	13	1280.06	5	1060.11	13

401	Min.	-4	84.07	13	-604.65	19	-24.03	13	371.61	13	-734.72	18	841.86	13	1280.06	5	1060.11	13
401	Max	-37	-75.91	13	-291.58	13	-162.33	9	-323.27	9	-1263.38	1	-135.16	9	13815.70	18	15270.20	18
401	Max	-84	-75.91	13	-291.58	13	-162.33	9	-323.27	9	-1263.38	1	-135.16	9	13815.70	18	15270.20	18
401	Max	-72	-75.91	13	-291.58	13	-162.33	9	-323.27	9	-1263.38	1	-135.16	9	13815.70	18	15270.20	18
401	Max	-33	-75.91	13	-291.58	13	-162.33	9	-323.27	9	-1263.38	1	-135.16	9	13815.70	18	15270.20	18
401	Min.	-37	-736.95	18	-653.30	17	-639.97	19	-790.73	19	-3153.48	18	-545.35	19	6033.55	5	6169.22	1
401	Min.	-84	-736.95	18	-653.30	17	-639.97	19	-790.73	19	-3153.48	18	-545.35	19	6033.55	5	6169.22	1
401	Min.	-72	-736.95	18	-653.30	17	-639.97	19	-790.73	19	-3153.48	18	-545.35	19	6033.55	5	6169.22	1
401	Min.	-33	-736.95	18	-653.30	17	-639.97	19	-790.73	19	-3153.48	18	-545.35	19	6033.55	5	6169.22	1
401	Max	-37	-239.12	13	423.81	18	80.46	18	-2231.98	1	-1126.90	5	463.86	18	13713.30	18	11492.70	18
401	Max	-33	-239.12	13	423.81	18	80.46	18	-2231.98	1	-1126.90	5	463.86	18	13713.30	18	11492.70	18
401	Max	-7	-239.12	13	423.81	18	80.46	18	-2231.98	1	-1126.90	5	463.86	18	13713.30	18	11492.70	18
401	Max	-8	-239.12	13	423.81	18	80.46	18	-2231.98	1	-1126.90	5	463.86	18	13713.30	18	11492.70	18
401	Min.	-37	-957.76	18	9.83	13	-46.26	1	-5356.16	18	-2665.50	19	133.54	9	5674.69	1	5019.29	1
401	Min.	-33	-957.76	18	9.83	13	-46.26	1	-5356.16	18	-2665.50	19	133.54	9	5674.69	1	5019.29	1
401	Min.	-7	-957.76	18	9.83	13	-46.26	1	-5356.16	18	-2665.50	19	133.54	9	5674.69	1	5019.29	1
401	Min.	-8	-957.76	18	9.83	13	-46.26	1	-5356.16	18	-2665.50	19	133.54	9	5674.69	1	5019.29	1
401	Max	-33	-19.88	13	-292.63	13	-156.15	9	442.61	18	4246.01	19	1303.02	18	4190.73	18	1122.38	19
401	Max	-72	-19.88	13	-292.63	13	-156.15	9	442.61	18	4246.01	19	1303.02	18	4190.73	18	1122.38	19
401	Max	-61	-19.88	13	-292.63	13	-156.15	9	442.61	18	4246.01	19	1303.02	18	4190.73	18	1122.38	19
401	Max	-30	-19.88	13	-292.63	13	-156.15	9	442.61	18	4246.01	19	1303.02	18	4190.73	18	1122.38	19
401	Min.	-33	-213.84	19	-696.90	19	-463.02	17	188.32	13	1761.26	1	492.85	1	1806.70	1	397.00	1
401	Min.	-72	-213.84	19	-696.90	19	-463.02	17	188.32	13	1761.26	1	492.85	1	1806.70	1	397.00	1
401	Min.	-61	-213.84	19	-696.90	19	-463.02	17	188.32	13	1761.26	1	492.85	1	1806.70	1	397.00	1
401	Min.	-30	-213.84	19	-696.90	19	-463.02	17	188.32	13	1761.26	1	492.85	1	1806.70	1	397.00	1
401	Max	-33	-171.46	13	98.13	17	259.81	18	4085.45	19	-111.99	1	794.62	19	-161.50	1	6169.08	18
401	Max	-30	-171.46	13	98.13	17	259.81	18	4085.45	19	-111.99	1	794.62	19	-161.50	1	6169.08	18
401	Max	-6	-171.46	13	98.13	17	259.81	18	4085.45	19	-111.99	1	794.62	19	-161.50	1	6169.08	18
401	Max	-7	-171.46	13	98.13	17	259.81	18	4085.45	19	-111.99	1	794.62	19	-161.50	1	6169.08	18
401	Min.	-33	-613.87	18	-40.65	18	52.48	13	1734.18	1	-334.01	18	330.94	9	-633.96	18	2629.31	1
401	Min.	-30	-613.87	18	-40.65	18	52.48	13	1734.18	1	-334.01	18	330.94	9	-633.96	18	2629.31	1
401	Min.	-6	-613.87	18	-40.65	18	52.48	13	1734.18	1	-334.01	18	330.94	9	-633.96	18	2629.31	1
401	Min.	-7	-613.87	18	-40.65	18	52.48	13	1734.18	1	-334.01	18	330.94	9	-633.96	18	2629.31	1
401	Max	-59	-59.41	21	127.69	13	1582.27	17	-1774.96	13	-1143.05	9	823.02	19	-8602.13	9	-7679.39	9
401	Max	-69	-59.41	21	127.69	13	1582.27	17	-1774.96	13	-1143.05	9	823.02	19	-8602.13	9	-7679.39	9
401	Max	-36	-59.41	21	127.69	13	1582.27	17	-1774.96	13	-1143.05	9	823.02	19	-8602.13	9	-7679.39	9
401	Max	-29	-59.41	21	127.69	13	1582.27	17	-1774.96	13	-1143.05	9	823.02	19	-8602.13	9	-7679.39	9
401	Min.	-59	-360.71	17	-1576.29	19	583.77	9	-4275.41	19	-2666.55	19	272.37	13	-21520.60	19	-17617.70	19
401	Min.	-69	-360.71	17	-1576.29	19	583.77	9	-4275.41	19	-2666.55	19	272.37	13	-21520.60	19	-17617.70	19
401	Min.	-36	-360.71	17	-1576.29	19	583.77	9	-4275.41	19	-2666.55	19	272.37	13	-21520.60	19	-17617.70	19
401	Min.	-29	-360.71	17	-1576.29	19	583.77	9	-4275.41	19	-2666.55	19	272.37	13	-21520.60	19	-17617.70	19
401	Max	-59	28.67	17	-287.45	13	-154.15	9	131.60	17	4446.99	18	-517.38	9	4677.59	19	-192.02	5
401	Max	-29	28.67	17	-287.45	13	-154.15	9	131.60	17	4446.99	18	-517.38	9	4677.59	19	-192.02	5
401	Max	-30	28.67	17	-287.45	13	-154.15	9	131.60	17	4446.99	18	-517.38	9	4677.59	19	-192.02	5
401	Max	-61	28.67	17	-287.45	13	-154.15	9	131.60	17	4446.99	18	-517.38	9	4677.59	19	-192.02	5
401	Min.	-59	-57.70	18	-722.27	18	-454.61	17	33.01	9	1846.63	5	-1306.18	19	2006.23	9	-639.49	18
401	Min.	-29	-57.70	18	-722.27	18	-454.61	17	33.01	9	1846.63	5	-1306.18	19	2006.23	9	-639.49	18
401	Min.	-30	-57.70	18	-722.27	18	-454.61	17	33.01	9	1846.63	5	-1306.18	19	2006.23	9	-639.49	18
401	Min.	-61	-57.70	18	-722.27	18	-454.61	17	33.01	9	1846.63	5	-1306.18	19	2006.23	9	-639.49	18
401	Max	-29	153.50	9	1077.20	19	-157.32	13	-1901.07	13	-1300.27	1	-399.55	13	12464.60	19	-6886.16	9
401	Max	-36	153.50	9	1077.20	19	-157.32	13	-1901.07	13	-1300.27	1	-399.55	13	12464.60	19	-6886.16	9
401	Max	-4	153.50	9	1077.20	19	-157.32	13	-1901.07	13	-1300.27	1	-399.55	13	12464.60	19	-6886.16	9
401	Max	-5	153.50	9	1077.20	19	-157.32	13	-1901.07	13	-1300.27	1	-399.55	13	12464.60	19	-6886.16	9
401	Min.	-29	-213.21	18	12.08	13	-798.51	19	-4616.17	19	-3069.83	19	-1141.04	19	5123.59	9	-16043.20	19
401	Min.	-36	-213.21	18	12.08	13	-798.51	19	-4616.17	19	-3069.83	19	-1141.04	19	5123.59	9	-16043.20	19
401	Min.	-4	-213.21	18	12.08	13	-798.51	19	-4616.17	19	-3069.83	19	-1141.04	19	5123.59	9	-16043.20	19
401	Min.	-5	-213.21	18	12.08	13	-798.51	19	-4616.17	19	-3069.83	19	-1141.04	19	5123.59	9	-16043.20	19
401	Max	-29	-122.89	13	-50.83	13	9.43	18	-119.58	9	5066.01	18	20.31	9	5118.75	19	-781.56	9
401	Max	-5	-122.89	13	-50.83	13	9.43	18	-119.58	9	5066.01	18	20.31	9	5118.75	19	-781.56	9
401	Max	-6	-122.89	13	-50.83	13	9.43	18	-119.58	9	5066.01	18	20.31	9	5118.75	19	-781.56	9
401	Max	-30	-122.89	13	-50.83	13	9.43	18	-119.58	9	5066.01	18	20.31	9	5118.75	19	-781.56	9
401	Min.	-29	-764.53	19	-333.73	18	-75.01	17	-332.35	19	2165.48	1	-58.84	1	2185.81	9	-2054.39	19
401	Min.	-5	-764.53	19	-333.73	18	-75.01	17	-332.35	19	2165.48	1	-58.84	1	2185.81	9	-2054.39	19
401	Min.	-6	-764.53	19	-333.73	18	-75.01	17	-332.35	19	2165.48	1	-58.84	1	2185.81	9	-2054.39	19
401	Min.	-30	-764.53	19	-333.73	18	-75.01	17	-332.35	19	2165.48	1	-58.84	1	2185.81	9	-2054.39	19
401	Max	-92	152.71	17	-271.72	21	105.36	17	500.03	19	3771.13	19	435.12	19	-241.72	9	-924.38	9
401	Max	-109	152.71	17	-271.72	21	105.36	17	500.03	19	3771.13	19	435.12	19	-241.72	9	-924.38	9
401	Max	-107	152.71	17	-271.72	21	105.36	17	500.03	19	3771.13	19	435.12	19	-241.72	9	-924.38	9
401	Max	-90	152.71	17	-271.72	21	105.36	17	500.03	19	3771.13	19	435.12	19	-241.72	9	-924.38	9
401	Min.	-92	-210.19	19	-715.13	17	2.71	21	182.75	13	1543.46	5	156.46	9	-689.92	19	-2183.59	19
401	Min.	-109	-210.19	19	-715.13	17	2.71	21	182.75	13	1543.46	5	156.46	9	-689.92	19	-2183.59	19
401	Min.	-107	-210.19	19	-715.13	17	2.71	21	182.75	13	1543.46	5	156.46	9	-689.92	19	-2183.59	19
401	Min.	-90	-210.19	19	-715.13	17	2.71	21	182.75	13	1543.46	5	156.46	9	-689.92	19	-2183.59	19
401	Max	-92	-459.05	9	35.21	13	434.83	19	3522.18	19	1247.24	18	-89.87	1	-458.39	1	2821.91	18
401	Max	-90	-459.05	9	35.21	13	434.83	19	3522.18	19	1247.24	18	-89.87	1	-458.39	1	2821.91	18
401	Max	-61	-459.05	9	35.21	13	434.83	19	3522.18	19	1247.24	18	-89.87	1	-458.39	1	2821.91	18
401	Max	-72	-459.05	9	35.21	13	434.83	19	3522.18	19	1247.24	18	-89.87	1	-458.39	1	2821.91	18
401	Min.	-92	-1018.55	17	-235.01	19	145.99	9	1400.72	1	525.30	9	-301.74	18	-1287.93	18	1160.97	1
401	Min.	-90	-1018.55	17	-235.01	19	145.99	9	1400.72	1	525.30	9	-301.74	18	-1287.93	18	1160.97	1
401	Min.	-61	-1018.55	17	-235.01	19	145.99	9	1400.72	1	525.30	9	-301.74	18	-1287.93	18	1160.97	1
401	Min.	-72	-1018.55	17	-235.01	19	145.99	9	1400.72	1	525.30	9	-301.74	18	-1287.93	18	1160.97	1
401	Max	-69	-1089.28	9	651.45	17	449.89	19	-133.51	13	4691.17	19	8.24	13	2807.78	19	2375.31	18
401	Max	-59	-1089.28	9	651.45	17	449.89	19	-133.51	13	4691.17	19	8.24	13	2807.78	19	2375.31	18
401	Max	-88	-1089.28	9	651.45	17	449.89	19	-133.51	13	4691.17	19	8.24	13	2807.78	19	2375.31	18
401	Max	-96	-1089.28	9	651.45	17	449.89	19	-133.51	13	4691.17	19	8.24	13	2807.78	19	2375.31	18
401	Min.	-69	-2715.03	17	235.88	20	43.75	9	-786.26	19	1855.19	9	-236.57	19	1176.67	9	609.65	1
401	Min.	-59	-2715.03	17	235.88	20	43.75	9	-786.26	19	1855.19	9	-236.57	19	1176.67	9	609.65	1
401	Min.	-88	-2715.03	17	235.88	20	43.75	9	-786.26	19	1855.19	9	-236.57	19	1176.67	9	609.65	1
401	Min.	-96	-2715.03	17	235.88	20	43.75	9	-786.26	19	1855.19	9	-236.57	19	1176.67	9	609.65	1
401	Max	-59	-503.48	9	166.97	17	677.71	17	3115.15	18	1242.87	19	273.15	17	2098.84	19	3839.09	19
401	Max	-61	-503.48	9	166.97	17	677.71	17	3115.15	18	1242.87	19	273.15	17	2098.84	19	3839.09	19
401	Max	-90	-503.48	9	166.97	17	677.71	17	3115.15	18	1242.87	19	273.15	17	2098.84	19	3839.09	19
401	Max	-88	-503.48	9	166.97	17	677.71	17	3115.15	18	1242.87	19	273.15	17	2098.84	19	3839.09	19
401	Min.	-59	-1170.73	17	-211.63	19	251.76	9	1207.54	5	480.67	9	88.85	9	794.45	9	1621.59	13
401	Min.	-61	-1170.73	17	-211.63	19	251.76	9	1207.54	5	480.67	9	88.85	9	794.45	9	1621.59	13
401	Min.	-90	-1170.73	17	-211.63	19	251.76	9	1207.54	5	480.67	9	88.85	9	794.45	9	1621.59	13
401	Min.	-88	-1170.73	17	-211.63	19	251.76	9	1207.54	5	480.67	9	88.85	9	794.45	9	1621.59	13
401	Max	-88	-972.93	1	543.42	17	167.36	19	1324.03	18	2084.12	19	-318.68	9	-960.42	1	2414.74	19
401	Max	-90	-972.93	1	543.42	17	167.36	19	1324.03	18	2084.12	19	-318.68	9	-960.42	1	2414.74	19
401	Max	-107	-972.93	1	543.42	17	167.36	19	1324.03	18	2084.12	19	-318.68	9	-960.42	1	2414.74	19
401	Max	-96	-972.93	1	543.42	17	167.36	19	1324.03	18	2084.12	19	-318.68	9	-960.42	1	2414.74	19
401	Min.	-88	-2418.46	17	108.76	21	-6.65	13	307.18	5	796.86	9	-846.08	19	-2193.97	19	851.81	9
401	Min.	-90	-2418.46	17	108.76	21	-6.65	13	307.18	5	796.86	9	-846.08	19	-2193.97	19	851.81	9
401	Min.	-107	-2418.46	17	108.76	21	-6.65	13	307.18	5	796.86	9	-846.08	19	-2193.97	19	851.81	9
401	Min.	-96	-2418.46	17	108.76	21	-6.65	13	307.18	5	796.86	9	-846.08	19	-2193.97	19	851.81	9
401	Max	-107	-393.51	1	-36.27	13	672.57	19	6010.57	18	-149.45	5	-74.18	13	2680.16	19	395.93	19
401	Max	-109	-393.51	1	-36.27	13	672.57	19	6010.57	18	-149.45	5	-74.18	13	2680.16	19	395.93	19
401	Max	-130	-393.51	1	-36.27	13	672.57	19	6010.57	18	-149.45	5	-74.18	13	2680.16	19	395.93	19
401	Max	-128	-393.51	1	-36.27	13	672.57	19	6010.57	18	-149.45	5	-74.18	13	2680.16	19	395.93	19

401	Min.	-107	-920.18	17	-838.85	19	141.38	9	2503.72	1	-287.04	17	-334.32	19	1075.02	13	123.19	9
401	Min.	-109	-920.18	17	-838.85	19	141.38	9	2503.72	1	-287.04	17	-334.32	19	1075.02	13	123.19	9
401	Min.	-130	-920.18	17	-838.85	19	141.38	9	2503.72	1	-287.04	17	-334.32	19	1075.02	13	123.19	9
401	Min.	-128	-920.18	17	-838.85	19	141.38	9	2503.72	1	-287.04	17	-334.32	19	1075.02	13	123.19	9
401	Max	-107	845.97	19	417.96	17	1243.34	17	-1014.77	9	-783.80	13	1028.62	19	-8377.34	9	-5628.94	9
401	Max	-128	845.97	19	417.96	17	1243.34	17	-1014.77	9	-783.80	13	1028.62	19	-8377.34	9	-5628.94	9
401	Max	-119	845.97	19	417.96	17	1243.34	17	-1014.77	9	-783.80	13	1028.62	19	-8377.34	9	-5628.94	9
401	Max	-96	845.97	19	417.96	17	1243.34	17	-1014.77	9	-783.80	13	1028.62	19	-8377.34	9	-5628.94	9
401	Min.	-107	26.79	13	103.79	9	462.01	9	-2450.89	19	-1929.44	19	374.84	9	-19511.10	19	-13586.20	19
401	Min.	-128	26.79	13	103.79	9	462.01	9	-2450.89	19	-1929.44	19	374.84	9	-19511.10	19	-13586.20	19
401	Min.	-119	26.79	13	103.79	9	462.01	9	-2450.89	19	-1929.44	19	374.84	9	-19511.10	19	-13586.20	19
401	Min.	-96	26.79	13	103.79	9	462.01	9	-2450.89	19	-1929.44	19	374.84	9	-19511.10	19	-13586.20	19
401	Max	-130	188.07	19	-501.51	9	64.41	9	-864.74	1	-509.55	9	173.72	19	-8122.68	1	7145.09	18
401	Max	-109	188.07	19	-501.51	9	64.41	9	-864.74	1	-509.55	9	173.72	19	-8122.68	1	7145.09	18
401	Max	-111	188.07	19	-501.51	9	64.41	9	-864.74	1	-509.55	9	173.72	19	-8122.68	1	7145.09	18
401	Max	-120	188.07	19	-501.51	9	64.41	9	-864.74	1	-509.55	9	173.72	19	-8122.68	1	7145.09	18
401	Min.	-130	41.06	9	-1472.97	17	-269.99	18	-2174.44	18	-1311.65	18	26.77	1	-18886.20	18	3014.34	1
401	Min.	-109	41.06	9	-1472.97	17	-269.99	18	-2174.44	18	-1311.65	18	26.77	1	-18886.20	18	3014.34	1
401	Min.	-111	41.06	9	-1472.97	17	-269.99	18	-2174.44	18	-1311.65	18	26.77	1	-18886.20	18	3014.34	1
401	Min.	-120	41.06	9	-1472.97	17	-269.99	18	-2174.44	18	-1311.65	18	26.77	1	-18886.20	18	3014.34	1
401	Max	-109	-27.95	13	-418.85	1	-83.29	13	925.05	19	3291.73	19	-253.97	1	-3159.63	1	1182.56	19
401	Max	-92	-27.95	13	-418.85	1	-83.29	13	925.05	19	3291.73	19	-253.97	1	-3159.63	1	1182.56	19
401	Max	-94	-27.95	13	-418.85	1	-83.29	13	925.05	19	3291.73	19	-253.97	1	-3159.63	1	1182.56	19
401	Max	-111	-27.95	13	-418.85	1	-83.29	13	925.05	19	3291.73	19	-253.97	1	-3159.63	1	1182.56	19
401	Min.	-109	-402.01	19	-1001.07	17	-443.17	19	373.03	9	1352.22	1	-771.17	18	-7289.53	18	478.31	1
401	Min.	-92	-402.01	19	-1001.07	17	-443.17	19	373.03	9	1352.22	1	-771.17	18	-7289.53	18	478.31	1
401	Min.	-94	-402.01	19	-1001.07	17	-443.17	19	373.03	9	1352.22	1	-771.17	18	-7289.53	18	478.31	1
401	Min.	-111	-402.01	19	-1001.07	17	-443.17	19	373.03	9	1352.22	1	-771.17	18	-7289.53	18	478.31	1
401	Max	-120	-204.97	20	-90.82	9	810.04	18	-1469.55	1	-3.41	9	2073.01	18	4227.15	18	18012.50	18
401	Max	-111	-204.97	20	-90.82	9	810.04	18	-1469.55	1	-3.41	9	2073.01	18	4227.15	18	18012.50	18
401	Max	-94	-204.97	20	-90.82	9	810.04	18	-1469.55	1	-3.41	9	2073.01	18	4227.15	18	18012.50	18
401	Max	-84	-204.97	20	-90.82	9	810.04	18	-1469.55	1	-3.41	9	2073.01	18	4227.15	18	18012.50	18
401	Min.	-120	-798.58	17	-348.00	19	179.35	13	-3432.35	18	-253.47	18	822.85	9	1377.26	1	7510.91	1
401	Min.	-111	-798.58	17	-348.00	19	179.35	13	-3432.35	18	-253.47	18	822.85	9	1377.26	1	7510.91	1
401	Min.	-94	-798.58	17	-348.00	19	179.35	13	-3432.35	18	-253.47	18	822.85	9	1377.26	1	7510.91	1
401	Min.	-84	-798.58	17	-348.00	19	179.35	13	-3432.35	18	-253.47	18	822.85	9	1377.26	1	7510.91	1
401	Max	-92	-71.48	9	-63.67	1	-47.50	9	1348.90	19	902.60	19	112.10	9	-680.86	1	1591.27	18
401	Max	-72	-71.48	9	-63.67	1	-47.50	9	1348.90	19	902.60	19	112.10	9	-680.86	1	1591.27	18
401	Max	-84	-71.48	9	-63.67	1	-47.50	9	1348.90	19	902.60	19	112.10	9	-680.86	1	1591.27	18
401	Max	-94	-71.48	9	-63.67	1	-47.50	9	1348.90	19	902.60	19	112.10	9	-680.86	1	1591.27	18
401	Min.	-92	-327.42	19	-393.40	17	-257.51	19	538.67	1	125.72	1	-218.09	1	-1700.20	18	576.45	9
401	Min.	-72	-327.42	19	-393.40	17	-257.51	19	538.67	1	125.72	1	-218.09	1	-1700.20	18	576.45	9
401	Min.	-84	-327.42	19	-393.40	17	-257.51	19	538.67	1	125.72	1	-218.09	1	-1700.20	18	576.45	9
401	Min.	-94	-327.42	19	-393.40	17	-257.51	19	538.67	1	125.72	1	-218.09	1	-1700.20	18	576.45	9
401	Max	-192	-95.21	13	552.77	19	-902.59	9	-1294.00	1	-155.48	9	1581.18	17	12540.30	18	5359.83	18
401	Max	-209	-95.21	13	552.77	19	-902.59	9	-1294.00	1	-155.48	9	1581.18	17	12540.30	18	5359.83	18
401	Max	-184	-95.21	13	552.77	19	-902.59	9	-1294.00	1	-155.48	9	1581.18	17	12540.30	18	5359.83	18
401	Max	-172	-95.21	13	552.77	19	-902.59	9	-1294.00	1	-155.48	9	1581.18	17	12540.30	18	5359.83	18
401	Min.	-192	-399.80	19	-1592.47	17	-2736.61	19	-3042.20	19	-932.96	18	897.05	5	4880.04	1	2311.91	1
401	Min.	-209	-399.80	19	-1592.47	17	-2736.61	19	-3042.20	19	-932.96	18	897.05	5	4880.04	1	2311.91	1
401	Min.	-184	-399.80	19	-1592.47	17	-2736.61	19	-3042.20	19	-932.96	18	897.05	5	4880.04	1	2311.91	1
401	Min.	-172	-399.80	19	-1592.47	17	-2736.61	19	-3042.20	19	-932.96	18	897.05	5	4880.04	1	2311.91	1
401	Max	-192	3570.50	19	7516.87	17	8383.50	19	-706.10	9	402.73	9	-41.77	9	12031.70	18	12236.20	18
401	Max	-172	3570.50	19	7516.87	17	8383.50	19	-706.10	9	402.73	9	-41.77	9	12031.70	18	12236.20	18
401	Max	-169	3570.50	19	7516.87	17	8383.50	19	-706.10	9	402.73	9	-41.77	9	12031.70	18	12236.20	18
401	Max	-193	3570.50	19	7516.87	17	8383.50	19	-706.10	9	402.73	9	-41.77	9	12031.70	18	12236.20	18
401	Min.	-192	234.75	13	2686.66	21	959.29	13	-1586.77	18	-2681.58	1	-786.42	17	4884.66	1	5031.29	1
401	Min.	-172	234.75	13	2686.66	21	959.29	13	-1586.77	18	-2681.58	1	-786.42	17	4884.66	1	5031.29	1
401	Min.	-169	234.75	13	2686.66	21	959.29	13	-1586.77	18	-2681.58	1	-786.42	17	4884.66	1	5031.29	1
401	Min.	-193	234.75	13	2686.66	21	959.29	13	-1586.77	18	-2681.58	1	-786.42	17	4884.66	1	5031.29	1
401	Max	-172	3554.97	17	-525.34	1	519.48	17	-857.33	1	3117.86	19	-150.58	5	524.85	18	27.58	1
401	Max	-184	3554.97	17	-525.34	1	519.48	17	-857.33	1	3117.86	19	-150.58	5	524.85	18	27.58	1
401	Max	-144	3554.97	17	-525.34	1	519.48	17	-857.33	1	3117.86	19	-150.58	5	524.85	18	27.58	1
401	Max	-149	3554.97	17	-525.34	1	519.48	17	-857.33	1	3117.86	19	-150.58	5	524.85	18	27.58	1
401	Min.	-172	1371.27	9	-1485.66	17	-579.40	19	-1932.97	19	1188.08	1	-408.33	17	230.60	5	-1681.79	9
401	Min.	-184	1371.27	9	-1485.66	17	-579.40	19	-1932.97	19	1188.08	1	-408.33	17	230.60	5	-1681.79	9
401	Min.	-144	1371.27	9	-1485.66	17	-579.40	19	-1932.97	19	1188.08	1	-408.33	17	230.60	5	-1681.79	9
401	Min.	-149	1371.27	9	-1485.66	17	-579.40	19	-1932.97	19	1188.08	1	-408.33	17	230.60	5	-1681.79	9
401	Max	-172	1639.29	17	3964.82	17	4680.16	19	2655.23	19	2070.41	9	281.76	13	3824.32	9	709.73	19
401	Max	-149	1639.29	17	3964.82	17	4680.16	19	2655.23	19	2070.41	9	281.76	13	3824.32	9	709.73	19
401	Max	-146	1639.29	17	3964.82	17	4680.16	19	2655.23	19	2070.41	9	281.76	13	3824.32	9	709.73	19
401	Max	-169	1639.29	17	3964.82	17	4680.16	19	2655.23	19	2070.41	9	281.76	13	3824.32	9	709.73	19
401	Min.	-172	-290.65	19	1514.70	1	-520.82	13	920.95	1	-1299.41	1	-244.65	19	-312.56	1	-178.83	13
401	Min.	-149	-290.65	19	1514.70	1	-520.82	13	920.95	1	-1299.41	1	-244.65	19	-312.56	1	-178.83	13
401	Min.	-146	-290.65	19	1514.70	1	-520.82	13	920.95	1	-1299.41	1	-244.65	19	-312.56	1	-178.83	13
401	Min.	-169	-290.65	19	1514.70	1	-520.82	13	920.95	1	-1299.41	1	-244.65	19	-312.56	1	-178.83	13
401	Max	-149	-416.76	21	380.76	13	2796.58	17	-661.96	1	-680.34	1	-1080.50	5	-3825.09	9	7201.09	19
401	Max	-144	-416.76	21	380.76	13	2796.58	17	-661.96	1	-680.34	1	-1080.50	5	-3825.09	9	7201.09	19
401	Max	-113	-416.76	21	380.76	13	2796.58	17	-661.96	1	-680.34	1	-1080.50	5	-3825.09	9	7201.09	19
401	Max	-117	-416.76	21	380.76	13	2796.58	17	-661.96	1	-680.34	1	-1080.50	5	-3825.09	9	7201.09	19
401	Min.	-149	-1576.76	17	-2062.30	19	1070.24	1	-1837.34	18	-1719.89	19	-1928.98	18	-11149.50	19	2837.18	9
401	Min.	-144	-1576.76	17	-2062.30	19	1070.24	1	-1837.34	18	-1719.89	19	-1928.98	18	-11149.50	19	2837.18	9
401	Min.	-113	-1576.76	17	-2062.30	19	1070.24	1	-1837.34	18	-1719.89	19	-1928.98	18	-11149.50	19	2837.18	9
401	Min.	-117	-1576.76	17	-2062.30	19	1070.24	1	-1837.34	18	-1719.89	19	-1928.98	18	-11149.50	19	2837.18	9
401	Max	-149	1536.56	17	7322.02	17	1846.28	19	-663.77	1	361.64	9	785.65	17	14804.40	19	-5046.84	1
401	Max	-117	1536.56	17	7322.02	17	1846.28	19	-663.77	1	361.64	9	785.65	17	14804.40	19	-5046.84	1
401	Max	-118	1536.56	17	7322.02	17	1846.28	19	-663.77	1	361.64	9	785.65	17	14804.40	19	-5046.84	1
401	Max	-146	1536.56	17	7322.02	17	1846.28	19	-663.77	1	361.64	9	785.65	17	14804.40	19	-5046.84	1
401	Min.	-149	-3715.36	19	2707.36	9	-3421.93	17	-1408.33	18	-2678.92	1	-1.75	1	4571.63	9	-12369.10	19
401	Min.	-117	-3715.36	19	2707.36	9	-3421.93	17	-1408.33	18	-2678.92	1	-1.75	1	4571.63	9	-12369.10	19
401	Min.	-118	-3715.36	19	2707.36	9	-3421.93	17	-1408.33	18	-2678.92	1	-1.75	1	4571.63	9	-12369.10	19
401	Min.	-146	-3715.36	19	2707.36	9	-3421.93	17	-1408.33	18	-2678.92	1	-1.75	1	4571.63	9	-12369.10	19
401	Max	-80	31.24	13	703.57	17	-594.93	21	-35.42	1	-901.97	9	1607.78	19	-1343.44	1	-2923.08	9
401	Max	-42	31.24	13	703.57	17	-594.93	21	-35.42	1	-901.97	9	1607.78	19	-1343.44	1	-2923.08	9
401	Max	-35	31.24	13	703.57	17	-594.93	21	-35.42	1	-901.97	9	1607.78	19	-1343.44	1	-2923.08	9
401	Max	-83	31.24	13	703.57	17	-594.93	21	-35.42	1	-901.97	9	1607.78	19	-1343.44	1	-2923.08	9
401	Min.	-80	-1815.88	19	269.03	9	-1794.83	17	-178.73	9	-2213.12	19	656.49	13	-3611.37	18	-9851.10	19
401	Min.	-42	-1815.88	19	269.03	9	-1794.83	17	-178.73	9	-2213.12	19	656.49	13	-3611.37	18	-9851.10	19
401	Min.	-35	-1815.88	19	269.03	9	-1794.83	17	-178.73	9	-2213.12	19	656.49	13	-3611.37	18	-9851.10	19
401	Min.	-83	-1815.88	19	269.03	9	-1794.83	17	-178.73	9	-2213.12	19	656.49	13	-3611.37	18	-9851.10	19
401	Max	-80	133.74	17	528.47	19	-978.95	9	-1033.72	13	-110.66	5	1938.84	19	-3040.77	9	-1623.44	1
401	Max	-83	133.74	17	528.47	19	-978.95	9	-1033.72	13	-110.66	5	1938.84	19	-3040.77	9	-1623.44	1
401	Max	-117	133.74	17	528.47	19	-978.95	9	-1033.72	13	-110.66	5	1938.84	19	-3040.77	9	-1623.44	1
401	Max	-113	133.74	17	528.47	19	-978.95	9	-1033.72	13	-110.66	5	1938.84	19	-3040.77	9	-1623.44	1
401	Min.	-80	-156.37	19	-199.56	13	-2477.33	17	-2440.94	19	-250.29	19	683.13	13	-8949.48	19	-3778.92	18
401	Min.	-83	-156.37	19	-199.56	13	-2477.33	17	-2440.94	19	-250.29	19	683.13	13	-8949.48	19	-3778.92	18
401	Min.	-117	-156.37	19	-199.56	13	-2477.33	17	-2440.94	19	-250.29	19	683.13	13	-8949.48	19	-3778.92	18
401	Min.	-113	-156.37	19	-199.56	13	-2477.33	17	-2440.94	19	-250.29	19	683.13	13	-8949.48	19	-3778.92	18
401	Max	-26	1156.44	17	3609.18	17	-153.18	21	-1377.36	9	396.11	1	2140.22	19	-5258.83	13	14640.10	19

401	Max	-49	1156.44	17	3609.18	17	-153.18	21	-1377.36	9	396.11	1	2140.22	19	-5258.83	13	14640.10	19
401	Max	-56	1156.44	17	3609.18	17	-153.18	21	-1377.36	9	396.11	1	2140.22	19	-5258.83	13	14640.10	19
401	Max	-35	1156.44	17	3609.18	17	-153.18	21	-1377.36	9	396.11	1	2140.22	19	-5258.83	13	14640.10	19
401	Min.	-26	-2476.71	19	1548.16	13	-3125.24	17	-3056.61	19	-857.51	9	455.83	9	-19652.50	19	3534.64	13
401	Min.	-49	-2476.71	19	1548.16	13	-3125.24	17	-3056.61	19	-857.51	9	455.83	9	-19652.50	19	3534.64	13
401	Min.	-56	-2476.71	19	1548.16	13	-3125.24	17	-3056.61	19	-857.51	9	455.83	9	-19652.50	19	3534.64	13
401	Min.	-35	-2476.71	19	1548.16	13	-3125.24	17	-3056.61	19	-857.51	9	455.83	9	-19652.50	19	3534.64	13
401	Max	-49	358.33	13	6108.48	17	1557.17	19	2788.07	19	3835.46	19	1002.90	17	-1298.17	13	3512.73	18
401	Max	-66	358.33	13	6108.48	17	1557.17	19	2788.07	19	3835.46	19	1002.90	17	-1298.17	13	3512.73	18
401	Max	-64	358.33	13	6108.48	17	1557.17	19	2788.07	19	3835.46	19	1002.90	17	-1298.17	13	3512.73	18
401	Max	-56	358.33	13	6108.48	17	1557.17	19	2788.07	19	3835.46	19	1002.90	17	-1298.17	13	3512.73	18
401	Min.	-49	-1860.21	19	2564.96	9	-1885.77	17	116.16	13	-1210.26	9	-45.77	9	-11590.90	19	1472.33	9
401	Min.	-66	-1860.21	19	2564.96	9	-1885.77	17	116.16	13	-1210.26	9	-45.77	9	-11590.90	19	1472.33	9
401	Min.	-64	-1860.21	19	2564.96	9	-1885.77	17	116.16	13	-1210.26	9	-45.77	9	-11590.90	19	1472.33	9
401	Min.	-56	-1860.21	19	2564.96	9	-1885.77	17	116.16	13	-1210.26	9	-45.77	9	-11590.90	19	1472.33	9
401	Max	-35	5810.98	17	61.24	19	251.35	13	-1412.65	9	1585.53	19	980.67	19	3735.39	18	20169.60	19
401	Max	-56	5810.98	17	61.24	19	251.35	13	-1412.65	9	1585.53	19	980.67	19	3735.39	18	20169.60	19
401	Max	-64	5810.98	17	61.24	19	251.35	13	-1412.65	9	1585.53	19	980.67	19	3735.39	18	20169.60	19
401	Max	-83	5810.98	17	61.24	19	251.35	13	-1412.65	9	1585.53	19	980.67	19	3735.39	18	20169.60	19
401	Min.	-35	622.65	21	-549.11	17	-3016.37	19	-4605.37	19	379.98	13	35.61	9	1475.66	1	5191.91	9
401	Min.	-56	622.65	21	-549.11	17	-3016.37	19	-4605.37	19	379.98	13	35.61	9	1475.66	1	5191.91	9
401	Min.	-64	622.65	21	-549.11	17	-3016.37	19	-4605.37	19	379.98	13	35.61	9	1475.66	1	5191.91	9
401	Min.	-83	622.65	21	-549.11	17	-3016.37	19	-4605.37	19	379.98	13	35.61	9	1475.66	1	5191.91	9
401	Max	-66	1656.75	17	3896.93	17	2972.67	19	2065.89	19	2535.06	1	460.90	17	1210.08	9	1725.33	18
401	Max	-98	1656.75	17	3896.93	17	2972.67	19	2065.89	19	2535.06	1	460.90	17	1210.08	9	1725.33	18
401	Max	-83	1656.75	17	3896.93	17	2972.67	19	2065.89	19	2535.06	1	460.90	17	1210.08	9	1725.33	18
401	Max	-64	1656.75	17	3896.93	17	2972.67	19	2065.89	19	2535.06	1	460.90	17	1210.08	9	1725.33	18
401	Min.	-66	-643.32	19	1431.28	1	-563.73	13	404.97	13	-1510.02	9	179.54	1	-4778.87	19	854.71	5
401	Min.	-98	-643.32	19	1431.28	1	-563.73	13	404.97	13	-1510.02	9	179.54	1	-4778.87	19	854.71	5
401	Min.	-83	-643.32	19	1431.28	1	-563.73	13	404.97	13	-1510.02	9	179.54	1	-4778.87	19	854.71	5
401	Min.	-64	-643.32	19	1431.28	1	-563.73	13	404.97	13	-1510.02	9	179.54	1	-4778.87	19	854.71	5
401	Max	-98	251.85	5	8883.73	17	5274.00	19	162.28	1	368.57	1	155.26	13	-5063.66	9	-2781.12	13
401	Max	-118	251.85	5	8883.73	17	5274.00	19	162.28	1	368.57	1	155.26	13	-5063.66	9	-2781.12	13
401	Max	-117	251.85	5	8883.73	17	5274.00	19	162.28	1	368.57	1	155.26	13	-5063.66	9	-2781.12	13
401	Max	-83	251.85	5	8883.73	17	5274.00	19	162.28	1	368.57	1	155.26	13	-5063.66	9	-2781.12	13
401	Min.	-98	-220.59	19	3296.10	9	133.91	13	-318.97	9	-2896.58	9	-653.96	19	-17768.90	19	-9089.01	19
401	Min.	-118	-220.59	19	3296.10	9	133.91	13	-318.97	9	-2896.58	9	-653.96	19	-17768.90	19	-9089.01	19
401	Min.	-117	-220.59	19	3296.10	9	133.91	13	-318.97	9	-2896.58	9	-653.96	19	-17768.90	19	-9089.01	19
401	Min.	-83	-220.59	19	3296.10	9	133.91	13	-318.97	9	-2896.58	9	-653.96	19	-17768.90	19	-9089.01	19
401	Max	-35	-0.51	13	386.91	19	-90.46	21	-1012.55	9	-927.81	9	1334.43	19	7344.88	19	3519.51	18
401	Max	-42	-0.51	13	386.91	19	-90.46	21	-1012.55	9	-927.81	9	1334.43	19	7344.88	19	3519.51	18
401	Max	-1	-0.51	13	386.91	19	-90.46	21	-1012.55	9	-927.81	9	1334.43	19	7344.88	19	3519.51	18
401	Max	-2	-0.51	13	386.91	19	-90.46	21	-1012.55	9	-927.81	9	1334.43	19	7344.88	19	3519.51	18
401	Min.	-35	-280.37	19	-38.57	13	-526.84	17	-2776.75	19	-2266.27	19	448.68	13	2938.42	13	1360.86	1
401	Min.	-42	-280.37	19	-38.57	13	-526.84	17	-2776.75	19	-2266.27	19	448.68	13	2938.42	13	1360.86	1
401	Min.	-1	-280.37	19	-38.57	13	-526.84	17	-2776.75	19	-2266.27	19	448.68	13	2938.42	13	1360.86	1
401	Min.	-2	-280.37	19	-38.57	13	-526.84	17	-2776.75	19	-2266.27	19	448.68	13	2938.42	13	1360.86	1
401	Max	-35	1214.93	19	1511.40	17	1976.03	19	-660.06	5	-434.85	1	1378.03	19	10280.00	19	8420.25	19
401	Max	-2	1214.93	19	1511.40	17	1976.03	19	-660.06	5	-434.85	1	1378.03	19	10280.00	19	8420.25	19
401	Max	-3	1214.93	19	1511.40	17	1976.03	19	-660.06	5	-434.85	1	1378.03	19	10280.00	19	8420.25	19
401	Max	-26	1214.93	19	1511.40	17	1976.03	19	-660.06	5	-434.85	1	1378.03	19	10280.00	19	8420.25	19
401	Min.	-35	-44.84	13	638.52	9	85.05	13	-1591.32	18	-1122.95	18	475.90	13	3180.82	13	3301.85	13
401	Min.	-2	-44.84	13	638.52	9	85.05	13	-1591.32	18	-1122.95	18	475.90	13	3180.82	13	3301.85	13
401	Min.	-3	-44.84	13	638.52	9	85.05	13	-1591.32	18	-1122.95	18	475.90	13	3180.82	13	3301.85	13
401	Min.	-26	-44.84	13	638.52	9	85.05	13	-1591.32	18	-1122.95	18	475.90	13	3180.82	13	3301.85	13
401	Max	-195	200.92	17	-469.63	1	19.00	9	-1496.85	9	-1182.33	5	162.74	1	20843.20	19	17967.40	19
401	Max	-217	200.92	17	-469.63	1	19.00	9	-1496.85	9	-1182.33	5	162.74	1	20843.20	19	17967.40	19
401	Max	-223	200.92	17	-469.63	1	19.00	9	-1496.85	9	-1182.33	5	162.74	1	20843.20	19	17967.40	19
401	Max	-188	200.92	17	-469.63	1	19.00	9	-1496.85	9	-1182.33	5	162.74	1	20843.20	19	17967.40	19
401	Min.	-195	-440.21	18	-1263.45	17	-251.81	19	-3556.78	19	-2592.06	19	-111.14	18	8945.08	9	7430.41	9
401	Min.	-217	-440.21	18	-1263.45	17	-251.81	19	-3556.78	19	-2592.06	19	-111.14	18	8945.08	9	7430.41	9
401	Min.	-223	-440.21	18	-1263.45	17	-251.81	19	-3556.78	19	-2592.06	19	-111.14	18	8945.08	9	7430.41	9
401	Min.	-188	-440.21	18	-1263.45	17	-251.81	19	-3556.78	19	-2592.06	19	-111.14	18	8945.08	9	7430.41	9
401	Max	-195	-496.70	1	345.00	18	352.41	18	-675.22	1	-116.30	1	279.48	9	7826.36	19	15630.30	19
401	Max	-188	-496.70	1	345.00	18	352.41	18	-675.22	1	-116.30	1	279.48	9	7826.36	19	15630.30	19
401	Max	-157	-496.70	1	345.00	18	352.41	18	-675.22	1	-116.30	1	279.48	9	7826.36	19	15630.30	19
401	Max	-159	-496.70	1	345.00	18	352.41	18	-675.22	1	-116.30	1	279.48	9	7826.36	19	15630.30	19
401	Min.	-195	-1244.07	17	-52.43	9	-96.25	9	-1529.74	19	-354.54	18	10.24	1	2961.26	9	6675.60	9
401	Min.	-188	-1244.07	17	-52.43	9	-96.25	9	-1529.74	19	-354.54	18	10.24	1	2961.26	9	6675.60	9
401	Min.	-157	-1244.07	17	-52.43	9	-96.25	9	-1529.74	19	-354.54	18	10.24	1	2961.26	9	6675.60	9
401	Min.	-159	-1244.07	17	-52.43	9	-96.25	9	-1529.74	19	-354.54	18	10.24	1	2961.26	9	6675.60	9
401	Max	-188	145.01	18	-423.93	1	321.83	17	-183.76	1	5731.79	18	-1.89	5	-162.15	5	-228.47	1
401	Max	-223	145.01	18	-423.93	1	321.83	17	-183.76	1	5731.79	18	-1.89	5	-162.15	5	-228.47	1
401	Max	-221	145.01	18	-423.93	1	321.83	17	-183.76	1	5731.79	18	-1.89	5	-162.15	5	-228.47	1
401	Max	-186	145.01	18	-423.93	1	321.83	17	-183.76	1	5731.79	18	-1.89	5	-162.15	5	-228.47	1
401	Min.	-188	-44.45	13	-999.25	17	-50.41	19	-330.47	18	2287.88	9	-43.48	13	-303.08	17	-741.25	19
401	Min.	-223	-44.45	13	-999.25	17	-50.41	19	-330.47	18	2287.88	9	-43.48	13	-303.08	17	-741.25	19
401	Min.	-221	-44.45	13	-999.25	17	-50.41	19	-330.47	18	2287.88	9	-43.48	13	-303.08	17	-741.25	19
401	Min.	-186	-44.45	13	-999.25	17	-50.41	19	-330.47	18	2287.88	9	-43.48	13	-303.08	17	-741.25	19
401	Max	-188	-549.84	1	412.06	17	107.53	19	5015.80	18	291.10	18	-118.07	9	184.73	9	-569.98	1
401	Max	-186	-549.84	1	412.06	17	107.53	19	5015.80	18	291.10	18	-118.07	9	184.73	9	-569.98	1
401	Max	-155	-549.84	1	412.06	17	107.53	19	5015.80	18	291.10	18	-118.07	9	184.73	9	-569.98	1
401	Max	-157	-549.84	1	412.06	17	107.53	19	5015.80	18	291.10	18	-118.07	9	184.73	9	-569.98	1
401	Min.	-188	-1316.43	17	32.39	20	-101.28	17	1987.30	9	66.93	9	-317.67	19	-184.32	19	-1260.35	18
401	Min.	-186	-1316.43	17	32.39	20	-101.28	17	1987.30	9	66.93	9	-317.67	19	-184.32	19	-1260.35	18
401	Min.	-155	-1316.43	17	32.39	20	-101.28	17	1987.30	9	66.93	9	-317.67	19	-184.32	19	-1260.35	18
401	Min.	-157	-1316.43	17	32.39	20	-101.28	17	1987.30	9	66.93	9	-317.67	19	-184.32	19	-1260.35	18
401	Max	-217	8.96	1	-191.23	20	286.93	17	2774.92	19	355.33	18	1749.26	19	6944.60	19	7403.34	19
401	Max	-246	8.96	1	-191.23	20	286.93	17	2774.92	19	355.33	18	1749.26	19	6944.60	19	7403.34	19
401	Max	-244	8.96	1	-191.23	20	286.93	17	2774.92	19	355.33	18	1749.26	19	6944.60	19	7403.34	19
401	Max	-223	8.96	1	-191.23	20	286.93	17	2774.92	19	355.33	18	1749.26	19	6944.60	19	7403.34	19
401	Min.	-217	-420.56	18	-613.78	17	40.59	21	1113.89	9	-208.75	9	751.18	9	2995.17	9	3066.92	9
401	Min.	-246	-420.56	18	-613.78	17	40.59	21	1113.89	9	-208.75	9	751.18	9	2995.17	9	3066.92	9
401	Min.	-244	-420.56	18	-613.78	17	40.59	21	1113.89	9	-208.75	9	751.18	9	2995.17	9	3066.92	9
401	Min.	-223	-420.56	18	-613.78	17	40.59	21	1113.89	9	-208.75	9	751.18	9	2995.17	9	3066.92	9
401	Max	-246	41.10	18	-101.73	20	347.11	18	4551.93	19	-629.77	1	-61.33	9	2524.31	18	104.41	17
401	Max	-279	41.10	18	-101.73	20	347.11	18	4551.93	19	-629.77	1	-61.33	9	2524.31	18	104.41	17
401	Max	-267	41.10	18	-101.73	20	347.11	18	4551.93	19	-629.77	1	-61.33	9	2524.31	18	104.41	17
401	Max	-244	41.10	18	-101.73	20	347.11	18	4551.93	19	-629.77	1	-61.33	9	2524.31	18	104.41	17
401	Min.	-246	-17.60	9	-588.79	17	38.43	1	1914.55	9	-1410.72	19	-316.31	19	789.46	9	28.79	20
401	Min.	-279	-17.60	9	-588.79	17	38.43	1	1914.55	9	-1410.72	19	-316.31	19	789.46	9	28.79	20
401	Min.	-267	-17.60	9	-588.79	17	38.43	1	1914.55	9	-1410.72	19	-316.31	19	789.46	9	28.79	20
401	Min.	-244	-17.60	9	-588.79	17	38.43	1	1914.55	9	-1410.72	19	-316.31	19	789.46	9	28.79	20
401	Max	-244	28.89	17	-213.95	20	190.72	17	2447.66	19	1940.69	18	460.22	19	4180.58	19	2151.90	19
401	Max	-267	28.89	17	-213.95	20	190.72	17	2447.66	19	1940.69	18	460.22	19	4180.58	19	2151.90	19
401	Max	-263	28.89	17	-213.95	20	190.72	17	2447.66	19	1940.69	18	460.22	19	4180.58	19	2151.90	19
401	Max	-223	28.89	17	-213.95	20	190.72	17	2447.66	19	1940.69	18	460.22	19	4180.58	19	2151.90	19
401	Min.	-244	-34.14	18	-757.86	17	-59.15	19	1049.16	1	482.06	9	192.03	9	1782.65	9	912.57	9
401	Min.	-267	-34.14	18	-757.86	17	-59.15	19	1049.16	1	482.06	9	192.03	9	1782.65	9	912.57	9

401	Min.	-263	-34.14	18	-757.86	17	-59.15	19	1049.16	1	482.06	9	192.03	9	1782.65	9	912.57	9
401	Min.	-223	-34.14	18	-757.86	17	-59.15	19	1049.16	1	482.06	9	192.03	9	1782.65	9	912.57	9
401	Max	-263	-452.88	1	202.84	19	105.35	19	4461.60	18	1964.82	18	-61.64	9	-901.62	5	1365.11	19
401	Max	-252	-452.88	1	202.84	19	105.35	19	4461.60	18	1964.82	18	-61.64	9	-901.62	5	1365.11	19
401	Max	-221	-452.88	1	202.84	19	105.35	19	4461.60	18	1964.82	18	-61.64	9	-901.62	5	1365.11	19
401	Max	-223	-452.88	1	202.84	19	105.35	19	4461.60	18	1964.82	18	-61.64	9	-901.62	5	1365.11	19
401	Min.	-263	-1086.72	17	64.72	13	-114.95	17	1654.19	13	897.41	5	-244.81	19	-1946.97	18	511.89	9
401	Min.	-252	-1086.72	17	64.72	13	-114.95	17	1654.19	13	897.41	5	-244.81	19	-1946.97	18	511.89	9
401	Min.	-221	-1086.72	17	64.72	13	-114.95	17	1654.19	13	897.41	5	-244.81	19	-1946.97	18	511.89	9
401	Min.	-223	-1086.72	17	64.72	13	-114.95	17	1654.19	13	897.41	5	-244.81	19	-1946.97	18	511.89	9
401	Max	-157	-613.30	9	306.48	18	632.48	19	5603.25	18	917.39	18	132.82	17	2141.19	19	800.59	19
401	Max	-155	-613.30	9	306.48	18	632.48	19	5603.25	18	917.39	18	132.82	17	2141.19	19	800.59	19
401	Max	-128	-613.30	9	306.48	18	632.48	19	5603.25	18	917.39	18	132.82	17	2141.19	19	800.59	19
401	Max	-130	-613.30	9	306.48	18	632.48	19	5603.25	18	917.39	18	132.82	17	2141.19	19	800.59	19
401	Min.	-157	-1505.54	17	36.99	13	123.18	9	2255.93	9	393.56	1	-5.68	19	1025.34	1	325.50	13
401	Min.	-155	-1505.54	17	36.99	13	123.18	9	2255.93	9	393.56	1	-5.68	19	1025.34	1	325.50	13
401	Min.	-128	-1505.54	17	36.99	13	123.18	9	2255.93	9	393.56	1	-5.68	19	1025.34	1	325.50	13
401	Min.	-130	-1505.54	17	36.99	13	123.18	9	2255.93	9	393.56	1	-5.68	19	1025.34	1	325.50	13
401	Max	-157	87.86	13	-487.63	9	-23.42	9	-54.65	5	-646.87	9	41.74	1	-5611.01	1	-4081.98	9
401	Max	-130	87.86	13	-487.63	9	-23.42	9	-54.65	5	-646.87	9	41.74	1	-5611.01	1	-4081.98	9
401	Max	-120	87.86	13	-487.63	9	-23.42	9	-54.65	5	-646.87	9	41.74	1	-5611.01	1	-4081.98	9
401	Max	-159	87.86	13	-487.63	9	-23.42	9	-54.65	5	-646.87	9	41.74	1	-5611.01	1	-4081.98	9
401	Min.	-157	-551.52	18	-1134.48	17	-393.27	19	-118.52	19	-1513.59	19	-284.49	18	-13021.00	18	-10486.70	18
401	Min.	-130	-551.52	18	-1134.48	17	-393.27	19	-118.52	19	-1513.59	19	-284.49	18	-13021.00	18	-10486.70	18
401	Min.	-120	-551.52	18	-1134.48	17	-393.27	19	-118.52	19	-1513.59	19	-284.49	18	-13021.00	18	-10486.70	18
401	Min.	-159	-551.52	18	-1134.48	17	-393.27	19	-118.52	19	-1513.59	19	-284.49	18	-13021.00	18	-10486.70	18
401	Max	-234	-15.67	9	230.84	18	149.97	13	2397.52	1	505.74	1	568.87	18	1264.27	18	3077.83	18
401	Max	-240	-15.67	9	230.84	18	149.97	13	2397.52	1	505.74	1	568.87	18	1264.27	18	3077.83	18
401	Max	-215	-15.67	9	230.84	18	149.97	13	2397.52	1	505.74	1	568.87	18	1264.27	18	3077.83	18
401	Max	-203	-15.67	9	230.84	18	149.97	13	2397.52	1	505.74	1	568.87	18	1264.27	18	3077.83	18
401	Min.	-234	-959.28	18	-293.20	5	-2031.81	18	-580.94	9	-124.71	9	-481.84	9	-1106.22	1	-973.77	1
401	Min.	-240	-959.28	18	-293.20	5	-2031.81	18	-580.94	9	-124.71	9	-481.84	9	-1106.22	1	-973.77	1
401	Min.	-215	-959.28	18	-293.20	5	-2031.81	18	-580.94	9	-124.71	9	-481.84	9	-1106.22	1	-973.77	1
401	Min.	-203	-959.28	18	-293.20	5	-2031.81	18	-580.94	9	-124.71	9	-481.84	9	-1106.22	1	-973.77	1
401	Max	-240	-55.05	9	156.68	18	142.20	13	868.00	1	1105.87	19	1261.79	18	-1506.39	9	-568.96	9
401	Max	-242	-55.05	9	156.68	18	142.20	13	868.00	1	1105.87	19	1261.79	18	-1506.39	9	-568.96	9
401	Max	-213	-55.05	9	156.68	18	142.20	13	868.00	1	1105.87	19	1261.79	18	-1506.39	9	-568.96	9
401	Max	-215	-55.05	9	156.68	18	142.20	13	868.00	1	1105.87	19	1261.79	18	-1506.39	9	-568.96	9
401	Min.	-240	-779.34	18	-112.03	13	-1474.66	18	-493.18	9	483.98	9	330.72	13	-3526.42	19	-3864.82	19
401	Min.	-242	-779.34	18	-112.03	13	-1474.66	18	-493.18	9	483.98	9	330.72	13	-3526.42	19	-3864.82	19
401	Min.	-213	-779.34	18	-112.03	13	-1474.66	18	-493.18	9	483.98	9	330.72	13	-3526.42	19	-3864.82	19
401	Min.	-215	-779.34	18	-112.03	13	-1474.66	18	-493.18	9	483.98	9	330.72	13	-3526.42	19	-3864.82	19
401	Max	-215	-52.52	9	105.20	18	144.11	13	2801.45	19	-14.36	1	1223.05	18	1351.06	18	-635.17	9
401	Max	-213	-52.52	9	105.20	18	144.11	13	2801.45	19	-14.36	1	1223.05	18	1351.06	18	-635.17	9
401	Max	-190	-52.52	9	105.20	18	144.11	13	2801.45	19	-14.36	1	1223.05	18	1351.06	18	-635.17	9
401	Max	-203	-52.52	9	105.20	18	144.11	13	2801.45	19	-14.36	1	1223.05	18	1351.06	18	-635.17	9
401	Min.	-215	-1088.81	18	-155.80	13	-2213.86	18	253.96	9	-413.56	18	147.29	13	15.11	1	-3834.33	19
401	Min.	-213	-1088.81	18	-155.80	13	-2213.86	18	253.96	9	-413.56	18	147.29	13	15.11	1	-3834.33	19
401	Min.	-190	-1088.81	18	-155.80	13	-2213.86	18	253.96	9	-413.56	18	147.29	13	15.11	1	-3834.33	19
401	Min.	-203	-1088.81	18	-155.80	13	-2213.86	18	253.96	9	-413.56	18	147.29	13	15.11	1	-3834.33	19
401	Max	-203	917.38	18	-991.32	13	51.14	9	1326.87	1	-415.88	1	1071.14	1	12299.60	17	-4753.96	1
401	Max	-196	917.38	18	-991.32	13	51.14	9	1326.87	1	-415.88	1	1071.14	1	12299.60	17	-4753.96	1
401	Max	-235	917.38	18	-991.32	13	51.14	9	1326.87	1	-415.88	1	1071.14	1	12299.60	17	-4753.96	1
401	Max	-234	917.38	18	-991.32	13	51.14	9	1326.87	1	-415.88	1	1071.14	1	12299.60	17	-4753.96	1
401	Min.	-203	-71.68	1	-12864.20	18	-633.93	19	-2746.95	9	-1678.07	9	-1805.13	9	5016.01	20	-12965.60	19
401	Min.	-196	-71.68	1	-12864.20	18	-633.93	19	-2746.95	9	-1678.07	9	-1805.13	9	5016.01	20	-12965.60	19
401	Min.	-235	-71.68	1	-12864.20	18	-633.93	19	-2746.95	9	-1678.07	9	-1805.13	9	5016.01	20	-12965.60	19
401	Min.	-234	-71.68	1	-12864.20	18	-633.93	19	-2746.95	9	-1678.07	9	-1805.13	9	5016.01	20	-12965.60	19
401	Max	-240	140.72	9	-141.18	1	18.04	9	1967.52	1	1684.24	17	61.95	1	1553.84	17	1241.76	1
401	Max	-234	140.72	9	-141.18	1	18.04	9	1967.52	1	1684.24	17	61.95	1	1553.84	17	1241.76	1
401	Max	-265	140.72	9	-141.18	1	18.04	9	1967.52	1	1684.24	17	61.95	1	1553.84	17	1241.76	1
401	Max	-273	140.72	9	-141.18	1	18.04	9	1967.52	1	1684.24	17	61.95	1	1553.84	17	1241.76	1
401	Min.	-240	-75.52	1	-827.66	18	-670.51	18	-1249.90	9	616.06	20	-560.94	9	506.82	20	-4618.97	18
401	Min.	-234	-75.52	1	-827.66	18	-670.51	18	-1249.90	9	616.06	20	-560.94	9	506.82	20	-4618.97	18
401	Min.	-265	-75.52	1	-827.66	18	-670.51	18	-1249.90	9	616.06	20	-560.94	9	506.82	20	-4618.97	18
401	Min.	-273	-75.52	1	-827.66	18	-670.51	18	-1249.90	9	616.06	20	-560.94	9	506.82	20	-4618.97	18
401	Max	-240	94.91	18	578.17	18	1045.84	18	2137.16	19	840.46	1	340.02	19	632.96	9	282.71	17
401	Max	-273	94.91	18	578.17	18	1045.84	18	2137.16	19	840.46	1	340.02	19	632.96	9	282.71	17
401	Max	-275	94.91	18	578.17	18	1045.84	18	2137.16	19	840.46	1	340.02	19	632.96	9	282.71	17
401	Max	-242	94.91	18	578.17	18	1045.84	18	2137.16	19	840.46	1	340.02	19	632.96	9	282.71	17
401	Min.	-240	-109.86	13	-252.44	17	-15.45	13	919.84	9	-466.53	9	26.26	1	-1814.60	1	68.40	1
401	Min.	-273	-109.86	13	-252.44	17	-15.45	13	919.84	9	-466.53	9	26.26	1	-1814.60	1	68.40	1
401	Min.	-275	-109.86	13	-252.44	17	-15.45	13	919.84	9	-466.53	9	26.26	1	-1814.60	1	68.40	1
401	Min.	-242	-109.86	13	-252.44	17	-15.45	13	919.84	9	-466.53	9	26.26	1	-1814.60	1	68.40	1
401	Max	-234	128.13	9	1252.93	17	-105.89	9	4472.41	1	3542.63	17	874.16	9	1474.07	9	6224.40	1
401	Max	-235	128.13	9	1252.93	17	-105.89	9	4472.41	1	3542.63	17	874.16	9	1474.07	9	6224.40	1
401	Max	-257	128.13	9	1252.93	17	-105.89	9	4472.41	1	3542.63	17	874.16	9	1474.07	9	6224.40	1
401	Max	-265	128.13	9	1252.93	17	-105.89	9	4472.41	1	3542.63	17	874.16	9	1474.07	9	6224.40	1
401	Min.	-234	-461.87	19	-1128.29	18	-8930.34	18	-4581.41	9	853.77	20	-1335.33	1	-1034.21	18	-7032.92	18
401	Min.	-235	-461.87	19	-1128.29	18	-8930.34	18	-4581.41	9	853.77	20	-1335.33	1	-1034.21	18	-7032.92	18
401	Min.	-257	-461.87	19	-1128.29	18	-8930.34	18	-4581.41	9	853.77	20	-1335.33	1	-1034.21	18	-7032.92	18
401	Min.	-265	-461.87	19	-1128.29	18	-8930.34	18	-4581.41	9	853.77	20	-1335.33	1	-1034.21	18	-7032.92	18
401	Max	-246	39.22	13	18.25	18	830.39	18	2325.48	19	-1437.34	5	161.60	9	1514.82	1	-3587.95	9
401	Max	-217	39.22	13	18.25	18	830.39	18	2325.48	19	-1437.34	5	161.60	9	1514.82	1	-3587.95	9
401	Max	-213	39.22	13	18.25	18	830.39	18	2325.48	19	-1437.34	5	161.60	9	1514.82	1	-3587.95	9
401	Max	-242	39.22	13	18.25	18	830.39	18	2325.48	19	-1437.34	5	161.60	9	1514.82	1	-3587.95	9
401	Min.	-246	-802.00	18	-580.31	17	30.58	13	890.55	9	-3125.53	19	-154.51	18	-34.59	9	-8941.69	19
401	Min.	-217	-802.00	18	-580.31	17	30.58	13	890.55	9	-3125.53	19	-154.51	18	-34.59	9	-8941.69	19
401	Min.	-213	-802.00	18	-580.31	17	30.58	13	890.55	9	-3125.53	19	-154.51	18	-34.59	9	-8941.69	19
401	Min.	-242	-802.00	18	-580.31	17	30.58	13	890.55	9	-3125.53	19	-154.51	18	-34.59	9	-8941.69	19
401	Max	-246	30.57	18	29.38	18	7.23	1	-679.40	1	3854.09	19	202.31	1	-305.09	9	1169.03	1
401	Max	-242	30.57	18	29.38	18	7.23	1	-679.40	1	3854.09	19	202.31	1	-305.09	9	1169.03	1
401	Max	-275	30.57	18	29.38	18	7.23	1	-679.40	1	3854.09	19	202.31	1	-305.09	9	1169.03	1
401	Max	-279	30.57	18	29.38	18	7.23	1	-679.40	1	3854.09	19	202.31	1	-305.09	9	1169.03	1
401	Min.	-246	-413.82	17	-48.21	13	-929.08	18	-1517.07	19	1623.17	9	-56.93	9	-965.05	18	-92.87	9
401	Min.	-242	-413.82	17	-48.21	13	-929.08	18	-1517.07	19	1623.17	9	-56.93	9	-965.05	18	-92.87	9
401	Min.	-275	-413.82	17	-48.21	13	-929.08	18	-1517.07	19	1623.17	9	-56.93	9	-965.05	18	-92.87	9
401	Min.	-279	-413.82	17	-48.21	13	-929.08	18	-1517.07	19	1623.17	9	-56.93	9	-965.05	18	-92.87	9
401	Max	-217	-10.07	13	160.89	9	1321.10	18	-2135.37	9	-1072.87	9	-553.23	5	20475.00	19	-7068.29	9
401	Max	-195	-10.07	13	160.89	9	1321.10	18	-2135.37	9	-1072.87	9	-553.23	5	20475.00	19	-7068.29	9
401	Max	-190	-10.07	13	160.89	9	1321.10	18	-2135.37	9	-1072.87	9	-553.23	5	20475.00	19	-7068.29	9
401	Max	-213	-10.07	13	160.89	9	1321.10	18	-2135.37	9	-1072.87	9	-553.23	5	20475.00	19	-7068.29	9
401	Min.	-217	-581.02	18	-992.84	18	-282.74	17	-5030.52	19	-2503.67	19	-1754.74	18	7105.30	9	-16884.20	19
401	Min.	-195	-581.02	18	-992.84	18	-282.74	17	-5030.52	19	-2503.67	19	-1754.74	18	7105.30	9	-16884.20	19
401	Min.	-190	-581.02	18	-992.84	18	-282.74	17	-5030.52	19	-2503.67	19	-1754.74	18	7105.30	9	-16884.20	19
401	Min.	-213	-581.02	18	-992.84	18	-282.74	17	-5030.52	19	-2503.67	19	-1754.74	18	7105.30	9	-16884.20	19
401	Max	-115	109.48	18	495.20	1	887.51	18	-896.53	13	39.19	9	721.63	1	-3235.66	1	2784.12	19
401	Max	-138	109.48	18	495.20	1	887.51	18	-896.53	13	39.19	9	721.63	1	-3235.66	1	2784.12	19
401	Max	-136	109.48	18	495.20	1	887.51	18	-896.53	13	39.19	9	721.63	1	-3235.66	1	2784.12	19

401	Max	-120	109.48	18	495.20	1	887.51	18	-896.53	13	39.19	9	721.63	1	-3235.66	1	2784.12	19
401	Min.	-115	-370.76	17	-1026.71	18	-301.63	13	-2471.39	18	-300.82	17	-95.29	9	-13210.10	18	1083.74	9
401	Min.	-138	-370.76	17	-1026.71	18	-301.63	13	-2471.39	18	-300.82	17	-95.29	9	-13210.10	18	1083.74	9
401	Min.	-136	-370.76	17	-1026.71	18	-301.63	13	-2471.39	18	-300.82	17	-95.29	9	-13210.10	18	1083.74	9
401	Min.	-120	-370.76	17	-1026.71	18	-301.63	13	-2471.39	18	-300.82	17	-95.29	9	-13210.10	18	1083.74	9
401	Max	-138	-11.96	13	118.38	9	699.60	18	1532.46	19	809.71	1	-380.64	1	228.36	9	675.38	18
401	Max	-163	-11.96	13	118.38	9	699.60	18	1532.46	19	809.71	1	-380.64	1	228.36	9	675.38	18
401	Max	-161	-11.96	13	118.38	9	699.60	18	1532.46	19	809.71	1	-380.64	1	228.36	9	675.38	18
401	Max	-136	-11.96	13	118.38	9	699.60	18	1532.46	19	809.71	1	-380.64	1	228.36	9	675.38	18
401	Min.	-138	-160.02	5	-689.71	18	-152.66	17	382.19	9	-644.23	9	-1174.94	18	-2631.71	1	-53.31	9
401	Min.	-163	-160.02	5	-689.71	18	-152.66	17	382.19	9	-644.23	9	-1174.94	18	-2631.71	1	-53.31	9
401	Min.	-161	-160.02	5	-689.71	18	-152.66	17	382.19	9	-644.23	9	-1174.94	18	-2631.71	1	-53.31	9
401	Min.	-136	-160.02	5	-689.71	18	-152.66	17	382.19	9	-644.23	9	-1174.94	18	-2631.71	1	-53.31	9
401	Max	-136	38.73	13	-46.20	1	644.05	18	190.68	18	-1698.31	1	272.20	1	-593.72	1	13244.20	18
401	Max	-161	38.73	13	-46.20	1	644.05	18	190.68	18	-1698.31	1	272.20	1	-593.72	1	13244.20	18
401	Max	-159	38.73	13	-46.20	1	644.05	18	190.68	18	-1698.31	1	272.20	1	-593.72	1	13244.20	18
401	Max	-120	38.73	13	-46.20	1	644.05	18	190.68	18	-1698.31	1	272.20	1	-593.72	1	13244.20	18
401	Min.	-136	-998.13	18	-551.75	17	-353.94	17	-15.83	1	-4192.34	18	-292.42	9	-4380.24	18	5055.54	9
401	Min.	-161	-998.13	18	-551.75	17	-353.94	17	-15.83	1	-4192.34	18	-292.42	9	-4380.24	18	5055.54	9
401	Min.	-159	-998.13	18	-551.75	17	-353.94	17	-15.83	1	-4192.34	18	-292.42	9	-4380.24	18	5055.54	9
401	Min.	-120	-998.13	18	-551.75	17	-353.94	17	-15.83	1	-4192.34	18	-292.42	9	-4380.24	18	5055.54	9
401	Max	-159	-119.35	9	764.41	18	42.65	1	-1777.90	9	376.44	19	222.63	9	-5311.77	9	4415.45	19
401	Max	-161	-119.35	9	764.41	18	42.65	1	-1777.90	9	376.44	19	222.63	9	-5311.77	9	4415.45	19
401	Max	-180	-119.35	9	764.41	18	42.65	1	-1777.90	9	376.44	19	222.63	9	-5311.77	9	4415.45	19
401	Max	-195	-119.35	9	764.41	18	42.65	1	-1777.90	9	376.44	19	222.63	9	-5311.77	9	4415.45	19
401	Min.	-159	-907.85	18	-95.30	13	-1123.93	18	-4254.55	19	132.95	9	-292.89	1	-13980.50	19	881.49	9
401	Min.	-161	-907.85	18	-95.30	13	-1123.93	18	-4254.55	19	132.95	9	-292.89	1	-13980.50	19	881.49	9
401	Min.	-180	-907.85	18	-95.30	13	-1123.93	18	-4254.55	19	132.95	9	-292.89	1	-13980.50	19	881.49	9
401	Min.	-195	-907.85	18	-95.30	13	-1123.93	18	-4254.55	19	132.95	9	-292.89	1	-13980.50	19	881.49	9
401	Max	-161	66.02	9	-4.56	9	27.38	13	652.28	1	1746.65	18	-344.89	13	97.40	1	3644.99	19
401	Max	-163	66.02	9	-4.56	9	27.38	13	652.28	1	1746.65	18	-344.89	13	97.40	1	3644.99	19
401	Max	-182	66.02	9	-4.56	9	27.38	13	652.28	1	1746.65	18	-344.89	13	97.40	1	3644.99	19
401	Max	-180	66.02	9	-4.56	9	27.38	13	652.28	1	1746.65	18	-344.89	13	97.40	1	3644.99	19
401	Min.	-161	-479.28	1	-1174.47	18	-1438.74	18	-613.53	9	373.08	9	-840.98	19	-778.90	9	214.42	9
401	Min.	-163	-479.28	1	-1174.47	18	-1438.74	18	-613.53	9	373.08	9	-840.98	19	-778.90	9	214.42	9
401	Min.	-182	-479.28	1	-1174.47	18	-1438.74	18	-613.53	9	373.08	9	-840.98	19	-778.90	9	214.42	9
401	Min.	-180	-479.28	1	-1174.47	18	-1438.74	18	-613.53	9	373.08	9	-840.98	19	-778.90	9	214.42	9
401	Max	-180	358.17	9	-51.43	1	31.84	9	-274.57	9	-1274.60	9	-236.83	9	-2119.83	1	15719.50	19
401	Max	-182	358.17	9	-51.43	1	31.84	9	-274.57	9	-1274.60	9	-236.83	9	-2119.83	1	15719.50	19
401	Max	-190	358.17	9	-51.43	1	31.84	9	-274.57	9	-1274.60	9	-236.83	9	-2119.83	1	15719.50	19
401	Max	-195	358.17	9	-51.43	1	31.84	9	-274.57	9	-1274.60	9	-236.83	9	-2119.83	1	15719.50	19
401	Min.	-180	-390.75	1	-217.90	18	-1836.10	18	-749.71	17	-2953.07	19	-754.72	19	-5717.98	18	4875.72	9
401	Min.	-182	-390.75	1	-217.90	18	-1836.10	18	-749.71	17	-2953.07	19	-754.72	19	-5717.98	18	4875.72	9
401	Min.	-190	-390.75	1	-217.90	18	-1836.10	18	-749.71	17	-2953.07	19	-754.72	19	-5717.98	18	4875.72	9
401	Min.	-195	-390.75	1	-217.90	18	-1836.10	18	-749.71	17	-2953.07	19	-754.72	19	-5717.98	18	4875.72	9
401	Max	-147	1129.95	18	498.20	13	-103.48	1	2718.69	9	-484.13	1	1668.77	1	-7739.21	9	7349.72	18
401	Max	-142	1129.95	18	498.20	13	-103.48	1	2718.69	9	-484.13	1	1668.77	1	-7739.21	9	7349.72	18
401	Max	-134	1129.95	18	498.20	13	-103.48	1	2718.69	9	-484.13	1	1668.77	1	-7739.21	9	7349.72	18
401	Max	-121	1129.95	18	498.20	13	-103.48	1	2718.69	9	-484.13	1	1668.77	1	-7739.21	9	7349.72	18
401	Min.	-147	-448.45	9	-10851.70	18	-4052.80	18	-4824.70	1	-1073.79	19	-1761.73	9	-16714.00	18	207.65	9
401	Min.	-142	-448.45	9	-10851.70	18	-4052.80	18	-4824.70	1	-1073.79	19	-1761.73	9	-16714.00	18	207.65	9
401	Min.	-134	-448.45	9	-10851.70	18	-4052.80	18	-4824.70	1	-1073.79	19	-1761.73	9	-16714.00	18	207.65	9
401	Min.	-121	-448.45	9	-10851.70	18	-4052.80	18	-4824.70	1	-1073.79	19	-1761.73	9	-16714.00	18	207.65	9
401	Max	-142	282.24	9	570.89	13	331.80	9	3429.28	1	744.79	18	-293.85	1	-913.65	9	3355.80	1
401	Max	-140	282.24	9	570.89	13	331.80	9	3429.28	1	744.79	18	-293.85	1	-913.65	9	3355.80	1
401	Max	-132	282.24	9	570.89	13	331.80	9	3429.28	1	744.79	18	-293.85	1	-913.65	9	3355.80	1
401	Max	-134	282.24	9	570.89	13	331.80	9	3429.28	1	744.79	18	-293.85	1	-913.65	9	3355.80	1
401	Min.	-142	-1231.97	18	-2134.31	18	-1025.57	18	-2586.72	9	316.18	9	-1260.62	18	-5790.62	18	-1937.35	9
401	Min.	-140	-1231.97	18	-2134.31	18	-1025.57	18	-2586.72	9	316.18	9	-1260.62	18	-5790.62	18	-1937.35	9
401	Min.	-132	-1231.97	18	-2134.31	18	-1025.57	18	-2586.72	9	316.18	9	-1260.62	18	-5790.62	18	-1937.35	9
401	Min.	-134	-1231.97	18	-2134.31	18	-1025.57	18	-2586.72	9	316.18	9	-1260.62	18	-5790.62	18	-1937.35	9
401	Max	-121	304.28	9	-28.03	13	2357.87	18	-274.04	9	721.02	1	1575.02	18	3947.87	18	17573.70	18
401	Max	-134	304.28	9	-28.03	13	2357.87	18	-274.04	9	721.02	1	1575.02	18	3947.87	18	17573.70	18
401	Max	-132	304.28	9	-28.03	13	2357.87	18	-274.04	9	721.02	1	1575.02	18	3947.87	18	17573.70	18
401	Max	-115	304.28	9	-28.03	13	2357.87	18	-274.04	9	721.02	1	1575.02	18	3947.87	18	17573.70	18
401	Min.	-121	-2431.34	18	-2982.60	18	-255.87	1	-2267.71	19	-1835.27	9	816.50	9	540.97	1	6514.19	1
401	Min.	-134	-2431.34	18	-2982.60	18	-255.87	1	-2267.71	19	-1835.27	9	816.50	9	540.97	1	6514.19	1
401	Min.	-132	-2431.34	18	-2982.60	18	-255.87	1	-2267.71	19	-1835.27	9	816.50	9	540.97	1	6514.19	1
401	Min.	-115	-2431.34	18	-2982.60	18	-255.87	1	-2267.71	19	-1835.27	9	816.50	9	540.97	1	6514.19	1
401	Max	-140	161.91	13	-98.41	5	154.79	17	1482.15	1	-224.74	9	-219.40	1	350.16	9	4350.64	18
401	Max	-138	161.91	13	-98.41	5	154.79	17	1482.15	1	-224.74	9	-219.40	1	350.16	9	4350.64	18
401	Max	-115	161.91	13	-98.41	5	154.79	17	1482.15	1	-224.74	9	-219.40	1	350.16	9	4350.64	18
401	Max	-132	161.91	13	-98.41	5	154.79	17	1482.15	1	-224.74	9	-219.40	1	350.16	9	4350.64	18
401	Min.	-140	-1092.49	18	-262.67	17	-59.34	18	-750.33	9	-1115.58	18	-860.37	18	-708.44	1	302.72	1
401	Min.	-138	-1092.49	18	-262.67	17	-59.34	18	-750.33	9	-1115.58	18	-860.37	18	-708.44	1	302.72	1
401	Min.	-115	-1092.49	18	-262.67	17	-59.34	18	-750.33	9	-1115.58	18	-860.37	18	-708.44	1	302.72	1
401	Min.	-132	-1092.49	18	-262.67	17	-59.34	18	-750.33	9	-1115.58	18	-860.37	18	-708.44	1	302.72	1
401	Max	-178	1255.86	17	746.02	9	2214.65	18	2152.21	18	4762.75	1	-77.69	9	5547.89	1	2603.56	19
401	Max	-167	1255.86	17	746.02	9	2214.65	18	2152.21	18	4762.75	1	-77.69	9	5547.89	1	2603.56	19
401	Max	-164	1255.86	17	746.02	9	2214.65	18	2152.21	18	4762.75	1	-77.69	9	5547.89	1	2603.56	19
401	Max	-170	1255.86	17	746.02	9	2214.65	18	2152.21	18	4762.75	1	-77.69	9	5547.89	1	2603.56	19
401	Min.	-178	528.02	20	-873.26	1	-806.71	13	643.00	9	-4718.41	9	-687.84	1	-3443.66	9	1206.21	5
401	Min.	-167	528.02	20	-873.26	1	-806.71	13	643.00	9	-4718.41	9	-687.84	1	-3443.66	9	1206.21	5
401	Min.	-164	528.02	20	-873.26	1	-806.71	13	643.00	9	-4718.41	9	-687.84	1	-3443.66	9	1206.21	5
401	Min.	-170	528.02	20	-873.26	1	-806.71	13	643.00	9	-4718.41	9	-687.84	1	-3443.66	9	1206.21	5
401	Max	-167	183.80	13	685.90	1	1401.04	18	1769.46	18	3621.19	1	330.87	9	3950.88	1	-529.06	9
401	Max	-140	183.80	13	685.90	1	1401.04	18	1769.46	18	3621.19	1	330.87	9	3950.88	1	-529.06	9
401	Max	-142	183.80	13	685.90	1	1401.04	18	1769.46	18	3621.19	1	330.87	9	3950.88	1	-529.06	9
401	Max	-164	183.80	13	685.90	1	1401.04	18	1769.46	18	3621.19	1	330.87	9	3950.88	1	-529.06	9
401	Min.	-167	-2283.98	18	-357.13	9	-373.67	13	743.72	9	-3257.44	9	-34.67	1	-3594.51	9	-2464.92	18
401	Min.	-140	-2283.98	18	-357.13	9	-373.67	13	743.72	9	-3257.44	9	-34.67	1	-3594.51	9	-2464.92	18
401	Min.	-142	-2283.98	18	-357.13	9	-373.67	13	743.72	9	-3257.44	9	-34.67	1	-3594.51	9	-2464.92	18
401	Min.	-164	-2283.98	18	-357.13	9	-373.67	13	743.72	9	-3257.44	9	-34.67	1	-3594.51	9	-2464.92	18
401	Max	-164	3788.59	17	413.50	1	4946.27	18	3677.70	18	6313.62	1	600.08	9	7017.46	1	-385.28	9
401	Max	-142	3788.59	17	413.50	1	4946.27	18	3677.70	18	6313.62	1	600.08	9	7017.46	1	-385.28	9
401	Max	-147	3788.59	17	413.50	1	4946.27	18	3677.70	18	6313.62	1	600.08	9	7017.46	1	-385.28	9
401	Max	-170	3788.59	17	413.50	1	4946.27	18	3677.70	18	6313.62	1	600.08	9	7017.46	1	-385.28	9
401	Min.	-164	1054.08	20	-1393.87	9	-198.17	13	1577.91	9	-6151.57	9	-308.48	1	-4052.34	9	-1998.93	17
401	Min.	-142	1054.08	20	-1393.87	9	-198.17	13	1577.91	9	-6151.57	9	-308.48	1	-4052.34	9	-1998.93	17
401	Min.	-147	1054.08	20	-1393.87	9	-198.17	13	1577.91	9	-6151.57	9	-308.48	1	-4052.34	9	-1998.93	17
401	Min.	-170	1054.08	20	-1393.87	9	-198.17	13	1577.91	9	-6151.57	9	-308.48	1	-4052.34	9	-1998.93	17
401	Max	-170	3779.39	18	55.14	18	1.24	9	-832.12	1	976.38	1	903.42	1	14249.70	19	-5504.61	1
401	Max	-196	3779.39	18	55.14	18	1.24	9	-832.12	1	976.38	1	903.42	1	14249.70	19	-5504.61	1
401	Max	-203	3779.39	18	55.14	18	1.24	9	-832.12	1	976.38	1	903.42	1	14249.70	19	-5504.61	1
401	Max	-178	3779.39	18	55.14	18	1.24	9	-832.12	1	976.38	1	903.42	1	14249.70	19	-5504.61	1
401	Min.	-170	-1914.54	5	-150.69	17	-762.84	1	-2093.13	19	-2257.98	9	-1844.07	9	6459.98	9	-11581.80	19
401	Min.	-196	-1914.54	5	-150.69	17	-762.84	1	-2093.13	19	-2257.98	9	-1844.07	9	6459.98	9	-11581.80	19
401	Min.	-203	-1914.54	5	-150.69	17	-762.84	1	-2093.13	19	-2257.98	9	-1844.07	9	6459.98	9	-11581.80	19
401	Min.	-178	-1914.54	5	-150.69	17	-762.84	1	-2093.13	19	-2257.98	9	-1844.07	9	6459.98	9	-11581.80	19

401	Max	-167	-160.83	9	1122.90	18	254.99	18	1105.37	18	2105.90	1	-233.41	9	2540.31	9	-1301.28	1
401	Max	-178	-160.83	9	1122.90	18	254.99	18	1105.37	18	2105.90	1	-233.41	9	2540.31	9	-1301.28	1
401	Max	-182	-160.83	9	1122.90	18	254.99	18	1105.37	18	2105.90	1	-233.41	9	2540.31	9	-1301.28	1
401	Max	-163	-160.83	9	1122.90	18	254.99	18	1105.37	18	2105.90	1	-233.41	9	2540.31	9	-1301.28	1
401	Min.	-167	-743.69	18	-337.85	1	-32.99	9	212.20	9	-1277.85	9	-459.91	19	-2436.41	1	-3170.26	19
401	Min.	-178	-743.69	18	-337.85	1	-32.99	9	212.20	9	-1277.85	9	-459.91	19	-2436.41	1	-3170.26	19
401	Min.	-182	-743.69	18	-337.85	1	-32.99	9	212.20	9	-1277.85	9	-459.91	19	-2436.41	1	-3170.26	19
401	Min.	-163	-743.69	18	-337.85	1	-32.99	9	212.20	9	-1277.85	9	-459.91	19	-2436.41	1	-3170.26	19
401	Max	-167	552.10	9	10.78	9	224.48	13	2405.15	1	1193.86	19	-76.85	1	-35.73	9	1744.94	9
401	Max	-163	552.10	9	10.78	9	224.48	13	2405.15	1	1193.86	19	-76.85	1	-35.73	9	1744.94	9
401	Max	-138	552.10	9	10.78	9	224.48	13	2405.15	1	1193.86	19	-76.85	1	-35.73	9	1744.94	9
401	Max	-140	552.10	9	10.78	9	224.48	13	2405.15	1	1193.86	19	-76.85	1	-35.73	9	1744.94	9
401	Min.	-167	-676.76	18	-730.95	18	-589.43	18	-1304.64	9	292.31	9	-236.07	17	-1979.64	18	-3637.39	1
401	Min.	-163	-676.76	18	-730.95	18	-589.43	18	-1304.64	9	292.31	9	-236.07	17	-1979.64	18	-3637.39	1
401	Min.	-138	-676.76	18	-730.95	18	-589.43	18	-1304.64	9	292.31	9	-236.07	17	-1979.64	18	-3637.39	1
401	Min.	-140	-676.76	18	-730.95	18	-589.43	18	-1304.64	9	292.31	9	-236.07	17	-1979.64	18	-3637.39	1
401	Max	-178	52.92	9	-44.23	9	2519.59	18	-347.56	1	2788.89	19	141.74	9	1677.70	9	1567.81	1
401	Max	-203	52.92	9	-44.23	9	2519.59	18	-347.56	1	2788.89	19	141.74	9	1677.70	9	1567.81	1
401	Max	-190	52.92	9	-44.23	9	2519.59	18	-347.56	1	2788.89	19	141.74	9	1677.70	9	1567.81	1
401	Max	-182	52.92	9	-44.23	9	2519.59	18	-347.56	1	2788.89	19	141.74	9	1677.70	9	1567.81	1
401	Min.	-178	-2041.75	18	-463.77	17	-35.70	13	-1091.16	19	21.13	9	-304.99	18	-1286.27	1	-777.34	9
401	Min.	-203	-2041.75	18	-463.77	17	-35.70	13	-1091.16	19	21.13	9	-304.99	18	-1286.27	1	-777.34	9
401	Min.	-190	-2041.75	18	-463.77	17	-35.70	13	-1091.16	19	21.13	9	-304.99	18	-1286.27	1	-777.34	9
401	Min.	-182	-2041.75	18	-463.77	17	-35.70	13	-1091.16	19	21.13	9	-304.99	18	-1286.27	1	-777.34	9
401	Max	-194	263.23	19	-664.44	13	5939.96	17	-4685.42	5	-2741.02	5	385.93	13	58609.60	18	11279.90	19
401	Max	-205	263.23	19	-664.44	13	5939.96	17	-4685.42	5	-2741.02	5	385.93	13	58609.60	18	11279.90	19
401	Max	-207	263.23	19	-664.44	13	5939.96	17	-4685.42	5	-2741.02	5	385.93	13	58609.60	18	11279.90	19
401	Max	-201	263.23	19	-664.44	13	5939.96	17	-4685.42	5	-2741.02	5	385.93	13	58609.60	18	11279.90	19
401	Min.	-194	-1548.71	17	-11252.00	19	2306.34	1	-10232.80	18	-5253.45	17	-1137.61	19	27563.20	1	3638.83	9
401	Min.	-205	-1548.71	17	-11252.00	19	2306.34	1	-10232.80	18	-5253.45	17	-1137.61	19	27563.20	1	3638.83	9
401	Min.	-207	-1548.71	17	-11252.00	19	2306.34	1	-10232.80	18	-5253.45	17	-1137.61	19	27563.20	1	3638.83	9
401	Min.	-201	-1548.71	17	-11252.00	19	2306.34	1	-10232.80	18	-5253.45	17	-1137.61	19	27563.20	1	3638.83	9
401	Max	-205	855.90	17	-981.58	21	96.73	13	-103.46	13	-3079.26	5	749.13	19	2615.24	17	20510.60	18
401	Max	-227	855.90	17	-981.58	21	96.73	13	-103.46	13	-3079.26	5	749.13	19	2615.24	17	20510.60	18
401	Max	-231	855.90	17	-981.58	21	96.73	13	-103.46	13	-3079.26	5	749.13	19	2615.24	17	20510.60	18
401	Max	-207	855.90	17	-981.58	21	96.73	13	-103.46	13	-3079.26	5	749.13	19	2615.24	17	20510.60	18
401	Min.	-205	-1590.08	19	-2663.22	17	-1372.75	19	-776.35	19	-6360.30	18	114.81	13	-18.44	19	9595.72	1
401	Min.	-227	-1590.08	19	-2663.22	17	-1372.75	19	-776.35	19	-6360.30	18	114.81	13	-18.44	19	9595.72	1
401	Min.	-231	-1590.08	19	-2663.22	17	-1372.75	19	-776.35	19	-6360.30	18	114.81	13	-18.44	19	9595.72	1
401	Min.	-207	-1590.08	19	-2663.22	17	-1372.75	19	-776.35	19	-6360.30	18	114.81	13	-18.44	19	9595.72	1
401	Max	-207	345.12	17	-2376.24	9	602.63	13	-321.46	13	87.18	1	3215.63	19	17797.60	17	10574.20	18
401	Max	-231	345.12	17	-2376.24	9	602.63	13	-321.46	13	87.18	1	3215.63	19	17797.60	17	10574.20	18
401	Max	-229	345.12	17	-2376.24	9	602.63	13	-321.46	13	87.18	1	3215.63	19	17797.60	17	10574.20	18
401	Max	-201	345.12	17	-2376.24	9	602.63	13	-321.46	13	87.18	1	3215.63	19	17797.60	17	10574.20	18
401	Min.	-207	-464.90	19	-6052.01	17	-5433.73	19	-1332.53	19	-1617.09	18	1307.43	13	8018.34	1	5269.85	5
401	Min.	-231	-464.90	19	-6052.01	17	-5433.73	19	-1332.53	19	-1617.09	18	1307.43	13	8018.34	1	5269.85	5
401	Min.	-229	-464.90	19	-6052.01	17	-5433.73	19	-1332.53	19	-1617.09	18	1307.43	13	8018.34	1	5269.85	5
401	Min.	-201	-464.90	19	-6052.01	17	-5433.73	19	-1332.53	19	-1617.09	18	1307.43	13	8018.34	1	5269.85	5
401	Max	-186	218.62	17	-343.25	13	-115.90	13	-168.28	13	1865.31	19	-833.46	1	-6443.78	1	9386.69	18
401	Max	-221	218.62	17	-343.25	13	-115.90	13	-168.28	13	1865.31	19	-833.46	1	-6443.78	1	9386.69	18
401	Max	-227	218.62	17	-343.25	13	-115.90	13	-168.28	13	1865.31	19	-833.46	1	-6443.78	1	9386.69	18
401	Max	-205	218.62	17	-343.25	13	-115.90	13	-168.28	13	1865.31	19	-833.46	1	-6443.78	1	9386.69	18
401	Min.	-186	-64.50	19	-1147.88	19	-611.07	19	-436.66	19	397.55	13	-1755.44	18	-14538.80	18	4344.46	1
401	Min.	-221	-64.50	19	-1147.88	19	-611.07	19	-436.66	19	397.55	13	-1755.44	18	-14538.80	18	4344.46	1
401	Min.	-227	-64.50	19	-1147.88	19	-611.07	19	-436.66	19	397.55	13	-1755.44	18	-14538.80	18	4344.46	1
401	Min.	-205	-64.50	19	-1147.88	19	-611.07	19	-436.66	19	397.55	13	-1755.44	18	-14538.80	18	4344.46	1
401	Max	-186	3125.76	19	-292.46	21	431.86	17	-1276.71	13	-3436.58	1	-108.22	9	-4137.17	5	-17116.70	1
401	Max	-205	3125.76	19	-292.46	21	431.86	17	-1276.71	13	-3436.58	1	-108.22	9	-4137.17	5	-17116.70	1
401	Max	-194	3125.76	19	-292.46	21	431.86	17	-1276.71	13	-3436.58	1	-108.22	9	-4137.17	5	-17116.70	1
401	Max	-176	3125.76	19	-292.46	21	431.86	17	-1276.71	13	-3436.58	1	-108.22	9	-4137.17	5	-17116.70	1
401	Min.	-186	979.57	9	-1388.03	17	-643.71	19	-3179.43	19	-7352.41	18	-639.08	19	-9556.01	18	-38388.10	18
401	Min.	-205	979.57	9	-1388.03	17	-643.71	19	-3179.43	19	-7352.41	18	-639.08	19	-9556.01	18	-38388.10	18
401	Min.	-194	979.57	9	-1388.03	17	-643.71	19	-3179.43	19	-7352.41	18	-639.08	19	-9556.01	18	-38388.10	18
401	Min.	-176	979.57	9	-1388.03	17	-643.71	19	-3179.43	19	-7352.41	18	-639.08	19	-9556.01	18	-38388.10	18
401	Max	-176	478.95	17	-1283.39	1	558.72	17	2723.18	19	-158.47	19	1134.16	19	4862.20	19	3197.01	18
401	Max	-153	478.95	17	-1283.39	1	558.72	17	2723.18	19	-158.47	19	1134.16	19	4862.20	19	3197.01	18
401	Max	-155	478.95	17	-1283.39	1	558.72	17	2723.18	19	-158.47	19	1134.16	19	4862.20	19	3197.01	18
401	Max	-186	478.95	17	-1283.39	1	558.72	17	2723.18	19	-158.47	19	1134.16	19	4862.20	19	3197.01	18
401	Min.	-176	173.66	9	-3313.57	17	-265.37	19	1160.57	1	-878.08	17	441.44	13	1619.21	9	1415.61	1
401	Min.	-153	173.66	9	-3313.57	17	-265.37	19	1160.57	1	-878.08	17	441.44	13	1619.21	9	1415.61	1
401	Min.	-155	173.66	9	-3313.57	17	-265.37	19	1160.57	1	-878.08	17	441.44	13	1619.21	9	1415.61	1
401	Min.	-186	173.66	9	-3313.57	17	-265.37	19	1160.57	1	-878.08	17	441.44	13	1619.21	9	1415.61	1
401	Max	-261	-1492.53	1	1248.57	19	2815.94	19	1208.03	17	3392.42	17	-413.53	1	-410.23	1	8406.04	17
401	Max	-259	-1492.53	1	1248.57	19	2815.94	19	1208.03	17	3392.42	17	-413.53	1	-410.23	1	8406.04	17
401	Max	-229	-1492.53	1	1248.57	19	2815.94	19	1208.03	17	3392.42	17	-413.53	1	-410.23	1	8406.04	17
401	Max	-231	-1492.53	1	1248.57	19	2815.94	19	1208.03	17	3392.42	17	-413.53	1	-410.23	1	8406.04	17
401	Min.	-261	-3554.40	17	-277.23	13	-1435.52	17	-421.91	1	1659.75	5	-955.49	19	-2043.29	18	2889.27	1
401	Min.	-259	-3554.40	17	-277.23	13	-1435.52	17	-421.91	1	1659.75	5	-955.49	19	-2043.29	18	2889.27	1
401	Min.	-229	-3554.40	17	-277.23	13	-1435.52	17	-421.91	1	1659.75	5	-955.49	19	-2043.29	18	2889.27	1
401	Min.	-231	-3554.40	17	-277.23	13	-1435.52	17	-421.91	1	1659.75	5	-955.49	19	-2043.29	18	2889.27	1
401	Max	-261	438.62	17	-773.56	21	506.26	17	3910.33	18	-1201.78	5	-40.89	1	2634.18	19	-2530.85	5
401	Max	-231	438.62	17	-773.56	21	506.26	17	3910.33	18	-1201.78	5	-40.89	1	2634.18	19	-2530.85	5
401	Max	-227	438.62	17	-773.56	21	506.26	17	3910.33	18	-1201.78	5	-40.89	1	2634.18	19	-2530.85	5
401	Max	-254	438.62	17	-773.56	21	506.26	17	3910.33	18	-1201.78	5	-40.89	1	2634.18	19	-2530.85	5
401	Min.	-261	-288.12	19	-2783.02	17	-1230.90	19	1913.49	5	-2454.92	18	-182.09	18	-377.79	9	-5156.44	18
401	Min.	-231	-288.12	19	-2783.02	17	-1230.90	19	1913.49	5	-2454.92	18	-182.09	18	-377.79	9	-5156.44	18
401	Min.	-227	-288.12	19	-2783.02	17	-1230.90	19	1913.49	5	-2454.92	18	-182.09	18	-377.79	9	-5156.44	18
401	Min.	-254	-288.12	19	-2783.02	17	-1230.90	19	1913.49	5	-2454.92	18	-182.09	18	-377.79	9	-5156.44	18
401	Max	-227	-656.98	1	323.25	17	27.76	19	1771.67	19	3252.91	18	394.29	19	3668.02	18	4592.49	19
401	Max	-221	-656.98	1	323.25	17	27.76	19	1771.67	19	3252.91	18	394.29	19	3668.02	18	4592.49	19
401	Max	-252	-656.98	1	323.25	17	27.76	19	1771.67	19	3252.91	18	394.29	19	3668.02	18	4592.49	19
401	Max	-254	-656.98	1	323.25	17	27.76	19	1771.67	19	3252.91	18	394.29	19	3668.02	18	4592.49	19
401	Min.	-227	-1545.94	17	129.90	9	-507.11	17	214.67	13	1510.32	1	96.48	13	1721.83	5	1701.45	9
401	Min.	-221	-1545.94	17	129.90	9	-507.11	17	214.67	13	1510.32	1	96.48	13	1721.83	5	1701.45	9
401	Min.	-252	-1545.94	17	129.90	9	-507.11	17	214.67	13	1510.32	1	96.48	13	1721.83	5	1701.45	9
401	Min.	-254	-1545.94	17	129.90	9	-507.11	17	214.67	13	1510.32	1	96.48	13	1721.83	5	1701.45	9
401	Max	-229	329.43	5	-2279.80	21	1309.74	17	3471.81	17	6700.59	17	453.15	19	10029.50	17	170.89	9
401	Max	-259	329.43	5	-2279.80	21	1309.74	17	3471.81	17	6700.59	17	453.15	19	10029.50	17	170.89	9
401	Max	-256	329.43	5	-2279.80	21	1309.74	17	3471.81	17	6700.59	17	453.15	19	10029.50	17	170.89	9
401	Max	-233	329.43	5	-2279.80	21	1309.74	17	3471.81	17	6700.59	17	453.15	19	10029.50	17	170.89	9
401	Min.	-229	-70.71	13	-5397.12	17	-6149.61	19	1371.24	21	1299.22	1	80.47	1	1919.56	21	-2400.95	19
401	Min.	-259	-70.71	13	-5397.12	17	-6149.61	19	1371.24	21	1299.22	1	80.47	1	1919.56	21	-2400.95	19
401	Min.	-256	-70.71	13	-5397.12	17	-6149.61	19	1371.24	21	1299.22	1	80.47	1	1919.56	21	-2400.95	19
401	Min.	-233	-70.71	13	-5397.12	17	-6149.61	19	1371.24	21	1299.22	1	80.47	1	1919.56	21	-2400.95	19
401	Max	-229	-2488.13	9	1880.60	19	4572.64	19	9275.19	17	661.34	13	971.71	17	1728.66	19	14667.90	17
401	Max	-233	-2488.13	9	1880.60	19	4572.64	19	9275.19	17	661.34	13	971.71	17	1728.66	19	14667.90	17
401	Max	-193	-2488.13	9	1880.60	19	4572.64	19	9275.19	17	661.34	13	971.71	17	1728.66	19	14667.90	17
401	Max	-201	-2488.13	9	1880.60	19	4572.64	19	9275.19	17	661.34	13	971.71	17	1728.66	19	14667.90	17
401	Min.	-229	-7054.63	19	-414.56	13	-1528.75	17	2677.04	1	-518.77	19	82.53	1	-381.14	9	5037.94	1

401	Min.	-233	-7054.63	19	-414.56	13	-1528.75	17	2677.04	1	-518.77	19	82.53	1	-381.14	9	5037.94	1
401	Min.	-193	-7054.63	19	-414.56	13	-1528.75	17	2677.04	1	-518.77	19	82.53	1	-381.14	9	5037.94	1
401	Min.	-201	-7054.63	19	-414.56	13	-1528.75	17	2677.04	1	-518.77	19	82.53	1	-381.14	9	5037.94	1
401	Max	-169	-77.46	1	-2488.41	9	471.46	13	2239.03	19	7546.72	17	161.50	19	-4519.10	1	-54.11	5
401	Max	-146	-77.46	1	-2488.41	9	471.46	13	2239.03	19	7546.72	17	161.50	19	-4519.10	1	-54.11	5
401	Max	-151	-77.46	1	-2488.41	9	471.46	13	2239.03	19	7546.72	17	161.50	19	-4519.10	1	-54.11	5
401	Max	-174	-77.46	1	-2488.41	9	471.46	13	2239.03	19	7546.72	17	161.50	19	-4519.10	1	-54.11	5
401	Min.	-169	-2278.60	19	-6386.00	17	-4587.12	19	890.28	1	1689.48	1	-156.61	13	-12656.70	17	-539.58	13
401	Min.	-146	-2278.60	19	-6386.00	17	-4587.12	19	890.28	1	1689.48	1	-156.61	13	-12656.70	17	-539.58	13
401	Min.	-151	-2278.60	19	-6386.00	17	-4587.12	19	890.28	1	1689.48	1	-156.61	13	-12656.70	17	-539.58	13
401	Min.	-174	-2278.60	19	-6386.00	17	-4587.12	19	890.28	1	1689.48	1	-156.61	13	-12656.70	17	-539.58	13
401	Max	-169	-2289.49	21	349.36	17	4658.20	19	9241.73	17	491.82	17	-14.92	13	263.75	13	-5662.33	1
401	Max	-174	-2289.49	21	349.36	17	4658.20	19	9241.73	17	491.82	17	-14.92	13	263.75	13	-5662.33	1
401	Max	-201	-2289.49	21	349.36	17	4658.20	19	9241.73	17	491.82	17	-14.92	13	263.75	13	-5662.33	1
401	Max	-193	-2289.49	21	349.36	17	4658.20	19	9241.73	17	491.82	17	-14.92	13	263.75	13	-5662.33	1
401	Min.	-169	-7104.98	17	-2994.91	19	-644.08	13	2689.39	1	-35.52	1	-237.84	17	-1456.76	19	-15051.20	17
401	Min.	-174	-7104.98	17	-2994.91	19	-644.08	13	2689.39	1	-35.52	1	-237.84	17	-1456.76	19	-15051.20	17
401	Min.	-201	-7104.98	17	-2994.91	19	-644.08	13	2689.39	1	-35.52	1	-237.84	17	-1456.76	19	-15051.20	17
401	Min.	-193	-7104.98	17	-2994.91	19	-644.08	13	2689.39	1	-35.52	1	-237.84	17	-1456.76	19	-15051.20	17
401	Max	-174	-145.30	1	-1358.48	9	398.13	13	4415.99	19	-67.04	1	784.09	19	-927.23	1	2572.94	19
401	Max	-151	-145.30	1	-1358.48	9	398.13	13	4415.99	19	-67.04	1	784.09	19	-927.23	1	2572.94	19
401	Max	-153	-145.30	1	-1358.48	9	398.13	13	4415.99	19	-67.04	1	784.09	19	-927.23	1	2572.94	19
401	Max	-176	-145.30	1	-1358.48	9	398.13	13	4415.99	19	-67.04	1	784.09	19	-927.23	1	2572.94	19
401	Min.	-174	-936.20	19	-3527.15	17	-3039.47	19	1900.33	1	-2059.32	18	0.46	13	-4817.21	17	1068.38	9
401	Min.	-151	-936.20	19	-3527.15	17	-3039.47	19	1900.33	1	-2059.32	18	0.46	13	-4817.21	17	1068.38	9
401	Min.	-153	-936.20	19	-3527.15	17	-3039.47	19	1900.33	1	-2059.32	18	0.46	13	-4817.21	17	1068.38	9
401	Min.	-176	-936.20	19	-3527.15	17	-3039.47	19	1900.33	1	-2059.32	18	0.46	13	-4817.21	17	1068.38	9
401	Max	-174	-3074.38	21	1465.05	19	4473.50	19	-1414.68	1	-1644.98	1	1331.66	18	-10535.80	1	-14443.20	1
401	Max	-176	-3074.38	21	1465.05	19	4473.50	19	-1414.68	1	-1644.98	1	1331.66	18	-10535.80	1	-14443.20	1
401	Max	-194	-3074.38	21	1465.05	19	4473.50	19	-1414.68	1	-1644.98	1	1331.66	18	-10535.80	1	-14443.20	1
401	Max	-201	-3074.38	21	1465.05	19	4473.50	19	-1414.68	1	-1644.98	1	1331.66	18	-10535.80	1	-14443.20	1
401	Min.	-174	-8958.30	17	78.37	13	-1280.46	17	-3330.39	18	-3516.64	18	493.02	5	-23738.80	18	-30762.90	18
401	Min.	-176	-8958.30	17	78.37	13	-1280.46	17	-3330.39	18	-3516.64	18	493.02	5	-23738.80	18	-30762.90	18
401	Min.	-194	-8958.30	17	78.37	13	-1280.46	17	-3330.39	18	-3516.64	18	493.02	5	-23738.80	18	-30762.90	18
401	Min.	-201	-8958.30	17	78.37	13	-1280.46	17	-3330.39	18	-3516.64	18	493.02	5	-23738.80	18	-30762.90	18
401	Max	-126	217.68	5	-2679.75	9	65.60	13	643.85	17	9762.60	17	660.66	19	14863.80	17	1493.92	17
401	Max	-151	217.68	5	-2679.75	9	65.60	13	643.85	17	9762.60	17	660.66	19	14863.80	17	1493.92	17
401	Max	-146	217.68	5	-2679.75	9	65.60	13	643.85	17	9762.60	17	660.66	19	14863.80	17	1493.92	17
401	Max	-118	217.68	5	-2679.75	9	65.60	13	643.85	17	9762.60	17	660.66	19	14863.80	17	1493.92	17
401	Min.	-126	-938.49	19	-7125.05	17	-4530.13	19	78.29	1	3118.64	9	83.97	13	5921.13	9	433.79	5
401	Min.	-151	-938.49	19	-7125.05	17	-4530.13	19	78.29	1	3118.64	9	83.97	13	5921.13	9	433.79	5
401	Min.	-146	-938.49	19	-7125.05	17	-4530.13	19	78.29	1	3118.64	9	83.97	13	5921.13	9	433.79	5
401	Min.	-118	-938.49	19	-7125.05	17	-4530.13	19	78.29	1	3118.64	9	83.97	13	5921.13	9	433.79	5
401	Max	-153	-2512.67	1	25.70	13	5941.58	19	-1648.69	9	-1012.87	5	-206.47	13	-11387.20	9	22193.20	19
401	Max	-151	-2512.67	1	25.70	13	5941.58	19	-1648.69	9	-1012.87	5	-206.47	13	-11387.20	9	22193.20	19
401	Max	-126	-2512.67	1	25.70	13	5941.58	19	-1648.69	9	-1012.87	5	-206.47	13	-11387.20	9	22193.20	19
401	Max	-119	-2512.67	1	25.70	13	5941.58	19	-1648.69	9	-1012.87	5	-206.47	13	-11387.20	9	22193.20	19
401	Min.	-153	-6773.25	17	-5171.38	19	1119.89	13	-4847.24	19	-2046.90	18	-1512.86	19	-26004.90	19	9243.43	9
401	Min.	-151	-6773.25	17	-5171.38	19	1119.89	13	-4847.24	19	-2046.90	18	-1512.86	19	-26004.90	19	9243.43	9
401	Min.	-126	-6773.25	17	-5171.38	19	1119.89	13	-4847.24	19	-2046.90	18	-1512.86	19	-26004.90	19	9243.43	9
401	Min.	-119	-6773.25	17	-5171.38	19	1119.89	13	-4847.24	19	-2046.90	18	-1512.86	19	-26004.90	19	9243.43	9
401	Max	-153	625.01	17	-522.08	9	-564.77	9	-575.66	1	-1206.07	5	-467.43	1	12699.80	19	-8039.72	9
401	Max	-119	625.01	17	-522.08	9	-564.77	9	-575.66	1	-1206.07	5	-467.43	1	12699.80	19	-8039.72	9
401	Max	-128	625.01	17	-522.08	9	-564.77	9	-575.66	1	-1206.07	5	-467.43	1	12699.80	19	-8039.72	9
401	Max	-155	625.01	17	-522.08	9	-564.77	9	-575.66	1	-1206.07	5	-467.43	1	12699.80	19	-8039.72	9
401	Min.	-153	-1419.09	19	-1293.06	17	-1655.63	19	-1274.97	18	-2307.80	19	-984.78	17	5506.39	13	-18575.20	19
401	Min.	-119	-1419.09	19	-1293.06	17	-1655.63	19	-1274.97	18	-2307.80	19	-984.78	17	5506.39	13	-18575.20	19
401	Min.	-128	-1419.09	19	-1293.06	17	-1655.63	19	-1274.97	18	-2307.80	19	-984.78	17	5506.39	13	-18575.20	19
401	Min.	-155	-1419.09	19	-1293.06	17	-1655.63	19	-1274.97	18	-2307.80	19	-984.78	17	5506.39	13	-18575.20	19
401	Max	-322	1746.65	18	139.79	17	459.83	18	-1832.43	9	-1033.05	13	1803.59	18	19512.40	19	24179.50	19
401	Max	-308	1746.65	18	139.79	17	459.83	18	-1832.43	9	-1033.05	13	1803.59	18	19512.40	19	24179.50	19
401	Max	-337	1746.65	18	139.79	17	459.83	18	-1832.43	9	-1033.05	13	1803.59	18	19512.40	19	24179.50	19
401	Max	-350	1746.65	18	139.79	17	459.83	18	-1832.43	9	-1033.05	13	1803.59	18	19512.40	19	24179.50	19
401	Min.	-322	-60.76	5	-1042.54	18	76.82	1	-4405.97	19	-2826.68	18	661.62	13	8244.37	9	10036.70	9
401	Min.	-308	-60.76	5	-1042.54	18	76.82	1	-4405.97	19	-2826.68	18	661.62	13	8244.37	9	10036.70	9
401	Min.	-337	-60.76	5	-1042.54	18	76.82	1	-4405.97	19	-2826.68	18	661.62	13	8244.37	9	10036.70	9
401	Min.	-350	-60.76	5	-1042.54	18	76.82	1	-4405.97	19	-2826.68	18	661.62	13	8244.37	9	10036.70	9
401	Max	-308	735.29	18	271.00	18	-68.56	1	748.56	18	-1446.39	9	-65.48	5	-2035.05	9	9188.51	19
401	Max	-306	735.29	18	271.00	18	-68.56	1	748.56	18	-1446.39	9	-65.48	5	-2035.05	9	9188.51	19
401	Max	-335	735.29	18	271.00	18	-68.56	1	748.56	18	-1446.39	9	-65.48	5	-2035.05	9	9188.51	19
401	Max	-337	735.29	18	271.00	18	-68.56	1	748.56	18	-1446.39	9	-65.48	5	-2035.05	9	9188.51	19
401	Min.	-308	-6.76	5	-162.30	17	-1409.64	18	145.31	9	-3517.27	18	-948.61	18	-5168.28	19	3703.03	9
401	Min.	-306	-6.76	5	-162.30	17	-1409.64	18	145.31	9	-3517.27	18	-948.61	18	-5168.28	19	3703.03	9
401	Min.	-335	-6.76	5	-162.30	17	-1409.64	18	145.31	9	-3517.27	18	-948.61	18	-5168.28	19	3703.03	9
401	Min.	-337	-6.76	5	-162.30	17	-1409.64	18	145.31	9	-3517.27	18	-948.61	18	-5168.28	19	3703.03	9
401	Max	-350	762.89	18	-90.70	1	48.31	19	-1595.34	9	922.25	19	-164.18	9	4565.40	18	-1197.30	9
401	Max	-337	762.89	18	-90.70	1	48.31	19	-1595.34	9	922.25	19	-164.18	9	4565.40	18	-1197.30	9
401	Max	-335	762.89	18	-90.70	1	48.31	19	-1595.34	9	922.25	19	-164.18	9	4565.40	18	-1197.30	9
401	Max	-351	762.89	18	-90.70	1	48.31	19	-1595.34	9	922.25	19	-164.18	9	4565.40	18	-1197.30	9
401	Min.	-350	-34.69	13	-1022.07	18	-188.52	17	-3625.66	19	366.12	1	-369.45	19	1764.08	9	-2745.73	19
401	Min.	-337	-34.69	13	-1022.07	18	-188.52	17	-3625.66	19	366.12	1	-369.45	19	1764.08	9	-2745.73	19
401	Min.	-335	-34.69	13	-1022.07	18	-188.52	17	-3625.66	19	366.12	1	-369.45	19	1764.08	9	-2745.73	19
401	Min.	-351	-34.69	13	-1022.07	18	-188.52	17	-3625.66	19	366.12	1	-369.45	19	1764.08	9	-2745.73	19
401	Max	-306	-79.79	1	1639.45	18	-32.49	5	2123.81	19	-665.43	13	-114.25	1	-897.49	9	501.98	19
401	Max	-312	-79.79	1	1639.45	18	-32.49	5	2123.81	19	-665.43	13	-114.25	1	-897.49	9	501.98	19
401	Max	-351	-79.79	1	1639.45	18	-32.49	5	2123.81	19	-665.43	13	-114.25	1	-897.49	9	501.98	19
401	Max	-335	-79.79	1	1639.45	18	-32.49	5	2123.81	19	-665.43	13	-114.25	1	-897.49	9	501.98	19
401	Min.	-306	-437.42	18	-16.38	5	-1057.16	18	774.10	9	-1406.45	19	-866.41	18	-2292.60	19	143.31	9
401	Min.	-312	-437.42	18	-16.38	5	-1057.16	18	774.10	9	-1406.45	19	-866.41	18	-2292.60	19	143.31	9
401	Min.	-351	-437.42	18	-16.38	5	-1057.16	18	774.10	9	-1406.45	19	-866.41	18	-2292.60	19	143.31	9
401	Min.	-335	-437.42	18	-16.38	5	-1057.16	18	774.10	9	-1406.45	19	-866.41	18	-2292.60	19	143.31	9
401	Max	-322	-71.76	21	2334.11	18	963.13	18	-3133.14	9	-1842.98	9	1228.64	18	21885.10	19	31607.10	19
401	Max	-304	-71.76	21	2334.11	18	963.13	18	-3133.14	9	-1842.98	9	1228.64	18	21885.10	19	31607.10	19
401	Max	-302	-71.76	21	2334.11	18	963.13	18	-3133.14	9	-1842.98	9	1228.64	18	21885.10	19	31607.10	19
401	Max	-308	-71.76	21	2334.11	18	963.13	18	-3133.14	9	-1842.98	9	1228.64	18	21885.10	19	31607.10	19
401	Min.	-322	-1009.16	17	48.84	1	-60.30	13	-7334.87	18	-4610.34	19	408.80	9	9089.60	9	13578.00	9
401	Min.	-304	-1009.16	17	48.84	1	-60.30	13	-7334.87	18	-4610.34	19	408.80	9	9089.60	9	13578.00	9
401	Min.	-302	-1009.16	17	48.84	1	-60.30	13	-7334.87	18	-4610.34	19	408.80	9	9089.60	9	13578.00	9
401	Min.	-308	-1009.16	17	48.84	1	-60.30	13	-7334.87	18	-4610.34	19	408.80	9	9089.60	9	13578.00	9
401	Max	-304	179.19	18	114.56	18	403.65	18	467.36	19	-1134.99	9	1852.53	19	-1238.53	9	15065.80	19
401	Max	-285	179.19	18	114.56	18	403.65	18	467.36	19	-1134.99	9	1852.53	19	-1238.53	9	15065.80	19
401	Max	-281	179.19	18	114.56	18	403.65	18	467.36	19	-1134.99	9	1852.53	19	-1238.53	9	15065.80	19
401	Max	-302	179.19	18	114.56	18	403.65	18	467.36	19	-1134.99	9	1852.53	19	-1238.53	9	15065.80	19
401	Min.	-304	-725.99	17	-44.78	1	108.74	1	137.54	9	-2803.99	19	837.30	5	-3153.09	18	6461.48	9
401	Min.	-285	-725.99	17	-44.78	1	108.74	1	137.54	9	-2803.99	19	837.30	5	-3153.09	18	6461.48	9
401	Min.	-281	-725.99	17	-44.78	1	108.74	1	137.54	9	-2803.99	19	837.30	5	-3153.09	18	6461.48	9
401	Min.	-302	-725.99	17	-44.78	1	108.74	1	137.54	9	-2803.99	19	837.30	5	-3153.09	18	6461.48	9
401	Max	-308	-177.61	1	1422.14	18	-23.51	1	-2109.27	9	321.89	18	1368.85	19	14909.00	19	6066.93	18
401	Max	-302	-177.61	1	1422.14	18	-23.51	1	-2109.27	9	321.89	18	1368.85	19	14909.00	19	6066.93	18

401	Max	-281	-177.61	1	1422.14	18	-23.51	1	-2109.27	9	321.89	18	1368.85	19	14909.00	19	6066.93	18
401	Max	-279	-177.61	1	1422.14	18	-23.51	1	-2109.27	9	321.89	18	1368.85	19	14909.00	19	6066.93	18
401	Min.	-308	-506.07	18	-73.95	5	-477.02	18	-4817.55	19	-96.55	1	569.30	9	6187.64	9	2515.50	9
401	Min.	-302	-506.07	18	-73.95	5	-477.02	18	-4817.55	19	-96.55	1	569.30	9	6187.64	9	2515.50	9
401	Min.	-281	-506.07	18	-73.95	5	-477.02	18	-4817.55	19	-96.55	1	569.30	9	6187.64	9	2515.50	9
401	Min.	-279	-506.07	18	-73.95	5	-477.02	18	-4817.55	19	-96.55	1	569.30	9	6187.64	9	2515.50	9
401	Max	-285	356.89	18	-106.15	21	264.98	18	2488.07	19	-585.09	1	-505.18	9	-2554.20	9	5947.85	19
401	Max	-267	356.89	18	-106.15	21	264.98	18	2488.07	19	-585.09	1	-505.18	9	-2554.20	9	5947.85	19
401	Max	-279	356.89	18	-106.15	21	264.98	18	2488.07	19	-585.09	1	-505.18	9	-2554.20	9	5947.85	19
401	Max	-281	356.89	18	-106.15	21	264.98	18	2488.07	19	-585.09	1	-505.18	9	-2554.20	9	5947.85	19
401	Min.	-285	-21.43	13	-614.42	17	56.79	1	1090.52	1	-1247.08	19	-1333.00	19	-6084.41	19	2443.66	9
401	Min.	-267	-21.43	13	-614.42	17	56.79	1	1090.52	1	-1247.08	19	-1333.00	19	-6084.41	19	2443.66	9
401	Min.	-279	-21.43	13	-614.42	17	56.79	1	1090.52	1	-1247.08	19	-1333.00	19	-6084.41	19	2443.66	9
401	Min.	-281	-21.43	13	-614.42	17	56.79	1	1090.52	1	-1247.08	19	-1333.00	19	-6084.41	19	2443.66	9
401	Max	-279	515.38	18	466.22	18	-40.32	1	-207.30	1	1169.31	19	-476.71	1	-3219.88	9	4800.11	19
401	Max	-275	515.38	18	466.22	18	-40.32	1	-207.30	1	1169.31	19	-476.71	1	-3219.88	9	4800.11	19
401	Max	-306	515.38	18	466.22	18	-40.32	1	-207.30	1	1169.31	19	-476.71	1	-3219.88	9	4800.11	19
401	Max	-308	515.38	18	466.22	18	-40.32	1	-207.30	1	1169.31	19	-476.71	1	-3219.88	9	4800.11	19
401	Min.	-279	-242.59	17	-80.44	13	-1294.01	18	-556.40	17	535.21	13	-1842.34	18	-8167.56	19	1708.31	9
401	Min.	-275	-242.59	17	-80.44	13	-1294.01	18	-556.40	17	535.21	13	-1842.34	18	-8167.56	19	1708.31	9
401	Min.	-306	-242.59	17	-80.44	13	-1294.01	18	-556.40	17	535.21	13	-1842.34	18	-8167.56	19	1708.31	9
401	Min.	-308	-242.59	17	-80.44	13	-1294.01	18	-556.40	17	535.21	13	-1842.34	18	-8167.56	19	1708.31	9
401	Max	-275	926.19	18	225.72	18	-52.26	1	1777.75	18	662.72	17	170.10	17	-440.93	9	926.65	1
401	Max	-273	926.19	18	225.72	18	-52.26	1	1777.75	18	662.72	17	170.10	17	-440.93	9	926.65	1
401	Max	-312	926.19	18	225.72	18	-52.26	1	1777.75	18	662.72	17	170.10	17	-440.93	9	926.65	1
401	Max	-306	926.19	18	225.72	18	-52.26	1	1777.75	18	662.72	17	170.10	17	-440.93	9	926.65	1
401	Min.	-275	-128.06	17	-71.90	13	-1424.30	18	249.13	9	156.15	20	-521.18	18	-2208.28	19	-431.10	9
401	Min.	-273	-128.06	17	-71.90	13	-1424.30	18	249.13	9	156.15	20	-521.18	18	-2208.28	19	-431.10	9
401	Min.	-312	-128.06	17	-71.90	13	-1424.30	18	249.13	9	156.15	20	-521.18	18	-2208.28	19	-431.10	9
401	Min.	-306	-128.06	17	-71.90	13	-1424.30	18	249.13	9	156.15	20	-521.18	18	-2208.28	19	-431.10	9
401	Max	-285	-45.52	20	4.40	19	-63.57	21	2660.83	18	2633.36	19	589.30	18	3304.83	19	4705.78	19
401	Max	-300	-45.52	20	4.40	19	-63.57	21	2660.83	18	2633.36	19	589.30	18	3304.83	19	4705.78	19
401	Max	-263	-45.52	20	4.40	19	-63.57	21	2660.83	18	2633.36	19	589.30	18	3304.83	19	4705.78	19
401	Max	-267	-45.52	20	4.40	19	-63.57	21	2660.83	18	2633.36	19	589.30	18	3304.83	19	4705.78	19
401	Min.	-285	-485.01	17	-201.79	17	-498.16	17	872.83	9	1128.00	1	174.52	9	1377.33	13	2054.78	9
401	Min.	-300	-485.01	17	-201.79	17	-498.16	17	872.83	9	1128.00	1	174.52	9	1377.33	13	2054.78	9
401	Min.	-263	-485.01	17	-201.79	17	-498.16	17	872.83	9	1128.00	1	174.52	9	1377.33	13	2054.78	9
401	Min.	-267	-485.01	17	-201.79	17	-498.16	17	872.83	9	1128.00	1	174.52	9	1377.33	13	2054.78	9
401	Max	-285	-38.97	21	354.03	18	398.46	17	2217.93	19	686.58	18	-419.66	13	3356.12	19	-4380.37	9
401	Max	-304	-38.97	21	354.03	18	398.46	17	2217.93	19	686.58	18	-419.66	13	3356.12	19	-4380.37	9
401	Max	-310	-38.97	21	354.03	18	398.46	17	2217.93	19	686.58	18	-419.66	13	3356.12	19	-4380.37	9
401	Max	-300	-38.97	21	354.03	18	398.46	17	2217.93	19	686.58	18	-419.66	13	3356.12	19	-4380.37	9
401	Min.	-285	-700.73	17	-4.07	1	49.50	21	887.99	9	63.40	1	-1251.78	18	1487.38	13	-10152.70	19
401	Min.	-304	-700.73	17	-4.07	1	49.50	21	887.99	9	63.40	1	-1251.78	18	1487.38	13	-10152.70	19
401	Min.	-310	-700.73	17	-4.07	1	49.50	21	887.99	9	63.40	1	-1251.78	18	1487.38	13	-10152.70	19
401	Min.	-300	-700.73	17	-4.07	1	49.50	21	887.99	9	63.40	1	-1251.78	18	1487.38	13	-10152.70	19
401	Max	-304	72.44	19	76.84	17	635.35	18	-2100.07	1	-1621.89	9	81.79	9	10698.70	18	-12135.30	9
401	Max	-322	72.44	19	76.84	17	635.35	18	-2100.07	1	-1621.89	9	81.79	9	10698.70	18	-12135.30	9
401	Max	-333	72.44	19	76.84	17	635.35	18	-2100.07	1	-1621.89	9	81.79	9	10698.70	18	-12135.30	9
401	Max	-310	72.44	19	76.84	17	635.35	18	-2100.07	1	-1621.89	9	81.79	9	10698.70	18	-12135.30	9
401	Min.	-304	-996.50	17	13.92	21	166.47	1	-4912.53	18	-3944.64	19	-85.84	1	4473.93	9	-28183.90	19
401	Min.	-322	-996.50	17	13.92	21	166.47	1	-4912.53	18	-3944.64	19	-85.84	1	4473.93	9	-28183.90	19
401	Min.	-333	-996.50	17	13.92	21	166.47	1	-4912.53	18	-3944.64	19	-85.84	1	4473.93	9	-28183.90	19
401	Min.	-310	-996.50	17	13.92	21	166.47	1	-4912.53	18	-3944.64	19	-85.84	1	4473.93	9	-28183.90	19
401	Max	-310	35.09	18	138.36	18	448.68	17	257.49	19	3630.51	18	-753.34	9	7063.12	19	-1281.21	9
401	Max	-333	35.09	18	138.36	18	448.68	17	257.49	19	3630.51	18	-753.34	9	7063.12	19	-1281.21	9
401	Max	-331	35.09	18	138.36	18	448.68	17	257.49	19	3630.51	18	-753.34	9	7063.12	19	-1281.21	9
401	Max	-300	35.09	18	138.36	18	448.68	17	257.49	19	3630.51	18	-753.34	9	7063.12	19	-1281.21	9
401	Min.	-310	-137.99	17	-294.50	17	55.46	21	105.92	1	1427.27	9	-1963.92	19	3056.19	9	-3140.70	18
401	Min.	-333	-137.99	17	-294.50	17	55.46	21	105.92	1	1427.27	9	-1963.92	19	3056.19	9	-3140.70	18
401	Min.	-331	-137.99	17	-294.50	17	55.46	21	105.92	1	1427.27	9	-1963.92	19	3056.19	9	-3140.70	18
401	Min.	-300	-137.99	17	-294.50	17	55.46	21	105.92	1	1427.27	9	-1963.92	19	3056.19	9	-3140.70	18
401	Max	-333	299.76	18	87.86	17	419.74	18	-2195.31	9	-1031.11	13	-558.61	1	9802.30	18	-7181.18	9
401	Max	-322	299.76	18	87.86	17	419.74	18	-2195.31	9	-1031.11	13	-558.61	1	9802.30	18	-7181.18	9
401	Max	-350	299.76	18	87.86	17	419.74	18	-2195.31	9	-1031.11	13	-558.61	1	9802.30	18	-7181.18	9
401	Max	-349	299.76	18	87.86	17	419.74	18	-2195.31	9	-1031.11	13	-558.61	1	9802.30	18	-7181.18	9
401	Min.	-333	-449.52	17	-592.65	18	-177.80	17	-5038.38	19	-2684.25	18	-1270.15	19	4169.40	9	-16641.80	19
401	Min.	-322	-449.52	17	-592.65	18	-177.80	17	-5038.38	19	-2684.25	18	-1270.15	19	4169.40	9	-16641.80	19
401	Min.	-350	-449.52	17	-592.65	18	-177.80	17	-5038.38	19	-2684.25	18	-1270.15	19	4169.40	9	-16641.80	19
401	Min.	-349	-449.52	17	-592.65	18	-177.80	17	-5038.38	19	-2684.25	18	-1270.15	19	4169.40	9	-16641.80	19
401	Max	-333	336.60	18	289.39	18	211.81	17	-24.13	9	4856.76	18	-135.88	9	6325.40	19	-1126.10	9
401	Max	-349	336.60	18	289.39	18	211.81	17	-24.13	9	4856.76	18	-135.88	9	6325.40	19	-1126.10	9
401	Max	-348	336.60	18	289.39	18	211.81	17	-24.13	9	4856.76	18	-135.88	9	6325.40	19	-1126.10	9
401	Max	-331	336.60	18	289.39	18	211.81	17	-24.13	9	4856.76	18	-135.88	9	6325.40	19	-1126.10	9
401	Min.	-333	-17.86	5	-126.64	17	-176.84	18	-67.93	19	2047.93	9	-490.61	19	2635.49	9	-2749.93	19
401	Min.	-349	-17.86	5	-126.64	17	-176.84	18	-67.93	19	2047.93	9	-490.61	19	2635.49	9	-2749.93	19
401	Min.	-348	-17.86	5	-126.64	17	-176.84	18	-67.93	19	2047.93	9	-490.61	19	2635.49	9	-2749.93	19
401	Min.	-331	-17.86	5	-126.64	17	-176.84	18	-67.93	19	2047.93	9	-490.61	19	2635.49	9	-2749.93	19
401	Max	-273	2695.79	18	781.04	18	-97.48	1	1010.64	1	1160.08	17	351.90	9	-977.99	9	163.18	1
401	Max	-265	2695.79	18	781.04	18	-97.48	1	1010.64	1	1160.08	17	351.90	9	-977.99	9	163.18	1
401	Max	-283	2695.79	18	781.04	18	-97.48	1	1010.64	1	1160.08	17	351.90	9	-977.99	9	163.18	1
401	Max	-312	2695.79	18	781.04	18	-97.48	1	1010.64	1	1160.08	17	351.90	9	-977.99	9	163.18	1
401	Min.	-273	-18.66	5	-32.18	9	-1973.04	18	-1401.48	9	75.80	18	-67.66	18	-4123.27	19	-4741.46	18
401	Min.	-265	-18.66	5	-32.18	9	-1973.04	18	-1401.48	9	75.80	18	-67.66	18	-4123.27	19	-4741.46	18
401	Min.	-283	-18.66	5	-32.18	9	-1973.04	18	-1401.48	9	75.80	18	-67.66	18	-4123.27	19	-4741.46	18
401	Min.	-312	-18.66	5	-32.18	9	-1973.04	18	-1401.48	9	75.80	18	-67.66	18	-4123.27	19	-4741.46	18
401	Max	-265	154.37	9	13399.90	18	-72.52	5	1623.53	1	2639.16	17	1299.81	9	2069.08	18	2325.70	5
401	Max	-257	154.37	9	13399.90	18	-72.52	5	1623.53	1	2639.16	17	1299.81	9	2069.08	18	2325.70	5
401	Max	-287	154.37	9	13399.90	18	-72.52	5	1623.53	1	2639.16	17	1299.81	9	2069.08	18	2325.70	5
401	Max	-283	154.37	9	13399.90	18	-72.52	5	1623.53	1	2639.16	17	1299.81	9	2069.08	18	2325.70	5
401	Min.	-265	-1097.50	18	199.21	13	-7450.20	18	-2720.26	18	1113.20	20	-907.71	1	-5346.45	17	-4401.27	18
401	Min.	-257	-1097.50	18	199.21	13	-7450.20	18	-2720.26	18	1113.20	20	-907.71	1	-5346.45	17	-4401.27	18
401	Min.	-287	-1097.50	18	199.21	13	-7450.20	18	-2720.26	18	1113.20	20	-907.71	1	-5346.45	17	-4401.27	18
401	Min.	-283	-1097.50	18	199.21	13	-7450.20	18	-2720.26	18	1113.20	20	-907.71	1	-5346.45	17	-4401.27	18
401	Max	-283	-126.99	1	9976.16	18	337.72	18	-829.98	13	-1032.19	20	762.09	9	-7392.12	13	-3080.81	9
401	Max	-287	-126.99	1	9976.16	18	337.72	18	-829.98	13	-1032.19	20	762.09	9	-7392.12	13	-3080.81	9
401	Max	-323	-126.99	1	9976.16	18	337.72	18	-829.98	13	-1032.19	20	762.09	9	-7392.12	13	-3080.81	9
401	Max	-312	-126.99	1	9976.16	18	337.72	18	-829.98	13	-1032.19	20	762.09	9	-7392.12	13	-3080.81	9
401	Min.	-283	-1848.84	18	143.66	5	-37.44	9	-2590.26	18	-2219.30	17	-250.12	1	-14896.50	19	-8076.39	19
401	Min.	-287	-1848.84	18	143.66	5	-37.44	9	-2590.26	18	-2219.30	17	-250.12	1	-14896.50	19	-8076.39	19
401	Min.	-323	-1848.84	18	143.66	5	-37.44	9	-2590.26	18	-2219.30	17	-250.12	1	-14896.50	19	-8076.39	19
401	Min.	-312	-1848.84	18	143.66	5	-37.44	9	-2590.26	18	-2219.30	17	-250.12	1	-14896.50	19	-8076.39	19
401	Max	-323	123.47	18	-117.18	1	7.03	5	-1493.32	9	-662.90	9	1055.76	19	11809.70	19	6107.05	18
401	Max	-352	123.47	18	-117.18	1	7.03	5	-1493.32	9	-662.90	9	1055.76	19	11809.70	19	6107.05	18
401	Max	-351	123.47	18	-117.18	1	7.03	5	-1493.32	9	-662.90	9	1055.76	19	11809.70	19	6107.05	18
401	Max	-312	123.47	18	-117.18	1	7.03	5	-1493.32	9	-662.90	9	1055.76	19	11809.70	19	6107.05	18
401	Min.	-323	-4.40	1	-1096.77	18	-1178.02	18	-3342.46	19	-1650.99	18	462.47	9	5365.26	9	2549.89	1
401	Min.	-352	-4.40	1	-1096.77	18	-1178.02	18	-3342.46	19	-1650.99	18	462.47	9	5365.26	9	2549.89	1
401	Min.	-351	-4.40	1	-1096.77	18	-1178.02	18	-3342.46	19	-1650.99	18	462.47	9	5365.26	9	2549.89	1

401	Min.	-312	-4.40	1	-1096.77	18	-1178.02	18	-3342.46	19	-1650.99	18	462.47	9	5365.26	9	2549.89	1
401	Max	-296	1610.53	19	3.80	9	1066.11	17	-1378.21	1	-1312.75	5	541.41	17	-7880.37	1	-8820.83	1
401	Max	-329	1610.53	19	3.80	9	1066.11	17	-1378.21	1	-1312.75	5	541.41	17	-7880.37	1	-8820.83	1
401	Max	-321	1610.53	19	3.80	9	1066.11	17	-1378.21	1	-1312.75	5	541.41	17	-7880.37	1	-8820.83	1
401	Max	-292	1610.53	19	3.80	9	1066.11	17	-1378.21	1	-1312.75	5	541.41	17	-7880.37	1	-8820.83	1
401	Min.	-296	-239.32	13	-100.79	19	163.97	21	-3093.83	18	-2809.09	18	194.29	21	-18045.70	18	-19562.00	18
401	Min.	-329	-239.32	13	-100.79	19	163.97	21	-3093.83	18	-2809.09	18	194.29	21	-18045.70	18	-19562.00	18
401	Min.	-321	-239.32	13	-100.79	19	163.97	21	-3093.83	18	-2809.09	18	194.29	21	-18045.70	18	-19562.00	18
401	Min.	-292	-239.32	13	-100.79	19	163.97	21	-3093.83	18	-2809.09	18	194.29	21	-18045.70	18	-19562.00	18
401	Max	-296	-323.30	21	627.78	19	6.93	19	1452.48	19	3076.58	18	-519.09	1	3814.73	18	-1906.83	9
401	Max	-292	-323.30	21	627.78	19	6.93	19	1452.48	19	3076.58	18	-519.09	1	3814.73	18	-1906.83	9
401	Max	-254	-323.30	21	627.78	19	6.93	19	1452.48	19	3076.58	18	-519.09	1	3814.73	18	-1906.83	9
401	Max	-252	-323.30	21	627.78	19	6.93	19	1452.48	19	3076.58	18	-519.09	1	3814.73	18	-1906.83	9
401	Min.	-296	-1473.26	17	19.95	13	-671.40	17	125.14	13	1454.58	5	-1071.24	18	1635.35	1	-4694.85	18
401	Min.	-292	-1473.26	17	19.95	13	-671.40	17	125.14	13	1454.58	5	-1071.24	18	1635.35	1	-4694.85	18
401	Min.	-254	-1473.26	17	19.95	13	-671.40	17	125.14	13	1454.58	5	-1071.24	18	1635.35	1	-4694.85	18
401	Min.	-252	-1473.26	17	19.95	13	-671.40	17	125.14	13	1454.58	5	-1071.24	18	1635.35	1	-4694.85	18
401	Max	-329	157.95	13	607.61	18	401.82	19	-941.00	13	-1818.45	5	-416.72	5	-6773.73	1	10628.20	18
401	Max	-347	157.95	13	607.61	18	401.82	19	-941.00	13	-1818.45	5	-416.72	5	-6773.73	1	10628.20	18
401	Max	-346	157.95	13	607.61	18	401.82	19	-941.00	13	-1818.45	5	-416.72	5	-6773.73	1	10628.20	18
401	Max	-321	157.95	13	607.61	18	401.82	19	-941.00	13	-1818.45	5	-416.72	5	-6773.73	1	10628.20	18
401	Min.	-329	-1064.56	19	146.81	1	-273.41	17	-2569.51	19	-4094.53	18	-876.69	18	-15388.10	18	4665.66	1
401	Min.	-347	-1064.56	19	146.81	1	-273.41	17	-2569.51	19	-4094.53	18	-876.69	18	-15388.10	18	4665.66	1
401	Min.	-346	-1064.56	19	146.81	1	-273.41	17	-2569.51	19	-4094.53	18	-876.69	18	-15388.10	18	4665.66	1
401	Min.	-321	-1064.56	19	146.81	1	-273.41	17	-2569.51	19	-4094.53	18	-876.69	18	-15388.10	18	4665.66	1
401	Max	-300	178.12	17	108.71	18	248.96	17	914.43	18	4758.89	19	1964.09	18	-816.09	5	-215.67	13
401	Max	-331	178.12	17	108.71	18	248.96	17	914.43	18	4758.89	19	1964.09	18	-816.09	5	-215.67	13
401	Max	-329	178.12	17	108.71	18	248.96	17	914.43	18	4758.89	19	1964.09	18	-816.09	5	-215.67	13
401	Max	-296	178.12	17	108.71	18	248.96	17	914.43	18	4758.89	19	1964.09	18	-816.09	5	-215.67	13
401	Min.	-300	19.59	21	-646.69	17	13.78	21	429.03	1	1848.95	13	822.17	1	-1822.80	18	-913.64	19
401	Min.	-331	19.59	21	-646.69	17	13.78	21	429.03	1	1848.95	13	822.17	1	-1822.80	18	-913.64	19
401	Min.	-329	19.59	21	-646.69	17	13.78	21	429.03	1	1848.95	13	822.17	1	-1822.80	18	-913.64	19
401	Min.	-296	19.59	21	-646.69	17	13.78	21	429.03	1	1848.95	13	822.17	1	-1822.80	18	-913.64	19
401	Max	-300	-152.90	20	235.16	18	-60.25	21	4413.13	18	2014.90	18	-167.55	1	1917.40	18	-640.64	5
401	Max	-296	-152.90	20	235.16	18	-60.25	21	4413.13	18	2014.90	18	-167.55	1	1917.40	18	-640.64	5
401	Max	-252	-152.90	20	235.16	18	-60.25	21	4413.13	18	2014.90	18	-167.55	1	1917.40	18	-640.64	5
401	Max	-263	-152.90	20	235.16	18	-60.25	21	4413.13	18	2014.90	18	-167.55	1	1917.40	18	-640.64	5
401	Min.	-300	-895.10	17	87.04	9	-372.77	17	1611.16	13	938.93	5	-438.94	18	762.02	9	-1418.05	18
401	Min.	-296	-895.10	17	87.04	9	-372.77	17	1611.16	13	938.93	5	-438.94	18	762.02	9	-1418.05	18
401	Min.	-252	-895.10	17	87.04	9	-372.77	17	1611.16	13	938.93	5	-438.94	18	762.02	9	-1418.05	18
401	Min.	-263	-895.10	17	87.04	9	-372.77	17	1611.16	13	938.93	5	-438.94	18	762.02	9	-1418.05	18
401	Max	-331	456.67	19	358.68	18	127.22	18	-118.15	1	5512.55	18	29.62	9	-2062.79	1	-640.98	1
401	Max	-348	456.67	19	358.68	18	127.22	18	-118.15	1	5512.55	18	29.62	9	-2062.79	1	-640.98	1
401	Max	-347	456.67	19	358.68	18	127.22	18	-118.15	1	5512.55	18	29.62	9	-2062.79	1	-640.98	1
401	Max	-329	456.67	19	358.68	18	127.22	18	-118.15	1	5512.55	18	29.62	9	-2062.79	1	-640.98	1
401	Min.	-331	-253.94	17	43.16	1	46.77	1	-238.61	18	2336.83	9	-163.38	19	-4772.37	18	-1455.36	18
401	Min.	-348	-253.94	17	43.16	1	46.77	1	-238.61	18	2336.83	9	-163.38	19	-4772.37	18	-1455.36	18
401	Min.	-347	-253.94	17	43.16	1	46.77	1	-238.61	18	2336.83	9	-163.38	19	-4772.37	18	-1455.36	18
401	Min.	-329	-253.94	17	43.16	1	46.77	1	-238.61	18	2336.83	9	-163.38	19	-4772.37	18	-1455.36	18
401	Max	-294	8272.21	19	-812.95	1	2460.25	17	1633.96	17	3990.63	17	56.36	9	655.52	19	5753.06	17
401	Max	-256	8272.21	19	-812.95	1	2460.25	17	1633.96	17	3990.63	17	56.36	9	655.52	19	5753.06	17
401	Max	-259	8272.21	19	-812.95	1	2460.25	17	1633.96	17	3990.63	17	56.36	9	655.52	19	5753.06	17
401	Max	-290	8272.21	19	-812.95	1	2460.25	17	1633.96	17	3990.63	17	56.36	9	655.52	19	5753.06	17
401	Min.	-294	-825.61	13	-2024.97	17	-3529.98	19	547.66	21	1267.92	1	-1028.91	19	-4427.54	17	568.81	19
401	Min.	-256	-825.61	13	-2024.97	17	-3529.98	19	547.66	21	1267.92	1	-1028.91	19	-4427.54	17	568.81	19
401	Min.	-259	-825.61	13	-2024.97	17	-3529.98	19	547.66	21	1267.92	1	-1028.91	19	-4427.54	17	568.81	19
401	Min.	-290	-825.61	13	-2024.97	17	-3529.98	19	547.66	21	1267.92	1	-1028.91	19	-4427.54	17	568.81	19
401	Max	-294	243.38	17	3430.83	19	-157.58	21	2508.03	17	-448.94	5	699.99	19	-1215.77	21	77.96	9
401	Max	-290	243.38	17	3430.83	19	-157.58	21	2508.03	17	-448.94	5	699.99	19	-1215.77	21	77.96	9
401	Max	-318	243.38	17	3430.83	19	-157.58	21	2508.03	17	-448.94	5	699.99	19	-1215.77	21	77.96	9
401	Max	-327	243.38	17	3430.83	19	-157.58	21	2508.03	17	-448.94	5	699.99	19	-1215.77	21	77.96	9
401	Min.	-294	-1012.84	19	-610.13	17	-965.53	17	1309.61	5	-942.50	18	122.49	9	-2922.33	17	-683.23	19
401	Min.	-290	-1012.84	19	-610.13	17	-965.53	17	1309.61	5	-942.50	18	122.49	9	-2922.33	17	-683.23	19
401	Min.	-318	-1012.84	19	-610.13	17	-965.53	17	1309.61	5	-942.50	18	122.49	9	-2922.33	17	-683.23	19
401	Min.	-327	-1012.84	19	-610.13	17	-965.53	17	1309.61	5	-942.50	18	122.49	9	-2922.33	17	-683.23	19
401	Max	-261	-562.77	9	1538.27	19	824.34	19	-1129.00	1	3493.46	18	-178.62	21	-3089.79	1	2549.25	19
401	Max	-254	-562.77	9	1538.27	19	824.34	19	-1129.00	1	3493.46	18	-178.62	21	-3089.79	1	2549.25	19
401	Max	-292	-562.77	9	1538.27	19	824.34	19	-1129.00	1	3493.46	18	-178.62	21	-3089.79	1	2549.25	19
401	Max	-288	-562.77	9	1538.27	19	824.34	19	-1129.00	1	3493.46	18	-178.62	21	-3089.79	1	2549.25	19
401	Min.	-261	-1276.76	17	-570.56	17	-1387.39	17	-2714.57	18	1671.34	5	-630.94	17	-6836.52	18	-286.34	9
401	Min.	-254	-1276.76	17	-570.56	17	-1387.39	17	-2714.57	18	1671.34	5	-630.94	17	-6836.52	18	-286.34	9
401	Min.	-292	-1276.76	17	-570.56	17	-1387.39	17	-2714.57	18	1671.34	5	-630.94	17	-6836.52	18	-286.34	9
401	Min.	-288	-1276.76	17	-570.56	17	-1387.39	17	-2714.57	18	1671.34	5	-630.94	17	-6836.52	18	-286.34	9
401	Max	-261	1274.86	19	-144.93	21	2074.15	17	2175.78	17	789.38	17	-68.22	13	6840.96	17	-2733.94	1
401	Max	-288	1274.86	19	-144.93	21	2074.15	17	2175.78	17	789.38	17	-68.22	13	6840.96	17	-2733.94	1
401	Max	-290	1274.86	19	-144.93	21	2074.15	17	2175.78	17	789.38	17	-68.22	13	6840.96	17	-2733.94	1
401	Max	-259	1274.86	19	-144.93	21	2074.15	17	2175.78	17	789.38	17	-68.22	13	6840.96	17	-2733.94	1
401	Min.	-261	-418.73	17	-2449.64	17	-2501.34	19	1061.14	5	-254.13	1	-1307.76	19	3027.02	5	-6005.06	17
401	Min.	-288	-418.73	17	-2449.64	17	-2501.34	19	1061.14	5	-254.13	1	-1307.76	19	3027.02	5	-6005.06	17
401	Min.	-290	-418.73	17	-2449.64	17	-2501.34	19	1061.14	5	-254.13	1	-1307.76	19	3027.02	5	-6005.06	17
401	Min.	-259	-418.73	17	-2449.64	17	-2501.34	19	1061.14	5	-254.13	1	-1307.76	19	3027.02	5	-6005.06	17
401	Max	-288	-159.17	21	3434.25	19	2349.24	19	-2246.47	5	-2143.82	1	1670.01	19	-13061.50	1	-8157.28	5
401	Max	-292	-159.17	21	3434.25	19	2349.24	19	-2246.47	5	-2143.82	1	1670.01	19	-13061.50	1	-8157.28	5
401	Max	-321	-159.17	21	3434.25	19	2349.24	19	-2246.47	5	-2143.82	1	1670.01	19	-13061.50	1	-8157.28	5
401	Max	-316	-159.17	21	3434.25	19	2349.24	19	-2246.47	5	-2143.82	1	1670.01	19	-13061.50	1	-8157.28	5
401	Min.	-288	-1793.42	17	-1121.42	17	-2359.91	17	-4692.39	18	-4530.98	18	-166.24	13	-28188.40	18	-16819.60	18
401	Min.	-292	-1793.42	17	-1121.42	17	-2359.91	17	-4692.39	18	-4530.98	18	-166.24	13	-28188.40	18	-16819.60	18
401	Min.	-321	-1793.42	17	-1121.42	17	-2359.91	17	-4692.39	18	-4530.98	18	-166.24	13	-28188.40	18	-16819.60	18
401	Min.	-316	-1793.42	17	-1121.42	17	-2359.91	17	-4692.39	18	-4530.98	18	-166.24	13	-28188.40	18	-16819.60	18
401	Max	-288	1597.61	19	806.36	19	1608.56	17	-594.13	13	1680.60	18	43.56	13	8527.47	18	-2112.59	1
401	Max	-316	1597.61	19	806.36	19	1608.56	17	-594.13	13	1680.60	18	43.56	13	8527.47	18	-2112.59	1
401	Max	-318	1597.61	19	806.36	19	1608.56	17	-594.13	13	1680.60	18	43.56	13	8527.47	18	-2112.59	1
401	Max	-290	1597.61	19	806.36	19	1608.56	17	-594.13	13	1680.60	18	43.56	13	8527.47	18	-2112.59	1
401	Min.	-288	-131.00	13	-1668.15	17	-2632.17	19	-1963.96	19	703.18	1	-1218.68	19	4448.15	5	-4354.58	17
401	Min.	-316	-131.00	13	-1668.15	17	-2632.17	19	-1963.96	19	703.18	1	-1218.68	19	4448.15	5	-4354.58	17
401	Min.	-318	-131.00	13	-1668.15	17	-2632.17	19	-1963.96	19	703.18	1	-1218.68	19	4448.15	5	-4354.58	17
401	Min.	-290	-131.00	13	-1668.15	17	-2632.17	19	-1963.96	19	703.18	1	-1218.68	19	4448.15	5	-4354.58	17
401	Max	-327	186.38	13	1566.38	19	-4.25	21	2525.56	18	-581.03	5	323.91	19	-608.38	5	-937.82	5
401	Max	-318	186.38	13	1566.38	19	-4.25	21	2525.56	18	-581.03	5	323.91	19	-608.38	5	-937.82	5
401	Max	-341	186.38	13	1566.38	19	-4.25	21	2525.56	18	-581.03	5	323.91	19	-608.38	5	-937.82	5
401	Max	-345	186.38	13	1566.38	19	-4.25	21	2525.56	18	-581.03	5	323.91	19	-608.38	5	-937.82	5
401	Min.	-327	-1203.69	19	-134.95	13	-301.41	17	1305.50	5	-1188.36	18	84.25	9	-1271.11	18	-2100.49	18
401	Min.	-318	-1203.69	19	-134.95	13	-301.41	17	1305.50	5	-1188.36	18	84.25	9	-1271.11	18	-2100.49	18
401	Min.	-341	-1203.69	19	-134.95	13	-301.41	17	1305.50	5	-1188.36	18	84.25	9	-1271.11	18	-2100.49	18
401	Min.	-345	-1203.69	19	-134.95	13	-301.41	17	1305.50	5	-1188.36	18	84.25	9	-1271.11	18	-2100.49	18
401	Max	-318	-244.16	9	1990.19	19	1339.80	19	1645.70	18	-1858.09	1	-544.62	5	-523.74	1	-4399.69	5
401	Max	-316	-244.16	9	1990.19	19	1339.80	19	1645.70	18	-1858.09	1	-544.62	5	-523.74	1	-4399.69	5
401	Max	-339	-244.16	9	1990.19	19	1339.80	19	1645.70	18	-1858.09	1	-544.62	5	-523.74	1	-4399.69	5
401	Max	-341	-244.16	9	1990.19	19	1339.80	19	1645.70	18	-1858.09	1	-544.62	5	-523.74	1	-4399.69	5

401	Min.	-318	-1205.29	19	-222.70	13	-653.55	17	816.32	5	-4000.94	18	-1042.36	17	-1050.93	18	-9271.25	18
401	Min.	-316	-1205.29	19	-222.70	13	-653.55	17	816.32	5	-4000.94	18	-1042.36	17	-1050.93	18	-9271.25	18
401	Min.	-339	-1205.29	19	-222.70	13	-653.55	17	816.32	5	-4000.94	18	-1042.36	17	-1050.93	18	-9271.25	18
401	Min.	-341	-1205.29	19	-222.70	13	-653.55	17	816.32	5	-4000.94	18	-1042.36	17	-1050.93	18	-9271.25	18
401	Max	-345	146.68	13	308.78	17	348.08	17	246.35	17	-1367.49	1	1444.69	18	-172.56	13	-2595.69	1
401	Max	-341	146.68	13	308.78	17	348.08	17	246.35	17	-1367.49	1	1444.69	18	-172.56	13	-2595.69	1
401	Max	-339	146.68	13	308.78	17	348.08	17	246.35	17	-1367.49	1	1444.69	18	-172.56	13	-2595.69	1
401	Max	-346	146.68	13	308.78	17	348.08	17	246.35	17	-1367.49	1	1444.69	18	-172.56	13	-2595.69	1
401	Min.	-345	-994.98	19	-101.84	19	-1365.18	19	47.65	21	-3144.07	18	719.03	5	-1043.33	19	-5788.63	18
401	Min.	-341	-994.98	19	-101.84	19	-1365.18	19	47.65	21	-3144.07	18	719.03	5	-1043.33	19	-5788.63	18
401	Min.	-339	-994.98	19	-101.84	19	-1365.18	19	47.65	21	-3144.07	18	719.03	5	-1043.33	19	-5788.63	18
401	Min.	-346	-994.98	19	-101.84	19	-1365.18	19	47.65	21	-3144.07	18	719.03	5	-1043.33	19	-5788.63	18
401	Max	-316	251.84	19	317.94	17	2558.05	19	-1676.56	5	-1697.76	13	-1168.78	5	11514.90	18	-10201.80	5
401	Max	-321	251.84	19	317.94	17	2558.05	19	-1676.56	5	-1697.76	13	-1168.78	5	11514.90	18	-10201.80	5
401	Max	-346	251.84	19	317.94	17	2558.05	19	-1676.56	5	-1697.76	13	-1168.78	5	11514.90	18	-10201.80	5
401	Max	-339	251.84	19	317.94	17	2558.05	19	-1676.56	5	-1697.76	13	-1168.78	5	11514.90	18	-10201.80	5
401	Min.	-316	-1362.60	17	-1107.15	19	-374.79	13	-3405.69	18	-4191.24	19	-2308.26	18	5103.32	1	-21885.70	18
401	Min.	-321	-1362.60	17	-1107.15	19	-374.79	13	-3405.69	18	-4191.24	19	-2308.26	18	5103.32	1	-21885.70	18
401	Min.	-346	-1362.60	17	-1107.15	19	-374.79	13	-3405.69	18	-4191.24	19	-2308.26	18	5103.32	1	-21885.70	18
401	Min.	-339	-1362.60	17	-1107.15	19	-374.79	13	-3405.69	18	-4191.24	19	-2308.26	18	5103.32	1	-21885.70	18
401	Max	-320	932.03	17	40.27	19	88.08	13	-180.35	13	-1052.11	5	752.29	17	4535.72	19	9037.59	18
401	Max	-327	932.03	17	40.27	19	88.08	13	-180.35	13	-1052.11	5	752.29	17	4535.72	19	9037.59	18
401	Max	-345	932.03	17	40.27	19	88.08	13	-180.35	13	-1052.11	5	752.29	17	4535.72	19	9037.59	18
401	Max	-344	932.03	17	40.27	19	88.08	13	-180.35	13	-1052.11	5	752.29	17	4535.72	19	9037.59	18
401	Min.	-320	-688.99	19	-159.30	17	-1867.84	19	-637.61	19	-2333.67	18	375.24	5	1898.52	13	4160.37	5
401	Min.	-327	-688.99	19	-159.30	17	-1867.84	19	-637.61	19	-2333.67	18	375.24	5	1898.52	13	4160.37	5
401	Min.	-345	-688.99	19	-159.30	17	-1867.84	19	-637.61	19	-2333.67	18	375.24	5	1898.52	13	4160.37	5
401	Min.	-344	-688.99	19	-159.30	17	-1867.84	19	-637.61	19	-2333.67	18	375.24	5	1898.52	13	4160.37	5
401	Max	-320	327.51	17	-69.06	5	-98.89	13	-1312.12	1	-707.22	9	956.50	18	6153.19	18	4629.29	18
401	Max	-344	327.51	17	-69.06	5	-98.89	13	-1312.12	1	-707.22	9	956.50	18	6153.19	18	4629.29	18
401	Max	-343	327.51	17	-69.06	5	-98.89	13	-1312.12	1	-707.22	9	956.50	18	6153.19	18	4629.29	18
401	Max	-314	327.51	17	-69.06	5	-98.89	13	-1312.12	1	-707.22	9	956.50	18	6153.19	18	4629.29	18
401	Min.	-320	81.81	21	-150.86	17	-794.51	19	-3111.21	18	-1891.16	19	416.12	1	2614.65	1	2062.15	5
401	Min.	-344	81.81	21	-150.86	17	-794.51	19	-3111.21	18	-1891.16	19	416.12	1	2614.65	1	2062.15	5
401	Min.	-343	81.81	21	-150.86	17	-794.51	19	-3111.21	18	-1891.16	19	416.12	1	2614.65	1	2062.15	5
401	Min.	-314	81.81	21	-150.86	17	-794.51	19	-3111.21	18	-1891.16	19	416.12	1	2614.65	1	2062.15	5
401	Max	-277	2049.81	19	-44.07	9	1098.56	19	-369.23	1	-878.20	5	-510.12	5	4487.16	19	-3989.83	1
401	Max	-320	2049.81	19	-44.07	9	1098.56	19	-369.23	1	-878.20	5	-510.12	5	4487.16	19	-3989.83	1
401	Max	-314	2049.81	19	-44.07	9	1098.56	19	-369.23	1	-878.20	5	-510.12	5	4487.16	19	-3989.83	1
401	Max	-269	2049.81	19	-44.07	9	1098.56	19	-369.23	1	-878.20	5	-510.12	5	4487.16	19	-3989.83	1
401	Min.	-277	-287.66	13	-305.06	19	408.49	9	-929.42	19	-1982.64	18	-1065.98	17	1873.06	9	-9616.72	18
401	Min.	-320	-287.66	13	-305.06	19	408.49	9	-929.42	19	-1982.64	18	-1065.98	17	1873.06	9	-9616.72	18
401	Min.	-314	-287.66	13	-305.06	19	408.49	9	-929.42	19	-1982.64	18	-1065.98	17	1873.06	9	-9616.72	18
401	Min.	-269	-287.66	13	-305.06	19	408.49	9	-929.42	19	-1982.64	18	-1065.98	17	1873.06	9	-9616.72	18
401	Max	-277	3221.56	19	2941.15	19	-448.14	13	-1206.30	1	40.67	9	989.68	17	-4164.41	1	7510.13	18
401	Max	-271	3221.56	19	2941.15	19	-448.14	13	-1206.30	1	40.67	9	989.68	17	-4164.41	1	7510.13	18
401	Max	-298	3221.56	19	2941.15	19	-448.14	13	-1206.30	1	40.67	9	989.68	17	-4164.41	1	7510.13	18
401	Max	-320	3221.56	19	2941.15	19	-448.14	13	-1206.30	1	40.67	9	989.68	17	-4164.41	1	7510.13	18
401	Min.	-277	570.60	13	-127.57	13	-5675.05	19	-2620.82	18	-682.24	19	-136.53	19	-9219.05	18	3828.47	5
401	Min.	-271	570.60	13	-127.57	13	-5675.05	19	-2620.82	18	-682.24	19	-136.53	19	-9219.05	18	3828.47	5
401	Min.	-298	570.60	13	-127.57	13	-5675.05	19	-2620.82	18	-682.24	19	-136.53	19	-9219.05	18	3828.47	5
401	Min.	-320	570.60	13	-127.57	13	-5675.05	19	-2620.82	18	-682.24	19	-136.53	19	-9219.05	18	3828.47	5
401	Max	-271	3069.37	19	5507.94	19	-191.20	13	1667.91	9	2128.95	17	1048.77	17	-614.92	19	4115.09	17
401	Max	-256	3069.37	19	5507.94	19	-191.20	13	1667.91	9	2128.95	17	1048.77	17	-614.92	19	4115.09	17
401	Max	-294	3069.37	19	5507.94	19	-191.20	13	1667.91	9	2128.95	17	1048.77	17	-614.92	19	4115.09	17
401	Max	-298	3069.37	19	5507.94	19	-191.20	13	1667.91	9	2128.95	17	1048.77	17	-614.92	19	4115.09	17
401	Min.	-271	590.63	9	-790.32	13	-8036.80	19	54.53	1	785.31	21	2.28	19	-3917.28	17	-298.14	19
401	Min.	-256	590.63	9	-790.32	13	-8036.80	19	54.53	1	785.31	21	2.28	19	-3917.28	17	-298.14	19
401	Min.	-294	590.63	9	-790.32	13	-8036.80	19	54.53	1	785.31	21	2.28	19	-3917.28	17	-298.14	19
401	Min.	-298	590.63	9	-790.32	13	-8036.80	19	54.53	1	785.31	21	2.28	19	-3917.28	17	-298.14	19
401	Max	-298	2322.98	19	3168.85	19	-253.02	13	-426.65	1	-1064.46	1	1286.81	17	-2335.60	5	11983.90	18
401	Max	-294	2322.98	19	3168.85	19	-253.02	13	-426.65	1	-1064.46	1	1286.81	17	-2335.60	5	11983.90	18
401	Max	-327	2322.98	19	3168.85	19	-253.02	13	-426.65	1	-1064.46	1	1286.81	17	-2335.60	5	11983.90	18
401	Max	-320	2322.98	19	3168.85	19	-253.02	13	-426.65	1	-1064.46	1	1286.81	17	-2335.60	5	11983.90	18
401	Min.	-298	552.09	13	-322.51	13	-4791.23	19	-1036.75	18	-2361.18	18	313.85	21	-4470.79	18	5953.36	5
401	Min.	-294	552.09	13	-322.51	13	-4791.23	19	-1036.75	18	-2361.18	18	313.85	21	-4470.79	18	5953.36	5
401	Min.	-327	552.09	13	-322.51	13	-4791.23	19	-1036.75	18	-2361.18	18	313.85	21	-4470.79	18	5953.36	5
401	Min.	-320	552.09	13	-322.51	13	-4791.23	19	-1036.75	18	-2361.18	18	313.85	21	-4470.79	18	5953.36	5
401	Max	-271	2903.78	19	182.68	19	23.05	13	-167.57	9	2724.48	17	-90.17	9	-70.29	9	981.19	19
401	Max	-277	2903.78	19	182.68	19	23.05	13	-167.57	9	2724.48	17	-90.17	9	-70.29	9	981.19	19
401	Max	-248	2903.78	19	182.68	19	23.05	13	-167.57	9	2724.48	17	-90.17	9	-70.29	9	981.19	19
401	Max	-238	2903.78	19	182.68	19	23.05	13	-167.57	9	2724.48	17	-90.17	9	-70.29	9	981.19	19
401	Min.	-271	868.10	13	-217.96	17	-3436.60	19	-1314.80	17	1377.07	5	-476.85	18	-859.88	17	-1850.55	9
401	Min.	-277	868.10	13	-217.96	17	-3436.60	19	-1314.80	17	1377.07	5	-476.85	18	-859.88	17	-1850.55	9
401	Min.	-248	868.10	13	-217.96	17	-3436.60	19	-1314.80	17	1377.07	5	-476.85	18	-859.88	17	-1850.55	9
401	Min.	-238	868.10	13	-217.96	17	-3436.60	19	-1314.80	17	1377.07	5	-476.85	18	-859.88	17	-1850.55	9
401	Max	-271	3085.58	19	3701.63	17	8419.06	19	2285.82	17	2344.55	9	-358.86	1	5156.40	13	1612.77	19
401	Max	-238	3085.58	19	3701.63	17	8419.06	19	2285.82	17	2344.55	9	-358.86	1	5156.40	13	1612.77	19
401	Max	-233	3085.58	19	3701.63	17	8419.06	19	2285.82	17	2344.55	9	-358.86	1	5156.40	13	1612.77	19
401	Max	-256	3085.58	19	3701.63	17	8419.06	19	2285.82	17	2344.55	9	-358.86	1	5156.40	13	1612.77	19
401	Min.	-271	29.76	13	572.36	21	-61.92	13	739.40	21	-1036.17	1	-1630.55	17	-2736.32	19	-264.69	1
401	Min.	-238	29.76	13	572.36	21	-61.92	13	739.40	21	-1036.17	1	-1630.55	17	-2736.32	19	-264.69	1
401	Min.	-233	29.76	13	572.36	21	-61.92	13	739.40	21	-1036.17	1	-1630.55	17	-2736.32	19	-264.69	1
401	Min.	-256	29.76	13	572.36	21	-61.92	13	739.40	21	-1036.17	1	-1630.55	17	-2736.32	19	-264.69	1
401	Max	-233	7544.63	19	1817.95	17	2323.59	17	1674.21	9	619.44	13	740.08	19	-2046.77	5	-1909.81	1
401	Max	-238	7544.63	19	1817.95	17	2323.59	17	1674.21	9	619.44	13	740.08	19	-2046.77	5	-1909.81	1
401	Max	-211	7544.63	19	1817.95	17	2323.59	17	1674.21	9	619.44	13	740.08	19	-2046.77	5	-1909.81	1
401	Max	-193	7544.63	19	1817.95	17	2323.59	17	1674.21	9	619.44	13	740.08	19	-2046.77	5	-1909.81	1
401	Min.	-233	2445.71	9	-2960.14	19	-5021.17	19	-2577.05	1	-78.27	19	-69.39	9	-5314.49	17	-8545.07	9
401	Min.	-238	2445.71	9	-2960.14	19	-5021.17	19	-2577.05	1	-78.27	19	-69.39	9	-5314.49	17	-8545.07	9
401	Min.	-211	2445.71	9	-2960.14	19	-5021.17	19	-2577.05	1	-78.27	19	-69.39	9	-5314.49	17	-8545.07	9
401	Min.	-193	2445.71	9	-2960.14	19	-5021.17	19	-2577.05	1	-78.27	19	-69.39	9	-5314.49	17	-8545.07	9
401	Max	-238	3624.91	19	286.11	13	853.94	17	-148.18	9	2017.54	18	703.61	19	-3267.51	5	1127.66	19
401	Max	-248	3624.91	19	286.11	13	853.94	17	-148.18	9	2017.54	18	703.61	19	-3267.51	5	1127.66	19
401	Max	-219	3624.91	19	286.11	13	853.94	17	-148.18	9	2017.54	18	703.61	19	-3267.51	5	1127.66	19
401	Max	-211	3624.91	19	286.11	13	853.94	17	-148.18	9	2017.54	18	703.61	19	-3267.51	5	1127.66	19
401	Min.	-238	1145.03	9	-2633.93	19	-3646.53	19	-2186.48	19	997.49	5	133.20	13	-6073.63	17	-2255.50	9
401	Min.	-248	1145.03	9	-2633.93	19	-3646.53	19	-2186.48	19	997.49	5	133.20	13	-6073.63	17	-2255.50	9
401	Min.	-219	1145.03	9	-2633.93	19	-3646.53	19	-2186.48	19	997.49	5	133.20	13	-6073.63	17	-2255.50	9
401	Min.	-211	1145.03	9	-2633.93	19	-3646.53	19	-2186.48	19	997.49	5	133.20	13	-6073.63	17	-2255.50	9
401	Max	-211	8171.31	17	702.86	13	4571.99	17	-527.10	9	-1407.12	5	-73.41	19	-8920.89	5	-4178.74	1
401	Max	-219	8171.31	17	702.86	13	4571.99	17	-527.10	9	-1407.12	5	-73.41	19	-8920.89	5	-4178.74	1
401	Max	-192	8171.31	17	702.86	13	4571.99	17	-527.10	9	-1407.12	5	-73.41	19	-8920.89	5	-4178.74	1
401	Max	-193	8171.31	17	702.86	13	4571.99	17	-527.10	9	-1407.12	5	-73.41	19	-8920.89	5	-4178.74	1
401	Min.	-211	2959.36	9	-5733.36	19	-2329.63	19	-3543.33	17	-2664.31	18	-1235.34	17	-18172.20	18	-10211.30	17
401	Min.	-219	2959.36	9	-5733.36	19	-2329.63	19	-3543.33	17	-2664.31	18	-1235.34	17	-18172.20	18	-10211.30	17
401	Min.	-192	2959.36	9	-5733.36	19	-2329.63	19	-3543.33	17	-2664.31	18	-1235.34	17	-18172.20	18	-10211.30	17
401	Min.	-193	2959.36	9	-5733.36	19	-2329.63	19	-3543.33	17	-2664.31	18	-1235.34	17	-18172.20	18	-10211.30	17
401	Max	-192	154.78	13	529.21	19	-1456.71	9	-914.08	5	-1524.90	5	1917.09	17	3860.61	19	15901.90	18

401	Max	-219	154.78	13	529.21	19	-1456.71	9	-914.08	5	-1524.90	5	1917.09	17	3860.61	19	15901.90	18
401	Max	-225	154.78	13	529.21	19	-1456.71	9	-914.08	5	-1524.90	5	1917.09	17	3860.61	19	15901.90	18
401	Max	-209	154.78	13	529.21	19	-1456.71	9	-914.08	5	-1524.90	5	1917.09	17	3860.61	19	15901.90	18
401	Min.	-192	-5240.45	19	27.76	13	-3654.48	17	-1913.76	18	-3354.17	18	901.66	5	1031.08	9	7165.47	1
401	Min.	-219	-5240.45	19	27.76	13	-3654.48	17	-1913.76	18	-3354.17	18	901.66	5	1031.08	9	7165.47	1
401	Min.	-225	-5240.45	19	27.76	13	-3654.48	17	-1913.76	18	-3354.17	18	901.66	5	1031.08	9	7165.47	1
401	Min.	-209	-5240.45	19	27.76	13	-3654.48	17	-1913.76	18	-3354.17	18	901.66	5	1031.08	9	7165.47	1
401	Max	-219	-288.76	13	2759.79	17	1741.87	19	2405.75	18	-1239.62	1	245.90	9	171.01	1	5960.78	18
401	Max	-248	-288.76	13	2759.79	17	1741.87	19	2405.75	18	-1239.62	1	245.90	9	171.01	1	5960.78	18
401	Max	-250	-288.76	13	2759.79	17	1741.87	19	2405.75	18	-1239.62	1	245.90	9	171.01	1	5960.78	18
401	Max	-225	-288.76	13	2759.79	17	1741.87	19	2405.75	18	-1239.62	1	245.90	9	171.01	1	5960.78	18
401	Min.	-219	-2439.02	19	1107.19	9	-152.05	13	1109.34	1	-2580.75	18	-14.07	1	-1680.24	9	2913.11	5
401	Min.	-248	-2439.02	19	1107.19	9	-152.05	13	1109.34	1	-2580.75	18	-14.07	1	-1680.24	9	2913.11	5
401	Min.	-250	-2439.02	19	1107.19	9	-152.05	13	1109.34	1	-2580.75	18	-14.07	1	-1680.24	9	2913.11	5
401	Min.	-225	-2439.02	19	1107.19	9	-152.05	13	1109.34	1	-2580.75	18	-14.07	1	-1680.24	9	2913.11	5
401	Max	-209	1035.06	19	-656.86	1	129.79	19	-650.38	1	1559.90	18	1040.78	18	3459.90	18	161.01	1
401	Max	-225	1035.06	19	-656.86	1	129.79	19	-650.38	1	1559.90	18	1040.78	18	3459.90	18	161.01	1
401	Max	-250	1035.06	19	-656.86	1	129.79	19	-650.38	1	1559.90	18	1040.78	18	3459.90	18	161.01	1
401	Max	-269	1035.06	19	-656.86	1	129.79	19	-650.38	1	1559.90	18	1040.78	18	3459.90	18	161.01	1
401	Min.	-209	72.10	13	-1553.88	17	-666.46	17	-1590.52	18	734.32	5	516.70	5	1675.80	5	-348.88	9
401	Min.	-225	72.10	13	-1553.88	17	-666.46	17	-1590.52	18	734.32	5	516.70	5	1675.80	5	-348.88	9
401	Min.	-250	72.10	13	-1553.88	17	-666.46	17	-1590.52	18	734.32	5	516.70	5	1675.80	5	-348.88	9
401	Min.	-269	72.10	13	-1553.88	17	-666.46	17	-1590.52	18	734.32	5	516.70	5	1675.80	5	-348.88	9
401	Max	-248	606.42	19	557.69	17	1277.28	19	2865.16	18	-100.21	9	-403.38	5	26.31	1	1077.57	19
401	Max	-277	606.42	19	557.69	17	1277.28	19	2865.16	18	-100.21	9	-403.38	5	26.31	1	1077.57	19
401	Max	-269	606.42	19	557.69	17	1277.28	19	2865.16	18	-100.21	9	-403.38	5	26.31	1	1077.57	19
401	Max	-250	606.42	19	557.69	17	1277.28	19	2865.16	18	-100.21	9	-403.38	5	26.31	1	1077.57	19
401	Min.	-248	-296.10	17	233.41	9	200.47	13	1356.19	5	-459.70	18	-821.68	17	-810.60	9	228.35	9
401	Min.	-277	-296.10	17	233.41	9	200.47	13	1356.19	5	-459.70	18	-821.68	17	-810.60	9	228.35	9
401	Min.	-269	-296.10	17	233.41	9	200.47	13	1356.19	5	-459.70	18	-821.68	17	-810.60	9	228.35	9
401	Min.	-250	-296.10	17	233.41	9	200.47	13	1356.19	5	-459.70	18	-821.68	17	-810.60	9	228.35	9
401	Max	-84	-2.14	1	407.26	18	16.89	13	-1651.80	1	743.48	18	96.18	9	-5134.30	1	3189.77	18
401	Max	-77	-2.14	1	407.26	18	16.89	13	-1651.80	1	743.48	18	96.18	9	-5134.30	1	3189.77	18
401	Max	-105	-2.14	1	407.26	18	16.89	13	-1651.80	1	743.48	18	96.18	9	-5134.30	1	3189.77	18
401	Max	-120	-2.14	1	407.26	18	16.89	13	-1651.80	1	743.48	18	96.18	9	-5134.30	1	3189.77	18
401	Min.	-84	-530.95	18	-40.95	13	-761.75	18	-4188.82	18	156.21	1	-281.51	1	-13057.00	18	155.09	1
401	Min.	-77	-530.95	18	-40.95	13	-761.75	18	-4188.82	18	156.21	1	-281.51	1	-13057.00	18	155.09	1
401	Min.	-105	-530.95	18	-40.95	13	-761.75	18	-4188.82	18	156.21	1	-281.51	1	-13057.00	18	155.09	1
401	Min.	-120	-530.95	18	-40.95	13	-761.75	18	-4188.82	18	156.21	1	-281.51	1	-13057.00	18	155.09	1
401	Max	-77	120.25	1	102.67	17	125.23	13	90.83	9	2440.83	18	-266.58	13	128.60	1	3923.95	18
401	Max	-76	120.25	1	102.67	17	125.23	13	90.83	9	2440.83	18	-266.58	13	128.60	1	3923.95	18
401	Max	-103	120.25	1	102.67	17	125.23	13	90.83	9	2440.83	18	-266.58	13	128.60	1	3923.95	18
401	Max	-105	120.25	1	102.67	17	125.23	13	90.83	9	2440.83	18	-266.58	13	128.60	1	3923.95	18
401	Min.	-77	-390.62	9	-398.41	18	-872.36	18	-910.13	18	752.08	1	-628.74	19	-296.70	9	468.17	1
401	Min.	-76	-390.62	9	-398.41	18	-872.36	18	-910.13	18	752.08	1	-628.74	19	-296.70	9	468.17	1
401	Min.	-103	-390.62	9	-398.41	18	-872.36	18	-910.13	18	752.08	1	-628.74	19	-296.70	9	468.17	1
401	Min.	-105	-390.62	9	-398.41	18	-872.36	18	-910.13	18	752.08	1	-628.74	19	-296.70	9	468.17	1
401	Max	-120	956.57	18	86.72	9	458.59	18	-331.73	1	334.15	9	616.85	19	4748.30	18	13663.20	18
401	Max	-105	956.57	18	86.72	9	458.59	18	-331.73	1	334.15	9	616.85	19	4748.30	18	13663.20	18
401	Max	-103	956.57	18	86.72	9	458.59	18	-331.73	1	334.15	9	616.85	19	4748.30	18	13663.20	18
401	Max	-115	956.57	18	86.72	9	458.59	18	-331.73	1	334.15	9	616.85	19	4748.30	18	13663.20	18
401	Min.	-120	-162.73	9	-1406.69	18	-353.13	9	-1266.47	18	-646.76	1	73.43	1	534.95	1	3769.03	1
401	Min.	-105	-162.73	9	-1406.69	18	-353.13	9	-1266.47	18	-646.76	1	73.43	1	534.95	1	3769.03	1
401	Min.	-103	-162.73	9	-1406.69	18	-353.13	9	-1266.47	18	-646.76	1	73.43	1	534.95	1	3769.03	1
401	Min.	-115	-162.73	9	-1406.69	18	-353.13	9	-1266.47	18	-646.76	1	73.43	1	534.95	1	3769.03	1
401	Max	-76	308.18	1	276.84	17	114.91	13	1752.14	9	954.42	18	290.48	1	1592.16	1	3923.19	9
401	Max	-82	308.18	1	276.84	17	114.91	13	1752.14	9	954.42	18	290.48	1	1592.16	1	3923.19	9
401	Max	-115	308.18	1	276.84	17	114.91	13	1752.14	9	954.42	18	290.48	1	1592.16	1	3923.19	9
401	Max	-103	308.18	1	276.84	17	114.91	13	1752.14	9	954.42	18	290.48	1	1592.16	1	3923.19	9
401	Min.	-76	-479.06	9	-799.27	18	-1000.57	18	-888.19	1	133.27	1	-227.97	9	-1313.15	9	-943.94	1
401	Min.	-82	-479.06	9	-799.27	18	-1000.57	18	-888.19	1	133.27	1	-227.97	9	-1313.15	9	-943.94	1
401	Min.	-115	-479.06	9	-799.27	18	-1000.57	18	-888.19	1	133.27	1	-227.97	9	-1313.15	9	-943.94	1
401	Min.	-103	-479.06	9	-799.27	18	-1000.57	18	-888.19	1	133.27	1	-227.97	9	-1313.15	9	-943.94	1
401	Max	-77	-24.13	1	132.16	13	381.45	1	-1747.67	1	-86.28	9	270.00	1	-6602.82	1	-1887.34	1
401	Max	-84	-24.13	1	132.16	13	381.45	1	-1747.67	1	-86.28	9	270.00	1	-6602.82	1	-1887.34	1
401	Max	-37	-24.13	1	132.16	13	381.45	1	-1747.67	1	-86.28	9	270.00	1	-6602.82	1	-1887.34	1
401	Max	-52	-24.13	1	132.16	13	381.45	1	-1747.67	1	-86.28	9	270.00	1	-6602.82	1	-1887.34	1
401	Min.	-77	-332.71	17	-846.69	18	-183.05	18	-4603.62	18	-377.08	18	-324.28	9	-17595.90	18	-6844.88	18
401	Min.	-84	-332.71	17	-846.69	18	-183.05	18	-4603.62	18	-377.08	18	-324.28	9	-17595.90	18	-6844.88	18
401	Min.	-37	-332.71	17	-846.69	18	-183.05	18	-4603.62	18	-377.08	18	-324.28	9	-17595.90	18	-6844.88	18
401	Min.	-52	-332.71	17	-846.69	18	-183.05	18	-4603.62	18	-377.08	18	-324.28	9	-17595.90	18	-6844.88	18
401	Max	-77	46.80	9	207.77	1	422.99	18	665.49	18	612.08	9	-398.29	1	5527.50	18	-583.36	1
401	Max	-52	46.80	9	207.77	1	422.99	18	665.49	18	612.08	9	-398.29	1	5527.50	18	-583.36	1
401	Max	-54	46.80	9	207.77	1	422.99	18	665.49	18	612.08	9	-398.29	1	5527.50	18	-583.36	1
401	Max	-76	46.80	9	207.77	1	422.99	18	665.49	18	612.08	9	-398.29	1	5527.50	18	-583.36	1
401	Min.	-77	-227.85	18	-398.16	18	-234.84	1	-17.64	1	-152.84	1	-1154.46	19	945.06	1	-1843.27	18
401	Min.	-52	-227.85	18	-398.16	18	-234.84	1	-17.64	1	-152.84	1	-1154.46	19	945.06	1	-1843.27	18
401	Min.	-54	-227.85	18	-398.16	18	-234.84	1	-17.64	1	-152.84	1	-1154.46	19	945.06	1	-1843.27	18
401	Min.	-76	-227.85	18	-398.16	18	-234.84	1	-17.64	1	-152.84	1	-1154.46	19	945.06	1	-1843.27	18
401	Max	-54	180.38	1	43.45	13	261.68	1	2089.65	9	997.91	18	354.29	9	1934.90	9	1273.63	9
401	Max	-46	180.38	1	43.45	13	261.68	1	2089.65	9	997.91	18	354.29	9	1934.90	9	1273.63	9
401	Max	-82	180.38	1	43.45	13	261.68	1	2089.65	9	997.91	18	354.29	9	1934.90	9	1273.63	9
401	Max	-76	180.38	1	43.45	13	261.68	1	2089.65	9	997.91	18	354.29	9	1934.90	9	1273.63	9
401	Min.	-54	-276.62	9	-296.27	18	-177.87	9	-524.20	1	-104.58	1	-305.17	1	-501.67	1	-2170.25	1
401	Min.	-46	-276.62	9	-296.27	18	-177.87	9	-524.20	1	-104.58	1	-305.17	1	-501.67	1	-2170.25	1
401	Min.	-82	-276.62	9	-296.27	18	-177.87	9	-524.20	1	-104.58	1	-305.17	1	-501.67	1	-2170.25	1
401	Min.	-76	-276.62	9	-296.27	18	-177.87	9	-524.20	1	-104.58	1	-305.17	1	-501.67	1	-2170.25	1
401	Max	-46	-71.22	1	88.79	13	161.36	1	2508.53	18	-606.29	9	57.43	5	356.38	1	484.06	1
401	Max	-54	-71.22	1	88.79	13	161.36	1	2508.53	18	-606.29	9	57.43	5	356.38	1	484.06	1
401	Max	-24	-71.22	1	88.79	13	161.36	1	2508.53	18	-606.29	9	57.43	5	356.38	1	484.06	1
401	Max	-9	-71.22	1	88.79	13	161.36	1	2508.53	18	-606.29	9	57.43	5	356.38	1	484.06	1
401	Min.	-46	-228.45	17	-417.59	18	-354.64	18	297.15	1	-1646.33	18	-276.81	18	-1030.44	9	-1366.81	9
401	Min.	-54	-228.45	17	-417.59	18	-354.64	18	297.15	1	-1646.33	18	-276.81	18	-1030.44	9	-1366.81	9
401	Min.	-24	-228.45	17	-417.59	18	-354.64	18	297.15	1	-1646.33	18	-276.81	18	-1030.44	9	-1366.81	9
401	Min.	-9	-228.45	17	-417.59	18	-354.64	18	297.15	1	-1646.33	18	-276.81	18	-1030.44	9	-1366.81	9
401	Max	-54	358.29	1	-9.55	9	142.68	1	1458.29	19	-1082.26	5	-300.90	1	-440.52	1	-1769.48	1
401	Max	-52	358.29	1	-9.55	9	142.68	1	1458.29	19	-1082.26	5	-300.90	1	-440.52	1	-1769.48	1
401	Max	-22	358.29	1	-9.55	9	142.68	1	1458.29	19	-1082.26	5	-300.90	1	-440.52	1	-1769.48	1
401	Max	-24	358.29	1	-9.55	9	142.68	1	1458.29	19	-1082.26	5	-300.90	1	-440.52	1	-1769.48	1
401	Min.	-54	-365.07	18	-236.96	19	-261.22	18	286.82	1	-2671.08	19	-1155.12	18	-1404.76	19	-7530.76	18
401	Min.	-52	-365.07	18	-236.96	19	-261.22	18	286.82	1	-2671.08	19	-1155.12	18	-1404.76	19	-7530.76	18
401	Min.	-22	-365.07	18	-236.96	19	-261.22	18	286.82	1	-2671.08	19	-1155.12	18	-1404.76	19	-7530.76	18
401	Min.	-24	-365.07	18	-236.96	19	-261.22	18	286.82	1	-2671.08	19	-1155.12	18	-1404.76	19	-7530.76	18
401	Max	-9	222.46	18	-133.91	13	111.81	18	211.06	9	-695.13	1	2243.69	18	-267.17	1	-1760.01	1
401	Max	-24	222.46	18	-133.91	13	111.81	18	211.06	9	-695.13	1	2243.69	18	-267.17	1	-1760.01	1
401	Max	-22	222.46	18	-133.91	13	111.81	18	211.06	9	-695.13	1	2243.69	18	-267.17	1	-1760.01	1
401	Max	-8	222.46	18	-133.91	13	111.81	18	211.06	9	-695.13	1	2243.69	18	-267.17	1	-1760.01	1
401	Min.	-9	-21.70	13	-473.55	18	-149.25	17	-225.27	1	-2089.76	18	733.54	1	-1642.19	19	-4670.78	18
401	Min.	-24	-21.70	13	-473.55	18	-149.25	17	-225.27	1	-2089.76	18	733.54	1	-1642.19	19	-4670.78	18

401	Min.	-22	-21.70	13	-473.55	18	-149.25	17	-225.27	1	-2089.76	18	733.54	1	-1642.19	19	-4670.78	18
401	Min.	-8	-21.70	13	-473.55	18	-149.25	17	-225.27	1	-2089.76	18	733.54	1	-1642.19	19	-4670.78	18
401	Max	-52	266.66	1	519.64	18	28.05	9	-1171.07	1	-1360.33	5	-648.44	5	13207.20	18	-5739.20	1
401	Max	-37	266.66	1	519.64	18	28.05	9	-1171.07	1	-1360.33	5	-648.44	5	13207.20	18	-5739.20	1
401	Max	-8	266.66	1	519.64	18	28.05	9	-1171.07	1	-1360.33	5	-648.44	5	13207.20	18	-5739.20	1
401	Max	-22	266.66	1	519.64	18	28.05	9	-1171.07	1	-1360.33	5	-648.44	5	13207.20	18	-5739.20	1
401	Min.	-52	-678.91	18	-46.97	13	-300.13	19	-3721.34	18	-3246.07	19	-1510.47	19	4937.24	1	-16821.40	18
401	Min.	-37	-678.91	18	-46.97	13	-300.13	19	-3721.34	18	-3246.07	19	-1510.47	19	4937.24	1	-16821.40	18
401	Min.	-8	-678.91	18	-46.97	13	-300.13	19	-3721.34	18	-3246.07	19	-1510.47	19	4937.24	1	-16821.40	18
401	Min.	-22	-678.91	18	-46.97	13	-300.13	19	-3721.34	18	-3246.07	19	-1510.47	19	4937.24	1	-16821.40	18
401	Max	-46	522.49	1	229.55	9	521.64	1	2761.69	9	1829.54	18	-193.50	9	6922.04	18	2922.37	9
401	Max	-48	522.49	1	229.55	9	521.64	1	2761.69	9	1829.54	18	-193.50	9	6922.04	18	2922.37	9
401	Max	-63	522.49	1	229.55	9	521.64	1	2761.69	9	1829.54	18	-193.50	9	6922.04	18	2922.37	9
401	Max	-82	522.49	1	229.55	9	521.64	1	2761.69	9	1829.54	18	-193.50	9	6922.04	18	2922.37	9
401	Min.	-46	-599.86	18	-635.20	18	-44.55	9	-2493.75	1	256.74	5	-1100.49	18	1166.28	1	-3496.91	1
401	Min.	-48	-599.86	18	-635.20	18	-44.55	9	-2493.75	1	256.74	5	-1100.49	18	1166.28	1	-3496.91	1
401	Min.	-63	-599.86	18	-635.20	18	-44.55	9	-2493.75	1	256.74	5	-1100.49	18	1166.28	1	-3496.91	1
401	Min.	-82	-599.86	18	-635.20	18	-44.55	9	-2493.75	1	256.74	5	-1100.49	18	1166.28	1	-3496.91	1
401	Max	-48	59.78	1	1493.96	17	218.35	1	4550.93	9	2487.21	18	668.24	9	12682.20	18	3792.95	9
401	Max	-50	59.78	1	1493.96	17	218.35	1	4550.93	9	2487.21	18	668.24	9	12682.20	18	3792.95	9
401	Max	-67	59.78	1	1493.96	17	218.35	1	4550.93	9	2487.21	18	668.24	9	12682.20	18	3792.95	9
401	Max	-63	59.78	1	1493.96	17	218.35	1	4550.93	9	2487.21	18	668.24	9	12682.20	18	3792.95	9
401	Min.	-48	-724.05	9	-1052.17	18	-2461.07	18	-5322.57	1	266.10	5	-1559.17	1	3711.26	1	-3387.54	1
401	Min.	-50	-724.05	9	-1052.17	18	-2461.07	18	-5322.57	1	266.10	5	-1559.17	1	3711.26	1	-3387.54	1
401	Min.	-67	-724.05	9	-1052.17	18	-2461.07	18	-5322.57	1	266.10	5	-1559.17	1	3711.26	1	-3387.54	1
401	Min.	-63	-724.05	9	-1052.17	18	-2461.07	18	-5322.57	1	266.10	5	-1559.17	1	3711.26	1	-3387.54	1
401	Max	-63	801.91	1	2472.08	17	580.62	13	5603.88	9	5301.54	18	708.18	1	2073.97	17	6598.57	9
401	Max	-67	801.91	1	2472.08	17	580.62	13	5603.88	9	5301.54	18	708.18	1	2073.97	17	6598.57	9
401	Max	-99	801.91	1	2472.08	17	580.62	13	5603.88	9	5301.54	18	708.18	1	2073.97	17	6598.57	9
401	Max	-82	801.91	1	2472.08	17	580.62	13	5603.88	9	5301.54	18	708.18	1	2073.97	17	6598.57	9
401	Min.	-63	-1215.01	9	1279.82	5	-1373.41	18	-4962.37	1	1604.27	5	-564.78	9	642.55	1	-4024.27	1
401	Min.	-67	-1215.01	9	1279.82	5	-1373.41	18	-4962.37	1	1604.27	5	-564.78	9	642.55	1	-4024.27	1
401	Min.	-99	-1215.01	9	1279.82	5	-1373.41	18	-4962.37	1	1604.27	5	-564.78	9	642.55	1	-4024.27	1
401	Min.	-82	-1215.01	9	1279.82	5	-1373.41	18	-4962.37	1	1604.27	5	-564.78	9	642.55	1	-4024.27	1
401	Max	-99	973.67	18	270.38	1	1.00	1	-305.38	9	2878.10	9	488.01	9	7488.38	19	-5120.14	5
401	Max	-121	973.67	18	270.38	1	1.00	1	-305.38	9	2878.10	9	488.01	9	7488.38	19	-5120.14	5
401	Max	-115	973.67	18	270.38	1	1.00	1	-305.38	9	2878.10	9	488.01	9	7488.38	19	-5120.14	5
401	Max	-82	973.67	18	270.38	1	1.00	1	-305.38	9	2878.10	9	488.01	9	7488.38	19	-5120.14	5
401	Min.	-99	-1028.43	17	-570.21	9	-811.29	9	-1152.97	18	-2930.72	1	-1361.14	1	1643.13	9	-14997.70	18
401	Min.	-121	-1028.43	17	-570.21	9	-811.29	9	-1152.97	18	-2930.72	1	-1361.14	1	1643.13	9	-14997.70	18
401	Min.	-115	-1028.43	17	-570.21	9	-811.29	9	-1152.97	18	-2930.72	1	-1361.14	1	1643.13	9	-14997.70	18
401	Min.	-82	-1028.43	17	-570.21	9	-811.29	9	-1152.97	18	-2930.72	1	-1361.14	1	1643.13	9	-14997.70	18
401	Max	-10	128.88	18	487.85	18	136.84	5	-1390.99	13	-832.30	9	-493.35	13	14579.20	18	-2851.36	9
401	Max	-38	128.88	18	487.85	18	136.84	5	-1390.99	13	-832.30	9	-493.35	13	14579.20	18	-2851.36	9
401	Max	-28	128.88	18	487.85	18	136.84	5	-1390.99	13	-832.30	9	-493.35	13	14579.20	18	-2851.36	9
401	Max	-9	128.88	18	487.85	18	136.84	5	-1390.99	13	-832.30	9	-493.35	13	14579.20	18	-2851.36	9
401	Min.	-10	-81.10	17	-222.72	5	-688.05	18	-3369.17	18	-2157.41	19	-1474.19	18	5021.44	1	-7616.80	18
401	Min.	-38	-81.10	17	-222.72	5	-688.05	18	-3369.17	18	-2157.41	19	-1474.19	18	5021.44	1	-7616.80	18
401	Min.	-28	-81.10	17	-222.72	5	-688.05	18	-3369.17	18	-2157.41	19	-1474.19	18	5021.44	1	-7616.80	18
401	Min.	-9	-81.10	17	-222.72	5	-688.05	18	-3369.17	18	-2157.41	19	-1474.19	18	5021.44	1	-7616.80	18
401	Max	-38	371.53	5	570.60	9	418.12	13	-2015.54	9	-1010.71	1	2059.76	1	31941.80	18	37653.30	18
401	Max	-50	371.53	5	570.60	9	418.12	13	-2015.54	9	-1010.71	1	2059.76	1	31941.80	18	37653.30	18
401	Max	-48	371.53	5	570.60	9	418.12	13	-2015.54	9	-1010.71	1	2059.76	1	31941.80	18	37653.30	18
401	Max	-28	371.53	5	570.60	9	418.12	13	-2015.54	9	-1010.71	1	2059.76	1	31941.80	18	37653.30	18
401	Min.	-38	-6859.41	18	-789.11	1	-954.97	18	-7380.55	18	-3128.91	19	-2179.40	9	11447.10	5	9165.45	5
401	Min.	-50	-6859.41	18	-789.11	1	-954.97	18	-7380.55	18	-3128.91	19	-2179.40	9	11447.10	5	9165.45	5
401	Min.	-48	-6859.41	18	-789.11	1	-954.97	18	-7380.55	18	-3128.91	19	-2179.40	9	11447.10	5	9165.45	5
401	Min.	-28	-6859.41	18	-789.11	1	-954.97	18	-7380.55	18	-3128.91	19	-2179.40	9	11447.10	5	9165.45	5
401	Max	-28	274.12	1	-73.03	20	499.05	18	-681.86	9	1949.98	18	230.76	1	8033.79	18	1466.27	9
401	Max	-48	274.12	1	-73.03	20	499.05	18	-681.86	9	1949.98	18	230.76	1	8033.79	18	1466.27	9
401	Max	-46	274.12	1	-73.03	20	499.05	18	-681.86	9	1949.98	18	230.76	1	8033.79	18	1466.27	9
401	Max	-9	274.12	1	-73.03	20	499.05	18	-681.86	9	1949.98	18	230.76	1	8033.79	18	1466.27	9
401	Min.	-28	-176.22	18	-334.26	17	-15.21	5	-2163.45	18	0.60	1	-732.37	9	3221.02	1	-1593.95	1
401	Min.	-48	-176.22	18	-334.26	17	-15.21	5	-2163.45	18	0.60	1	-732.37	9	3221.02	1	-1593.95	1
401	Min.	-46	-176.22	18	-334.26	17	-15.21	5	-2163.45	18	0.60	1	-732.37	9	3221.02	1	-1593.95	1
401	Min.	-9	-176.22	18	-334.26	17	-15.21	5	-2163.45	18	0.60	1	-732.37	9	3221.02	1	-1593.95	1
401	Max	-274	159.11	19	-141.33	9	648.37	18	1965.33	9	1665.61	17	612.12	1	-433.51	20	1222.49	9
401	Max	-266	159.11	19	-141.33	9	648.37	18	1965.33	9	1665.61	17	612.12	1	-433.51	20	1222.49	9
401	Max	-236	159.11	19	-141.33	9	648.37	18	1965.33	9	1665.61	17	612.12	1	-433.51	20	1222.49	9
401	Max	-241	159.11	19	-141.33	9	648.37	18	1965.33	9	1665.61	17	612.12	1	-433.51	20	1222.49	9
401	Min.	-274	-75.70	9	-858.18	18	-21.27	1	-1224.28	1	609.98	20	-81.16	9	-1525.53	17	-4634.42	18
401	Min.	-266	-75.70	9	-858.18	18	-21.27	1	-1224.28	1	609.98	20	-81.16	9	-1525.53	17	-4634.42	18
401	Min.	-236	-75.70	9	-858.18	18	-21.27	1	-1224.28	1	609.98	20	-81.16	9	-1525.53	17	-4634.42	18
401	Min.	-241	-75.70	9	-858.18	18	-21.27	1	-1224.28	1	609.98	20	-81.16	9	-1525.53	17	-4634.42	18
401	Max	-274	100.50	18	572.36	18	15.41	5	2121.84	19	840.20	9	-24.81	9	632.59	1	-64.63	9
401	Max	-241	100.50	18	572.36	18	15.41	5	2121.84	19	840.20	9	-24.81	9	632.59	1	-64.63	9
401	Max	-243	100.50	18	572.36	18	15.41	5	2121.84	19	840.20	9	-24.81	9	632.59	1	-64.63	9
401	Max	-276	100.50	18	572.36	18	15.41	5	2121.84	19	840.20	9	-24.81	9	632.59	1	-64.63	9
401	Min.	-274	-109.78	5	-253.41	17	-1047.46	18	921.40	1	-468.23	1	-340.36	19	-1814.29	9	-280.47	17
401	Min.	-241	-109.78	5	-253.41	17	-1047.46	18	921.40	1	-468.23	1	-340.36	19	-1814.29	9	-280.47	17
401	Min.	-243	-109.78	5	-253.41	17	-1047.46	18	921.40	1	-468.23	1	-340.36	19	-1814.29	9	-280.47	17
401	Min.	-276	-109.78	5	-253.41	17	-1047.46	18	921.40	1	-468.23	1	-340.36	19	-1814.29	9	-280.47	17
401	Max	-266	1840.46	18	1000.31	17	8549.75	18	4778.57	9	3398.58	17	1064.37	9	1920.11	18	6212.33	9
401	Max	-257	1840.46	18	1000.31	17	8549.75	18	4778.57	9	3398.58	17	1064.37	9	1920.11	18	6212.33	9
401	Max	-235	1840.46	18	1000.31	17	8549.75	18	4778.57	9	3398.58	17	1064.37	9	1920.11	18	6212.33	9
401	Max	-236	1840.46	18	1000.31	17	8549.75	18	4778.57	9	3398.58	17	1064.37	9	1920.11	18	6212.33	9
401	Min.	-266	-398.52	9	-3369.62	18	256.42	1	-4703.87	1	778.31	20	-73.70	1	-1198.36	1	-6846.36	18
401	Min.	-257	-398.52	9	-3369.62	18	256.42	1	-4703.87	1	778.31	20	-73.70	1	-1198.36	1	-6846.36	18
401	Min.	-235	-398.52	9	-3369.62	18	256.42	1	-4703.87	1	778.31	20	-73.70	1	-1198.36	1	-6846.36	18
401	Min.	-236	-398.52	9	-3369.62	18	256.42	1	-4703.87	1	778.31	20	-73.70	1	-1198.36	1	-6846.36	18
401	Max	-204	-1037.57	5	709.20	18	1782.91	18	-2.60	9	914.65	9	1294.20	9	-6048.89	9	10616.80	17
401	Max	-236	-1037.57	5	709.20	18	1782.91	18	-2.60	9	914.65	9	1294.20	9	-6048.89	9	10616.80	17
401	Max	-235	-1037.57	5	709.20	18	1782.91	18	-2.60	9	914.65	9	1294.20	9	-6048.89	9	10616.80	17
401	Max	-196	-1037.57	5	709.20	18	1782.91	18	-2.60	9	914.65	9	1294.20	9	-6048.89	9	10616.80	17
401	Min.	-204	-12656.60	18	52.26	5	-356.95	9	-2322.31	1	-2429.31	18	-1870.29	1	-14495.40	19	3397.05	20
401	Min.	-236	-12656.60	18	52.26	5	-356.95	9	-2322.31	1	-2429.31	18	-1870.29	1	-14495.40	19	3397.05	20
401	Min.	-235	-12656.60	18	52.26	5	-356.95	9	-2322.31	1	-2429.31	18	-1870.29	1	-14495.40	19	3397.05	20
401	Min.	-196	-12656.60	18	52.26	5	-356.95	9	-2322.31	1	-2429.31	18	-1870.29	1	-14495.40	19	3397.05	20
401	Max	-191	1234.95	18	-80.01	1	193.36	1	14.83	13	3114.31	18	154.65	18	3476.65	9	-665.40	9
401	Max	-214	1234.95	18	-80.01	1	193.36	1	14.83	13	3114.31	18	154.65	18	3476.65	9	-665.40	9
401	Max	-216	1234.95	18	-80.01	1	193.36	1	14.83	13	3114.31	18	154.65	18	3476.65	9	-665.40	9
401	Max	-204	1234.95	18	-80.01	1	193.36	1	14.83	13	3114.31	18	154.65	18	3476.65	9	-665.40	9
401	Min.	-191	-244.69	5	-2217.81	18	-1511.02	18	-831.12	18	346.77	1	-414.08	9	453.51	1	-2303.66	18
401	Min.	-214	-244.69	5	-2217.81	18	-1511.02	18	-831.12	18	346.77	1	-414.08	9	453.51	1	-2303.66	18
401	Min.	-216	-244.69	5	-2217.81	18	-1511.02	18	-831.12	18	346.77	1	-414.08	9	453.51	1	-2303.66	18
401	Min.	-204	-244.69	5	-2217.81	18	-1511.02	18	-831.12	18	346.77	1	-414.08	9	453.51	1	-2303.66	18
401	Max	-214	28.50	18	-55.52	1	139.37	5	1188.81	19	826.81	9	1248.84	18	3650.01	19	3671.73	19
401	Max	-243	28.50	18	-55.52	1	139.37	5	1188.81	19	826.81	9	1248.84	18	3650.01	19	3671.73	19
401	Max	-241	28.50	18	-55.52	1	139.37	5	1188.81	19	826.81	9	1248.84	18	3650.01	19	3671.73	19

401	Max	-216	28.50	18	-55.52	1	139.37	5	1188.81	19	826.81	9	1248.84	18	3650.01	19	3671.73	19
401	Min.	-214	-99.52	5	-650.50	18	-1510.07	18	515.17	1	-521.05	1	293.94	1	502.62	1	1529.66	1
401	Min.	-243	-99.52	5	-650.50	18	-1510.07	18	515.17	1	-521.05	1	293.94	1	502.62	1	1529.66	1
401	Min.	-241	-99.52	5	-650.50	18	-1510.07	18	515.17	1	-521.05	1	293.94	1	502.62	1	1529.66	1
401	Min.	-216	-99.52	5	-650.50	18	-1510.07	18	515.17	1	-521.05	1	293.94	1	502.62	1	1529.66	1
401	Max	-216	663.13	18	-7.15	1	141.64	5	497.05	9	2405.13	9	392.47	18	1089.06	9	991.68	9
401	Max	-241	663.13	18	-7.15	1	141.64	5	497.05	9	2405.13	9	392.47	18	1089.06	9	991.68	9
401	Max	-236	663.13	18	-7.15	1	141.64	5	497.05	9	2405.13	9	392.47	18	1089.06	9	991.68	9
401	Max	-204	663.13	18	-7.15	1	141.64	5	497.05	9	2405.13	9	392.47	18	1089.06	9	991.68	9
401	Min.	-216	-319.78	13	-1391.63	18	-1852.54	18	-45.58	1	-660.30	1	-418.49	1	-3199.79	18	-916.78	18
401	Min.	-241	-319.78	13	-1391.63	18	-1852.54	18	-45.58	1	-660.30	1	-418.49	1	-3199.79	18	-916.78	18
401	Min.	-236	-319.78	13	-1391.63	18	-1852.54	18	-45.58	1	-660.30	1	-418.49	1	-3199.79	18	-916.78	18
401	Min.	-204	-319.78	13	-1391.63	18	-1852.54	18	-45.58	1	-660.30	1	-418.49	1	-3199.79	18	-916.78	18
401	Max	-218	124.36	1	67.00	5	1306.66	18	-1355.53	1	-1852.41	1	-636.33	13	-8262.78	1	16924.60	19
401	Max	-214	124.36	1	67.00	5	1306.66	18	-1355.53	1	-1852.41	1	-636.33	13	-8262.78	1	16924.60	19
401	Max	-191	124.36	1	67.00	5	1306.66	18	-1355.53	1	-1852.41	1	-636.33	13	-8262.78	1	16924.60	19
401	Max	-197	124.36	1	67.00	5	1306.66	18	-1355.53	1	-1852.41	1	-636.33	13	-8262.78	1	16924.60	19
401	Min.	-218	-496.56	18	-1076.23	18	-255.57	17	-3175.38	19	-4341.92	19	-2133.15	18	-20326.90	19	5670.41	1
401	Min.	-214	-496.56	18	-1076.23	18	-255.57	17	-3175.38	19	-4341.92	19	-2133.15	18	-20326.90	19	5670.41	1
401	Min.	-191	-496.56	18	-1076.23	18	-255.57	17	-3175.38	19	-4341.92	19	-2133.15	18	-20326.90	19	5670.41	1
401	Min.	-197	-496.56	18	-1076.23	18	-255.57	17	-3175.38	19	-4341.92	19	-2133.15	18	-20326.90	19	5670.41	1
401	Max	-243	75.79	17	-214.60	20	43.06	5	2104.85	19	-1339.84	13	1127.03	18	-642.55	1	-3529.96	1
401	Max	-214	75.79	17	-214.60	20	43.06	5	2104.85	19	-1339.84	13	1127.03	18	-642.55	1	-3529.96	1
401	Max	-218	75.79	17	-214.60	20	43.06	5	2104.85	19	-1339.84	13	1127.03	18	-642.55	1	-3529.96	1
401	Max	-247	75.79	17	-214.60	20	43.06	5	2104.85	19	-1339.84	13	1127.03	18	-642.55	1	-3529.96	1
401	Min.	-243	-464.82	18	-624.15	17	-924.47	18	853.27	1	-2917.62	19	301.92	1	-2919.09	19	-8518.92	19
401	Min.	-214	-464.82	18	-624.15	17	-924.47	18	853.27	1	-2917.62	19	301.92	1	-2919.09	19	-8518.92	19
401	Min.	-218	-464.82	18	-624.15	17	-924.47	18	853.27	1	-2917.62	19	301.92	1	-2919.09	19	-8518.92	19
401	Min.	-247	-464.82	18	-624.15	17	-924.47	18	853.27	1	-2917.62	19	301.92	1	-2919.09	19	-8518.92	19
401	Max	-243	-14.01	20	82.20	18	928.19	18	-666.43	9	3831.28	19	-13.97	1	-304.07	1	101.65	1
401	Max	-247	-14.01	20	82.20	18	928.19	18	-666.43	9	3831.28	19	-13.97	1	-304.07	1	101.65	1
401	Max	-280	-14.01	20	82.20	18	928.19	18	-666.43	9	3831.28	19	-13.97	1	-304.07	1	101.65	1
401	Max	-276	-14.01	20	82.20	18	928.19	18	-666.43	9	3831.28	19	-13.97	1	-304.07	1	101.65	1
401	Min.	-243	-421.65	17	-47.80	5	-12.36	9	-1511.07	19	1624.46	1	-280.63	9	-982.21	18	-1154.77	9
401	Min.	-247	-421.65	17	-47.80	5	-12.36	9	-1511.07	19	1624.46	1	-280.63	9	-982.21	18	-1154.77	9
401	Min.	-280	-421.65	17	-47.80	5	-12.36	9	-1511.07	19	1624.46	1	-280.63	9	-982.21	18	-1154.77	9
401	Min.	-276	-421.65	17	-47.80	5	-12.36	9	-1511.07	19	1624.46	1	-280.63	9	-982.21	18	-1154.77	9
401	Max	-166	-135.07	13	941.07	18	54.51	1	912.78	18	2140.10	9	538.24	1	1964.13	9	-756.12	9
401	Max	-183	-135.07	13	941.07	18	54.51	1	912.78	18	2140.10	9	538.24	1	1964.13	9	-756.12	9
401	Max	-179	-135.07	13	941.07	18	54.51	1	912.78	18	2140.10	9	538.24	1	1964.13	9	-756.12	9
401	Max	-168	-135.07	13	941.07	18	54.51	1	912.78	18	2140.10	9	538.24	1	1964.13	9	-756.12	9
401	Min.	-166	-559.42	18	-319.64	9	-609.35	18	46.74	1	-1111.91	1	-73.50	9	-2770.19	1	-3024.94	19
401	Min.	-183	-559.42	18	-319.64	9	-609.35	18	46.74	1	-1111.91	1	-73.50	9	-2770.19	1	-3024.94	19
401	Min.	-179	-559.42	18	-319.64	9	-609.35	18	46.74	1	-1111.91	1	-73.50	9	-2770.19	1	-3024.94	19
401	Min.	-168	-559.42	18	-319.64	9	-609.35	18	46.74	1	-1111.91	1	-73.50	9	-2770.19	1	-3024.94	19
401	Max	-166	535.35	1	10.71	1	590.28	18	2415.86	9	1176.41	19	239.33	17	30.25	1	3587.89	9
401	Max	-168	535.35	1	10.71	1	590.28	18	2415.86	9	1176.41	19	239.33	17	30.25	1	3587.89	9
401	Max	-141	535.35	1	10.71	1	590.28	18	2415.86	9	1176.41	19	239.33	17	30.25	1	3587.89	9
401	Max	-139	535.35	1	10.71	1	590.28	18	2415.86	9	1176.41	19	239.33	17	30.25	1	3587.89	9
401	Min.	-166	-631.51	18	-766.02	18	-247.99	1	-1298.88	1	282.99	1	109.84	13	-2018.05	18	-1748.19	1
401	Min.	-168	-631.51	18	-766.02	18	-247.99	1	-1298.88	1	282.99	1	109.84	13	-2018.05	18	-1748.19	1
401	Min.	-141	-631.51	18	-766.02	18	-247.99	1	-1298.88	1	282.99	1	109.84	13	-2018.05	18	-1748.19	1
401	Min.	-139	-631.51	18	-766.02	18	-247.99	1	-1298.88	1	282.99	1	109.84	13	-2018.05	18	-1748.19	1
401	Max	-183	151.83	9	-146.35	1	102.43	5	-167.31	9	2657.34	18	-62.23	1	1107.44	9	1885.96	9
401	Max	-191	151.83	9	-146.35	1	102.43	5	-167.31	9	2657.34	18	-62.23	1	1107.44	9	1885.96	9
401	Max	-204	151.83	9	-146.35	1	102.43	5	-167.31	9	2657.34	18	-62.23	1	1107.44	9	1885.96	9
401	Max	-179	151.83	9	-146.35	1	102.43	5	-167.31	9	2657.34	18	-62.23	1	1107.44	9	1885.96	9
401	Min.	-183	-890.62	18	-1542.49	18	-2631.27	18	-975.41	19	38.58	1	-775.59	9	-1319.03	1	-1027.46	1
401	Min.	-191	-890.62	18	-1542.49	18	-2631.27	18	-975.41	19	38.58	1	-775.59	9	-1319.03	1	-1027.46	1
401	Min.	-204	-890.62	18	-1542.49	18	-2631.27	18	-975.41	19	38.58	1	-775.59	9	-1319.03	1	-1027.46	1
401	Min.	-179	-890.62	18	-1542.49	18	-2631.27	18	-975.41	19	38.58	1	-775.59	9	-1319.03	1	-1027.46	1
401	Max	-147	345.14	1	3880.59	17	4658.53	18	6328.04	9	3715.52	18	176.52	1	1764.85	19	3987.63	1
401	Max	-143	345.14	1	3880.59	17	4658.53	18	6328.04	9	3715.52	18	176.52	1	1764.85	19	3987.63	1
401	Max	-165	345.14	1	3880.59	17	4658.53	18	6328.04	9	3715.52	18	176.52	1	1764.85	19	3987.63	1
401	Max	-170	345.14	1	3880.59	17	4658.53	18	6328.04	9	3715.52	18	176.52	1	1764.85	19	3987.63	1
401	Min.	-147	-1425.04	9	1846.24	20	-541.29	5	-6186.45	1	1604.43	9	-370.80	9	654.04	5	-7188.36	9
401	Min.	-143	-1425.04	9	1846.24	20	-541.29	5	-6186.45	1	1604.43	9	-370.80	9	654.04	5	-7188.36	9
401	Min.	-165	-1425.04	9	1846.24	20	-541.29	5	-6186.45	1	1604.43	9	-370.80	9	654.04	5	-7188.36	9
401	Min.	-170	-1425.04	9	1846.24	20	-541.29	5	-6186.45	1	1604.43	9	-370.80	9	654.04	5	-7188.36	9
401	Max	-143	728.70	9	134.10	5	1581.57	18	3616.16	9	1796.91	18	167.65	17	2505.95	18	3551.30	1
401	Max	-141	728.70	9	134.10	5	1581.57	18	3616.16	9	1796.91	18	167.65	17	2505.95	18	3551.30	1
401	Max	-168	728.70	9	134.10	5	1581.57	18	3616.16	9	1796.91	18	167.65	17	2505.95	18	3551.30	1
401	Max	-165	728.70	9	134.10	5	1581.57	18	3616.16	9	1796.91	18	167.65	17	2505.95	18	3551.30	1
401	Min.	-143	-356.55	1	-2054.00	18	-355.08	5	-3285.29	1	765.03	1	21.45	9	796.47	1	-4094.33	9
401	Min.	-141	-356.55	1	-2054.00	18	-355.08	5	-3285.29	1	765.03	1	21.45	9	796.47	1	-4094.33	9
401	Min.	-168	-356.55	1	-2054.00	18	-355.08	5	-3285.29	1	765.03	1	21.45	9	796.47	1	-4094.33	9
401	Min.	-165	-356.55	1	-2054.00	18	-355.08	5	-3285.29	1	765.03	1	21.45	9	796.47	1	-4094.33	9
401	Max	-165	830.92	1	1190.32	18	2098.91	18	4876.53	9	2001.80	18	-316.82	1	-961.50	9	3579.51	1
401	Max	-168	830.92	1	1190.32	18	2098.91	18	4876.53	9	2001.80	18	-316.82	1	-961.50	9	3579.51	1
401	Max	-179	830.92	1	1190.32	18	2098.91	18	4876.53	9	2001.80	18	-316.82	1	-961.50	9	3579.51	1
401	Max	-170	830.92	1	1190.32	18	2098.91	18	4876.53	9	2001.80	18	-316.82	1	-961.50	9	3579.51	1
401	Min.	-165	-761.77	9	501.14	5	-903.98	5	-4637.87	1	557.34	1	-840.00	17	-2618.66	19	-5376.35	9
401	Min.	-168	-761.77	9	501.14	5	-903.98	5	-4637.87	1	557.34	1	-840.00	17	-2618.66	19	-5376.35	9
401	Min.	-179	-761.77	9	501.14	5	-903.98	5	-4637.87	1	557.34	1	-840.00	17	-2618.66	19	-5376.35	9
401	Min.	-170	-761.77	9	501.14	5	-903.98	5	-4637.87	1	557.34	1	-840.00	17	-2618.66	19	-5376.35	9
401	Max	-179	3613.60	18	220.70	18	1060.22	18	-649.73	9	798.98	9	1879.18	1	-7114.00	1	-4744.74	9
401	Max	-204	3613.60	18	220.70	18	1060.22	18	-649.73	9	798.98	9	1879.18	1	-7114.00	1	-4744.74	9
401	Max	-196	3613.60	18	220.70	18	1060.22	18	-649.73	9	798.98	9	1879.18	1	-7114.00	1	-4744.74	9
401	Max	-170	3613.60	18	220.70	18	1060.22	18	-649.73	9	798.98	9	1879.18	1	-7114.00	1	-4744.74	9
401	Min.	-179	-2004.11	13	-93.50	1	-63.62	1	-2244.82	19	-1915.96	1	-1053.46	9	-15270.50	19	-10240.40	18
401	Min.	-204	-2004.11	13	-93.50	1	-63.62	1	-2244.82	19	-1915.96	1	-1053.46	9	-15270.50	19	-10240.40	18
401	Min.	-196	-2004.11	13	-93.50	1	-63.62	1	-2244.82	19	-1915.96	1	-1053.46	9	-15270.50	19	-10240.40	18
401	Min.	-170	-2004.11	13	-93.50	1	-63.62	1	-2244.82	19	-1915.96	1	-1053.46	9	-15270.50	19	-10240.40	18
401	Max	-139	157.41	5	-87.59	13	107.33	18	1563.67	9	-267.92	1	751.53	18	527.33	1	-317.02	9
401	Max	-141	157.41	5	-87.59	13	107.33	18	1563.67	9	-267.92	1	751.53	18	527.33	1	-317.02	9
401	Max	-133	157.41	5	-87.59	13	107.33	18	1563.67	9	-267.92	1	751.53	18	527.33	1	-317.02	9
401	Max	-116	157.41	5	-87.59	13	107.33	18	1563.67	9	-267.92	1	751.53	18	527.33	1	-317.02	9
401	Min.	-139	-1102.29	18	-259.91	19	-167.72	17	-744.49	1	-1174.73	18	233.34	9	-658.71	9	-4319.63	18
401	Min.	-141	-1102.29	18	-259.91	19	-167.72	17	-744.49	1	-1174.73	18	233.34	9	-658.71	9	-4319.63	18
401	Min.	-133	-1102.29	18	-259.91	19	-167.72	17	-744.49	1	-1174.73	18	233.34	9	-658.71	9	-4319.63	18
401	Min.	-116	-1102.29	18	-259.91	19	-167.72	17	-744.49	1	-1174.73	18	233.34	9	-658.71	9	-4319.63	18
401	Max	-141	267.02	1	577.94	5	990.53	18	3443.39	9	682.08	18	1261.69	18	-813.97	1	1768.90	1
401	Max	-143	267.02	1	577.94	5	990.53	18	3443.39	9	682.08	18	1261.69	18	-813.97	1	1768.90	1
401	Max	-135	267.02	1	577.94	5	990.53	18	3443.39	9	682.08	18	1261.69	18	-813.97	1	1768.90	1
401	Max	-133	267.02	1	577.94	5	990.53	18	3443.39	9	682.08	18	1261.69	18	-813.97	1	1768.90	1
401	Min.	-141	-1176.67	18	-2176.97	18	-337.30	1	-2534.70	1	253.62	1	208.16	9	-5691.23	18	-3396.23	9
401	Min.	-143	-1176.67	18	-2176.97	18	-337.30	1	-2534.70	1	253.62	1	208.16	9	-5691.23	18	-3396.23	9
401	Min.	-135	-1176.67	18	-2176.97	18	-337.30	1	-2534.70	1	253.62	1	208.16	9	-5691.23	18	-3396.23	9
401	Min.	-133	-1176.67	18	-2176.97	18	-337.30	1	-2534.70	1	253.62	1	208.16	9	-5691.23	18	-3396.23	9

401	Max	-116	18.76	5	368.36	1	2240.74	18	532.08	9	-109.68	1	1654.87	18	-6657.32	9	469.03	9
401	Max	-133	18.76	5	368.36	1	2240.74	18	532.08	9	-109.68	1	1654.87	18	-6657.32	9	469.03	9
401	Max	-135	18.76	5	368.36	1	2240.74	18	532.08	9	-109.68	1	1654.87	18	-6657.32	9	469.03	9
401	Max	-121	18.76	5	368.36	1	2240.74	18	532.08	9	-109.68	1	1654.87	18	-6657.32	9	469.03	9
401	Min.	-116	-3484.20	18	-1962.95	18	-216.60	9	-2011.58	1	-1917.49	19	625.17	1	-17902.70	18	-2221.41	18
401	Min.	-133	-3484.20	18	-1962.95	18	-216.60	9	-2011.58	1	-1917.49	19	625.17	1	-17902.70	18	-2221.41	18
401	Min.	-135	-3484.20	18	-1962.95	18	-216.60	9	-2011.58	1	-1917.49	19	625.17	1	-17902.70	18	-2221.41	18
401	Min.	-121	-3484.20	18	-1962.95	18	-216.60	9	-2011.58	1	-1917.49	19	625.17	1	-17902.70	18	-2221.41	18
401	Max	-143	1256.81	18	483.05	5	3848.48	18	2670.82	1	-426.77	9	1829.06	1	-7658.60	1	-408.36	1
401	Max	-147	1256.81	18	483.05	5	3848.48	18	2670.82	1	-426.77	9	1829.06	1	-7658.60	1	-408.36	1
401	Max	-121	1256.81	18	483.05	5	3848.48	18	2670.82	1	-426.77	9	1829.06	1	-7658.60	1	-408.36	1
401	Max	-135	1256.81	18	483.05	5	3848.48	18	2670.82	1	-426.77	9	1829.06	1	-7658.60	1	-408.36	1
401	Min.	-143	-415.77	1	-10973.80	18	90.17	9	-4773.82	9	-1070.70	19	-1720.20	9	-16590.90	18	-7669.91	18
401	Min.	-147	-415.77	1	-10973.80	18	90.17	9	-4773.82	9	-1070.70	19	-1720.20	9	-16590.90	18	-7669.91	18
401	Min.	-121	-415.77	1	-10973.80	18	90.17	9	-4773.82	9	-1070.70	19	-1720.20	9	-16590.90	18	-7669.91	18
401	Min.	-135	-415.77	1	-10973.80	18	90.17	9	-4773.82	9	-1070.70	19	-1720.20	9	-16590.90	18	-7669.91	18
401	Max	-191	1070.68	18	122.00	1	128.70	9	-775.96	1	-685.22	5	-490.99	1	-3760.57	1	11035.70	19
401	Max	-183	1070.68	18	122.00	1	128.70	9	-775.96	1	-685.22	5	-490.99	1	-3760.57	1	11035.70	19
401	Max	-181	1070.68	18	122.00	1	128.70	9	-775.96	1	-685.22	5	-490.99	1	-3760.57	1	11035.70	19
401	Max	-197	1070.68	18	122.00	1	128.70	9	-775.96	1	-685.22	5	-490.99	1	-3760.57	1	11035.70	19
401	Min.	-191	-154.90	5	-1244.72	18	-1434.96	18	-2132.34	18	-1315.06	19	-1392.15	19	-12487.30	19	3756.30	1
401	Min.	-183	-154.90	5	-1244.72	18	-1434.96	18	-2132.34	18	-1315.06	19	-1392.15	19	-12487.30	19	3756.30	1
401	Min.	-181	-154.90	5	-1244.72	18	-1434.96	18	-2132.34	18	-1315.06	19	-1392.15	19	-12487.30	19	3756.30	1
401	Min.	-197	-154.90	5	-1244.72	18	-1434.96	18	-2132.34	18	-1315.06	19	-1392.15	19	-12487.30	19	3756.30	1
401	Max	-183	6.87	1	51.99	1	38.51	5	1806.47	18	614.11	9	-310.54	5	-216.74	1	912.00	1
401	Max	-166	6.87	1	51.99	1	38.51	5	1806.47	18	614.11	9	-310.54	5	-216.74	1	912.00	1
401	Max	-162	6.87	1	51.99	1	38.51	5	1806.47	18	614.11	9	-310.54	5	-216.74	1	912.00	1
401	Max	-181	6.87	1	51.99	1	38.51	5	1806.47	18	614.11	9	-310.54	5	-216.74	1	912.00	1
401	Min.	-183	-1052.17	18	-477.20	9	-1482.86	18	401.99	1	-641.18	1	-767.48	19	-3599.82	18	-88.96	9
401	Min.	-166	-1052.17	18	-477.20	9	-1482.86	18	401.99	1	-641.18	1	-767.48	19	-3599.82	18	-88.96	9
401	Min.	-162	-1052.17	18	-477.20	9	-1482.86	18	401.99	1	-641.18	1	-767.48	19	-3599.82	18	-88.96	9
401	Min.	-181	-1052.17	18	-477.20	9	-1482.86	18	401.99	1	-641.18	1	-767.48	19	-3599.82	18	-88.96	9
401	Max	-181	761.61	18	-117.64	1	41.05	9	373.21	19	-1776.35	1	215.30	1	-897.65	1	13952.30	19
401	Max	-162	761.61	18	-117.64	1	41.05	9	373.21	19	-1776.35	1	215.30	1	-897.65	1	13952.30	19
401	Max	-160	761.61	18	-117.64	1	41.05	9	373.21	19	-1776.35	1	215.30	1	-897.65	1	13952.30	19
401	Max	-197	761.61	18	-117.64	1	41.05	9	373.21	19	-1776.35	1	215.30	1	-897.65	1	13952.30	19
401	Min.	-181	-94.95	5	-901.19	18	-1133.08	18	132.07	1	-4247.87	19	-298.85	9	-4437.06	19	5309.16	1
401	Min.	-162	-94.95	5	-901.19	18	-1133.08	18	132.07	1	-4247.87	19	-298.85	9	-4437.06	19	5309.16	1
401	Min.	-160	-94.95	5	-901.19	18	-1133.08	18	132.07	1	-4247.87	19	-298.85	9	-4437.06	19	5309.16	1
401	Min.	-197	-94.95	5	-901.19	18	-1133.08	18	132.07	1	-4247.87	19	-298.85	9	-4437.06	19	5309.16	1
401	Max	-160	-46.92	9	40.25	5	643.00	18	-1698.36	9	192.35	18	280.06	9	-5054.04	1	4327.01	18
401	Max	-162	-46.92	9	40.25	5	643.00	18	-1698.36	9	192.35	18	280.06	9	-5054.04	1	4327.01	18
401	Max	-137	-46.92	9	40.25	5	643.00	18	-1698.36	9	192.35	18	280.06	9	-5054.04	1	4327.01	18
401	Max	-122	-46.92	9	40.25	5	643.00	18	-1698.36	9	192.35	18	280.06	9	-5054.04	1	4327.01	18
401	Min.	-160	-552.00	17	-1003.79	18	-350.69	17	-4192.22	18	-14.52	9	-287.20	1	-13249.40	18	575.26	9
401	Min.	-162	-552.00	17	-1003.79	18	-350.69	17	-4192.22	18	-14.52	9	-287.20	1	-13249.40	18	575.26	9
401	Min.	-137	-552.00	17	-1003.79	18	-350.69	17	-4192.22	18	-14.52	9	-287.20	1	-13249.40	18	575.26	9
401	Min.	-122	-552.00	17	-1003.79	18	-350.69	17	-4192.22	18	-14.52	9	-287.20	1	-13249.40	18	575.26	9
401	Max	-162	91.89	1	-8.81	5	748.38	18	735.86	9	1742.78	19	-334.79	13	75.99	1	2587.62	9
401	Max	-166	91.89	1	-8.81	5	748.38	18	735.86	9	1742.78	19	-334.79	13	75.99	1	2587.62	9
401	Max	-139	91.89	1	-8.81	5	748.38	18	735.86	9	1742.78	19	-334.79	13	75.99	1	2587.62	9
401	Max	-137	91.89	1	-8.81	5	748.38	18	735.86	9	1742.78	19	-334.79	13	75.99	1	2587.62	9
401	Min.	-162	-549.29	18	-229.15	18	-163.83	5	-733.49	1	477.20	1	-1038.78	18	-908.38	18	-222.84	1
401	Min.	-166	-549.29	18	-229.15	18	-163.83	5	-733.49	1	477.20	1	-1038.78	18	-908.38	18	-222.84	1
401	Min.	-139	-549.29	18	-229.15	18	-163.83	5	-733.49	1	477.20	1	-1038.78	18	-908.38	18	-222.84	1
401	Min.	-137	-549.29	18	-229.15	18	-163.83	5	-733.49	1	477.20	1	-1038.78	18	-908.38	18	-222.84	1
401	Max	-137	441.72	9	-87.87	5	1020.09	18	220.69	1	-997.96	5	556.79	9	-1708.57	1	12612.60	18
401	Max	-139	441.72	9	-87.87	5	1020.09	18	220.69	1	-997.96	5	556.79	9	-1708.57	1	12612.60	18
401	Max	-116	441.72	9	-87.87	5	1020.09	18	220.69	1	-997.96	5	556.79	9	-1708.57	1	12612.60	18
401	Max	-122	441.72	9	-87.87	5	1020.09	18	220.69	1	-997.96	5	556.79	9	-1708.57	1	12612.60	18
401	Min.	-137	-742.28	18	-271.53	17	-350.16	17	-306.06	9	-2548.72	18	-207.95	1	-4636.20	18	3009.07	9
401	Min.	-139	-742.28	18	-271.53	17	-350.16	17	-306.06	9	-2548.72	18	-207.95	1	-4636.20	18	3009.07	9
401	Min.	-116	-742.28	18	-271.53	17	-350.16	17	-306.06	9	-2548.72	18	-207.95	1	-4636.20	18	3009.07	9
401	Min.	-122	-742.28	18	-271.53	17	-350.16	17	-306.06	9	-2548.72	18	-207.95	1	-4636.20	18	3009.07	9
401	Max	-197	421.35	18	-484.78	9	-108.18	9	-130.15	9	-599.93	9	2.71	1	11421.80	18	13202.50	19
401	Max	-160	421.35	18	-484.78	9	-108.18	9	-130.15	9	-599.93	9	2.71	1	11421.80	18	13202.50	19
401	Max	-158	421.35	18	-484.78	9	-108.18	9	-130.15	9	-599.93	9	2.71	1	11421.80	18	13202.50	19
401	Max	-189	421.35	18	-484.78	9	-108.18	9	-130.15	9	-599.93	9	2.71	1	11421.80	18	13202.50	19
401	Min.	-197	-187.35	17	-1040.56	17	-464.23	17	-351.96	18	-1546.56	19	-242.10	18	4963.97	1	5294.53	1
401	Min.	-160	-187.35	17	-1040.56	17	-464.23	17	-351.96	18	-1546.56	19	-242.10	18	4963.97	1	5294.53	1
401	Min.	-158	-187.35	17	-1040.56	17	-464.23	17	-351.96	18	-1546.56	19	-242.10	18	4963.97	1	5294.53	1
401	Min.	-189	-187.35	17	-1040.56	17	-464.23	17	-351.96	18	-1546.56	19	-242.10	18	4963.97	1	5294.53	1
401	Max	-197	-455.99	9	146.87	17	-71.09	1	-1168.73	9	-1520.60	1	225.08	9	20923.40	19	17755.60	18
401	Max	-189	-455.99	9	146.87	17	-71.09	1	-1168.73	9	-1520.60	1	225.08	9	20923.40	19	17755.60	18
401	Max	-224	-455.99	9	146.87	17	-71.09	1	-1168.73	9	-1520.60	1	225.08	9	20923.40	19	17755.60	18
401	Max	-218	-455.99	9	146.87	17	-71.09	1	-1168.73	9	-1520.60	1	225.08	9	20923.40	19	17755.60	18
401	Min.	-197	-1209.73	17	-525.23	18	-298.31	18	-2619.71	19	-3543.37	19	-50.14	1	8730.64	1	7680.73	1
401	Min.	-189	-1209.73	17	-525.23	18	-298.31	18	-2619.71	19	-3543.37	19	-50.14	1	8730.64	1	7680.73	1
401	Min.	-224	-1209.73	17	-525.23	18	-298.31	18	-2619.71	19	-3543.37	19	-50.14	1	8730.64	1	7680.73	1
401	Min.	-218	-1209.73	17	-525.23	18	-298.31	18	-2619.71	19	-3543.37	19	-50.14	1	8730.64	1	7680.73	1
401	Max	-189	374.55	17	-540.20	9	-33.65	20	276.35	18	5030.42	18	189.37	19	-549.21	9	109.69	1
401	Max	-158	374.55	17	-540.20	9	-33.65	20	276.35	18	5030.42	18	189.37	19	-549.21	9	109.69	1
401	Max	-156	374.55	17	-540.20	9	-33.65	20	276.35	18	5030.42	18	189.37	19	-549.21	9	109.69	1
401	Max	-187	374.55	17	-540.20	9	-33.65	20	276.35	18	5030.42	18	189.37	19	-549.21	9	109.69	1
401	Min.	-189	33.59	20	-1278.54	17	-272.36	17	62.05	1	1992.03	1	13.28	9	-1272.74	19	-299.24	18
401	Min.	-158	33.59	20	-1278.54	17	-272.36	17	62.05	1	1992.03	1	13.28	9	-1272.74	19	-299.24	18
401	Min.	-156	33.59	20	-1278.54	17	-272.36	17	62.05	1	1992.03	1	13.28	9	-1272.74	19	-299.24	18
401	Min.	-187	33.59	20	-1278.54	17	-272.36	17	62.05	1	1992.03	1	13.28	9	-1272.74	19	-299.24	18
401	Max	-189	-438.51	9	138.31	18	187.57	17	5635.48	18	-141.74	13	759.74	18	-248.91	9	-123.17	13
401	Max	-187	-438.51	9	138.31	18	187.57	17	5635.48	18	-141.74	13	759.74	18	-248.91	9	-123.17	13
401	Max	-222	-438.51	9	138.31	18	187.57	17	5635.48	18	-141.74	13	759.74	18	-248.91	9	-123.17	13
401	Max	-224	-438.51	9	138.31	18	187.57	17	5635.48	18	-141.74	13	759.74	18	-248.91	9	-123.17	13
401	Min.	-189	-1066.08	17	-8.67	5	-84.81	18	2256.01	1	-269.77	17	281.38	5	-796.54	19	-259.84	19
401	Min.	-187	-1066.08	17	-8.67	5	-84.81	18	2256.01	1	-269.77	17	281.38	5	-796.54	19	-259.84	19
401	Min.	-222	-1066.08	17	-8.67	5	-84.81	18	2256.01	1	-269.77	17	281.38	5	-796.54	19	-259.84	19
401	Min.	-224	-1066.08	17	-8.67	5	-84.81	18	2256.01	1	-269.77	17	281.38	5	-796.54	19	-259.84	19
401	Max	-264	-210.89	20	54.67	17	124.82	17	1871.04	18	2526.65	19	407.53	18	-1058.04	1	-1692.65	1
401	Max	-268	-210.89	20	54.67	17	124.82	17	1871.04	18	2526.65	19	407.53	18	-1058.04	1	-1692.65	1
401	Max	-245	-210.89	20	54.67	17	124.82	17	1871.04	18	2526.65	19	407.53	18	-1058.04	1	-1692.65	1
401	Max	-224	-210.89	20	54.67	17	124.82	17	1871.04	18	2526.65	19	407.53	18	-1058.04	1	-1692.65	1
401	Min.	-264	-783.50	17	-38.33	18	-40.83	18	455.39	1	1083.08	9	135.57	1	-2471.02	19	-3954.59	18
401	Min.	-268	-783.50	17	-38.33	18	-40.83	18	455.39	1	1083.08	9	135.57	1	-2471.02	19	-3954.59	18
401	Min.	-245	-783.50	17	-38.33	18	-40.83	18	455.39	1	1083.08	9	135.57	1	-2471.02	19	-3954.59	18
401	Min.	-224	-783.50	17	-38.33	18	-40.83	18	455.39	1	1083.08	9	135.57	1	-2471.02	19	-3954.59	18
401	Max	-268	-198.84	20	186.68	18	266.50	18	-464.64	13	4090.19	19	-627.50	1	-217.60	9	-759.08	1
401	Max	-280	-198.84	20	186.68	18	266.50	18	-464.64	13	4090.19	19	-627.50	1	-217.60	9	-759.08	1
401	Max	-247	-198.84	20	186.68	18	266.50	18	-464.64	13	4090.19	19	-627.50	1	-217.60	9	-759.08	1
401	Max	-245	-198.84	20	186.68	18	266.50	18	-464.64	13	4090.19	19	-627.50	1	-217.60	9	-759.08	1
401	Min.	-268	-647.57	17	-15.10	9	-28.70	9	-968.00	19	1750.89	1	-1616.27	19	-622.94	19	-2447.62	18

401	Min.	-280	-647.57	17	-15.10	9	-28.70	9	-968.00	19	1750.89	1	-1616.27	19	-622.94	19	-2447.62	18
401	Min.	-247	-647.57	17	-15.10	9	-28.70	9	-968.00	19	1750.89	1	-1616.27	19	-622.94	19	-2447.62	18
401	Min.	-245	-647.57	17	-15.10	9	-28.70	9	-968.00	19	1750.89	1	-1616.27	19	-622.94	19	-2447.62	18
401	Max	-245	-236.74	20	56.05	17	180.68	19	-179.04	9	3510.88	19	801.22	19	-3812.25	1	-1854.38	1
401	Max	-247	-236.74	20	56.05	17	180.68	19	-179.04	9	3510.88	19	801.22	19	-3812.25	1	-1854.38	1
401	Max	-218	-236.74	20	56.05	17	180.68	19	-179.04	9	3510.88	19	801.22	19	-3812.25	1	-1854.38	1
401	Max	-224	-236.74	20	56.05	17	180.68	19	-179.04	9	3510.88	19	801.22	19	-3812.25	1	-1854.38	1
401	Min.	-245	-723.80	17	-352.28	18	11.84	9	-648.85	17	1440.63	1	346.37	1	-9018.17	19	-4598.56	18
401	Min.	-247	-723.80	17	-352.28	18	11.84	9	-648.85	17	1440.63	1	346.37	1	-9018.17	19	-4598.56	18
401	Min.	-218	-723.80	17	-352.28	18	11.84	9	-648.85	17	1440.63	1	346.37	1	-9018.17	19	-4598.56	18
401	Min.	-224	-723.80	17	-352.28	18	11.84	9	-648.85	17	1440.63	1	346.37	1	-9018.17	19	-4598.56	18
401	Max	-224	-453.36	9	198.97	18	103.77	17	4457.38	18	2053.46	19	255.40	18	1987.92	19	1307.22	18
401	Max	-222	-453.36	9	198.97	18	103.77	17	4457.38	18	2053.46	19	255.40	18	1987.92	19	1307.22	18
401	Max	-253	-453.36	9	198.97	18	103.77	17	4457.38	18	2053.46	19	255.40	18	1987.92	19	1307.22	18
401	Max	-264	-453.36	9	198.97	18	103.77	17	4457.38	18	2053.46	19	255.40	18	1987.92	19	1307.22	18
401	Min.	-224	-1088.78	17	65.88	5	-97.10	18	1652.99	5	899.15	13	68.65	5	906.87	13	503.46	1
401	Min.	-222	-1088.78	17	65.88	5	-97.10	18	1652.99	5	899.15	13	68.65	5	906.87	13	503.46	1
401	Min.	-253	-1088.78	17	65.88	5	-97.10	18	1652.99	5	899.15	13	68.65	5	906.87	13	503.46	1
401	Min.	-264	-1088.78	17	65.88	5	-97.10	18	1652.99	5	899.15	13	68.65	5	906.87	13	503.46	1
401	Max	-158	-483.46	1	78.00	5	-52.60	1	-622.94	1	-66.19	13	1.26	9	-4373.63	1	-5384.98	9
401	Max	-160	-483.46	1	78.00	5	-52.60	1	-622.94	1	-66.19	13	1.26	9	-4373.63	1	-5384.98	9
401	Max	-122	-483.46	1	78.00	5	-52.60	1	-622.94	1	-66.19	13	1.26	9	-4373.63	1	-5384.98	9
401	Max	-131	-483.46	1	78.00	5	-52.60	1	-622.94	1	-66.19	13	1.26	9	-4373.63	1	-5384.98	9
401	Min.	-158	-1102.98	17	-584.02	18	-333.95	17	-1475.62	19	-159.77	19	-356.29	18	-11161.40	18	-12459.40	19
401	Min.	-160	-1102.98	17	-584.02	18	-333.95	17	-1475.62	19	-159.77	19	-356.29	18	-11161.40	18	-12459.40	19
401	Min.	-122	-1102.98	17	-584.02	18	-333.95	17	-1475.62	19	-159.77	19	-356.29	18	-11161.40	18	-12459.40	19
401	Min.	-131	-1102.98	17	-584.02	18	-333.95	17	-1475.62	19	-159.77	19	-356.29	18	-11161.40	18	-12459.40	19
401	Max	-158	351.22	18	-621.47	1	490.22	18	947.98	19	5598.05	18	232.06	17	707.03	18	2205.75	19
401	Max	-131	351.22	18	-621.47	1	490.22	18	947.98	19	5598.05	18	232.06	17	707.03	18	2205.75	19
401	Max	-129	351.22	18	-621.47	1	490.22	18	947.98	19	5598.05	18	232.06	17	707.03	18	2205.75	19
401	Max	-156	351.22	18	-621.47	1	490.22	18	947.98	19	5598.05	18	232.06	17	707.03	18	2205.75	19
401	Min.	-158	45.74	5	-1531.70	17	97.36	1	396.24	9	2252.38	1	77.57	9	279.62	5	1037.36	9
401	Min.	-131	45.74	5	-1531.70	17	97.36	1	396.24	9	2252.38	1	77.57	9	279.62	5	1037.36	9
401	Min.	-129	45.74	5	-1531.70	17	97.36	1	396.24	9	2252.38	1	77.57	9	279.62	5	1037.36	9
401	Min.	-156	45.74	5	-1531.70	17	97.36	1	396.24	9	2252.38	1	77.57	9	279.62	5	1037.36	9
401	Max	-177	-149.36	9	-1362.37	9	2623.75	18	4439.69	19	-76.69	9	56.20	5	4848.08	17	2519.06	18
401	Max	-154	-149.36	9	-1362.37	9	2623.75	18	4439.69	19	-76.69	9	56.20	5	4848.08	17	2519.06	18
401	Max	-152	-149.36	9	-1362.37	9	2623.75	18	4439.69	19	-76.69	9	56.20	5	4848.08	17	2519.06	18
401	Max	-175	-149.36	9	-1362.37	9	2623.75	18	4439.69	19	-76.69	9	56.20	5	4848.08	17	2519.06	18
401	Min.	-177	-938.97	18	-3530.42	17	-371.33	5	1908.91	9	-2091.60	19	-628.23	18	947.18	9	1048.03	1
401	Min.	-154	-938.97	18	-3530.42	17	-371.33	5	1908.91	9	-2091.60	19	-628.23	18	947.18	9	1048.03	1
401	Min.	-152	-938.97	18	-3530.42	17	-371.33	5	1908.91	9	-2091.60	19	-628.23	18	947.18	9	1048.03	1
401	Min.	-175	-938.97	18	-3530.42	17	-371.33	5	1908.91	9	-2091.60	19	-628.23	18	947.18	9	1048.03	1
401	Max	-177	-3246.51	9	2076.62	18	2290.50	17	-1538.94	9	-1500.01	1	-494.36	13	-12058.10	9	30453.30	19
401	Max	-175	-3246.51	9	2076.62	18	2290.50	17	-1538.94	9	-1500.01	1	-494.36	13	-12058.10	9	30453.30	19
401	Max	-202	-3246.51	9	2076.62	18	2290.50	17	-1538.94	9	-1500.01	1	-494.36	13	-12058.10	9	30453.30	19
401	Max	-198	-3246.51	9	2076.62	18	2290.50	17	-1538.94	9	-1500.01	1	-494.36	13	-12058.10	9	30453.30	19
401	Min.	-177	-8564.35	17	-213.98	5	-2941.90	18	-4061.27	19	-3291.39	19	-1714.20	19	-27487.90	19	13198.00	9
401	Min.	-175	-8564.35	17	-213.98	5	-2941.90	18	-4061.27	19	-3291.39	19	-1714.20	19	-27487.90	19	13198.00	9
401	Min.	-202	-8564.35	17	-213.98	5	-2941.90	18	-4061.27	19	-3291.39	19	-1714.20	19	-27487.90	19	13198.00	9
401	Min.	-198	-8564.35	17	-213.98	5	-2941.90	18	-4061.27	19	-3291.39	19	-1714.20	19	-27487.90	19	13198.00	9
401	Max	-175	-77.45	9	-2488.30	1	3944.93	18	2227.91	18	7547.18	17	157.70	5	12657.80	17	-51.98	13
401	Max	-152	-77.45	9	-2488.30	1	3944.93	18	2227.91	18	7547.18	17	157.70	5	12657.80	17	-51.98	13
401	Max	-148	-77.45	9	-2488.30	1	3944.93	18	2227.91	18	7547.18	17	157.70	5	12657.80	17	-51.98	13
401	Max	-171	-77.45	9	-2488.30	1	3944.93	18	2227.91	18	7547.18	17	157.70	5	12657.80	17	-51.98	13
401	Min.	-175	-1966.71	18	-6385.98	17	-472.10	5	890.32	9	1689.66	9	-142.32	18	4519.79	9	-536.82	5
401	Min.	-152	-1966.71	18	-6385.98	17	-472.10	5	890.32	9	1689.66	9	-142.32	18	4519.79	9	-536.82	5
401	Min.	-148	-1966.71	18	-6385.98	17	-472.10	5	890.32	9	1689.66	9	-142.32	18	4519.79	9	-536.82	5
401	Min.	-171	-1966.71	18	-6385.98	17	-472.10	5	890.32	9	1689.66	9	-142.32	18	4519.79	9	-536.82	5
401	Max	-175	-2368.94	20	357.11	17	581.05	5	9232.41	17	501.54	17	376.22	17	402.14	5	15056.10	17
401	Max	-171	-2368.94	20	357.11	17	581.05	5	9232.41	17	501.54	17	376.22	17	402.14	5	15056.10	17
401	Max	-199	-2368.94	20	357.11	17	581.05	5	9232.41	17	501.54	17	376.22	17	402.14	5	15056.10	17
401	Max	-202	-2368.94	20	357.11	17	581.05	5	9232.41	17	501.54	17	376.22	17	402.14	5	15056.10	17
401	Min.	-175	-7112.58	17	-2629.32	18	-3985.70	18	2685.64	9	-108.33	19	77.23	1	-1171.23	18	5667.13	9
401	Min.	-171	-7112.58	17	-2629.32	18	-3985.70	18	2685.64	9	-108.33	19	77.23	1	-1171.23	18	5667.13	9
401	Min.	-199	-7112.58	17	-2629.32	18	-3985.70	18	2685.64	9	-108.33	19	77.23	1	-1171.23	18	5667.13	9
401	Min.	-202	-7112.58	17	-2629.32	18	-3985.70	18	2685.64	9	-108.33	19	77.23	1	-1171.23	18	5667.13	9
401	Max	-187	975.41	17	1878.97	18	2112.64	17	-2754.99	9	-2023.19	9	2154.27	19	-9603.41	9	-14810.60	9
401	Max	-177	975.41	17	1878.97	18	2112.64	17	-2754.99	9	-2023.19	9	2154.27	19	-9603.41	9	-14810.60	9
401	Max	-198	975.41	17	1878.97	18	2112.64	17	-2754.99	9	-2023.19	9	2154.27	19	-9603.41	9	-14810.60	9
401	Max	-206	975.41	17	1878.97	18	2112.64	17	-2754.99	9	-2023.19	9	2154.27	19	-9603.41	9	-14810.60	9
401	Min.	-187	352.81	9	-18.50	5	775.08	9	-6076.41	19	-4608.56	19	1023.26	9	-22081.30	19	-34131.60	19
401	Min.	-177	352.81	9	-18.50	5	775.08	9	-6076.41	19	-4608.56	19	1023.26	9	-22081.30	19	-34131.60	19
401	Min.	-198	352.81	9	-18.50	5	775.08	9	-6076.41	19	-4608.56	19	1023.26	9	-22081.30	19	-34131.60	19
401	Min.	-206	352.81	9	-18.50	5	775.08	9	-6076.41	19	-4608.56	19	1023.26	9	-22081.30	19	-34131.60	19
401	Max	-187	-352.48	5	278.94	17	185.78	17	111.76	18	1436.67	19	-819.93	1	15134.40	19	-4049.41	9
401	Max	-206	-352.48	5	278.94	17	185.78	17	111.76	18	1436.67	19	-819.93	1	15134.40	19	-4049.41	9
401	Max	-228	-352.48	5	278.94	17	185.78	17	111.76	18	1436.67	19	-819.93	1	15134.40	19	-4049.41	9
401	Max	-222	-352.48	5	278.94	17	185.78	17	111.76	18	1436.67	19	-819.93	1	15134.40	19	-4049.41	9
401	Min.	-187	-1296.74	18	119.04	5	15.00	20	-546.21	17	569.03	9	-2015.68	19	6632.92	9	-9320.44	19
401	Min.	-206	-1296.74	18	119.04	5	15.00	20	-546.21	17	569.03	9	-2015.68	19	6632.92	9	-9320.44	19
401	Min.	-228	-1296.74	18	119.04	5	15.00	20	-546.21	17	569.03	9	-2015.68	19	6632.92	9	-9320.44	19
401	Min.	-222	-1296.74	18	119.04	5	15.00	20	-546.21	17	569.03	9	-2015.68	19	6632.92	9	-9320.44	19
401	Max	-230	-2391.04	9	352.96	17	489.27	5	-19.59	9	-227.90	5	3146.57	18	-5581.59	13	-7816.36	9
401	Max	-232	-2391.04	9	352.96	17	489.27	5	-19.59	9	-227.90	5	3146.57	18	-5581.59	13	-7816.36	9
401	Max	-208	-2391.04	9	352.96	17	489.27	5	-19.59	9	-227.90	5	3146.57	18	-5581.59	13	-7816.36	9
401	Max	-202	-2391.04	9	352.96	17	489.27	5	-19.59	9	-227.90	5	3146.57	18	-5581.59	13	-7816.36	9
401	Min.	-230	-6060.28	17	-688.51	18	-4803.65	18	-1991.30	19	-1073.91	18	1269.26	1	-12869.70	19	-18770.60	19
401	Min.	-232	-6060.28	17	-688.51	18	-4803.65	18	-1991.30	19	-1073.91	18	1269.26	1	-12869.70	19	-18770.60	19
401	Min.	-208	-6060.28	17	-688.51	18	-4803.65	18	-1991.30	19	-1073.91	18	1269.26	1	-12869.70	19	-18770.60	19
401	Min.	-202	-6060.28	17	-688.51	18	-4803.65	18	-1991.30	19	-1073.91	18	1269.26	1	-12869.70	19	-18770.60	19
401	Max	-232	-1021.28	20	855.84	17	99.38	5	-3078.56	13	-103.85	5	721.65	18	-9594.84	9	-144.60	18
401	Max	-228	-1021.28	20	855.84	17	99.38	5	-3078.56	13	-103.85	5	721.65	18	-9594.84	9	-144.60	18
401	Max	-206	-1021.28	20	855.84	17	99.38	5	-3078.56	13	-103.85	5	721.65	18	-9594.84	9	-144.60	18
401	Max	-208	-1021.28	20	855.84	17	99.38	5	-3078.56	13	-103.85	5	721.65	18	-9594.84	9	-144.60	18
401	Min.	-232	-2663.19	17	-1274.05	18	-1175.75	18	-6934.52	19	-760.84	18	119.66	5	-21948.80	19	-2637.01	17
401	Min.	-228	-2663.19	17	-1274.05	18	-1175.75	18	-6934.52	19	-760.84	18	119.66	5	-21948.80	19	-2637.01	17
401	Min.	-206	-2663.19	17	-1274.05	18	-1175.75	18	-6934.52	19	-760.84	18	119.66	5	-21948.80	19	-2637.01	17
401	Min.	-208	-2663.19	17	-1274.05	18	-1175.75	18	-6934.52	19	-760.84	18	119.66	5	-21948.80	19	-2637.01	17
401	Max	-208	-3117.19	1	3567.38	17	16.19	5	-3500.48	13	-3864.02	9	2604.28	18	-23040.20	9	-15869.10	9
401	Max	-206	-3117.19	1	3567.38	17	16.19	5	-3500.48	13	-3864.02	9	2604.28	18	-23040.20	9	-15869.10	9
401	Max	-198	-3117.19	1	3567.38	17	16.19	5	-3500.48	13	-3864.02	9	2604.28	18	-23040.20	9	-15869.10	9
401	Max	-202	-3117.19	1	3567.38	17	16.19	5	-3500.48	13	-3864.02	9	2604.28	18	-23040.20	9	-15869.10	9
401	Min.	-208	-8828.61	18	-1083.19	18	-5112.95	18	-7893.36	19	-9015.96	19	452.84	5	-52981.90	19	-36479.50	19
401	Min.	-206	-8828.61	18	-1083.19	18	-5112.95	18	-7893.36	19	-9015.96	19	452.84	5	-52981.90	19	-36479.50	19
401	Min.	-198	-8828.61	18	-1083.19	18	-5112.95	18	-7893.36	19	-9015.96	19	452.84	5	-52981.90	19	-36479.50	19
401	Min.	-202	-8828.61	18	-1083.19	18	-5112.95	18	-7893.36	19	-9015.96	19	452.84	5	-52981.90	19	-36479.50	19
401	Max	-187	559.14	17	-1301.02	9	501.89	18	2954.99	18	-333.68	20	-189.98	5	-1370.49	1	3870.31	19
401	Max	-156	559.14	17	-1301.02	9	501.89	18	2954.99	18	-333.68	20	-189.98	5	-1370.49	1	3870.31	19

401	Max	-154	559.14	17	-1301.02	9	501.89	18	2954.99	18	-333.68	20	-189.98	5	-1370.49	1	3870.31	19
401	Max	-177	559.14	17	-1301.02	9	501.89	18	2954.99	18	-333.68	20	-189.98	5	-1370.49	1	3870.31	19
401	Min.	-187	208.28	1	-3393.20	17	-106.34	5	1260.43	9	-1031.39	17	-718.77	18	-4414.48	18	1700.64	9
401	Min.	-156	208.28	1	-3393.20	17	-106.34	5	1260.43	9	-1031.39	17	-718.77	18	-4414.48	18	1700.64	9
401	Min.	-154	208.28	1	-3393.20	17	-106.34	5	1260.43	9	-1031.39	17	-718.77	18	-4414.48	18	1700.64	9
401	Min.	-177	208.28	1	-3393.20	17	-106.34	5	1260.43	9	-1031.39	17	-718.77	18	-4414.48	18	1700.64	9
401	Max	-262	-1028.14	20	213.23	17	965.28	17	-1142.83	13	4382.59	19	797.23	19	-2624.56	13	1720.53	18
401	Max	-255	-1028.14	20	213.23	17	965.28	17	-1142.83	13	4382.59	19	797.23	19	-2624.56	13	1720.53	18
401	Max	-228	-1028.14	20	213.23	17	965.28	17	-1142.83	13	4382.59	19	797.23	19	-2624.56	13	1720.53	18
401	Max	-232	-1028.14	20	213.23	17	965.28	17	-1142.83	13	4382.59	19	797.23	19	-2624.56	13	1720.53	18
401	Min.	-262	-2557.61	17	59.14	20	-792.01	18	-2809.40	19	1859.65	13	416.43	13	-5932.32	19	-830.30	1
401	Min.	-255	-2557.61	17	59.14	20	-792.01	18	-2809.40	19	1859.65	13	416.43	13	-5932.32	19	-830.30	1
401	Min.	-228	-2557.61	17	59.14	20	-792.01	18	-2809.40	19	1859.65	13	416.43	13	-5932.32	19	-830.30	1
401	Min.	-232	-2557.61	17	59.14	20	-792.01	18	-2809.40	19	1859.65	13	416.43	13	-5932.32	19	-830.30	1
401	Max	-262	523.50	18	-1368.66	20	2598.69	18	4246.85	19	1094.51	1	-285.00	13	8257.94	17	-1004.28	9
401	Max	-232	523.50	18	-1368.66	20	2598.69	18	4246.85	19	1094.51	1	-285.00	13	8257.94	17	-1004.28	9
401	Max	-230	523.50	18	-1368.66	20	2598.69	18	4246.85	19	1094.51	1	-285.00	13	8257.94	17	-1004.28	9
401	Max	-260	523.50	18	-1368.66	20	2598.69	18	4246.85	19	1094.51	1	-285.00	13	8257.94	17	-1004.28	9
401	Min.	-262	-70.28	5	-3824.06	17	-1045.49	17	1742.74	13	-515.08	9	-564.26	18	2725.67	9	-3217.58	19
401	Min.	-232	-70.28	5	-3824.06	17	-1045.49	17	1742.74	13	-515.08	9	-564.26	18	2725.67	9	-3217.58	19
401	Min.	-230	-70.28	5	-3824.06	17	-1045.49	17	1742.74	13	-515.08	9	-564.26	18	2725.67	9	-3217.58	19
401	Min.	-260	-70.28	5	-3824.06	17	-1045.49	17	1742.74	13	-515.08	9	-564.26	18	2725.67	9	-3217.58	19
401	Max	-255	-676.60	20	434.51	17	193.22	17	1885.81	18	3365.10	19	-281.55	13	-1386.01	9	5104.63	18
401	Max	-253	-676.60	20	434.51	17	193.22	17	1885.81	18	3365.10	19	-281.55	13	-1386.01	9	5104.63	18
401	Max	-222	-676.60	20	434.51	17	193.22	17	1885.81	18	3365.10	19	-281.55	13	-1386.01	9	5104.63	18
401	Max	-228	-676.60	20	434.51	17	193.22	17	1885.81	18	3365.10	19	-281.55	13	-1386.01	9	5104.63	18
401	Min.	-255	-1656.98	17	172.13	1	-162.94	18	283.03	5	1443.42	9	-694.28	19	-3100.91	19	1981.52	1
401	Min.	-253	-1656.98	17	172.13	1	-162.94	18	283.03	5	1443.42	9	-694.28	19	-3100.91	19	1981.52	1
401	Min.	-222	-1656.98	17	172.13	1	-162.94	18	283.03	5	1443.42	9	-694.28	19	-3100.91	19	1981.52	1
401	Min.	-228	-1656.98	17	172.13	1	-162.94	18	283.03	5	1443.42	9	-694.28	19	-3100.91	19	1981.52	1
401	Max	-230	20.68	5	-1668.88	20	5628.73	18	1375.49	17	8528.72	17	-1006.75	9	13577.60	17	-1953.50	13
401	Max	-202	20.68	5	-1668.88	20	5628.73	18	1375.49	17	8528.72	17	-1006.75	9	13577.60	17	-1953.50	13
401	Max	-199	20.68	5	-1668.88	20	5628.73	18	1375.49	17	8528.72	17	-1006.75	9	13577.60	17	-1953.50	13
401	Max	-237	20.68	5	-1668.88	20	5628.73	18	1375.49	17	8528.72	17	-1006.75	9	13577.60	17	-1953.50	13
401	Min.	-230	-2639.41	18	-6781.41	17	190.30	5	278.60	9	2257.01	9	-2644.86	18	4586.98	9	-5575.66	17
401	Min.	-202	-2639.41	18	-6781.41	17	190.30	5	278.60	9	2257.01	9	-2644.86	18	4586.98	9	-5575.66	17
401	Min.	-199	-2639.41	18	-6781.41	17	190.30	5	278.60	9	2257.01	9	-2644.86	18	4586.98	9	-5575.66	17
401	Min.	-237	-2639.41	18	-6781.41	17	190.30	5	278.60	9	2257.01	9	-2644.86	18	4586.98	9	-5575.66	17
401	Max	-230	-1803.57	5	2315.22	18	2533.46	17	6651.37	17	3688.15	19	403.07	1	-663.33	9	9574.95	17
401	Max	-237	-1803.57	5	2315.22	18	2533.46	17	6651.37	17	3688.15	19	403.07	1	-663.33	9	9574.95	17
401	Max	-258	-1803.57	5	2315.22	18	2533.46	17	6651.37	17	3688.15	19	403.07	1	-663.33	9	9574.95	17
401	Max	-260	-1803.57	5	2315.22	18	2533.46	17	6651.37	17	3688.15	19	403.07	1	-663.33	9	9574.95	17
401	Min.	-230	-5819.56	18	-828.70	5	-3568.63	18	1490.79	9	1348.46	13	-636.62	9	-3019.79	17	1942.62	20
401	Min.	-237	-5819.56	18	-828.70	5	-3568.63	18	1490.79	9	1348.46	13	-636.62	9	-3019.79	17	1942.62	20
401	Min.	-258	-5819.56	18	-828.70	5	-3568.63	18	1490.79	9	1348.46	13	-636.62	9	-3019.79	17	1942.62	20
401	Min.	-260	-5819.56	18	-828.70	5	-3568.63	18	1490.79	9	1348.46	13	-636.62	9	-3019.79	17	1942.62	20
401	Max	-154	40.82	1	-98.23	5	-675.61	9	-709.03	1	-970.88	9	-560.02	9	-5515.39	1	18501.80	18
401	Max	-156	40.82	1	-98.23	5	-675.61	9	-709.03	1	-970.88	9	-560.02	9	-5515.39	1	18501.80	18
401	Max	-129	40.82	1	-98.23	5	-675.61	9	-709.03	1	-970.88	9	-560.02	9	-5515.39	1	18501.80	18
401	Max	-123	40.82	1	-98.23	5	-675.61	9	-709.03	1	-970.88	9	-560.02	9	-5515.39	1	18501.80	18
401	Min.	-154	-85.14	18	-2214.06	18	-1809.32	17	-1583.85	18	-2067.56	19	-1066.77	17	-12760.50	18	8062.80	1
401	Min.	-156	-85.14	18	-2214.06	18	-1809.32	17	-1583.85	18	-2067.56	19	-1066.77	17	-12760.50	18	8062.80	1
401	Min.	-129	-85.14	18	-2214.06	18	-1809.32	17	-1583.85	18	-2067.56	19	-1066.77	17	-12760.50	18	8062.80	1
401	Min.	-123	-85.14	18	-2214.06	18	-1809.32	17	-1583.85	18	-2067.56	19	-1066.77	17	-12760.50	18	8062.80	1
401	Max	-154	533.12	17	-3065.47	1	4557.84	18	-1411.91	1	-1344.81	1	-408.82	5	29008.20	18	-7864.34	9
401	Max	-123	533.12	17	-3065.47	1	4557.84	18	-1411.91	1	-1344.81	1	-408.82	5	29008.20	18	-7864.34	9
401	Max	-127	533.12	17	-3065.47	1	4557.84	18	-1411.91	1	-1344.81	1	-408.82	5	29008.20	18	-7864.34	9
401	Max	-152	533.12	17	-3065.47	1	4557.84	18	-1411.91	1	-1344.81	1	-408.82	5	29008.20	18	-7864.34	9
401	Min.	-154	-1270.56	18	-8250.17	17	-32.51	5	-3190.54	18	-3660.46	18	-2012.47	18	12327.10	1	-17814.10	18
401	Min.	-123	-1270.56	18	-8250.17	17	-32.51	5	-3190.54	18	-3660.46	18	-2012.47	18	12327.10	1	-17814.10	18
401	Min.	-127	-1270.56	18	-8250.17	17	-32.51	5	-3190.54	18	-3660.46	18	-2012.47	18	12327.10	1	-17814.10	18
401	Min.	-152	-1270.56	18	-8250.17	17	-32.51	5	-3190.54	18	-3660.46	18	-2012.47	18	12327.10	1	-17814.10	18
401	Max	-127	-2648.59	1	96.31	9	-134.65	5	9689.66	17	717.31	17	1203.05	18	2435.73	17	14740.30	17
401	Max	-124	-2648.59	1	96.31	9	-134.65	5	9689.66	17	717.31	17	1203.05	18	2435.73	17	14740.30	17
401	Max	-148	-2648.59	1	96.31	9	-134.65	5	9689.66	17	717.31	17	1203.05	18	2435.73	17	14740.30	17
401	Max	-152	-2648.59	1	96.31	9	-134.65	5	9689.66	17	717.31	17	1203.05	18	2435.73	17	14740.30	17
401	Min.	-127	-6984.63	17	-1284.56	18	-4250.40	18	3095.01	1	114.26	9	284.49	1	867.21	9	5860.18	1
401	Min.	-124	-6984.63	17	-1284.56	18	-4250.40	18	3095.01	1	114.26	9	284.49	1	867.21	9	5860.18	1
401	Min.	-148	-6984.63	17	-1284.56	18	-4250.40	18	3095.01	1	114.26	9	284.49	1	867.21	9	5860.18	1
401	Min.	-152	-6984.63	17	-1284.56	18	-4250.40	18	3095.01	1	114.26	9	284.49	1	867.21	9	5860.18	1
401	Max	-325	-161.80	20	266.53	17	437.75	5	-1518.97	13	-1891.65	1	2676.57	19	10006.10	18	24196.40	19
401	Max	-317	-161.80	20	266.53	17	437.75	5	-1518.97	13	-1891.65	1	2676.57	19	10006.10	18	24196.40	19
401	Max	-340	-161.80	20	266.53	17	437.75	5	-1518.97	13	-1891.65	1	2676.57	19	10006.10	18	24196.40	19
401	Max	-358	-161.80	20	266.53	17	437.75	5	-1518.97	13	-1891.65	1	2676.57	19	10006.10	18	24196.40	19
401	Min.	-325	-1311.23	17	-609.60	18	-2233.36	18	-3522.25	19	-4489.61	18	1149.85	13	4390.53	5	10523.30	13
401	Min.	-317	-1311.23	17	-609.60	18	-2233.36	18	-3522.25	19	-4489.61	18	1149.85	13	4390.53	5	10523.30	13
401	Min.	-340	-1311.23	17	-609.60	18	-2233.36	18	-3522.25	19	-4489.61	18	1149.85	13	4390.53	5	10523.30	13
401	Min.	-358	-1311.23	17	-609.60	18	-2233.36	18	-3522.25	19	-4489.61	18	1149.85	13	4390.53	5	10523.30	13
401	Max	-317	-178.92	1	1897.79	18	700.60	17	2084.77	19	-1941.97	13	743.98	19	-938.35	13	9987.47	19
401	Max	-319	-178.92	1	1897.79	18	700.60	17	2084.77	19	-1941.97	13	743.98	19	-938.35	13	9987.47	19
401	Max	-342	-178.92	1	1897.79	18	700.60	17	2084.77	19	-1941.97	13	743.98	19	-938.35	13	9987.47	19
401	Max	-340	-178.92	1	1897.79	18	700.60	17	2084.77	19	-1941.97	13	743.98	19	-938.35	13	9987.47	19
401	Min.	-317	-1292.61	18	-303.93	5	-802.70	18	897.00	13	-4434.97	19	279.08	13	-2233.08	19	4330.87	13
401	Min.	-319	-1292.61	18	-303.93	5	-802.70	18	897.00	13	-4434.97	19	279.08	13	-2233.08	19	4330.87	13
401	Min.	-342	-1292.61	18	-303.93	5	-802.70	18	897.00	13	-4434.97	19	279.08	13	-2233.08	19	4330.87	13
401	Min.	-340	-1292.61	18	-303.93	5	-802.70	18	897.00	13	-4434.97	19	279.08	13	-2233.08	19	4330.87	13
401	Max	-358	683.69	18	409.51	17	304.02	17	-1669.16	13	929.53	19	26.98	5	5788.42	19	-715.40	13
401	Max	-340	683.69	18	409.51	17	304.02	17	-1669.16	13	929.53	19	26.98	5	5788.42	19	-715.40	13
401	Max	-342	683.69	18	409.51	17	304.02	17	-1669.16	13	929.53	19	26.98	5	5788.42	19	-715.40	13
401	Max	-359	683.69	18	409.51	17	304.02	17	-1669.16	13	929.53	19	26.98	5	5788.42	19	-715.40	13
401	Min.	-358	-49.30	5	-1519.43	18	-433.76	18	-3823.18	19	384.66	13	-201.05	18	2501.00	9	-1643.01	19
401	Min.	-340	-49.30	5	-1519.43	18	-433.76	18	-3823.18	19	384.66	13	-201.05	18	2501.00	9	-1643.01	19
401	Min.	-342	-49.30	5	-1519.43	18	-433.76	18	-3823.18	19	384.66	13	-201.05	18	2501.00	9	-1643.01	19
401	Min.	-359	-49.30	5	-1519.43	18	-433.76	18	-3823.18	19	384.66	13	-201.05	18	2501.00	9	-1643.01	19
401	Max	-319	244.93	17	1313.05	18	292.50	18	2920.67	19	-515.78	13	-313.38	9	-710.98	13	1964.97	19
401	Max	-328	244.93	17	1313.05	18	292.50	18	2920.67	19	-515.78	13	-313.38	9	-710.98	13	1964.97	19
401	Max	-359	244.93	17	1313.05	18	292.50	18	2920.67	19	-515.78	13	-313.38	9	-710.98	13	1964.97	19
401	Max	-342	244.93	17	1313.05	18	292.50	18	2920.67	19	-515.78	13	-313.38	9	-710.98	13	1964.97	19
401	Min.	-319	-944.96	18	-164.34	5	94.00	1	1249.51	13	-1201.46	19	-794.18	19	-1694.67	19	861.74	13
401	Min.	-328	-944.96	18	-164.34	5	94.00	1	1249.51	13	-1201.46	19	-794.18	19	-1694.67	19	861.74	13
401	Min.	-359	-944.96	18	-164.34	5	94.00	1	1249.51	13	-1201.46	19	-794.18	19	-1694.67	19	861.74	13
401	Min.	-342	-944.96	18	-164.34	5	94.00	1	1249.51	13	-1201.46	19	-794.18	19	-1694.67	19	861.74	13
401	Max	-295	2826.43	18	-36.22	5	492.97	18	-478.51	9	3156.20	19	-30.74	9	-337.45	9	-1194.76	13
401	Max	-328	2826.43	18	-36.22	5	492.97	18	-478.51	9	3156.20	19	-30.74	9	-337.45	9	-1194.76	13
401	Max	-319	2826.43	18	-36.22	5	492.97	18	-478.51	9	3156.20	19	-30.74	9	-337.45	9	-1194.76	13
401	Max	-291	2826.43	18	-36.22	5	492.97	18	-478.51	9	3156.20	19	-30.74	9	-337.45	9	-1194.76	13
401	Min.	-295	-346.25	5	-785.30	18	-1055.50	17	-1081.80	18	1340.44	13	-371.81	1	-1167.00	19	-3029.22	19
401	Min.	-328	-346.25	5	-785.30	18	-1055.50	17	-1081.80	18	1340.44	13	-371.81	1	-1167.00	19	-3029.22	19
401	Min.	-319	-346.25	5	-785.30	18	-1055.50	17	-1081.80	18	1340.44	13	-371.81	1	-1167.00	19	-3029.22	19

401	Min.	-291	-346.25	5	-785.30	18	-1055.50	17	-1081.80	18	1340.44	13	-371.81	1	-1167.00	19	-3029.22	19
401	Max	-295	-307.34	1	7727.90	18	2593.61	17	3671.38	17	2376.19	19	-42.58	1	6459.85	17	296.46	18
401	Max	-291	-307.34	1	7727.90	18	2593.61	17	3671.38	17	2376.19	19	-42.58	1	6459.85	17	296.46	18
401	Max	-260	-307.34	1	7727.90	18	2593.61	17	3671.38	17	2376.19	19	-42.58	1	6459.85	17	296.46	18
401	Max	-258	-307.34	1	7727.90	18	2593.61	17	3671.38	17	2376.19	19	-42.58	1	6459.85	17	296.46	18
401	Min.	-295	-2012.38	18	-1380.21	5	-1060.80	18	1205.45	20	874.00	13	-1141.96	18	1013.15	20	-3311.06	17
401	Min.	-291	-2012.38	18	-1380.21	5	-1060.80	18	1205.45	20	874.00	13	-1141.96	18	1013.15	20	-3311.06	17
401	Min.	-260	-2012.38	18	-1380.21	5	-1060.80	18	1205.45	20	874.00	13	-1141.96	18	1013.15	20	-3311.06	17
401	Min.	-258	-2012.38	18	-1380.21	5	-1060.80	18	1205.45	20	874.00	13	-1141.96	18	1013.15	20	-3311.06	17
401	Max	-317	-2.82	18	2447.85	18	2234.67	17	-2160.39	13	-2210.44	9	151.32	5	28063.50	19	-9514.13	13
401	Max	-325	-2.82	18	2447.85	18	2234.67	17	-2160.39	13	-2210.44	9	151.32	5	28063.50	19	-9514.13	13
401	Max	-293	-2.82	18	2447.85	18	2234.67	17	-2160.39	13	-2210.44	9	151.32	5	28063.50	19	-9514.13	13
401	Max	-289	-2.82	18	2447.85	18	2234.67	17	-2160.39	13	-2210.44	9	151.32	5	28063.50	19	-9514.13	13
401	Min.	-317	-2286.97	17	-627.61	17	-2018.28	18	-5073.09	19	-5079.99	19	-1563.87	18	12104.00	9	-22015.10	19
401	Min.	-325	-2286.97	17	-627.61	17	-2018.28	18	-5073.09	19	-5079.99	19	-1563.87	18	12104.00	9	-22015.10	19
401	Min.	-293	-2286.97	17	-627.61	17	-2018.28	18	-5073.09	19	-5079.99	19	-1563.87	18	12104.00	9	-22015.10	19
401	Min.	-289	-2286.97	17	-627.61	17	-2018.28	18	-5073.09	19	-5079.99	19	-1563.87	18	12104.00	9	-22015.10	19
401	Max	-317	1371.61	18	513.81	18	2057.77	18	-593.87	5	1864.10	19	1149.83	18	10496.00	19	5081.13	19
401	Max	-289	1371.61	18	513.81	18	2057.77	18	-593.87	5	1864.10	19	1149.83	18	10496.00	19	5081.13	19
401	Max	-291	1371.61	18	513.81	18	2057.77	18	-593.87	5	1864.10	19	1149.83	18	10496.00	19	5081.13	19
401	Max	-319	1371.61	18	513.81	18	2057.77	18	-593.87	5	1864.10	19	1149.83	18	10496.00	19	5081.13	19
401	Min.	-317	-124.34	5	-1678.12	17	-1603.18	17	-1927.92	18	704.39	9	-48.25	5	4454.25	13	2097.30	9
401	Min.	-289	-124.34	5	-1678.12	17	-1603.18	17	-1927.92	18	704.39	9	-48.25	5	4454.25	13	2097.30	9
401	Min.	-291	-124.34	5	-1678.12	17	-1603.18	17	-1927.92	18	704.39	9	-48.25	5	4454.25	13	2097.30	9
401	Min.	-319	-124.34	5	-1678.12	17	-1603.18	17	-1927.92	18	704.39	9	-48.25	5	4454.25	13	2097.30	9
401	Max	-289	-641.65	20	1164.86	18	1314.40	17	-1160.61	9	3984.31	19	256.13	17	7617.73	19	1877.63	18
401	Max	-293	-641.65	20	1164.86	18	1314.40	17	-1160.61	9	3984.31	19	256.13	17	7617.73	19	1877.63	18
401	Max	-255	-641.65	20	1164.86	18	1314.40	17	-1160.61	9	3984.31	19	256.13	17	7617.73	19	1877.63	18
401	Max	-262	-641.65	20	1164.86	18	1314.40	17	-1160.61	9	3984.31	19	256.13	17	7617.73	19	1877.63	18
401	Min.	-289	-1491.38	17	-355.80	17	-724.64	18	-3018.77	19	1689.09	13	-243.00	18	3143.83	9	-624.15	1
401	Min.	-293	-1491.38	17	-355.80	17	-724.64	18	-3018.77	19	1689.09	13	-243.00	18	3143.83	9	-624.15	1
401	Min.	-255	-1491.38	17	-355.80	17	-724.64	18	-3018.77	19	1689.09	13	-243.00	18	3143.83	9	-624.15	1
401	Min.	-262	-1491.38	17	-355.80	17	-724.64	18	-3018.77	19	1689.09	13	-243.00	18	3143.83	9	-624.15	1
401	Max	-289	1029.43	18	-279.52	20	1911.52	18	2671.34	19	793.89	17	1285.87	18	7348.18	19	6888.81	19
401	Max	-262	1029.43	18	-279.52	20	1911.52	18	2671.34	19	793.89	17	1285.87	18	7348.18	19	6888.81	19
401	Max	-260	1029.43	18	-279.52	20	1911.52	18	2671.34	19	793.89	17	1285.87	18	7348.18	19	6888.81	19
401	Max	-291	1029.43	18	-279.52	20	1911.52	18	2671.34	19	793.89	17	1285.87	18	7348.18	19	6888.81	19
401	Min.	-289	-389.63	17	-2478.59	17	-2059.70	17	1055.28	13	-250.55	9	78.39	5	3047.61	13	2712.05	9
401	Min.	-262	-389.63	17	-2478.59	17	-2059.70	17	1055.28	13	-250.55	9	78.39	5	3047.61	13	2712.05	9
401	Min.	-260	-389.63	17	-2478.59	17	-2059.70	17	1055.28	13	-250.55	9	78.39	5	3047.61	13	2712.05	9
401	Min.	-291	-389.63	17	-2478.59	17	-2059.70	17	1055.28	13	-250.55	9	78.39	5	3047.61	13	2712.05	9
401	Max	-297	138.17	17	117.01	18	-37.96	20	744.46	19	5009.99	18	-703.84	9	1929.45	19	-153.05	5
401	Max	-330	138.17	17	117.01	18	-37.96	20	744.46	19	5009.99	18	-703.84	9	1929.45	19	-153.05	5
401	Max	-332	138.17	17	117.01	18	-37.96	20	744.46	19	5009.99	18	-703.84	9	1929.45	19	-153.05	5
401	Max	-301	138.17	17	117.01	18	-37.96	20	744.46	19	5009.99	18	-703.84	9	1929.45	19	-153.05	5
401	Min.	-297	32.06	20	-606.78	17	-305.59	17	318.95	9	1970.76	5	-1731.63	19	837.77	13	-775.94	18
401	Min.	-330	32.06	20	-606.78	17	-305.59	17	318.95	9	1970.76	5	-1731.63	19	837.77	13	-775.94	18
401	Min.	-332	32.06	20	-606.78	17	-305.59	17	318.95	9	1970.76	5	-1731.63	19	837.77	13	-775.94	18
401	Min.	-301	32.06	20	-606.78	17	-305.59	17	318.95	9	1970.76	5	-1731.63	19	837.77	13	-775.94	18
401	Max	-297	-149.52	20	230.53	18	394.37	17	4429.40	18	2112.06	19	425.33	19	1889.61	18	1523.37	19
401	Max	-301	-149.52	20	230.53	18	394.37	17	4429.40	18	2112.06	19	425.33	19	1889.61	18	1523.37	19
401	Max	-264	-149.52	20	230.53	18	394.37	17	4429.40	18	2112.06	19	425.33	19	1889.61	18	1523.37	19
401	Max	-253	-149.52	20	230.53	18	394.37	17	4429.40	18	2112.06	19	425.33	19	1889.61	18	1523.37	19
401	Min.	-297	-880.18	17	81.32	1	88.99	20	1619.47	5	931.66	13	152.24	9	748.66	1	656.15	13
401	Min.	-301	-880.18	17	81.32	1	88.99	20	1619.47	5	931.66	13	152.24	9	748.66	1	656.15	13
401	Min.	-264	-880.18	17	81.32	1	88.99	20	1619.47	5	931.66	13	152.24	9	748.66	1	656.15	13
401	Min.	-253	-880.18	17	81.32	1	88.99	20	1619.47	5	931.66	13	152.24	9	748.66	1	656.15	13
401	Max	-330	367.94	18	329.86	18	-61.90	9	-100.14	13	5472.12	18	-214.11	9	4631.17	19	-868.69	9
401	Max	-357	367.94	18	329.86	18	-61.90	9	-100.14	13	5472.12	18	-214.11	9	4631.17	19	-868.69	9
401	Max	-356	367.94	18	329.86	18	-61.90	9	-100.14	13	5472.12	18	-214.11	9	4631.17	19	-868.69	9
401	Max	-332	367.94	18	329.86	18	-61.90	9	-100.14	13	5472.12	18	-214.11	9	4631.17	19	-868.69	9
401	Min.	-330	-220.57	17	30.79	9	-167.66	17	-232.32	19	2314.56	1	-555.68	19	1977.73	9	-2054.33	19
401	Min.	-357	-220.57	17	30.79	9	-167.66	17	-232.32	19	2314.56	1	-555.68	19	1977.73	9	-2054.33	19
401	Min.	-356	-220.57	17	30.79	9	-167.66	17	-232.32	19	2314.56	1	-555.68	19	1977.73	9	-2054.33	19
401	Min.	-332	-220.57	17	30.79	9	-167.66	17	-232.32	19	2314.56	1	-555.68	19	1977.73	9	-2054.33	19
401	Max	-297	576.21	18	-362.85	20	-16.35	20	3466.25	19	1313.15	18	-465.32	9	-1815.02	1	4165.17	19
401	Max	-253	576.21	18	-362.85	20	-16.35	20	3466.25	19	1313.15	18	-465.32	9	-1815.02	1	4165.17	19
401	Max	-255	576.21	18	-362.85	20	-16.35	20	3466.25	19	1313.15	18	-465.32	9	-1815.02	1	4165.17	19
401	Max	-293	576.21	18	-362.85	20	-16.35	20	3466.25	19	1313.15	18	-465.32	9	-1815.02	1	4165.17	19
401	Min.	-297	50.09	5	-1531.67	17	-593.98	17	1500.99	13	69.61	5	-1064.80	19	-4513.98	18	1730.96	9
401	Min.	-253	50.09	5	-1531.67	17	-593.98	17	1500.99	13	69.61	5	-1064.80	19	-4513.98	18	1730.96	9
401	Min.	-255	50.09	5	-1531.67	17	-593.98	17	1500.99	13	69.61	5	-1064.80	19	-4513.98	18	1730.96	9
401	Min.	-293	50.09	5	-1531.67	17	-593.98	17	1500.99	13	69.61	5	-1064.80	19	-4513.98	18	1730.96	9
401	Max	-297	367.68	19	1202.38	18	973.95	17	-1233.38	13	-1458.22	9	482.25	17	-7243.15	9	-9351.33	9
401	Max	-293	367.68	19	1202.38	18	973.95	17	-1233.38	13	-1458.22	9	482.25	17	-7243.15	9	-9351.33	9
401	Max	-325	367.68	19	1202.38	18	973.95	17	-1233.38	13	-1458.22	9	482.25	17	-7243.15	9	-9351.33	9
401	Max	-330	367.68	19	1202.38	18	973.95	17	-1233.38	13	-1458.22	9	482.25	17	-7243.15	9	-9351.33	9
401	Min.	-297	91.31	9	-557.65	17	380.63	9	-2832.55	19	-3363.18	19	169.09	20	-16827.20	19	-21485.20	19
401	Min.	-293	91.31	9	-557.65	17	380.63	9	-2832.55	19	-3363.18	19	169.09	20	-16827.20	19	-21485.20	19
401	Min.	-325	91.31	9	-557.65	17	380.63	9	-2832.55	19	-3363.18	19	169.09	20	-16827.20	19	-21485.20	19
401	Min.	-330	91.31	9	-557.65	17	380.63	9	-2832.55	19	-3363.18	19	169.09	20	-16827.20	19	-21485.20	19
401	Max	-325	134.35	5	558.71	18	252.92	17	-1008.22	5	-1760.08	13	1060.72	19	16264.60	19	9646.43	19
401	Max	-358	134.35	5	558.71	18	252.92	17	-1008.22	5	-1760.08	13	1060.72	19	16264.60	19	9646.43	19
401	Max	-357	134.35	5	558.71	18	252.92	17	-1008.22	5	-1760.08	13	1060.72	19	16264.60	19	9646.43	19
401	Max	-330	134.35	5	558.71	18	252.92	17	-1008.22	5	-1760.08	13	1060.72	19	16264.60	19	9646.43	19
401	Min.	-325	-861.51	18	162.29	9	-416.70	18	-2676.27	18	-4025.62	19	462.71	13	7067.62	9	4206.88	9
401	Min.	-358	-861.51	18	162.29	9	-416.70	18	-2676.27	18	-4025.62	19	462.71	13	7067.62	9	4206.88	9
401	Min.	-357	-861.51	18	162.29	9	-416.70	18	-2676.27	18	-4025.62	19	462.71	13	7067.62	9	4206.88	9
401	Min.	-330	-861.51	18	162.29	9	-416.70	18	-2676.27	18	-4025.62	19	462.71	13	7067.62	9	4206.88	9
401	Max	-332	52.44	18	122.74	19	332.99	17	4415.24	18	-172.52	5	-231.32	1	1004.43	18	-3306.52	5
401	Max	-334	52.44	18	122.74	19	332.99	17	4415.24	18	-172.52	5	-231.32	1	1004.43	18	-3306.52	5
401	Max	-311	52.44	18	122.74	19	332.99	17	4415.24	18	-172.52	5	-231.32	1	1004.43	18	-3306.52	5
401	Max	-301	52.44	18	122.74	19	332.99	17	4415.24	18	-172.52	5	-231.32	1	1004.43	18	-3306.52	5
401	Min.	-332	-526.98	17	27.28	9	97.64	20	1795.08	5	-550.36	18	-698.31	18	347.50	1	-7643.35	18
401	Min.	-334	-526.98	17	27.28	9	97.64	20	1795.08	5	-550.36	18	-698.31	18	347.50	1	-7643.35	18
401	Min.	-311	-526.98	17	27.28	9	97.64	20	1795.08	5	-550.36	18	-698.31	18	347.50	1	-7643.35	18
401	Min.	-301	-526.98	17	27.28	9	97.64	20	1795.08	5	-550.36	18	-698.31	18	347.50	1	-7643.35	18
401	Max	-334	-197.46	9	540.81	18	724.60	17	-1804.17	1	-2013.34	1	442.69	18	20267.00	19	-9610.92	5
401	Max	-324	-197.46	9	540.81	18	724.60	17	-1804.17	1	-2013.34	1	442.69	18	20267.00	19	-9610.92	5
401	Max	-305	-197.46	9	540.81	18	724.60	17	-1804.17	1	-2013.34	1	442.69	18	20267.00	19	-9610.92	5
401	Max	-311	-197.46	9	540.81	18	724.60	17	-1804.17	1	-2013.34	1	442.69	18	20267.00	19	-9610.92	5
401	Min.	-334	-603.51	19	-380.66	17	252.53	9	-4135.59	18	-4670.27	19	42.42	9	8719.77	1	-22223.30	18
401	Min.	-324	-603.51	19	-380.66	17	252.53	9	-4135.59	18	-4670.27	19	42.42	9	8719.77	1	-22223.30	18
401	Min.	-305	-603.51	19	-380.66	17	252.53	9	-4135.59	18	-4670.27	19	42.42	9	8719.77	1	-22223.30	18
401	Min.	-311	-603.51	19	-380.66	17	252.53	9	-4135.59	18	-4670.27	19	42.42	9	8719.77	1	-22223.30	18
401	Max	-311	194.83	18	39.43	18	565.88	17	1934.41	18	980.24	19	-508.93	1	7717.94	18	-3241.03	1
401	Max	-305	194.83	18	39.43	18	565.88	17	1934.41	18	980.24	19	-508.93	1	7717.94	18	-3241.03	1
401	Max	-286	194.83	18	39.43	18	565.88	17	1934.41	18	980.24	19	-508.93	1	7717.94	18	-3241.03	1
401	Max	-301	194.83	18	39.43	18	565.88	17	1934.41	18	980.24	19	-508.93	1	7717.94	18	-3241.03	1

401	Min.	-311	-348.36	17	-242.26	17	161.67	20	577.69	1	411.39	9	-1373.82	18	3307.89	1	-7351.62	18
401	Min.	-305	-348.36	17	-242.26	17	161.67	20	577.69	1	411.39	9	-1373.82	18	3307.89	1	-7351.62	18
401	Min.	-286	-348.36	17	-242.26	17	161.67	20	577.69	1	411.39	9	-1373.82	18	3307.89	1	-7351.62	18
401	Min.	-301	-348.36	17	-242.26	17	161.67	20	577.69	1	411.39	9	-1373.82	18	3307.89	1	-7351.62	18
401	Max	-286	116.18	17	-116.14	20	-54.69	9	2235.41	19	3080.30	18	408.41	19	5594.15	18	1178.74	18
401	Max	-268	116.18	17	-116.14	20	-54.69	9	2235.41	19	3080.30	18	408.41	19	5594.15	18	1178.74	18
401	Max	-264	116.18	17	-116.14	20	-54.69	9	2235.41	19	3080.30	18	408.41	19	5594.15	18	1178.74	18
401	Max	-301	116.18	17	-116.14	20	-54.69	9	2235.41	19	3080.30	18	408.41	19	5594.15	18	1178.74	18
401	Min.	-286	43.78	9	-802.94	17	-238.99	17	989.26	13	1106.11	1	119.63	1	2438.70	5	448.50	5
401	Min.	-268	43.78	9	-802.94	17	-238.99	17	989.26	13	1106.11	1	119.63	1	2438.70	5	448.50	5
401	Min.	-264	43.78	9	-802.94	17	-238.99	17	989.26	13	1106.11	1	119.63	1	2438.70	5	448.50	5
401	Min.	-301	43.78	9	-802.94	17	-238.99	17	989.26	13	1106.11	1	119.63	1	2438.70	5	448.50	5
401	Max	-334	392.09	18	255.80	19	143.74	17	4700.81	18	109.17	19	1009.12	19	-304.08	1	6801.26	18
401	Max	-332	392.09	18	255.80	19	143.74	17	4700.81	18	109.17	19	1009.12	19	-304.08	1	6801.26	18
401	Max	-356	392.09	18	255.80	19	143.74	17	4700.81	18	109.17	19	1009.12	19	-304.08	1	6801.26	18
401	Max	-355	392.09	18	255.80	19	143.74	17	4700.81	18	109.17	19	1009.12	19	-304.08	1	6801.26	18
401	Min.	-334	-235.49	17	29.42	9	-159.80	18	1971.57	5	12.51	9	411.89	9	-757.87	18	2849.62	1
401	Min.	-332	-235.49	17	29.42	9	-159.80	18	1971.57	5	12.51	9	411.89	9	-757.87	18	2849.62	1
401	Min.	-356	-235.49	17	29.42	9	-159.80	18	1971.57	5	12.51	9	411.89	9	-757.87	18	2849.62	1
401	Min.	-355	-235.49	17	29.42	9	-159.80	18	1971.57	5	12.51	9	411.89	9	-757.87	18	2849.62	1
401	Max	-334	127.60	17	401.70	18	273.70	18	-878.47	5	-2334.34	1	-379.63	9	-6498.32	1	12109.80	18
401	Max	-355	127.60	17	401.70	18	273.70	18	-878.47	5	-2334.34	1	-379.63	9	-6498.32	1	12109.80	18
401	Max	-354	127.60	17	401.70	18	273.70	18	-878.47	5	-2334.34	1	-379.63	9	-6498.32	1	12109.80	18
401	Max	-324	127.60	17	401.70	18	273.70	18	-878.47	5	-2334.34	1	-379.63	9	-6498.32	1	12109.80	18
401	Min.	-334	-694.74	18	-489.35	17	-92.87	17	-2372.30	18	-5318.29	18	-891.76	19	-14975.30	18	5169.81	1
401	Min.	-355	-694.74	18	-489.35	17	-92.87	17	-2372.30	18	-5318.29	18	-891.76	19	-14975.30	18	5169.81	1
401	Min.	-354	-694.74	18	-489.35	17	-92.87	17	-2372.30	18	-5318.29	18	-891.76	19	-14975.30	18	5169.81	1
401	Min.	-324	-694.74	18	-489.35	17	-92.87	17	-2372.30	18	-5318.29	18	-891.76	19	-14975.30	18	5169.81	1
401	Max	-268	175.89	18	19.03	18	-115.83	9	2912.83	19	-726.80	9	173.52	9	-1662.77	1	-3106.04	1
401	Max	-286	175.89	18	19.03	18	-115.83	9	2912.83	19	-726.80	9	173.52	9	-1662.77	1	-3106.04	1
401	Max	-282	175.89	18	19.03	18	-115.83	9	2912.83	19	-726.80	9	173.52	9	-1662.77	1	-3106.04	1
401	Max	-280	175.89	18	19.03	18	-115.83	9	2912.83	19	-726.80	9	173.52	9	-1662.77	1	-3106.04	1
401	Min.	-268	-157.50	17	-444.47	17	-426.74	19	1232.01	1	-1678.57	19	-21.02	1	-4206.54	18	-7367.76	19
401	Min.	-286	-157.50	17	-444.47	17	-426.74	19	1232.01	1	-1678.57	19	-21.02	1	-4206.54	18	-7367.76	19
401	Min.	-282	-157.50	17	-444.47	17	-426.74	19	1232.01	1	-1678.57	19	-21.02	1	-4206.54	18	-7367.76	19
401	Min.	-280	-157.50	17	-444.47	17	-426.74	19	1232.01	1	-1678.57	19	-21.02	1	-4206.54	18	-7367.76	19
401	Max	-286	113.64	18	180.85	18	-87.40	9	134.67	18	-988.98	1	-939.10	9	-677.45	1	-6558.50	1
401	Max	-305	113.64	18	180.85	18	-87.40	9	134.67	18	-988.98	1	-939.10	9	-677.45	1	-6558.50	1
401	Max	-303	113.64	18	180.85	18	-87.40	9	134.67	18	-988.98	1	-939.10	9	-677.45	1	-6558.50	1
401	Max	-282	113.64	18	180.85	18	-87.40	9	134.67	18	-988.98	1	-939.10	9	-677.45	1	-6558.50	1
401	Min.	-286	-773.00	17	-28.62	9	-404.12	18	-9.66	1	-2448.80	19	-2103.35	19	-1925.41	18	-15200.50	19
401	Min.	-305	-773.00	17	-28.62	9	-404.12	18	-9.66	1	-2448.80	19	-2103.35	19	-1925.41	18	-15200.50	19
401	Min.	-303	-773.00	17	-28.62	9	-404.12	18	-9.66	1	-2448.80	19	-2103.35	19	-1925.41	18	-15200.50	19
401	Min.	-282	-773.00	17	-28.62	9	-404.12	18	-9.66	1	-2448.80	19	-2103.35	19	-1925.41	18	-15200.50	19
401	Max	-280	1357.81	18	-165.63	9	590.28	18	-877.80	1	-884.15	9	2880.60	19	-5423.56	1	-4025.16	1
401	Max	-282	1357.81	18	-165.63	9	590.28	18	-877.80	1	-884.15	9	2880.60	19	-5423.56	1	-4025.16	1
401	Max	-303	1357.81	18	-165.63	9	590.28	18	-877.80	1	-884.15	9	2880.60	19	-5423.56	1	-4025.16	1
401	Max	-309	1357.81	18	-165.63	9	590.28	18	-877.80	1	-884.15	9	2880.60	19	-5423.56	1	-4025.16	1
401	Min.	-280	-75.91	9	-539.29	19	27.05	5	-2148.36	19	-2440.19	18	1284.26	5	-12602.40	19	-9904.41	19
401	Min.	-282	-75.91	9	-539.29	19	27.05	5	-2148.36	19	-2440.19	18	1284.26	5	-12602.40	19	-9904.41	19
401	Min.	-303	-75.91	9	-539.29	19	27.05	5	-2148.36	19	-2440.19	18	1284.26	5	-12602.40	19	-9904.41	19
401	Min.	-309	-75.91	9	-539.29	19	27.05	5	-2148.36	19	-2440.19	18	1284.26	5	-12602.40	19	-9904.41	19
401	Max	-305	-267.34	20	2476.76	18	115.79	17	-3198.71	1	-1753.28	1	-371.74	1	24377.70	19	-12769.90	1
401	Max	-324	-267.34	20	2476.76	18	115.79	17	-3198.71	1	-1753.28	1	-371.74	1	24377.70	19	-12769.90	1
401	Max	-309	-267.34	20	2476.76	18	115.79	17	-3198.71	1	-1753.28	1	-371.74	1	24377.70	19	-12769.90	1
401	Max	-303	-267.34	20	2476.76	18	115.79	17	-3198.71	1	-1753.28	1	-371.74	1	24377.70	19	-12769.90	1
401	Min.	-305	-999.21	17	40.65	9	-734.20	18	-7518.85	18	-4403.21	19	-961.59	18	10193.70	1	-29545.10	19
401	Min.	-324	-999.21	17	40.65	9	-734.20	18	-7518.85	18	-4403.21	19	-961.59	18	10193.70	1	-29545.10	19
401	Min.	-309	-999.21	17	40.65	9	-734.20	18	-7518.85	18	-4403.21	19	-961.59	18	10193.70	1	-29545.10	19
401	Min.	-303	-999.21	17	40.65	9	-734.20	18	-7518.85	18	-4403.21	19	-961.59	18	10193.70	1	-29545.10	19
401	Max	-309	428.90	18	552.58	18	1292.82	18	-240.90	9	1279.26	19	1787.44	18	8281.64	19	4502.79	19
401	Max	-307	428.90	18	552.58	18	1292.82	18	-240.90	9	1279.26	19	1787.44	18	8281.64	19	4502.79	19
401	Max	-276	428.90	18	552.58	18	1292.82	18	-240.90	9	1279.26	19	1787.44	18	8281.64	19	4502.79	19
401	Max	-280	428.90	18	552.58	18	1292.82	18	-240.90	9	1279.26	19	1787.44	18	8281.64	19	4502.79	19
401	Min.	-309	-258.79	17	-76.00	5	38.18	9	-672.49	19	583.68	5	446.33	9	3274.86	1	1600.21	1
401	Min.	-307	-258.79	17	-76.00	5	38.18	9	-672.49	19	583.68	5	446.33	9	3274.86	1	1600.21	1
401	Min.	-276	-258.79	17	-76.00	5	38.18	9	-672.49	19	583.68	5	446.33	9	3274.86	1	1600.21	1
401	Min.	-280	-258.79	17	-76.00	5	38.18	9	-672.49	19	583.68	5	446.33	9	3274.86	1	1600.21	1
401	Max	-307	417.74	18	734.06	18	1457.90	18	1601.21	19	617.56	17	760.68	18	2115.91	19	571.95	9
401	Max	-313	417.74	18	734.06	18	1457.90	18	1601.21	19	617.56	17	760.68	18	2115.91	19	571.95	9
401	Max	-274	417.74	18	734.06	18	1457.90	18	1601.21	19	617.56	17	760.68	18	2115.91	19	571.95	9
401	Max	-276	417.74	18	734.06	18	1457.90	18	1601.21	19	617.56	17	760.68	18	2115.91	19	571.95	9
401	Min.	-307	-199.79	17	-45.29	5	49.89	9	255.12	1	296.77	1	-129.92	5	359.33	1	-715.73	18
401	Min.	-313	-199.79	17	-45.29	5	49.89	9	255.12	1	296.77	1	-129.92	5	359.33	1	-715.73	18
401	Min.	-274	-199.79	17	-45.29	5	49.89	9	255.12	1	296.77	1	-129.92	5	359.33	1	-715.73	18
401	Min.	-276	-199.79	17	-45.29	5	49.89	9	255.12	1	296.77	1	-129.92	5	359.33	1	-715.73	18
401	Max	-313	-64.52	9	1302.57	18	1305.16	18	2253.80	19	-706.46	5	370.44	18	-868.31	1	-268.56	1
401	Max	-307	-64.52	9	1302.57	18	1305.16	18	2253.80	19	-706.46	5	370.44	18	-868.31	1	-268.56	1
401	Max	-336	-64.52	9	1302.57	18	1305.16	18	2253.80	19	-706.46	5	370.44	18	-868.31	1	-268.56	1
401	Max	-353	-64.52	9	1302.57	18	1305.16	18	2253.80	19	-706.46	5	370.44	18	-868.31	1	-268.56	1
401	Min.	-313	-198.16	17	-27.29	5	42.66	13	787.53	1	-1538.53	19	-142.73	13	-2182.58	19	-811.28	19
401	Min.	-307	-198.16	17	-27.29	5	42.66	13	787.53	1	-1538.53	19	-142.73	13	-2182.58	19	-811.28	19
401	Min.	-336	-198.16	17	-27.29	5	42.66	13	787.53	1	-1538.53	19	-142.73	13	-2182.58	19	-811.28	19
401	Min.	-353	-198.16	17	-27.29	5	42.66	13	787.53	1	-1538.53	19	-142.73	13	-2182.58	19	-811.28	19
401	Max	-307	1167.71	18	-91.75	13	1264.69	18	938.80	18	-1482.32	1	227.97	18	-1417.71	1	-3980.36	1
401	Max	-309	1167.71	18	-91.75	13	1264.69	18	938.80	18	-1482.32	1	227.97	18	-1417.71	1	-3980.36	1
401	Max	-338	1167.71	18	-91.75	13	1264.69	18	938.80	18	-1482.32	1	227.97	18	-1417.71	1	-3980.36	1
401	Max	-336	1167.71	18	-91.75	13	1264.69	18	938.80	18	-1482.32	1	227.97	18	-1417.71	1	-3980.36	1
401	Min.	-307	13.62	9	-252.12	19	51.23	9	181.26	1	-3707.50	18	-259.30	9	-3609.37	19	-9855.95	19
401	Min.	-309	13.62	9	-252.12	19	51.23	9	181.26	1	-3707.50	18	-259.30	9	-3609.37	19	-9855.95	19
401	Min.	-338	13.62	9	-252.12	19	51.23	9	181.26	1	-3707.50	18	-259.30	9	-3609.37	19	-9855.95	19
401	Min.	-336	13.62	9	-252.12	19	51.23	9	181.26	1	-3707.50	18	-259.30	9	-3609.37	19	-9855.95	19
401	Max	-353	30.96	17	47.53	18	-47.92	13	-131.67	13	-904.14	1	2158.18	19	-192.00	13	-2124.90	1
401	Max	-336	30.96	17	47.53	18	-47.92	13	-131.67	13	-904.14	1	2158.18	19	-192.00	13	-2124.90	1
401	Max	-338	30.96	17	47.53	18	-47.92	13	-131.67	13	-904.14	1	2158.18	19	-192.00	13	-2124.90	1
401	Max	-354	30.96	17	47.53	18	-47.92	13	-131.67	13	-904.14	1	2158.18	19	-192.00	13	-2124.90	1
401	Min.	-353	-306.85	18	-301.90	17	-874.83	18	-641.70	18	-2104.73	19	925.06	1	-813.18	18	-5257.80	18
401	Min.	-336	-306.85	18	-301.90	17	-874.83	18	-641.70	18	-2104.73	19	925.06	1	-813.18	18	-5257.80	18
401	Min.	-338	-306.85	18	-301.90	17	-874.83	18	-641.70	18	-2104.73	19	925.06	1	-813.18	18	-5257.80	18
401	Min.	-354	-306.85	18	-301.90	17	-874.83	18	-641.70	18	-2104.73	19	925.06	1	-813.18	18	-5257.80	18
401	Max	-309	1731.91	18	146.05	17	-75.10	9	-1854.76	1	-1012.98	5	-640.92	5	19811.80	19	-9908.23	1
401	Max	-324	1731.91	18	146.05	17	-75.10	9	-1854.76	1	-1012.98	5	-640.92	5	19811.80	19	-9908.23	1
401	Max	-354	1731.91	18	146.05	17	-75.10	9	-1854.76	1	-1012.98	5	-640.92	5	19811.80	19	-9908.23	1
401	Max	-338	1731.91	18	146.05	17	-75.10	9	-1854.76	1	-1012.98	5	-640.92	5	19811.80	19	-9908.23	1
401	Min.	-309	-63.64	13	-1027.89	18	-502.40	18	-4433.94	19	-2771.41	18	-1781.81	18	8398.08	1	-23803.90	19
401	Min.	-324	-63.64	13	-1027.89	18	-502.40	18	-4433.94	19	-2771.41	18	-1781.81	18	8398.08	1	-23803.90	19
401	Min.	-354	-63.64	13	-1027.89	18	-502.40	18	-4433.94	19	-2771.41	18	-1781.81	18	8398.08	1	-23803.90	19
401	Min.	-338	-63.64	13	-1027.89	18	-502.40	18	-4433.94	19	-2771.41	18	-1781.81	18	8398.08	1	-23803.90	19
401	Max	-323	9985.63	18	-129.82	9	42.16	9	-1015.17	20	-859.14	5	781.88	1	7550.25	19	15112.60	19

401	Max	-287	9985.63	18	-129.82	9	42.16	9	-1015.17	20	-859.14	5	781.88	1	7550.25	19	15112.60	19
401	Max	-284	9985.63	18	-129.82	9	42.16	9	-1015.17	20	-859.14	5	781.88	1	7550.25	19	15112.60	19
401	Max	-313	9985.63	18	-129.82	9	42.16	9	-1015.17	20	-859.14	5	781.88	1	7550.25	19	15112.60	19
401	Min.	-323	142.54	13	-1858.17	18	-94.44	19	-2193.38	17	-2614.30	18	-241.73	9	2827.11	1	7502.34	5
401	Min.	-287	142.54	13	-1858.17	18	-94.44	19	-2193.38	17	-2614.30	18	-241.73	9	2827.11	1	7502.34	5
401	Min.	-284	142.54	13	-1858.17	18	-94.44	19	-2193.38	17	-2614.30	18	-241.73	9	2827.11	1	7502.34	5
401	Min.	-313	142.54	13	-1858.17	18	-94.44	19	-2193.38	17	-2614.30	18	-241.73	9	2827.11	1	7502.34	5
401	Max	-287	14349.90	18	115.50	1	-27.45	13	2574.50	17	1509.00	9	1542.27	1	4249.62	18	5483.86	17
401	Max	-257	14349.90	18	115.50	1	-27.45	13	2574.50	17	1509.00	9	1542.27	1	4249.62	18	5483.86	17
401	Max	-266	14349.90	18	115.50	1	-27.45	13	2574.50	17	1509.00	9	1542.27	1	4249.62	18	5483.86	17
401	Max	-284	14349.90	18	115.50	1	-27.45	13	2574.50	17	1509.00	9	1542.27	1	4249.62	18	5483.86	17
401	Min.	-287	215.29	5	-2048.97	18	-6388.90	18	1114.68	20	-2727.97	18	-887.49	9	-1998.71	13	-2366.15	18
401	Min.	-257	215.29	5	-2048.97	18	-6388.90	18	1114.68	20	-2727.97	18	-887.49	9	-1998.71	13	-2366.15	18
401	Min.	-266	215.29	5	-2048.97	18	-6388.90	18	1114.68	20	-2727.97	18	-887.49	9	-1998.71	13	-2366.15	18
401	Min.	-284	215.29	5	-2048.97	18	-6388.90	18	1114.68	20	-2727.97	18	-887.49	9	-1998.71	13	-2366.15	18
401	Max	-284	1621.33	18	1855.08	18	-95.88	9	987.39	17	1008.98	9	731.60	1	5321.03	18	4047.25	9
401	Max	-266	1621.33	18	1855.08	18	-95.88	9	987.39	17	1008.98	9	731.60	1	5321.03	18	4047.25	9
401	Max	-274	1621.33	18	1855.08	18	-95.88	9	987.39	17	1008.98	9	731.60	1	5321.03	18	4047.25	9
401	Max	-313	1621.33	18	1855.08	18	-95.88	9	987.39	17	1008.98	9	731.60	1	5321.03	18	4047.25	9
401	Min.	-284	11.61	1	-124.79	17	-2189.40	18	80.91	18	-1206.87	1	-92.54	9	650.46	9	535.38	1
401	Min.	-266	11.61	1	-124.79	17	-2189.40	18	80.91	18	-1206.87	1	-92.54	9	650.46	9	535.38	1
401	Min.	-274	11.61	1	-124.79	17	-2189.40	18	80.91	18	-1206.87	1	-92.54	9	650.46	9	535.38	1
401	Min.	-313	11.61	1	-124.79	17	-2189.40	18	80.91	18	-1206.87	1	-92.54	9	650.46	9	535.38	1
401	Max	-313	-2.04	5	-110.10	9	1320.60	18	-1285.02	5	-916.28	1	-574.08	1	-4744.08	1	8209.49	19
401	Max	-353	-2.04	5	-110.10	9	1320.60	18	-1285.02	5	-916.28	1	-574.08	1	-4744.08	1	8209.49	19
401	Max	-352	-2.04	5	-110.10	9	1320.60	18	-1285.02	5	-916.28	1	-574.08	1	-4744.08	1	8209.49	19
401	Max	-323	-2.04	5	-110.10	9	1320.60	18	-1285.02	5	-916.28	1	-574.08	1	-4744.08	1	8209.49	19
401	Min.	-313	-359.84	18	-613.35	18	16.10	13	-2884.72	19	-2078.30	19	-1298.65	19	-10424.10	19	3646.33	13
401	Min.	-353	-359.84	18	-613.35	18	16.10	13	-2884.72	19	-2078.30	19	-1298.65	19	-10424.10	19	3646.33	13
401	Min.	-352	-359.84	18	-613.35	18	16.10	13	-2884.72	19	-2078.30	19	-1298.65	19	-10424.10	19	3646.33	13
401	Min.	-323	-359.84	18	-613.35	18	16.10	13	-2884.72	19	-2078.30	19	-1298.65	19	-10424.10	19	3646.33	13
401	Max	-328	4905.16	18	653.75	17	-447.40	5	-1297.78	13	-29.54	5	839.73	17	-5020.45	13	9764.13	19
401	Max	-295	4905.16	18	653.75	17	-447.40	5	-1297.78	13	-29.54	5	839.73	17	-5020.45	13	9764.13	19
401	Max	-299	4905.16	18	653.75	17	-447.40	5	-1297.78	13	-29.54	5	839.73	17	-5020.45	13	9764.13	19
401	Max	-326	4905.16	18	653.75	17	-447.40	5	-1297.78	13	-29.54	5	839.73	17	-5020.45	13	9764.13	19
401	Min.	-328	-119.91	5	-42.62	18	-3430.31	18	-2987.69	19	-886.21	18	47.44	18	-11655.50	19	3896.45	13
401	Min.	-295	-119.91	5	-42.62	18	-3430.31	18	-2987.69	19	-886.21	18	47.44	18	-11655.50	19	3896.45	13
401	Min.	-299	-119.91	5	-42.62	18	-3430.31	18	-2987.69	19	-886.21	18	47.44	18	-11655.50	19	3896.45	13
401	Min.	-326	-119.91	5	-42.62	18	-3430.31	18	-2987.69	19	-886.21	18	47.44	18	-11655.50	19	3896.45	13
401	Max	-295	8561.46	18	536.70	17	-590.08	5	2145.42	19	1891.05	19	1170.68	17	58.47	18	5204.60	19
401	Max	-258	8561.46	18	536.70	17	-590.08	5	2145.42	19	1891.05	19	1170.68	17	58.47	18	5204.60	19
401	Max	-272	8561.46	18	536.70	17	-590.08	5	2145.42	19	1891.05	19	1170.68	17	58.47	18	5204.60	19
401	Max	-299	8561.46	18	536.70	17	-590.08	5	2145.42	19	1891.05	19	1170.68	17	58.47	18	5204.60	19
401	Min.	-295	-537.95	5	-1118.15	18	-5171.54	18	667.54	13	427.78	20	39.62	9	-2802.12	19	1008.19	20
401	Min.	-258	-537.95	5	-1118.15	18	-5171.54	18	667.54	13	427.78	20	39.62	9	-2802.12	19	1008.19	20
401	Min.	-272	-537.95	5	-1118.15	18	-5171.54	18	667.54	13	427.78	20	39.62	9	-2802.12	19	1008.19	20
401	Min.	-299	-537.95	5	-1118.15	18	-5171.54	18	667.54	13	427.78	20	39.62	9	-2802.12	19	1008.19	20
401	Max	-299	5784.07	18	298.14	17	-568.04	5	-458.61	13	-851.75	1	1510.96	17	-2176.99	13	13603.60	19
401	Max	-272	5784.07	18	298.14	17	-568.04	5	-458.61	13	-851.75	1	1510.96	17	-2176.99	13	13603.60	19
401	Max	-278	5784.07	18	298.14	17	-568.04	5	-458.61	13	-851.75	1	1510.96	17	-2176.99	13	13603.60	19
401	Max	-326	5784.07	18	298.14	17	-568.04	5	-458.61	13	-851.75	1	1510.96	17	-2176.99	13	13603.60	19
401	Min.	-299	235.47	5	-296.60	18	-4026.54	18	-970.72	19	-2433.44	18	449.17	20	-5495.23	19	5262.95	9
401	Min.	-272	235.47	5	-296.60	18	-4026.54	18	-970.72	19	-2433.44	18	449.17	20	-5495.23	19	5262.95	9
401	Min.	-278	235.47	5	-296.60	18	-4026.54	18	-970.72	19	-2433.44	18	449.17	20	-5495.23	19	5262.95	9
401	Min.	-326	235.47	5	-296.60	18	-4026.54	18	-970.72	19	-2433.44	18	449.17	20	-5495.23	19	5262.95	9
401	Max	-278	-305.83	1	2157.42	18	803.19	17	-370.85	5	-766.14	13	-548.17	13	-3186.38	9	7520.94	19
401	Max	-270	-305.83	1	2157.42	18	803.19	17	-370.85	5	-766.14	13	-548.17	13	-3186.38	9	7520.94	19
401	Max	-315	-305.83	1	2157.42	18	803.19	17	-370.85	5	-766.14	13	-548.17	13	-3186.38	9	7520.94	19
401	Max	-326	-305.83	1	2157.42	18	803.19	17	-370.85	5	-766.14	13	-548.17	13	-3186.38	9	7520.94	19
401	Min.	-278	-757.92	17	-7.41	5	163.03	20	-1354.45	18	-1714.65	19	-1253.33	19	-8603.50	19	3058.41	9
401	Min.	-270	-757.92	17	-7.41	5	163.03	20	-1354.45	18	-1714.65	19	-1253.33	19	-8603.50	19	3058.41	9
401	Min.	-315	-757.92	17	-7.41	5	163.03	20	-1354.45	18	-1714.65	19	-1253.33	19	-8603.50	19	3058.41	9
401	Min.	-326	-757.92	17	-7.41	5	163.03	20	-1354.45	18	-1714.65	19	-1253.33	19	-8603.50	19	3058.41	9
401	Max	-326	400.54	18	53.29	5	-149.29	1	-1108.71	9	-912.25	1	1220.28	19	6711.84	19	3985.57	19
401	Max	-315	400.54	18	53.29	5	-149.29	1	-1108.71	9	-912.25	1	1220.28	19	6711.84	19	3985.57	19
401	Max	-361	400.54	18	53.29	5	-149.29	1	-1108.71	9	-912.25	1	1220.28	19	6711.84	19	3985.57	19
401	Max	-360	400.54	18	53.29	5	-149.29	1	-1108.71	9	-912.25	1	1220.28	19	6711.84	19	3985.57	19
401	Min.	-326	32.29	5	-401.54	18	-612.78	18	-2767.56	19	-2260.73	18	499.79	9	2907.38	9	1631.49	9
401	Min.	-315	32.29	5	-401.54	18	-612.78	18	-2767.56	19	-2260.73	18	499.79	9	2907.38	9	1631.49	9
401	Min.	-361	32.29	5	-401.54	18	-612.78	18	-2767.56	19	-2260.73	18	499.79	9	2907.38	9	1631.49	9
401	Min.	-360	32.29	5	-401.54	18	-612.78	18	-2767.56	19	-2260.73	18	499.79	9	2907.38	9	1631.49	9
401	Max	-326	11.44	5	912.28	17	239.22	5	-718.31	5	-507.24	13	1245.73	19	8130.55	19	6972.26	19
401	Max	-360	11.44	5	912.28	17	239.22	5	-718.31	5	-507.24	13	1245.73	19	8130.55	19	6972.26	19
401	Max	-359	11.44	5	912.28	17	239.22	5	-718.31	5	-507.24	13	1245.73	19	8130.55	19	6972.26	19
401	Max	-328	11.44	5	912.28	17	239.22	5	-718.31	5	-507.24	13	1245.73	19	8130.55	19	6972.26	19
401	Min.	-326	-874.78	18	289.39	20	-1481.39	18	-1858.09	18	-1163.46	19	533.21	13	3448.05	13	3051.34	13
401	Min.	-360	-874.78	18	289.39	20	-1481.39	18	-1858.09	18	-1163.46	19	533.21	13	3448.05	13	3051.34	13
401	Min.	-359	-874.78	18	289.39	20	-1481.39	18	-1858.09	18	-1163.46	19	533.21	13	3448.05	13	3051.34	13
401	Min.	-328	-874.78	18	289.39	20	-1481.39	18	-1858.09	18	-1163.46	19	533.21	13	3448.05	13	3051.34	13
401	Max	-200	524.13	5	8486.51	17	4287.24	17	-1388.06	13	-568.70	1	-133.97	20	13305.30	19	21926.50	19
401	Max	-220	524.13	5	8486.51	17	4287.24	17	-1388.06	13	-568.70	1	-133.97	20	13305.30	19	21926.50	19
401	Max	-212	524.13	5	8486.51	17	4287.24	17	-1388.06	13	-568.70	1	-133.97	20	13305.30	19	21926.50	19
401	Max	-199	524.13	5	8486.51	17	4287.24	17	-1388.06	13	-568.70	1	-133.97	20	13305.30	19	21926.50	19
401	Min.	-200	-4697.57	18	3105.44	1	-1919.64	18	-3253.45	19	-3630.12	17	-1191.41	17	4494.50	9	8743.99	13
401	Min.	-220	-4697.57	18	3105.44	1	-1919.64	18	-3253.45	19	-3630.12	17	-1191.41	17	4494.50	9	8743.99	13
401	Min.	-212	-4697.57	18	3105.44	1	-1919.64	18	-3253.45	19	-3630.12	17	-1191.41	17	4494.50	9	8743.99	13
401	Min.	-199	-4697.57	18	3105.44	1	-1919.64	18	-3253.45	19	-3630.12	17	-1191.41	17	4494.50	9	8743.99	13
401	Max	-220	62.36	1	3311.88	17	564.75	5	2408.15	19	-21.39	1	1324.78	18	3019.82	1	7761.03	19
401	Max	-249	62.36	1	3311.88	17	564.75	5	2408.15	19	-21.39	1	1324.78	18	3019.82	1	7761.03	19
401	Max	-239	62.36	1	3311.88	17	564.75	5	2408.15	19	-21.39	1	1324.78	18	3019.82	1	7761.03	19
401	Max	-212	62.36	1	3311.88	17	564.75	5	2408.15	19	-21.39	1	1324.78	18	3019.82	1	7761.03	19
401	Min.	-220	-1010.68	18	1335.86	9	-3797.13	18	836.67	13	-1794.24	18	511.32	1	-255.62	9	3281.27	13
401	Min.	-249	-1010.68	18	1335.86	9	-3797.13	18	836.67	13	-1794.24	18	511.32	1	-255.62	9	3281.27	13
401	Min.	-239	-1010.68	18	1335.86	9	-3797.13	18	836.67	13	-1794.24	18	511.32	1	-255.62	9	3281.27	13
401	Min.	-212	-1010.68	18	1335.86	9	-3797.13	18	836.67	13	-1794.24	18	511.32	1	-255.62	9	3281.27	13
401	Max	-212	1380.00	18	7775.59	17	740.69	5	369.22	5	1966.00	1	1196.17	18	10380.40	19	3147.79	19
401	Max	-239	1380.00	18	7775.59	17	740.69	5	369.22	5	1966.00	1	1196.17	18	10380.40	19	3147.79	19
401	Max	-237	1380.00	18	7775.59	17	740.69	5	369.22	5	1966.00	1	1196.17	18	10380.40	19	3147.79	19
401	Max	-199	1380.00	18	7775.59	17	740.69	5	369.22	5	1966.00	1	1196.17	18	10380.40	19	3147.79	19
401	Min.	-212	199.46	5	2343.03	20	-6127.09	18	-732.80	18	-2320.42	9	151.97	1	2587.95	9	772.81	20
401	Min.	-239	199.46	5	2343.03	20	-6127.09	18	-732.80	18	-2320.42	9	151.97	1	2587.95	9	772.81	20
401	Min.	-237	199.46	5	2343.03	20	-6127.09	18	-732.80	18	-2320.42	9	151.97	1	2587.95	9	772.81	20
401	Min.	-199	199.46	5	2343.03	20	-6127.09	18	-732.80	18	-2320.42	9	151.97	1	2587.95	9	772.81	20
401	Max	-239	2106.59	18	749.15	18	3186.30	18	-190.48	1	3601.71	19	165.65	19	849.27	9	692.19	18
401	Max	-249	2106.59	18	749.15	18	3186.30	18	-190.48	1	3601.71	19	165.65	19	849.27	9	692.19	18
401	Max	-278	2106.59	18	749.15	18	3186.30	18	-190.48	1	3601.71	19	165.65	19	849.27	9	692.19	18
401	Max	-272	2106.59	18	749.15	18	3186.30	18	-190.48	1	3601.71	19	165.65	19	849.27	9	692.19	18
401	Min.	-239	860.70	1	-140.86	5	77.24	5	-1354.37	18	1384.74	13	-290.93	17	-112.58	1	-1847.47	1
401	Min.	-249	860.70	1	-140.86	5	77.24	5	-1354.37	18	1384.74	13	-290.93	17	-112.58	1	-1847.47	1

401	Min.	-278	860.70	1	-140.86	5	77.24	5	-1354.37	18	1384.74	13	-290.93	17	-112.58	1	-1847.47	1
401	Min.	-272	860.70	1	-140.86	5	77.24	5	-1354.37	18	1384.74	13	-290.93	17	-112.58	1	-1847.47	1
401	Max	-239	2738.64	18	3704.35	17	63.73	5	2875.20	19	2342.36	1	1628.52	17	5155.59	5	264.87	9
401	Max	-272	2738.64	18	3704.35	17	63.73	5	2875.20	19	2342.36	1	1628.52	17	5155.59	5	264.87	9
401	Max	-258	2738.64	18	3704.35	17	63.73	5	2875.20	19	2342.36	1	1628.52	17	5155.59	5	264.87	9
401	Max	-237	2738.64	18	3704.35	17	63.73	5	2875.20	19	2342.36	1	1628.52	17	5155.59	5	264.87	9
401	Min.	-239	30.11	5	788.30	20	-7305.35	18	847.42	13	-1039.04	9	359.06	9	-1985.60	18	-1337.53	18
401	Min.	-272	30.11	5	788.30	20	-7305.35	18	847.42	13	-1039.04	9	359.06	9	-1985.60	18	-1337.53	18
401	Min.	-258	30.11	5	788.30	20	-7305.35	18	847.42	13	-1039.04	9	359.06	9	-1985.60	18	-1337.53	18
401	Min.	-237	30.11	5	788.30	20	-7305.35	18	847.42	13	-1039.04	9	359.06	9	-1985.60	18	-1337.53	18
401	Max	-278	267.82	18	681.03	18	-152.30	5	3675.08	19	-172.28	9	550.80	17	99.02	9	-302.72	1
401	Max	-249	267.82	18	681.03	18	-152.30	5	3675.08	19	-172.28	9	550.80	17	99.02	9	-302.72	1
401	Max	-251	267.82	18	681.03	18	-152.30	5	3675.08	19	-172.28	9	550.80	17	99.02	9	-302.72	1
401	Max	-270	267.82	18	681.03	18	-152.30	5	3675.08	19	-172.28	9	550.80	17	99.02	9	-302.72	1
401	Min.	-278	-397.68	17	268.40	1	-1135.61	18	1420.14	13	-588.89	19	242.55	13	-785.64	1	-1101.99	18
401	Min.	-249	-397.68	17	268.40	1	-1135.61	18	1420.14	13	-588.89	19	242.55	13	-785.64	1	-1101.99	18
401	Min.	-251	-397.68	17	268.40	1	-1135.61	18	1420.14	13	-588.89	19	242.55	13	-785.64	1	-1101.99	18
401	Min.	-270	-397.68	17	268.40	1	-1135.61	18	1420.14	13	-588.89	19	242.55	13	-785.64	1	-1101.99	18
401	Max	-249	-254.00	5	2750.58	18	282.29	17	2944.65	19	-1186.96	9	-208.89	9	423.44	9	-2918.44	13
401	Max	-220	-254.00	5	2750.58	18	282.29	17	2944.65	19	-1186.96	9	-208.89	9	423.44	9	-2918.44	13
401	Max	-226	-254.00	5	2750.58	18	282.29	17	2944.65	19	-1186.96	9	-208.89	9	423.44	9	-2918.44	13
401	Max	-251	-254.00	5	2750.58	18	282.29	17	2944.65	19	-1186.96	9	-208.89	9	423.44	9	-2918.44	13
401	Min.	-249	-2393.21	18	1079.88	1	-1076.95	18	1093.45	9	-2782.54	19	-857.25	19	-1391.10	1	-6910.93	19
401	Min.	-220	-2393.21	18	1079.88	1	-1076.95	18	1093.45	9	-2782.54	19	-857.25	19	-1391.10	1	-6910.93	19
401	Min.	-226	-2393.21	18	1079.88	1	-1076.95	18	1093.45	9	-2782.54	19	-857.25	19	-1391.10	1	-6910.93	19
401	Min.	-251	-2393.21	18	1079.88	1	-1076.95	18	1093.45	9	-2782.54	19	-857.25	19	-1391.10	1	-6910.93	19
401	Max	-270	-405.73	1	745.69	18	-394.86	20	872.98	19	-157.75	1	2122.21	19	-228.92	1	-1606.67	13
401	Max	-251	-405.73	1	745.69	18	-394.86	20	872.98	19	-157.75	1	2122.21	19	-228.92	1	-1606.67	13
401	Max	-226	-405.73	1	745.69	18	-394.86	20	872.98	19	-157.75	1	2122.21	19	-228.92	1	-1606.67	13
401	Max	-210	-405.73	1	745.69	18	-394.86	20	872.98	19	-157.75	1	2122.21	19	-228.92	1	-1606.67	13
401	Min.	-270	-1014.16	18	-220.91	5	-1098.98	17	283.32	9	-683.16	18	838.37	13	-1083.24	18	-3519.18	19
401	Min.	-251	-1014.16	18	-220.91	5	-1098.98	17	283.32	9	-683.16	18	838.37	13	-1083.24	18	-3519.18	19
401	Min.	-226	-1014.16	18	-220.91	5	-1098.98	17	283.32	9	-683.16	18	838.37	13	-1083.24	18	-3519.18	19
401	Min.	-210	-1014.16	18	-220.91	5	-1098.98	17	283.32	9	-683.16	18	838.37	13	-1083.24	18	-3519.18	19
401	Max	-220	588.76	5	-262.96	20	3618.82	17	-1172.50	13	-1243.32	9	-947.40	13	5969.36	18	-6879.20	9
401	Max	-200	588.76	5	-262.96	20	3618.82	17	-1172.50	13	-1243.32	9	-947.40	13	5969.36	18	-6879.20	9
401	Max	-210	588.76	5	-262.96	20	3618.82	17	-1172.50	13	-1243.32	9	-947.40	13	5969.36	18	-6879.20	9
401	Max	-226	588.76	5	-262.96	20	3618.82	17	-1172.50	13	-1243.32	9	-947.40	13	5969.36	18	-6879.20	9
401	Min.	-220	-3680.88	18	-851.47	17	1403.43	1	-2848.97	19	-3003.52	19	-2060.17	19	2446.09	5	-17502.00	19
401	Min.	-200	-3680.88	18	-851.47	17	1403.43	1	-2848.97	19	-3003.52	19	-2060.17	19	2446.09	5	-17502.00	19
401	Min.	-210	-3680.88	18	-851.47	17	1403.43	1	-2848.97	19	-3003.52	19	-2060.17	19	2446.09	5	-17502.00	19
401	Min.	-226	-3680.88	18	-851.47	17	1403.43	1	-2848.97	19	-3003.52	19	-2060.17	19	2446.09	5	-17502.00	19
401	Max	-99	776.41	18	241.38	18	472.76	9	1446.09	1	1128.58	1	1652.49	1	-1753.97	9	14455.70	18
401	Max	-87	776.41	18	241.38	18	472.76	9	1446.09	1	1128.58	1	1652.49	1	-1753.97	9	14455.70	18
401	Max	-116	776.41	18	241.38	18	472.76	9	1446.09	1	1128.58	1	1652.49	1	-1753.97	9	14455.70	18
401	Max	-121	776.41	18	241.38	18	472.76	9	1446.09	1	1128.58	1	1652.49	1	-1753.97	9	14455.70	18
401	Min.	-99	-79.15	9	-1456.72	1	-655.62	18	-974.04	9	-2698.03	9	-1541.24	9	-8423.70	18	5488.35	1
401	Min.	-87	-79.15	9	-1456.72	1	-655.62	18	-974.04	9	-2698.03	9	-1541.24	9	-8423.70	18	5488.35	1
401	Min.	-116	-79.15	9	-1456.72	1	-655.62	18	-974.04	9	-2698.03	9	-1541.24	9	-8423.70	18	5488.35	1
401	Min.	-121	-79.15	9	-1456.72	1	-655.62	18	-974.04	9	-2698.03	9	-1541.24	9	-8423.70	18	5488.35	1
401	Max	-99	2616.14	17	739.29	9	543.78	5	5311.22	18	5636.47	1	880.53	1	4084.86	9	-851.53	9
401	Max	-67	2616.14	17	739.29	9	543.78	5	5311.22	18	5636.47	1	880.53	1	4084.86	9	-851.53	9
401	Max	-71	2616.14	17	739.29	9	543.78	5	5311.22	18	5636.47	1	880.53	1	4084.86	9	-851.53	9
401	Max	-87	2616.14	17	739.29	9	543.78	5	5311.22	18	5636.47	1	880.53	1	4084.86	9	-851.53	9
401	Min.	-99	1409.42	5	-1231.06	1	-1685.19	18	1556.06	9	-5114.47	9	-1009.10	9	-6938.30	1	-2723.77	19
401	Min.	-67	1409.42	5	-1231.06	1	-1685.19	18	1556.06	9	-5114.47	9	-1009.10	9	-6938.30	1	-2723.77	19
401	Min.	-71	1409.42	5	-1231.06	1	-1685.19	18	1556.06	9	-5114.47	9	-1009.10	9	-6938.30	1	-2723.77	19
401	Min.	-87	1409.42	5	-1231.06	1	-1685.19	18	1556.06	9	-5114.47	9	-1009.10	9	-6938.30	1	-2723.77	19
401	Max	-67	1453.68	17	935.42	18	111.81	9	2458.26	18	5216.44	1	851.47	1	2775.38	9	-4551.25	13
401	Max	-50	1453.68	17	935.42	18	111.81	9	2458.26	18	5216.44	1	851.47	1	2775.38	9	-4551.25	13
401	Max	-58	1453.68	17	935.42	18	111.81	9	2458.26	18	5216.44	1	851.47	1	2775.38	9	-4551.25	13
401	Max	-71	1453.68	17	935.42	18	111.81	9	2458.26	18	5216.44	1	851.47	1	2775.38	9	-4551.25	13
401	Min.	-67	-2161.39	18	-777.37	1	-3564.12	18	-302.80	9	-5773.78	9	-1835.13	9	-5531.44	18	-14253.50	18
401	Min.	-50	-2161.39	18	-777.37	1	-3564.12	18	-302.80	9	-5773.78	9	-1835.13	9	-5531.44	18	-14253.50	18
401	Min.	-58	-2161.39	18	-777.37	1	-3564.12	18	-302.80	9	-5773.78	9	-1835.13	9	-5531.44	18	-14253.50	18
401	Min.	-71	-2161.39	18	-777.37	1	-3564.12	18	-302.80	9	-5773.78	9	-1835.13	9	-5531.44	18	-14253.50	18
401	Max	-87	15.70	9	1050.62	9	438.24	1	1766.27	1	1995.58	1	1642.64	9	3096.19	9	-2080.57	1
401	Max	-71	15.70	9	1050.62	9	438.24	1	1766.27	1	1995.58	1	1642.64	9	3096.19	9	-2080.57	1
401	Max	-58	15.70	9	1050.62	9	438.24	1	1766.27	1	1995.58	1	1642.64	9	3096.19	9	-2080.57	1
401	Max	-47	15.70	9	1050.62	9	438.24	1	1766.27	1	1995.58	1	1642.64	9	3096.19	9	-2080.57	1
401	Min.	-87	-716.47	18	-266.22	1	-201.51	9	-570.73	9	-2865.81	9	-921.76	1	-5617.85	1	-7124.18	18
401	Min.	-71	-716.47	18	-266.22	1	-201.51	9	-570.73	9	-2865.81	9	-921.76	1	-5617.85	1	-7124.18	18
401	Min.	-58	-716.47	18	-266.22	1	-201.51	9	-570.73	9	-2865.81	9	-921.76	1	-5617.85	1	-7124.18	18
401	Min.	-47	-716.47	18	-266.22	1	-201.51	9	-570.73	9	-2865.81	9	-921.76	1	-5617.85	1	-7124.18	18
401	Max	-50	783.05	5	31.94	9	201.49	9	-1597.58	13	1820.71	1	1891.55	1	2728.66	13	-12876.40	13
401	Max	-38	783.05	5	31.94	9	201.49	9	-1597.58	13	1820.71	1	1891.55	1	2728.66	13	-12876.40	13
401	Max	-47	783.05	5	31.94	9	201.49	9	-1597.58	13	1820.71	1	1891.55	1	2728.66	13	-12876.40	13
401	Max	-58	783.05	5	31.94	9	201.49	9	-1597.58	13	1820.71	1	1891.55	1	2728.66	13	-12876.40	13
401	Min.	-50	-7636.56	18	-527.88	1	-1804.71	18	-4898.26	18	-4022.80	9	-3211.36	9	-970.68	18	-46448.50	18
401	Min.	-38	-7636.56	18	-527.88	1	-1804.71	18	-4898.26	18	-4022.80	9	-3211.36	9	-970.68	18	-46448.50	18
401	Min.	-47	-7636.56	18	-527.88	1	-1804.71	18	-4898.26	18	-4022.80	9	-3211.36	9	-970.68	18	-46448.50	18
401	Min.	-58	-7636.56	18	-527.88	1	-1804.71	18	-4898.26	18	-4022.80	9	-3211.36	9	-970.68	18	-46448.50	18
401	Max	-38	71.23	18	196.18	18	541.17	18	-1275.10	1	-524.14	13	922.05	18	15556.30	18	6868.50	18
401	Max	-10	71.23	18	196.18	18	541.17	18	-1275.10	1	-524.14	13	922.05	18	15556.30	18	6868.50	18
401	Max	-11	71.23	18	196.18	18	541.17	18	-1275.10	1	-524.14	13	922.05	18	15556.30	18	6868.50	18
401	Max	-47	71.23	18	196.18	18	541.17	18	-1275.10	1	-524.14	13	922.05	18	15556.30	18	6868.50	18
401	Min.	-38	-39.89	1	-317.40	9	-118.64	13	-3085.80	18	-1305.70	19	204.01	9	5469.00	9	2476.97	1
401	Min.	-10	-39.89	1	-317.40	9	-118.64	13	-3085.80	18	-1305.70	19	204.01	9	5469.00	9	2476.97	1
401	Min.	-11	-39.89	1	-317.40	9	-118.64	13	-3085.80	18	-1305.70	19	204.01	9	5469.00	9	2476.97	1
401	Min.	-47	-39.89	1	-317.40	9	-118.64	13	-3085.80	18	-1305.70	19	204.01	9	5469.00	9	2476.97	1
401	Max	-55	136.27	1	330.14	9	156.10	1	1353.03	18	2355.17	1	-72.15	9	1918.59	1	1550.48	18
401	Max	-79	136.27	1	330.14	9	156.10	1	1353.03	18	2355.17	1	-72.15	9	1918.59	1	1550.48	18
401	Max	-87	136.27	1	330.14	9	156.10	1	1353.03	18	2355.17	1	-72.15	9	1918.59	1	1550.48	18
401	Max	-47	136.27	1	330.14	9	156.10	1	1353.03	18	2355.17	1	-72.15	9	1918.59	1	1550.48	18
401	Min.	-55	-110.09	9	-362.20	1	-166.68	18	105.99	9	-815.89	9	-426.54	18	-2582.09	9	24.00	9
401	Min.	-79	-110.09	9	-362.20	1	-166.68	18	105.99	9	-815.89	9	-426.54	18	-2582.09	9	24.00	9
401	Min.	-87	-110.09	9	-362.20	1	-166.68	18	105.99	9	-815.89	9	-426.54	18	-2582.09	9	24.00	9
401	Min.	-47	-110.09	9	-362.20	1	-166.68	18	105.99	9	-815.89	9	-426.54	18	-2582.09	9	24.00	9
401	Max	-78	168.29	9	74.53	5	432.55	18	649.67	1	1013.41	18	-349.00	9	-550.10	9	5221.60	18
401	Max	-79	168.29	9	74.53	5	432.55	18	649.67	1	1013.41	18	-349.00	9	-550.10	9	5221.60	18
401	Max	-55	168.29	9	74.53	5	432.55	18	649.67	1	1013.41	18	-349.00	9	-550.10	9	5221.60	18
401	Max	-53	168.29	9	74.53	5	432.55	18	649.67	1	1013.41	18	-349.00	9	-550.10	9	5221.60	18
401	Min.	-78	-325.60	1	-375.46	18	-242.94	9	-265.54	9	140.76	9	-1072.41	19	-2123.90	18	823.74	9
401	Min.	-79	-325.60	1	-375.46	18	-242.94	9	-265.54	9	140.76	9	-1072.41	19	-2123.90	18	823.74	9
401	Min.	-55	-325.60	1	-375.46	18	-242.94	9	-265.54	9	140.76	9	-1072.41	19	-2123.90	18	823.74	9
401	Min.	-53	-325.60	1	-375.46	18	-242.94	9	-265.54	9	140.76	9	-1072.41	19	-2123.90	18	823.74	9
401	Max	-78	-16.77	5	197.30	9	370.14	17	-228.09	1	-1482.45	9	1063.27	19	-3615.69	9	-5776.32	9
401	Max	-53	-16.77	5	197.30	9	370.14	17	-228.09	1	-1482.45	9	1063.27	19	-3615.69	9	-5776.32	9
401	Max	-39	-16.77	5	197.30	9	370.14	17	-228.09	1	-1482.45	9	1063.27	19	-3615.69	9	-5776.32	9

401	Max	-85	-16.77	5	197.30	9	370.14	17	-228.09	1	-1482.45	9	1063.27	19	-3615.69	9	-5776.32	9
401	Min.	-78	-712.34	18	-382.48	18	-302.13	18	-627.48	19	-4251.93	18	213.52	1	-11323.60	18	-14866.50	18
401	Min.	-53	-712.34	18	-382.48	18	-302.13	18	-627.48	19	-4251.93	18	213.52	1	-11323.60	18	-14866.50	18
401	Min.	-39	-712.34	18	-382.48	18	-302.13	18	-627.48	19	-4251.93	18	213.52	1	-11323.60	18	-14866.50	18
401	Min.	-85	-712.34	18	-382.48	18	-302.13	18	-627.48	19	-4251.93	18	213.52	1	-11323.60	18	-14866.50	18
401	Max	-39	316.62	9	470.96	18	469.01	18	-1011.77	9	-1440.60	13	1573.31	18	10533.20	18	17871.20	18
401	Max	-53	316.62	9	470.96	18	469.01	18	-1011.77	9	-1440.60	13	1573.31	18	10533.20	18	17871.20	18
401	Max	-23	316.62	9	470.96	18	469.01	18	-1011.77	9	-1440.60	13	1573.31	18	10533.20	18	17871.20	18
401	Max	-12	316.62	9	470.96	18	469.01	18	-1011.77	9	-1440.60	13	1573.31	18	10533.20	18	17871.20	18
401	Min.	-39	-497.66	18	-69.45	5	5.00	1	-3268.95	18	-3464.55	19	605.03	9	4081.63	9	6193.51	9
401	Min.	-53	-497.66	18	-69.45	5	5.00	1	-3268.95	18	-3464.55	19	605.03	9	4081.63	9	6193.51	9
401	Min.	-23	-497.66	18	-69.45	5	5.00	1	-3268.95	18	-3464.55	19	605.03	9	4081.63	9	6193.51	9
401	Min.	-12	-497.66	18	-69.45	5	5.00	1	-3268.95	18	-3464.55	19	605.03	9	4081.63	9	6193.51	9
401	Max	-53	306.68	9	-1.81	1	261.78	18	1875.37	19	-1069.84	13	645.84	18	-814.66	9	7067.36	18
401	Max	-55	306.68	9	-1.81	1	261.78	18	1875.37	19	-1069.84	13	645.84	18	-814.66	9	7067.36	18
401	Max	-25	306.68	9	-1.81	1	261.78	18	1875.37	19	-1069.84	13	645.84	18	-814.66	9	7067.36	18
401	Max	-23	306.68	9	-1.81	1	261.78	18	1875.37	19	-1069.84	13	645.84	18	-814.66	9	7067.36	18
401	Min.	-53	-254.50	1	-264.56	18	-220.21	9	320.22	9	-2588.65	19	96.18	9	-2958.83	18	1563.88	9
401	Min.	-55	-254.50	1	-264.56	18	-220.21	9	320.22	9	-2588.65	19	96.18	9	-2958.83	18	1563.88	9
401	Min.	-25	-254.50	1	-264.56	18	-220.21	9	320.22	9	-2588.65	19	96.18	9	-2958.83	18	1563.88	9
401	Min.	-23	-254.50	1	-264.56	18	-220.21	9	320.22	9	-2588.65	19	96.18	9	-2958.83	18	1563.88	9
401	Max	-12	25.96	5	204.48	18	-83.15	1	-1520.06	13	1317.02	18	113.74	9	3483.44	19	42.53	1
401	Max	-23	25.96	5	204.48	18	-83.15	1	-1520.06	13	1317.02	18	113.74	9	3483.44	19	42.53	1
401	Max	-25	25.96	5	204.48	18	-83.15	1	-1520.06	13	1317.02	18	113.74	9	3483.44	19	42.53	1
401	Max	-11	25.96	5	204.48	18	-83.15	1	-1520.06	13	1317.02	18	113.74	9	3483.44	19	42.53	1
401	Min.	-12	-501.53	18	-189.61	17	-234.00	17	-3617.48	18	225.79	9	-93.05	1	1250.37	9	-499.12	9
401	Min.	-23	-501.53	18	-189.61	17	-234.00	17	-3617.48	18	225.79	9	-93.05	1	1250.37	9	-499.12	9
401	Min.	-25	-501.53	18	-189.61	17	-234.00	17	-3617.48	18	225.79	9	-93.05	1	1250.37	9	-499.12	9
401	Min.	-11	-501.53	18	-189.61	17	-234.00	17	-3617.48	18	225.79	9	-93.05	1	1250.37	9	-499.12	9
401	Max	-55	-27.64	20	148.63	13	421.43	18	2415.47	18	-328.10	1	216.96	9	-238.36	9	880.46	1
401	Max	-47	-27.64	20	148.63	13	421.43	18	2415.47	18	-328.10	1	216.96	9	-238.36	9	880.46	1
401	Max	-11	-27.64	20	148.63	13	421.43	18	2415.47	18	-328.10	1	216.96	9	-238.36	9	880.46	1
401	Max	-25	-27.64	20	148.63	13	421.43	18	2415.47	18	-328.10	1	216.96	9	-238.36	9	880.46	1
401	Min.	-55	-187.34	17	-815.78	18	-166.81	9	128.05	9	-1411.97	18	-372.07	1	-2745.73	18	-769.42	9
401	Min.	-47	-187.34	17	-815.78	18	-166.81	9	128.05	9	-1411.97	18	-372.07	1	-2745.73	18	-769.42	9
401	Min.	-11	-187.34	17	-815.78	18	-166.81	9	128.05	9	-1411.97	18	-372.07	1	-2745.73	18	-769.42	9
401	Min.	-25	-187.34	17	-815.78	18	-166.81	9	128.05	9	-1411.97	18	-372.07	1	-2745.73	18	-769.42	9
401	Max	-87	378.78	9	232.65	13	886.73	18	1841.63	1	954.83	18	74.18	5	1478.64	9	1374.49	9
401	Max	-79	378.78	9	232.65	13	886.73	18	1841.63	1	954.83	18	74.18	5	1478.64	9	1374.49	9
401	Max	-104	378.78	9	232.65	13	886.73	18	1841.63	1	954.83	18	74.18	5	1478.64	9	1374.49	9
401	Max	-116	378.78	9	232.65	13	886.73	18	1841.63	1	954.83	18	74.18	5	1478.64	9	1374.49	9
401	Min.	-87	-498.29	1	-1015.88	18	-74.51	5	-1075.45	9	116.98	13	-322.47	18	-828.59	1	-3853.62	1
401	Min.	-79	-498.29	1	-1015.88	18	-74.51	5	-1075.45	9	116.98	13	-322.47	18	-828.59	1	-3853.62	1
401	Min.	-104	-498.29	1	-1015.88	18	-74.51	5	-1075.45	9	116.98	13	-322.47	18	-828.59	1	-3853.62	1
401	Min.	-116	-498.29	1	-1015.88	18	-74.51	5	-1075.45	9	116.98	13	-322.47	18	-828.59	1	-3853.62	1
401	Max	-79	139.32	9	109.57	17	891.14	18	204.79	1	2363.18	18	827.93	19	116.09	9	-413.45	9
401	Max	-78	139.32	9	109.57	17	891.14	18	204.79	1	2363.18	18	827.93	19	116.09	9	-413.45	9
401	Max	-106	139.32	9	109.57	17	891.14	18	204.79	1	2363.18	18	827.93	19	116.09	9	-413.45	9
401	Max	-104	139.32	9	109.57	17	891.14	18	204.79	1	2363.18	18	827.93	19	116.09	9	-413.45	9
401	Min.	-79	-390.30	1	-472.00	18	-117.19	5	-811.43	9	683.24	9	371.37	5	-228.37	1	-3899.79	18
401	Min.	-78	-390.30	1	-472.00	18	-117.19	5	-811.43	9	683.24	9	371.37	5	-228.37	1	-3899.79	18
401	Min.	-106	-390.30	1	-472.00	18	-117.19	5	-811.43	9	683.24	9	371.37	5	-228.37	1	-3899.79	18
401	Min.	-104	-390.30	1	-472.00	18	-117.19	5	-811.43	9	683.24	9	371.37	5	-228.37	1	-3899.79	18
401	Max	-116	65.28	5	995.84	18	92.19	1	-89.10	1	-179.26	13	815.61	19	-3649.35	9	866.69	1
401	Max	-104	65.28	5	995.84	18	92.19	1	-89.10	1	-179.26	13	815.61	19	-3649.35	9	866.69	1
401	Max	-106	65.28	5	995.84	18	92.19	1	-89.10	1	-179.26	13	815.61	19	-3649.35	9	866.69	1
401	Max	-122	65.28	5	995.84	18	92.19	1	-89.10	1	-179.26	13	815.61	19	-3649.35	9	866.69	1
401	Min.	-116	-1423.40	18	-425.83	1	-466.36	18	-773.79	19	-805.39	18	13.92	9	-14324.40	18	-477.73	9
401	Min.	-104	-1423.40	18	-425.83	1	-466.36	18	-773.79	19	-805.39	18	13.92	9	-14324.40	18	-477.73	9
401	Min.	-106	-1423.40	18	-425.83	1	-466.36	18	-773.79	19	-805.39	18	13.92	9	-14324.40	18	-477.73	9
401	Min.	-122	-1423.40	18	-425.83	1	-466.36	18	-773.79	19	-805.39	18	13.92	9	-14324.40	18	-477.73	9
401	Max	-78	36.62	9	233.61	18	869.34	18	-1574.75	9	665.25	18	686.21	19	-5102.83	9	-741.16	9
401	Max	-85	36.62	9	233.61	18	869.34	18	-1574.75	9	665.25	18	686.21	19	-5102.83	9	-741.16	9
401	Max	-122	36.62	9	233.61	18	869.34	18	-1574.75	9	665.25	18	686.21	19	-5102.83	9	-741.16	9
401	Max	-106	36.62	9	233.61	18	869.34	18	-1574.75	9	665.25	18	686.21	19	-5102.83	9	-741.16	9
401	Min.	-78	-457.67	1	-42.30	5	9.93	5	-4099.65	18	73.05	9	184.58	1	-12695.60	18	-4719.81	18
401	Min.	-85	-457.67	1	-42.30	5	9.93	5	-4099.65	18	73.05	9	184.58	1	-12695.60	18	-4719.81	18
401	Min.	-122	-457.67	1	-42.30	5	9.93	5	-4099.65	18	73.05	9	184.58	1	-12695.60	18	-4719.81	18
401	Min.	-106	-457.67	1	-42.30	5	9.93	5	-4099.65	18	73.05	9	184.58	1	-12695.60	18	-4719.81	18
401	Max	-39	191.82	18	-207.81	1	543.80	18	-1399.92	9	-1952.39	9	1284.79	18	16171.50	19	7814.49	19
401	Max	-12	191.82	18	-207.81	1	543.80	18	-1399.92	9	-1952.39	9	1284.79	18	16171.50	19	7814.49	19
401	Max	-13	191.82	18	-207.81	1	543.80	18	-1399.92	9	-1952.39	9	1284.79	18	16171.50	19	7814.49	19
401	Max	-34	191.82	18	-207.81	1	543.80	18	-1399.92	9	-1952.39	9	1284.79	18	16171.50	19	7814.49	19
401	Min.	-39	-19.80	5	-650.70	18	80.23	5	-3347.70	19	-4535.97	19	486.29	1	6940.00	9	3136.21	9
401	Min.	-12	-19.80	5	-650.70	18	80.23	5	-3347.70	19	-4535.97	19	486.29	1	6940.00	9	3136.21	9
401	Min.	-13	-19.80	5	-650.70	18	80.23	5	-3347.70	19	-4535.97	19	486.29	1	6940.00	9	3136.21	9
401	Min.	-34	-19.80	5	-650.70	18	80.23	5	-3347.70	19	-4535.97	19	486.29	1	6940.00	9	3136.21	9
401	Max	-39	-366.65	1	16.82	5	-102.17	1	-1369.85	9	-266.83	9	122.28	1	12028.70	18	16783.80	19
401	Max	-34	-366.65	1	16.82	5	-102.17	1	-1369.85	9	-266.83	9	122.28	1	12028.70	18	16783.80	19
401	Max	-73	-366.65	1	16.82	5	-102.17	1	-1369.85	9	-266.83	9	122.28	1	12028.70	18	16783.80	19
401	Max	-85	-366.65	1	16.82	5	-102.17	1	-1369.85	9	-266.83	9	122.28	1	12028.70	18	16783.80	19
401	Min.	-39	-894.26	17	-511.45	18	-526.72	18	-3275.68	18	-669.70	19	-127.33	9	4748.78	9	7266.47	9
401	Min.	-34	-894.26	17	-511.45	18	-526.72	18	-3275.68	18	-669.70	19	-127.33	9	4748.78	9	7266.47	9
401	Min.	-73	-894.26	17	-511.45	18	-526.72	18	-3275.68	18	-669.70	19	-127.33	9	4748.78	9	7266.47	9
401	Min.	-85	-894.26	17	-511.45	18	-526.72	18	-3275.68	18	-669.70	19	-127.33	9	4748.78	9	7266.47	9
401	Max	-34	34.23	13	-139.66	5	348.96	18	-181.72	1	4257.59	19	-65.50	9	5971.06	19	-741.01	9
401	Max	-13	34.23	13	-139.66	5	348.96	18	-181.72	1	4257.59	19	-65.50	9	5971.06	19	-741.01	9
401	Max	-14	34.23	13	-139.66	5	348.96	18	-181.72	1	4257.59	19	-65.50	9	5971.06	19	-741.01	9
401	Max	-31	34.23	13	-139.66	5	348.96	18	-181.72	1	4257.59	19	-65.50	9	5971.06	19	-741.01	9
401	Min.	-34	-173.33	18	-462.64	18	95.56	5	-459.46	18	1800.98	9	-266.09	19	2533.39	13	-1991.32	19
401	Min.	-13	-173.33	18	-462.64	18	95.56	5	-459.46	18	1800.98	9	-266.09	19	2533.39	13	-1991.32	19
401	Min.	-14	-173.33	18	-462.64	18	95.56	5	-459.46	18	1800.98	9	-266.09	19	2533.39	13	-1991.32	19
401	Min.	-31	-173.33	18	-462.64	18	95.56	5	-459.46	18	1800.98	9	-266.09	19	2533.39	13	-1991.32	19
401	Max	-34	-351.11	5	53.83	17	-95.41	1	4677.87	19	122.24	18	588.86	19	359.39	19	4378.36	19
401	Max	-31	-351.11	5	53.83	17	-95.41	1	4677.87	19	122.24	18	588.86	19	359.39	19	4378.36	19
401	Max	-62	-351.11	5	53.83	17	-95.41	1	4677.87	19	122.24	18	588.86	19	359.39	19	4378.36	19
401	Max	-73	-351.11	5	53.83	17	-95.41	1	4677.87	19	122.24	18	588.86	19	359.39	19	4378.36	19
401	Min.	-34	-833.15	17	-61.03	18	-327.91	17	1932.06	9	34.64	1	164.14	9	51.66	9	1860.78	13
401	Min.	-31	-833.15	17	-61.03	18	-327.91	17	1932.06	9	34.64	1	164.14	9	51.66	9	1860.78	13
401	Min.	-62	-833.15	17	-61.03	18	-327.91	17	1932.06	9	34.64	1	164.14	9	51.66	9	1860.78	13
401	Min.	-73	-833.15	17	-61.03	18	-327.91	17	1932.06	9	34.64	1	164.14	9	51.66	9	1860.78	13
401	Max	-15	113.93	1	1095.76	18	626.68	18	-1968.46	5	-1218.17	9	972.20	18	-5719.19	1	-6405.40	1
401	Max	-16	113.93	1	1095.76	18	626.68	18	-1968.46	5	-1218.17	9	972.20	18	-5719.19	1	-6405.40	1
401	Max	-40	113.93	1	1095.76	18	626.68	18	-1968.46	5	-1218.17	9	972.20	18	-5719.19	1	-6405.40	1
401	Max	-32	113.93	1	1095.76	18	626.68	18	-1968.46	5	-1218.17	9	972.20	18	-5719.19	1	-6405.40	1
401	Min.	-15	-326.34	18	40.95	5	162.66	5	-4769.20	18	-2900.55	19	342.79	5	-13763.10	18	-14827.80	18
401	Min.	-16	-326.34	18	40.95	5	162.66	5	-4769.20	18	-2900.55	19	342.79	5	-13763.10	18	-14827.80	18
401	Min.	-40	-326.34	18	40.95	5	162.66	5	-4769.20	18	-2900.55	19	342.79	5	-13763.10	18	-14827.80	18
401	Min.	-32	-326.34	18	40.95	5	162.66	5	-4769.20	18	-2900.55	19	342.79	5	-13763.10	18	-14827.80	18

401	Max	-15	-122.97	5	-51.91	5	75.00	17	-118.30	1	5175.65	19	57.19	9	5087.43	18	2027.05	18
401	Max	-32	-122.97	5	-51.91	5	75.00	17	-118.30	1	5175.65	19	57.19	9	5087.43	18	2027.05	18
401	Max	-31	-122.97	5	-51.91	5	75.00	17	-118.30	1	5175.65	19	57.19	9	5087.43	18	2027.05	18
401	Max	-14	-122.97	5	-51.91	5	75.00	17	-118.30	1	5175.65	19	57.19	9	5087.43	18	2027.05	18
401	Min.	-15	-690.99	18	-322.07	18	-9.97	18	-322.66	18	2169.93	9	-21.75	1	2188.74	1	783.91	1
401	Min.	-32	-690.99	18	-322.07	18	-9.97	18	-322.66	18	2169.93	9	-21.75	1	2188.74	1	783.91	1
401	Min.	-31	-690.99	18	-322.07	18	-9.97	18	-322.66	18	2169.93	9	-21.75	1	2188.74	1	783.91	1
401	Min.	-14	-690.99	18	-322.07	18	-9.97	18	-322.66	18	2169.93	9	-21.75	1	2188.74	1	783.91	1
401	Max	-32	15.31	18	42.95	5	-593.17	1	-1737.48	5	-1181.22	1	-306.89	5	20202.70	18	-8214.97	1
401	Max	-40	15.31	18	42.95	5	-593.17	1	-1737.48	5	-1181.22	1	-306.89	5	20202.70	18	-8214.97	1
401	Max	-70	15.31	18	42.95	5	-593.17	1	-1737.48	5	-1181.22	1	-306.89	5	20202.70	18	-8214.97	1
401	Max	-60	15.31	18	42.95	5	-593.17	1	-1737.48	5	-1181.22	1	-306.89	5	20202.70	18	-8214.97	1
401	Min.	-32	-157.92	17	-1572.24	18	-1581.84	17	-4132.84	18	-2765.14	18	-884.71	18	8103.11	1	-18913.50	18
401	Min.	-40	-157.92	17	-1572.24	18	-1581.84	17	-4132.84	18	-2765.14	18	-884.71	18	8103.11	1	-18913.50	18
401	Min.	-70	-157.92	17	-1572.24	18	-1581.84	17	-4132.84	18	-2765.14	18	-884.71	18	8103.11	1	-18913.50	18
401	Min.	-60	-157.92	17	-1572.24	18	-1581.84	17	-4132.84	18	-2765.14	18	-884.71	18	8103.11	1	-18913.50	18
401	Max	-32	12.88	5	-279.67	5	470.03	17	92.16	17	4668.45	19	1189.08	18	4674.51	18	649.73	19
401	Max	-60	12.88	5	-279.67	5	470.03	17	92.16	17	4668.45	19	1189.08	18	4674.51	18	649.73	19
401	Max	-62	12.88	5	-279.67	5	470.03	17	92.16	17	4668.45	19	1189.08	18	4674.51	18	649.73	19
401	Max	-31	12.88	5	-279.67	5	470.03	17	92.16	17	4668.45	19	1189.08	18	4674.51	18	649.73	19
401	Min.	-32	-77.37	18	-690.53	18	160.77	1	12.32	1	1876.60	13	472.23	1	2019.89	1	144.53	13
401	Min.	-60	-77.37	18	-690.53	18	160.77	1	12.32	1	1876.60	13	472.23	1	2019.89	1	144.53	13
401	Min.	-62	-77.37	18	-690.53	18	160.77	1	12.32	1	1876.60	13	472.23	1	2019.89	1	144.53	13
401	Min.	-31	-77.37	18	-690.53	18	160.77	1	12.32	1	1876.60	13	472.23	1	2019.89	1	144.53	13
401	Max	-129	-416.85	1	-16.24	5	-115.44	1	6089.29	19	-153.27	13	-71.31	13	-1082.78	5	187.61	18
401	Max	-131	-416.85	1	-16.24	5	-115.44	1	6089.29	19	-153.27	13	-71.31	13	-1082.78	5	187.61	18
401	Max	-110	-416.85	1	-16.24	5	-115.44	1	6089.29	19	-153.27	13	-71.31	13	-1082.78	5	187.61	18
401	Max	-108	-416.85	1	-16.24	5	-115.44	1	6089.29	19	-153.27	13	-71.31	13	-1082.78	5	187.61	18
401	Min.	-129	-980.18	17	-714.22	18	-556.91	18	2509.25	9	-299.45	19	-198.10	19	-2695.95	18	30.71	1
401	Min.	-131	-980.18	17	-714.22	18	-556.91	18	2509.25	9	-299.45	19	-198.10	19	-2695.95	18	30.71	1
401	Min.	-110	-980.18	17	-714.22	18	-556.91	18	2509.25	9	-299.45	19	-198.10	19	-2695.95	18	30.71	1
401	Min.	-108	-980.18	17	-714.22	18	-556.91	18	2509.25	9	-299.45	19	-198.10	19	-2695.95	18	30.71	1
401	Max	-129	965.88	18	203.45	17	-458.53	1	-949.10	1	-861.68	5	-383.15	1	-7860.88	1	15154.90	18
401	Max	-108	965.88	18	203.45	17	-458.53	1	-949.10	1	-861.68	5	-383.15	1	-7860.88	1	15154.90	18
401	Max	-97	965.88	18	203.45	17	-458.53	1	-949.10	1	-861.68	5	-383.15	1	-7860.88	1	15154.90	18
401	Max	-123	965.88	18	203.45	17	-458.53	1	-949.10	1	-861.68	5	-383.15	1	-7860.88	1	15154.90	18
401	Min.	-129	119.84	5	24.37	1	-1236.76	17	-2259.90	18	-2094.49	18	-1037.63	18	-18232.20	18	6338.72	1
401	Min.	-108	119.84	5	24.37	1	-1236.76	17	-2259.90	18	-2094.49	18	-1037.63	18	-18232.20	18	6338.72	1
401	Min.	-97	119.84	5	24.37	1	-1236.76	17	-2259.90	18	-2094.49	18	-1037.63	18	-18232.20	18	6338.72	1
401	Min.	-123	119.84	5	24.37	1	-1236.76	17	-2259.90	18	-2094.49	18	-1037.63	18	-18232.20	18	6338.72	1
401	Max	-108	355.35	17	-894.56	9	724.41	17	2410.91	18	1314.04	19	-173.19	13	-560.28	1	2701.26	18
401	Max	-91	355.35	17	-894.56	9	724.41	17	2410.91	18	1314.04	19	-173.19	13	-560.28	1	2701.26	18
401	Max	-89	355.35	17	-894.56	9	724.41	17	2410.91	18	1314.04	19	-173.19	13	-560.28	1	2701.26	18
401	Max	-97	355.35	17	-894.56	9	724.41	17	2410.91	18	1314.04	19	-173.19	13	-560.28	1	2701.26	18
401	Min.	-108	5.41	20	-2228.86	17	278.95	1	932.49	1	170.05	13	-640.12	19	-1813.24	18	1212.56	1
401	Min.	-91	5.41	20	-2228.86	17	278.95	1	932.49	1	170.05	13	-640.12	19	-1813.24	18	1212.56	1
401	Min.	-89	5.41	20	-2228.86	17	278.95	1	932.49	1	170.05	13	-640.12	19	-1813.24	18	1212.56	1
401	Min.	-97	5.41	20	-2228.86	17	278.95	1	932.49	1	170.05	13	-640.12	19	-1813.24	18	1212.56	1
401	Max	-91	77.21	5	-468.52	1	757.49	17	1212.16	18	3373.49	19	211.08	17	-1676.00	5	-682.01	1
401	Max	-62	77.21	5	-468.52	1	757.49	17	1212.16	18	3373.49	19	211.08	17	-1676.00	5	-682.01	1
401	Max	-60	77.21	5	-468.52	1	757.49	17	1212.16	18	3373.49	19	211.08	17	-1676.00	5	-682.01	1
401	Max	-89	77.21	5	-468.52	1	757.49	17	1212.16	18	3373.49	19	211.08	17	-1676.00	5	-682.01	1
401	Min.	-91	-252.26	18	-1076.32	17	287.59	1	476.34	1	1227.77	13	28.80	1	-3945.15	18	-1827.00	18
401	Min.	-62	-252.26	18	-1076.32	17	287.59	1	476.34	1	1227.77	13	28.80	1	-3945.15	18	-1827.00	18
401	Min.	-60	-252.26	18	-1076.32	17	287.59	1	476.34	1	1227.77	13	28.80	1	-3945.15	18	-1827.00	18
401	Min.	-89	-252.26	18	-1076.32	17	287.59	1	476.34	1	1227.77	13	28.80	1	-3945.15	18	-1827.00	18
401	Max	-89	488.41	17	-1038.26	1	776.28	18	4577.76	18	-71.31	5	656.54	18	-817.26	9	-945.84	1
401	Max	-60	488.41	17	-1038.26	1	776.28	18	4577.76	18	-71.31	5	656.54	18	-817.26	9	-945.84	1
401	Max	-70	488.41	17	-1038.26	1	776.28	18	4577.76	18	-71.31	5	656.54	18	-817.26	9	-945.84	1
401	Max	-97	488.41	17	-1038.26	1	776.28	18	4577.76	18	-71.31	5	656.54	18	-817.26	9	-945.84	1
401	Min.	-89	106.18	20	-2550.30	17	258.19	1	1810.24	1	-658.08	18	315.80	1	-2910.20	19	-2368.62	18
401	Min.	-60	106.18	20	-2550.30	17	258.19	1	1810.24	1	-658.08	18	315.80	1	-2910.20	19	-2368.62	18
401	Min.	-70	106.18	20	-2550.30	17	258.19	1	1810.24	1	-658.08	18	315.80	1	-2910.20	19	-2368.62	18
401	Min.	-97	106.18	20	-2550.30	17	258.19	1	1810.24	1	-658.08	18	315.80	1	-2910.20	19	-2368.62	18
401	Max	-91	144.27	17	-280.50	20	136.34	17	966.99	18	3430.28	19	-490.31	9	138.93	17	-964.60	1
401	Max	-108	144.27	17	-280.50	20	136.34	17	966.99	18	3430.28	19	-490.31	9	138.93	17	-964.60	1
401	Max	-110	144.27	17	-280.50	20	136.34	17	966.99	18	3430.28	19	-490.31	9	138.93	17	-964.60	1
401	Max	-93	144.27	17	-280.50	20	136.34	17	966.99	18	3430.28	19	-490.31	9	138.93	17	-964.60	1
401	Min.	-91	-195.35	18	-704.64	17	19.40	20	387.57	5	1349.31	13	-1245.31	19	-62.67	19	-2267.79	18
401	Min.	-108	-195.35	18	-704.64	17	19.40	20	387.57	5	1349.31	13	-1245.31	19	-62.67	19	-2267.79	18
401	Min.	-110	-195.35	18	-704.64	17	19.40	20	387.57	5	1349.31	13	-1245.31	19	-62.67	19	-2267.79	18
401	Min.	-93	-195.35	18	-704.64	17	19.40	20	387.57	5	1349.31	13	-1245.31	19	-62.67	19	-2267.79	18
401	Max	-91	-445.78	1	22.02	1	-165.29	1	3601.64	19	1282.08	18	425.06	19	-504.00	9	-1144.12	9
401	Max	-93	-445.78	1	22.02	1	-165.29	1	3601.64	19	1282.08	18	425.06	19	-504.00	9	-1144.12	9
401	Max	-73	-445.78	1	22.02	1	-165.29	1	3601.64	19	1282.08	18	425.06	19	-504.00	9	-1144.12	9
401	Max	-62	-445.78	1	22.02	1	-165.29	1	3601.64	19	1282.08	18	425.06	19	-504.00	9	-1144.12	9
401	Min.	-91	-982.50	17	-261.65	18	-441.79	17	1391.49	9	536.93	1	131.45	9	-1429.04	19	-2819.93	19
401	Min.	-93	-982.50	17	-261.65	18	-441.79	17	1391.49	9	536.93	1	131.45	9	-1429.04	19	-2819.93	19
401	Min.	-73	-982.50	17	-261.65	18	-441.79	17	1391.49	9	536.93	1	131.45	9	-1429.04	19	-2819.93	19
401	Min.	-62	-982.50	17	-261.65	18	-441.79	17	1391.49	9	536.93	1	131.45	9	-1429.04	19	-2819.93	19
401	Max	-73	-36.64	1	-74.00	9	213.33	18	1379.47	18	911.87	19	147.84	9	-571.85	9	-663.47	1
401	Max	-93	-36.64	1	-74.00	9	213.33	18	1379.47	18	911.87	19	147.84	9	-571.85	9	-663.47	1
401	Max	-95	-36.64	1	-74.00	9	213.33	18	1379.47	18	911.87	19	147.84	9	-571.85	9	-663.47	1
401	Max	-85	-36.64	1	-74.00	9	213.33	18	1379.47	18	911.87	19	147.84	9	-571.85	9	-663.47	1
401	Min.	-73	-194.02	18	-438.39	17	49.19	1	515.58	1	87.06	9	-97.29	1	-1519.18	19	-1793.92	18
401	Min.	-93	-194.02	18	-438.39	17	49.19	1	515.58	1	87.06	9	-97.29	1	-1519.18	19	-1793.92	18
401	Min.	-95	-194.02	18	-438.39	17	49.19	1	515.58	1	87.06	9	-97.29	1	-1519.18	19	-1793.92	18
401	Min.	-85	-194.02	18	-438.39	17	49.19	1	515.58	1	87.06	9	-97.29	1	-1519.18	19	-1793.92	18
401	Max	-93	-16.55	5	-436.14	9	364.03	18	1058.53	19	3200.87	19	941.84	18	-3107.60	9	-724.14	13
401	Max	-110	-16.55	5	-436.14	9	364.03	18	1058.53	19	3200.87	19	941.84	18	-3107.60	9	-724.14	13
401	Max	-112	-16.55	5	-436.14	9	364.03	18	1058.53	19	3200.87	19	941.84	18	-3107.60	9	-724.14	13
401	Max	-95	-16.55	5	-436.14	9	364.03	18	1058.53	19	3200.87	19	941.84	18	-3107.60	9	-724.14	13
401	Min.	-93	-324.11	18	-1029.40	17	46.31	1	447.98	1	1284.93	9	333.94	9	-7184.08	19	-1764.64	19
401	Min.	-110	-324.11	18	-1029.40	17	46.31	1	447.98	1	1284.93	9	333.94	9	-7184.08	19	-1764.64	19
401	Min.	-112	-324.11	18	-1029.40	17	46.31	1	447.98	1	1284.93	9	333.94	9	-7184.08	19	-1764.64	19
401	Min.	-95	-324.11	18	-1029.40	17	46.31	1	447.98	1	1284.93	9	333.94	9	-7184.08	19	-1764.64	19
401	Max	-85	-247.77	1	160.04	18	674.10	18	-633.57	1	-764.21	9	2616.16	18	-7582.26	9	1484.47	19
401	Max	-95	-247.77	1	160.04	18	674.10	18	-633.57	1	-764.21	9	2616.16	18	-7582.26	9	1484.47	19
401	Max	-112	-247.77	1	160.04	18	674.10	18	-633.57	1	-764.21	9	2616.16	18	-7582.26	9	1484.47	19
401	Max	-122	-247.77	1	160.04	18	674.10	18	-633.57	1	-764.21	9	2616.16	18	-7582.26	9	1484.47	19
401	Min.	-85	-722.78	18	-457.18	17	215.75	1	-1747.10	18	-1950.00	19	1128.59	1	-18477.50	18	238.59	1
401	Min.	-95	-722.78	18	-457.18	17	215.75	1	-1747.10	18	-1950.00	19	1128.59	1	-18477.50	18	238.59	1
401	Min.	-112	-722.78	18	-457.18	17	215.75	1	-1747.10	18	-1950.00	19	1128.59	1	-18477.50	18	238.59	1
401	Min.	-122	-722.78	18	-457.18	17	215.75	1	-1747.10	18	-1950.00	19	1128.59	1	-18477.50	18	238.59	1
401	Max	-110	234.30	18	-492.95	1	88.75	18	-890.97	9	-506.61	1	35.53	1	-7692.13	9	-3986.95	9
401	Max	-131	234.30	18	-492.95	1	88.75	18	-890.97	9	-506.61	1	35.53	1	-7692.13	9	-3986.95	9
401	Max	-122	234.30	18	-492.95	1	88.75	18	-890.97	9	-506.61	1	35.53	1	-7692.13	9	-3986.95	9
401	Max	-112	234.30	18	-492.95	1	88.75	18	-890.97	9	-506.61	1	35.53	1	-7692.13	9	-3986.95	9
401	Min.	-110	29.85	5	-1438.43	17	-241.69	17	-2201.29	19	-1284.55	18	-90.97	9	-17882.10	19	-9426.31	19

401	Min.	-131	29.85	5	-1438.43	17	-241.69	17	-2201.29	19	-1284.55	18	-90.97	9	-17882.10	19	-9426.31	19
401	Min.	-122	29.85	5	-1438.43	17	-241.69	17	-2201.29	19	-1284.55	18	-90.97	9	-17882.10	19	-9426.31	19
401	Min.	-112	29.85	5	-1438.43	17	-241.69	17	-2201.29	19	-1284.55	18	-90.97	9	-17882.10	19	-9426.31	19
401	Max	-17	27.83	5	2259.95	18	-20.84	9	-950.76	5	3218.35	18	487.27	19	-1529.78	5	-468.54	13
401	Max	-27	27.83	5	2259.95	18	-20.84	9	-950.76	5	3218.35	18	487.27	19	-1529.78	5	-468.54	13
401	Max	-21	27.83	5	2259.95	18	-20.84	9	-950.76	5	3218.35	18	487.27	19	-1529.78	5	-468.54	13
401	Max	-16	27.83	5	2259.95	18	-20.84	9	-950.76	5	3218.35	18	487.27	19	-1529.78	5	-468.54	13
401	Min.	-17	-1167.11	18	45.40	5	-129.96	17	-2123.65	18	902.61	5	78.54	9	-4177.56	18	-1330.35	19
401	Min.	-27	-1167.11	18	45.40	5	-129.96	17	-2123.65	18	902.61	5	78.54	9	-4177.56	18	-1330.35	19
401	Min.	-21	-1167.11	18	45.40	5	-129.96	17	-2123.65	18	902.61	5	78.54	9	-4177.56	18	-1330.35	19
401	Min.	-16	-1167.11	18	45.40	5	-129.96	17	-2123.65	18	902.61	5	78.54	9	-4177.56	18	-1330.35	19
401	Max	-27	258.41	5	-1209.50	1	3268.55	18	-92.92	13	5877.61	18	2461.68	18	-2673.84	5	6908.08	18
401	Max	-51	258.41	5	-1209.50	1	3268.55	18	-92.92	13	5877.61	18	2461.68	18	-2673.84	5	6908.08	18
401	Max	-45	258.41	5	-1209.50	1	3268.55	18	-92.92	13	5877.61	18	2461.68	18	-2673.84	5	6908.08	18
401	Max	-21	258.41	5	-1209.50	1	3268.55	18	-92.92	13	5877.61	18	2461.68	18	-2673.84	5	6908.08	18
401	Min.	-27	-1572.29	18	-2718.02	17	582.98	5	-1170.16	19	1745.75	1	586.52	1	-10160.40	18	1569.66	5
401	Min.	-51	-1572.29	18	-2718.02	17	582.98	5	-1170.16	19	1745.75	1	586.52	1	-10160.40	18	1569.66	5
401	Min.	-45	-1572.29	18	-2718.02	17	582.98	5	-1170.16	19	1745.75	1	586.52	1	-10160.40	18	1569.66	5
401	Min.	-21	-1572.29	18	-2718.02	17	582.98	5	-1170.16	19	1745.75	1	586.52	1	-10160.40	18	1569.66	5
401	Max	-21	1131.61	18	-1475.35	1	2319.21	18	-1734.19	9	-765.02	1	2558.95	18	-9787.60	5	-2956.76	1
401	Max	-45	1131.61	18	-1475.35	1	2319.21	18	-1734.19	9	-765.02	1	2558.95	18	-9787.60	5	-2956.76	1
401	Max	-40	1131.61	18	-1475.35	1	2319.21	18	-1734.19	9	-765.02	1	2558.95	18	-9787.60	5	-2956.76	1
401	Max	-16	1131.61	18	-1475.35	1	2319.21	18	-1734.19	9	-765.02	1	2558.95	18	-9787.60	5	-2956.76	1
401	Min.	-21	168.65	5	-3546.79	17	43.28	5	-4117.43	19	-2676.14	18	1010.17	5	-26131.90	18	-7918.41	18
401	Min.	-45	168.65	5	-3546.79	17	43.28	5	-4117.43	19	-2676.14	18	1010.17	5	-26131.90	18	-7918.41	18
401	Min.	-40	168.65	5	-3546.79	17	43.28	5	-4117.43	19	-2676.14	18	1010.17	5	-26131.90	18	-7918.41	18
401	Min.	-16	168.65	5	-3546.79	17	43.28	5	-4117.43	19	-2676.14	18	1010.17	5	-26131.90	18	-7918.41	18
401	Max	-45	-2319.75	1	772.35	17	-845.91	5	7487.47	18	2533.37	18	1113.59	18	3199.90	17	12409.70	18
401	Max	-51	-2319.75	1	772.35	17	-845.91	5	7487.47	18	2533.37	18	1113.59	18	3199.90	17	12409.70	18
401	Max	-68	-2319.75	1	772.35	17	-845.91	5	7487.47	18	2533.37	18	1113.59	18	3199.90	17	12409.70	18
401	Max	-75	-2319.75	1	772.35	17	-845.91	5	7487.47	18	2533.37	18	1113.59	18	3199.90	17	12409.70	18
401	Min.	-45	-5557.32	17	-320.51	18	-4177.35	18	1792.02	1	390.42	5	202.87	9	1273.21	1	3020.31	1
401	Min.	-51	-5557.32	17	-320.51	18	-4177.35	18	1792.02	1	390.42	5	202.87	9	1273.21	1	3020.31	1
401	Min.	-68	-5557.32	17	-320.51	18	-4177.35	18	1792.02	1	390.42	5	202.87	9	1273.21	1	3020.31	1
401	Min.	-75	-5557.32	17	-320.51	18	-4177.35	18	1792.02	1	390.42	5	202.87	9	1273.21	1	3020.31	1
401	Max	-45	139.91	5	-1879.83	1	4458.97	18	-773.84	13	-993.69	1	-95.75	13	-7363.89	1	23216.70	18
401	Max	-75	139.91	5	-1879.83	1	4458.97	18	-773.84	13	-993.69	1	-95.75	13	-7363.89	1	23216.70	18
401	Max	-70	139.91	5	-1879.83	1	4458.97	18	-773.84	13	-993.69	1	-95.75	13	-7363.89	1	23216.70	18
401	Max	-40	139.91	5	-1879.83	1	4458.97	18	-773.84	13	-993.69	1	-95.75	13	-7363.89	1	23216.70	18
401	Min.	-45	-2050.78	18	-4616.21	17	970.64	5	-1961.37	19	-3868.12	18	-1088.92	19	-20718.60	18	9021.34	1
401	Min.	-75	-2050.78	18	-4616.21	17	970.64	5	-1961.37	19	-3868.12	18	-1088.92	19	-20718.60	18	9021.34	1
401	Min.	-70	-2050.78	18	-4616.21	17	970.64	5	-1961.37	19	-3868.12	18	-1088.92	19	-20718.60	18	9021.34	1
401	Min.	-40	-2050.78	18	-4616.21	17	970.64	5	-1961.37	19	-3868.12	18	-1088.92	19	-20718.60	18	9021.34	1
401	Max	-127	-2726.87	1	1805.15	18	1424.89	17	-1815.79	1	-1062.44	5	-376.36	13	26272.90	18	-10534.40	1
401	Max	-123	-2726.87	1	1805.15	18	1424.89	17	-1815.79	1	-1062.44	5	-376.36	13	26272.90	18	-10534.40	1
401	Max	-97	-2726.87	1	1805.15	18	1424.89	17	-1815.79	1	-1062.44	5	-376.36	13	26272.90	18	-10534.40	1
401	Max	-102	-2726.87	1	1805.15	18	1424.89	17	-1815.79	1	-1062.44	5	-376.36	13	26272.90	18	-10534.40	1
401	Min.	-127	-7166.82	17	-25.25	5	-1714.04	18	-4864.14	18	-2520.60	18	-1521.81	19	10716.60	1	-25938.30	18
401	Min.	-123	-7166.82	17	-25.25	5	-1714.04	18	-4864.14	18	-2520.60	18	-1521.81	19	10716.60	1	-25938.30	18
401	Min.	-97	-7166.82	17	-25.25	5	-1714.04	18	-4864.14	18	-2520.60	18	-1521.81	19	10716.60	1	-25938.30	18
401	Min.	-102	-7166.82	17	-25.25	5	-1714.04	18	-4864.14	18	-2520.60	18	-1521.81	19	10716.60	1	-25938.30	18
401	Max	-127	245.60	5	-2502.11	9	2776.52	18	513.74	17	9595.66	17	128.14	5	14753.70	17	1073.75	18
401	Max	-102	245.60	5	-2502.11	9	2776.52	18	513.74	17	9595.66	17	128.14	5	14753.70	17	1073.75	18
401	Max	-100	245.60	5	-2502.11	9	2776.52	18	513.74	17	9595.66	17	128.14	5	14753.70	17	1073.75	18
401	Max	-124	245.60	5	-2502.11	9	2776.52	18	513.74	17	9595.66	17	128.14	5	14753.70	17	1073.75	18
401	Min.	-127	-2604.74	18	-6792.68	17	-290.04	5	-72.79	5	2969.30	1	-182.75	13	5533.04	1	-291.99	5
401	Min.	-102	-2604.74	18	-6792.68	17	-290.04	5	-72.79	5	2969.30	1	-182.75	13	5533.04	1	-291.99	5
401	Min.	-100	-2604.74	18	-6792.68	17	-290.04	5	-72.79	5	2969.30	1	-182.75	13	5533.04	1	-291.99	5
401	Min.	-124	-2604.74	18	-6792.68	17	-290.04	5	-72.79	5	2969.30	1	-182.75	13	5533.04	1	-291.99	5
401	Max	-102	-1223.56	1	16.02	5	-35.34	5	-522.61	1	4801.21	18	409.72	18	427.31	18	-82.80	1
401	Max	-97	-1223.56	1	16.02	5	-35.34	5	-522.61	1	4801.21	18	409.72	18	427.31	18	-82.80	1
401	Max	-70	-1223.56	1	16.02	5	-35.34	5	-522.61	1	4801.21	18	409.72	18	427.31	18	-82.80	1
401	Max	-75	-1223.56	1	16.02	5	-35.34	5	-522.61	1	4801.21	18	409.72	18	427.31	18	-82.80	1
401	Min.	-102	-3110.56	17	-464.33	18	-2047.46	18	-2648.75	18	1829.29	1	-105.58	5	15.13	5	-3258.20	17
401	Min.	-97	-3110.56	17	-464.33	18	-2047.46	18	-2648.75	18	1829.29	1	-105.58	5	15.13	5	-3258.20	17
401	Min.	-70	-3110.56	17	-464.33	18	-2047.46	18	-2648.75	18	1829.29	1	-105.58	5	15.13	5	-3258.20	17
401	Min.	-75	-3110.56	17	-464.33	18	-2047.46	18	-2648.75	18	1829.29	1	-105.58	5	15.13	5	-3258.20	17
401	Max	-102	94.41	13	-2432.37	1	2672.08	18	2930.92	18	6972.52	17	624.47	17	13446.80	18	3453.95	18
401	Max	-75	94.41	13	-2432.37	1	2672.08	18	2930.92	18	6972.52	17	624.47	17	13446.80	18	3453.95	18
401	Max	-68	94.41	13	-2432.37	1	2672.08	18	2930.92	18	6972.52	17	624.47	17	13446.80	18	3453.95	18
401	Max	-100	94.41	13	-2432.37	1	2672.08	18	2930.92	18	6972.52	17	624.47	17	13446.80	18	3453.95	18
401	Min.	-102	-907.54	18	-6304.45	17	-402.16	5	877.33	1	1232.92	1	284.89	9	3938.48	1	529.89	5
401	Min.	-75	-907.54	18	-6304.45	17	-402.16	5	877.33	1	1232.92	1	284.89	9	3938.48	1	529.89	5
401	Min.	-68	-907.54	18	-6304.45	17	-402.16	5	877.33	1	1232.92	1	284.89	9	3938.48	1	529.89	5
401	Min.	-100	-907.54	18	-6304.45	17	-402.16	5	877.33	1	1232.92	1	284.89	9	3938.48	1	529.89	5
401	Max	-41	2738.40	18	47.95	5	843.22	18	72.64	13	-1084.04	5	509.58	18	2715.61	19	12859.70	18
401	Max	-27	2738.40	18	47.95	5	843.22	18	72.64	13	-1084.04	5	509.58	18	2715.61	19	12859.70	18
401	Max	-17	2738.40	18	47.95	5	843.22	18	72.64	13	-1084.04	5	509.58	18	2715.61	19	12859.70	18
401	Max	-18	2738.40	18	47.95	5	843.22	18	72.64	13	-1084.04	5	509.58	18	2715.61	19	12859.70	18
401	Min.	-41	555.41	5	-385.84	18	-259.67	5	-312.48	19	-2629.28	18	171.12	5	930.07	13	4386.64	5
401	Min.	-27	555.41	5	-385.84	18	-259.67	5	-312.48	19	-2629.28	18	171.12	5	930.07	13	4386.64	5
401	Min.	-17	555.41	5	-385.84	18	-259.67	5	-312.48	19	-2629.28	18	171.12	5	930.07	13	4386.64	5
401	Min.	-18	555.41	5	-385.84	18	-259.67	5	-312.48	19	-2629.28	18	171.12	5	930.07	13	4386.64	5
401	Max	-41	401.53	17	-173.32	1	90.67	18	-1267.07	1	-659.49	9	1109.55	18	6032.74	18	5416.27	18
401	Max	-18	401.53	17	-173.32	1	90.67	18	-1267.07	1	-659.49	9	1109.55	18	6032.74	18	5416.27	18
401	Max	-19	401.53	17	-173.32	1	90.67	18	-1267.07	1	-659.49	9	1109.55	18	6032.74	18	5416.27	18
401	Max	-43	401.53	17	-173.32	1	90.67	18	-1267.07	1	-659.49	9	1109.55	18	6032.74	18	5416.27	18
401	Min.	-41	161.80	5	-427.80	17	-330.79	17	-3259.89	18	-1796.94	19	356.61	5	2384.73	1	2161.23	5
401	Min.	-18	161.80	5	-427.80	17	-330.79	17	-3259.89	18	-1796.94	19	356.61	5	2384.73	1	2161.23	5
401	Min.	-19	161.80	5	-427.80	17	-330.79	17	-3259.89	18	-1796.94	19	356.61	5	2384.73	1	2161.23	5
401	Min.	-43	161.80	5	-427.80	17	-330.79	17	-3259.89	18	-1796.94	19	356.61	5	2384.73	1	2161.23	5
401	Max	-100	1734.38	17	3819.63	17	702.27	5	1920.67	18	2554.08	9	58.00	9	1382.87	1	-943.38	9
401	Max	-68	1734.38	17	3819.63	17	702.27	5	1920.67	18	2554.08	9	58.00	9	1382.87	1	-943.38	9
401	Max	-65	1734.38	17	3819.63	17	702.27	5	1920.67	18	2554.08	9	58.00	9	1382.87	1	-943.38	9
401	Max	-86	1734.38	17	3819.63	17	702.27	5	1920.67	18	2554.08	9	58.00	9	1382.87	1	-943.38	9
401	Min.	-100	-1081.65	18	1409.34	1	-1979.69	18	281.46	5	-1359.27	1	-632.36	1	-4163.16	18	-2697.70	19
401	Min.	-68	-1081.65	18	1409.34	1	-1979.69	18	281.46	5	-1359.27	1	-632.36	1	-4163.16	18	-2697.70	19
401	Min.	-65	-1081.65	18	1409.34	1	-1979.69	18	281.46	5	-1359.27	1	-632.36	1	-4163.16	18	-2697.70	19
401	Min.	-86	-1081.65	18	1409.34	1	-1979.69	18	281.46	5	-1359.27	1	-632.36	1	-4163.16	18	-2697.70	19
401	Max	-68	562.17	5	5810.03	17	2285.34	17	2562.85	18	3729.47	18	161.99	1	-1183.72	5	-1576.76	1
401	Max	-51	562.17	5	5810.03	17	2285.34	17	2562.85	18	3729.47	18	161.99	1	-1183.72	5	-1576.76	1
401	Max	-57	562.17	5	5810.03	17	2285.34	17	2562.85	18	3729.47	18	161.99	1	-1183.72	5	-1576.76	1
401	Max	-65	562.17	5	5810.03	17	2285.34	17	2562.85	18	3729.47	18	161.99	1	-1183.72	5	-1576.76	1
401	Min.	-68	-1695.59	18	2453.72	1	-755.37	18	42.20	5	-1084.33	1	-1048.83	17	-10793.60	18	-4295.58	18
401	Min.	-51	-1695.59	18	2453.72	1	-755.37	18	42.20	5	-1084.33	1	-1048.83	17	-10793.60	18	-4295.58	18
401	Min.	-57	-1695.59	18	2453.72	1	-755.37	18	42.20	5	-1084.33	1	-1048.83	17	-10793.60	18	-4295.58	18
401	Min.	-65	-1695.59	18	2453.72	1	-755.37	18	42.20	5	-1084.33	1	-1048.83	17	-10793.60	18	-4295.58	18
401	Max	-86	1634.51	18	5024.62	17	-826.57	5	712.29	9	-1196.83	1	2502.59	18	-5417.71	1	2339.60	18
401	Max	-65	1634.51	18	5024.62	17	-826.57	5	712.29	9	-1196.83	1	2502.59	18	-5417.71	1	2339.60	18

401	Max	-57	1634.51	18	5024.62	17	-826.57	5	712.29	9	-1196.83	1	2502.59	18	-5417.71	1	2339.60	18
401	Max	-41	1634.51	18	5024.62	17	-826.57	5	712.29	9	-1196.83	1	2502.59	18	-5417.71	1	2339.60	18
401	Min.	-86	-226.00	5	-270.36	18	-2539.76	18	-144.44	1	-3424.79	18	653.82	1	-19926.80	18	-134.37	5
401	Min.	-65	-226.00	5	-270.36	18	-2539.76	18	-144.44	1	-3424.79	18	653.82	1	-19926.80	18	-134.37	5
401	Min.	-57	-226.00	5	-270.36	18	-2539.76	18	-144.44	1	-3424.79	18	653.82	1	-19926.80	18	-134.37	5
401	Min.	-41	-226.00	5	-270.36	18	-2539.76	18	-144.44	1	-3424.79	18	653.82	1	-19926.80	18	-134.37	5
401	Max	-51	1500.36	17	3265.35	17	3239.45	17	-1422.06	1	468.00	9	-368.86	1	-5060.26	5	-3813.37	5
401	Max	-27	1500.36	17	3265.35	17	3239.45	17	-1422.06	1	468.00	9	-368.86	1	-5060.26	5	-3813.37	5
401	Max	-41	1500.36	17	3265.35	17	3239.45	17	-1422.06	1	468.00	9	-368.86	1	-5060.26	5	-3813.37	5
401	Max	-57	1500.36	17	3265.35	17	3239.45	17	-1422.06	1	468.00	9	-368.86	1	-5060.26	5	-3813.37	5
401	Min.	-51	-1976.84	18	1353.97	5	491.23	20	-3269.24	18	-707.14	1	-1978.45	17	-18306.00	18	-15202.50	18
401	Min.	-27	-1976.84	18	1353.97	5	491.23	20	-3269.24	18	-707.14	1	-1978.45	17	-18306.00	18	-15202.50	18
401	Min.	-41	-1976.84	18	1353.97	5	491.23	20	-3269.24	18	-707.14	1	-1978.45	17	-18306.00	18	-15202.50	18
401	Min.	-57	-1976.84	18	1353.97	5	491.23	20	-3269.24	18	-707.14	1	-1978.45	17	-18306.00	18	-15202.50	18
401	Max	-86	1434.81	18	8206.83	17	-701.17	5	74.69	9	455.83	9	830.41	18	15935.00	18	-3690.54	1
401	Max	-125	1434.81	18	8206.83	17	-701.17	5	74.69	9	455.83	9	830.41	18	15935.00	18	-3690.54	1
401	Max	-124	1434.81	18	8206.83	17	-701.17	5	74.69	9	455.83	9	830.41	18	15935.00	18	-3690.54	1
401	Max	-100	1434.81	18	8206.83	17	-701.17	5	74.69	9	455.83	9	830.41	18	15935.00	18	-3690.54	1
401	Min.	-86	185.75	5	3016.59	9	-5527.48	18	-358.06	1	-2858.12	1	13.60	5	4550.49	1	-11501.50	18
401	Min.	-125	185.75	5	3016.59	9	-5527.48	18	-358.06	1	-2858.12	1	13.60	5	4550.49	1	-11501.50	18
401	Min.	-124	185.75	5	3016.59	9	-5527.48	18	-358.06	1	-2858.12	1	13.60	5	4550.49	1	-11501.50	18
401	Min.	-100	185.75	5	3016.59	9	-5527.48	18	-358.06	1	-2858.12	1	13.60	5	4550.49	1	-11501.50	18
401	Max	-86	333.66	5	269.07	18	1877.69	17	-307.92	9	-644.90	9	-752.77	5	5115.15	18	-2584.34	1
401	Max	-41	333.66	5	269.07	18	1877.69	17	-307.92	9	-644.90	9	-752.77	5	5115.15	18	-2584.34	1
401	Max	-43	333.66	5	269.07	18	1877.69	17	-307.92	9	-644.90	9	-752.77	5	5115.15	18	-2584.34	1
401	Max	-81	333.66	5	269.07	18	1877.69	17	-307.92	9	-644.90	9	-752.77	5	5115.15	18	-2584.34	1
401	Min.	-86	-1252.24	18	7.38	5	741.79	9	-715.18	19	-1704.65	19	-1821.04	18	2107.28	1	-9037.93	18
401	Min.	-41	-1252.24	18	7.38	5	741.79	9	-715.18	19	-1704.65	19	-1821.04	18	2107.28	1	-9037.93	18
401	Min.	-43	-1252.24	18	7.38	5	741.79	9	-715.18	19	-1704.65	19	-1821.04	18	2107.28	1	-9037.93	18
401	Min.	-81	-1252.24	18	7.38	5	741.79	9	-715.18	19	-1704.65	19	-1821.04	18	2107.28	1	-9037.93	18
401	Max	-86	504.12	17	201.80	18	2428.75	17	-1135.58	5	36.32	13	-608.28	5	-3164.95	1	3242.71	19
401	Max	-81	504.12	17	201.80	18	2428.75	17	-1135.58	5	36.32	13	-608.28	5	-3164.95	1	3242.71	19
401	Max	-114	504.12	17	201.80	18	2428.75	17	-1135.58	5	36.32	13	-608.28	5	-3164.95	1	3242.71	19
401	Max	-125	504.12	17	201.80	18	2428.75	17	-1135.58	5	36.32	13	-608.28	5	-3164.95	1	3242.71	19
401	Min.	-86	80.89	20	-512.60	17	956.53	1	-2701.25	18	-53.87	5	-1711.93	18	-9139.90	18	1251.01	9
401	Min.	-81	80.89	20	-512.60	17	956.53	1	-2701.25	18	-53.87	5	-1711.93	18	-9139.90	18	1251.01	9
401	Min.	-114	80.89	20	-512.60	17	956.53	1	-2701.25	18	-53.87	5	-1711.93	18	-9139.90	18	1251.01	9
401	Min.	-125	80.89	20	-512.60	17	956.53	1	-2701.25	18	-53.87	5	-1711.93	18	-9139.90	18	1251.01	9
401	Max	-200	8283.06	17	1305.57	18	7138.89	18	372.78	1	-674.69	5	-183.03	1	10572.30	18	16003.80	19
401	Max	-199	8283.06	17	1305.57	18	7138.89	18	372.78	1	-674.69	5	-183.03	1	10572.30	18	16003.80	19
401	Max	-171	8283.06	17	1305.57	18	7138.89	18	372.78	1	-674.69	5	-183.03	1	10572.30	18	16003.80	19
401	Max	-173	8283.06	17	1305.57	18	7138.89	18	372.78	1	-674.69	5	-183.03	1	10572.30	18	16003.80	19
401	Min.	-200	3142.08	1	42.46	5	512.60	5	-2823.60	9	-1543.77	19	-597.44	17	4355.31	9	5495.89	9
401	Min.	-199	3142.08	1	42.46	5	512.60	5	-2823.60	9	-1543.77	19	-597.44	17	4355.31	9	5495.89	9
401	Min.	-171	3142.08	1	42.46	5	512.60	5	-2823.60	9	-1543.77	19	-597.44	17	4355.31	9	5495.89	9
401	Min.	-173	3142.08	1	42.46	5	512.60	5	-2823.60	9	-1543.77	19	-597.44	17	4355.31	9	5495.89	9
401	Max	-200	2587.63	18	-1220.58	1	-130.75	20	-1493.76	9	247.28	17	1338.51	18	12692.70	19	6784.77	19
401	Max	-173	2587.63	18	-1220.58	1	-130.75	20	-1493.76	9	247.28	17	1338.51	18	12692.70	19	6784.77	19
401	Max	-185	2587.63	18	-1220.58	1	-130.75	20	-1493.76	9	247.28	17	1338.51	18	12692.70	19	6784.77	19
401	Max	-210	2587.63	18	-1220.58	1	-130.75	20	-1493.76	9	247.28	17	1338.51	18	12692.70	19	6784.77	19
401	Min.	-200	389.32	5	-3200.95	17	-1164.80	17	-3413.45	19	-695.72	18	711.14	13	4874.45	9	2323.49	9
401	Min.	-173	389.32	5	-3200.95	17	-1164.80	17	-3413.45	19	-695.72	18	711.14	13	4874.45	9	2323.49	9
401	Min.	-185	389.32	5	-3200.95	17	-1164.80	17	-3413.45	19	-695.72	18	711.14	13	4874.45	9	2323.49	9
401	Min.	-210	389.32	5	-3200.95	17	-1164.80	17	-3413.45	19	-695.72	18	711.14	13	4874.45	9	2323.49	9
401	Max	-173	3952.64	17	1651.79	17	3776.76	18	2092.09	1	2664.98	18	352.27	5	524.89	18	3816.17	1
401	Max	-171	3952.64	17	1651.79	17	3776.76	18	2092.09	1	2664.98	18	352.27	5	524.89	18	3816.17	1
401	Max	-148	3952.64	17	1651.79	17	3776.76	18	2092.09	1	2664.98	18	352.27	5	524.89	18	3816.17	1
401	Max	-150	3952.64	17	1651.79	17	3776.76	18	2092.09	1	2664.98	18	352.27	5	524.89	18	3816.17	1
401	Min.	-173	1489.75	1	-559.01	18	-591.05	5	-1294.88	9	915.96	9	-76.59	13	-329.93	5	-297.44	9
401	Min.	-171	1489.75	1	-559.01	18	-591.05	5	-1294.88	9	915.96	9	-76.59	13	-329.93	5	-297.44	9
401	Min.	-148	1489.75	1	-559.01	18	-591.05	5	-1294.88	9	915.96	9	-76.59	13	-329.93	5	-297.44	9
401	Min.	-150	1489.75	1	-559.01	18	-591.05	5	-1294.88	9	915.96	9	-76.59	13	-329.93	5	-297.44	9
401	Max	-173	-513.32	9	3565.92	17	-106.38	5	3079.98	19	-840.04	9	648.22	18	86.52	9	1033.68	19
401	Max	-150	-513.32	9	3565.92	17	-106.38	5	3079.98	19	-840.04	9	648.22	18	86.52	9	1033.68	19
401	Max	-145	-513.32	9	3565.92	17	-106.38	5	3079.98	19	-840.04	9	648.22	18	86.52	9	1033.68	19
401	Max	-185	-513.32	9	3565.92	17	-106.38	5	3079.98	19	-840.04	9	648.22	18	86.52	9	1033.68	19
401	Min.	-173	-1496.47	17	1394.53	1	-1147.03	18	1173.71	9	-1929.46	19	143.55	5	-1589.35	1	299.08	9
401	Min.	-150	-1496.47	17	1394.53	1	-1147.03	18	1173.71	9	-1929.46	19	143.55	5	-1589.35	1	299.08	9
401	Min.	-145	-1496.47	17	1394.53	1	-1147.03	18	1173.71	9	-1929.46	19	143.55	5	-1589.35	1	299.08	9
401	Min.	-185	-1496.47	17	1394.53	1	-1147.03	18	1173.71	9	-1929.46	19	143.55	5	-1589.35	1	299.08	9
401	Max	-150	8066.79	17	792.20	17	2316.32	18	310.33	1	-649.89	9	604.90	17	-4371.71	9	16027.70	18
401	Max	-148	8066.79	17	792.20	17	2316.32	18	310.33	1	-649.89	9	604.90	17	-4371.71	9	16027.70	18
401	Max	-124	8066.79	17	792.20	17	2316.32	18	310.33	1	-649.89	9	604.90	17	-4371.71	9	16027.70	18
401	Max	-125	8066.79	17	792.20	17	2316.32	18	310.33	1	-649.89	9	604.90	17	-4371.71	9	16027.70	18
401	Min.	-150	3050.42	9	-2576.80	18	-2617.07	17	-2792.05	9	-1394.92	19	51.09	18	-10650.70	19	5172.81	1
401	Min.	-148	3050.42	9	-2576.80	18	-2617.07	17	-2792.05	9	-1394.92	19	51.09	18	-10650.70	19	5172.81	1
401	Min.	-124	3050.42	9	-2576.80	18	-2617.07	17	-2792.05	9	-1394.92	19	51.09	18	-10650.70	19	5172.81	1
401	Min.	-125	3050.42	9	-2576.80	18	-2617.07	17	-2792.05	9	-1394.92	19	51.09	18	-10650.70	19	5172.81	1
401	Max	-150	1022.93	17	-767.08	20	2452.86	17	-962.22	9	-373.40	1	-1036.00	13	8580.81	18	-3419.66	1
401	Max	-125	1022.93	17	-767.08	20	2452.86	17	-962.22	9	-373.40	1	-1036.00	13	8580.81	18	-3419.66	1
401	Max	-114	1022.93	17	-767.08	20	2452.86	17	-962.22	9	-373.40	1	-1036.00	13	8580.81	18	-3419.66	1
401	Max	-145	1022.93	17	-767.08	20	2452.86	17	-962.22	9	-373.40	1	-1036.00	13	8580.81	18	-3419.66	1
401	Min.	-150	-1276.71	18	-2271.20	17	927.87	1	-2218.64	18	-1336.86	19	-1920.93	19	3314.10	1	-10044.70	18
401	Min.	-125	-1276.71	18	-2271.20	17	927.87	1	-2218.64	18	-1336.86	19	-1920.93	19	3314.10	1	-10044.70	18
401	Min.	-114	-1276.71	18	-2271.20	17	927.87	1	-2218.64	18	-1336.86	19	-1920.93	19	3314.10	1	-10044.70	18
401	Min.	-145	-1276.71	18	-2271.20	17	927.87	1	-2218.64	18	-1336.86	19	-1920.93	19	3314.10	1	-10044.70	18

Criteri di progetto utilizzati

Aste in acciaio

Generali

Verifica aste in acciaio

Numero punti di verifica	10.00
Numero CC da considerare di tipo I	99.00

Stati limite D.M. 08

Verifiche con EC3	No
Coeff. amplificativo sollecitazioni per effetti del secondo ordine	1.00

Stampe

Verifiche da riportare in relazione	Tutte

1

Specifici

Materiali

CNR 10011	
Tipo di acciaio	FE360
D.M. 08	
Tipo di acciaio per profilati a sezione aperta	S355 UNI EN 10025-2
Tipo di acciaio per profilati a sezione cava	S235H UNI EN 10210-1
EC3	
Tipo di acciaio	S460
-Fy <daN/cmq>	4600.00
-Fu <daN/cmq>	5400.00
γ M0	1.00
γ M1	1.00
γ M2	1.25
γ Rd	1.30
γ Ov	1.25
-Considera come elemento esistente (S.L. D.M. 08/EC3)	No
-Livello di conoscenza	LC1
-Fattore di confidenza	1.35

Verifiche di resistenza

Rapporto fra area effettiva e area nominale	1.00
Rapporto fra area netta e area nominale	1.00
Coeff. di forma intorno all'asse Y	1.00
Coeff. di forma intorno all'asse Z	1.00
Verifica le bielle solo con sollecitazioni di trazione moltiplicate per	Si
Valutare la τ per torsione nei punti di spigolo (CNR 10011)	No
-Pari a	
Stati limite D.M. 08/EC3	
-Fai sempre verifiche in campo elastico	No
-Effettua le verifiche della gerarchia delle resistenze per strutture intelaiate	Si
-Usa classe 1 in pressoflessione deviata se non presente in archivio	No
Stati limite D.M. 08	
-Usa prescrizioni EC3 quando più dettagliate	Si
-Considera prescrizioni relative ai ponti	Si

Verifiche di deformabilità

Max valore del rapporto tra la luce e la freccia (totale)	300.00
Max valore del rapporto tra la luce e la freccia (solo accidentali)	300.00
Max valore del rapporto tra altezza e spostamento orizz. (aste)	300.00
Max valore del rapporto tra altezza e spostamento orizz. (membrature)	500.00
Considerare anche spostamento relativo nodi per calcolo freccia	Si
Considerare solo la verifica di deformabilità delle membrature	No
Trascura deformazione dovuta al sisma (T.A.)	No

Verifiche di stabilità asta

Riduzione lunghezza libera d'inflessione	
-Distanza fra i nodi dell'asta	x
-Distanza ridotta delle zone rigide moltiplicate per il valore	
Tipo di accoppiamento aste composte	
-Separate	
-Calastrellate	
-Imbottite	
-Automatico	x
Calcolo momento medio usando valori assoluti	Si
Interasse calastrelli o imbottiture	
-Distanza pari a <m>	
-Interasse da normativa moltiplicato per il valore	0.80
-Aste rigidamente collegate	
Curva di stabilità (D.M. 08/EC3)	Automatica
Aste laminate	Si
Sigma max amm. senza verifiche di stabilità (CNR 10011) <%>	2.00
Verifiche di stabilità globale in dir. Y locale	Si
-Coeff. β intorno all'asse Y	1.00
Verifiche di stabilità globale in dir. Z locale	Si
-Coeff. β intorno all'asse Z	1.00
Verifiche di stabilità flesso - torsionale	Si
-Coeff. per calcolo interasse ritegni torsionali	1.00
Aste inflesse (D.M. 08/EC3)	
-Coeff. Ψ per calcolo momento critico	

-Valuta in base ai momenti dell'asta	x	
-Utilizza valore imposto		
-Fattore correttivo di distribuzione K_c		0.94
-Snellezza di riferimento $\lambda_{LT,0}$		0.40
-Coeff. β		0.75
Aste pressoinflesse (D.M. 08/EC3)		
-Considera come molto deformabile a torsione	No	
-Fattore correttivo di distribuzione α_{mY}/C_{mY}		0.95
-Fattore correttivo di distribuzione α_{mZ}/C_{mZ}		0.95
-Fattore correttivo di distribuzione α_{mLT}/C_{mLT}		0.95
Eseguire anche le verifiche al punto 7.3.2 (CNR 10011)	Si	
Carichi sull'estradosso (CNR 10011)	Si	
Verifiche di stabilità all'imbozzamento (CNR 10011)		
-Numero irrigidimenti orizzontali anima		0.00
-Interasse irrigidimenti verticali anima		
-Numero di suddivisioni		
-Distanza non inferiore a <cm>		
-Pari alla lunghezza dell'asta	x	
-Modalità di calcolo σ cr,id		
-Normativa		
-Massonet	x	
-Ballio		

Verifiche di stabilità membratura

Massimo numero aste costituenti unica membratura		1.00
Sforzo normale di verifica		
-Massimo valore fra tutte le aste	x	
-Media aritmetica dei valori di tutte le aste		
-Media pesata di tutte le aste		
Contributo eventuali sforzi di trazione	No	
Verifica nei piani principali	Si	
Incremento snellezza	Si	
Verifiche di stabilità globale in dir. Y locale	Si	
-Coeff. β calcolato in funzione dello sforzo normale		
-Coeff. β		1.00
Verifiche di stabilità globale in dir. Z locale	Si	
-Coeff. β calcolato in funzione dello sforzo normale		
-Coeff. β		1.00

Pareti

Generali

Parametri di disegno

Scala disegno pareti	50.00
Campitura disegno parete	Rada
Disegno armatura diffusa	No
Disegno prospetto e pianta	Sempre

Stampe

Tipo di relazione	Sintetica

1

Specifici

Materiali

Calcestruzzo		
-Tipo di calcestruzzo	C32/40	
-Rck calcestruzzo <daN/cmq>		400.00
-Modulo elastico <daN/cmq>		336428.00
-Resistenza caratteristica cilindrica (Fck) <daN/cmq>		332.00
-Resistenza caratteristica a trazione (Fctk) <daN/cmq>		21.69
-Riduci Fcd per tutte le verifiche secondo il D.M. 08	Si	
-γ_c per stati limite ultimi		
-Automatico	x	
-Pari a		
-σ amm. calcestruzzo <daN/cmq>		122.50
-τc0 <daN/cmq>		7.30
-τc1 <daN/cmq>		21.10
Acciaio		
-D.M. 92/96		
-Tipo di acciaio (Fe B 22÷44 k)	44	
-Modulo elastico <daN/cmq>		2.06E+006
-Tensione caratteristica di snervamento (Fyk) <daN/cmq>		4300.00
-Sigma amm. acciaio <daN/cmq>		2600.00
-Sigma amm. reti e tralicci <daN/cmq>		2600.00
-D.M. 08		

-Tipo di acciaio (B450A÷B450C)	B450C
-Modulo elastico <daN/cmq>	2.06E+006
-Tensione caratteristica di snervamento (Fyk) <daN/cmq>	4500.00
-γ_s per stati limite ultimi	
-Automatico	x
-Pari a	
Coeff. di omogeneizzazione	15.00

Parametri di calcolo

Copriferro <cm>	3.50
Fattore moltiplicativo per calcolo τ l	1.00
Fattore moltiplicativo per calcolo τ t	1.00
Fattore di riduzione per ancoraggio ferri	1.00
Lunghezza ancoraggi armature	
-Calcolata in funzione della σ f	
-Imposta come multiplo del diametro	20.00
Lunghezza minima pari a <m>	0.50
-Inserire solo armatura al centro della parete	No
Modalità di progettazione e verifica armatura verticale	
-In funzione delle zone di incidenza elementi	
-In funzione delle sollecitazioni globali	x
-Inserisci armatura di rinforzo nelle zone di incidenza elementi	Si
-Dimensione minima zone di incidenza elementi	Si
-Pari a multiplo dello spessore	1.00
-Passo di verifica	1.50
-Trascura zone con pilastro inglobato	Si
-Effettuare verifiche nel piano della parete	No
-Elimina armatura diffusa nelle zone di rinforzo	Si
Elimina armatura diffusa nell'architrave	Si
-Effettuare verifiche su sezioni verticali	No
-Passo di verifica	1.00
Controllare resistenza a taglio trasversale come sezione priva di armatura a taglio	No
Min. Af armatura diffusa <cmq/m>	3.00
Considera come parete debolmente armata ai sensi D.M. 08	Si
-Modalità di valutazione parametri nel caso di sisma diverso per X e Y	
-Usa valore massimo	x
-Componi in direzione parete	
-Incremento del 50% delle forze assiali	
Sempre	x
-Solo per analisi sismiche statiche	
-Mai	
Coeff. β per controllo snellezza <m>	1.00
Rispetta i disposti del punto 7.4.4.5.2.1 solo per stati limite sismici	Si

Armatura diffusa

Considera armatura con rete elettrosaldata	No
Armatura verticale o rete	
Elenco diametri utilizzabili 1 <mm>	10
Elenco diametri utilizzabili 2 <mm>	12
Elenco diametri utilizzabili 3 <mm>	
Elenco diametri utilizzabili 4 <mm>	
Elenco diametri utilizzabili 5 <mm>	
Elenco diametri utilizzabili 6 <mm>	
Elenco diametri utilizzabili 7 <mm>	
Passi utilizzabili	
-Minimo <cm>	12.00
-Massimo <cm>	30.00
-Incremento <cm>	2.00
-Modalità di completamento armatura	
-Adattata	x
-Terminata	
-Nessuna	
Armatura orizzontale	
Elenco diametri utilizzabili 1 <mm>	8
Elenco diametri utilizzabili 2 <mm>	10
Elenco diametri utilizzabili 3 <mm>	
Elenco diametri utilizzabili 4 <mm>	
Elenco diametri utilizzabili 5 <mm>	
Elenco diametri utilizzabili 6 <mm>	
Elenco diametri utilizzabili 7 <mm>	
Passi utilizzabili	
-Minimo <cm>	10.00
-Massimo <cm>	30.00
-Incremento <cm>	2.00
Tipo di armatura orizzontale	
-Dritta	x
-Con risvolti di estremità	
-Modalità di chiusura orizzontale	
-Nessuna chiusura	
-Chiusura con ferri ad U	x

-Chiusura con staffe
-Lunghezza armatura di chiusura
-Multiplo dello spessore pari a
-Lunghezza fissa pari a <cm> 0.50
-Tipo di ottimizzazione armatura
-Minimizza il peso complessivo dei ferri x
-Minimizza il numero dei ferri

Armatura di rinforzo

Elenco diametri utilizzabili 1 <mm> 12
Elenco diametri utilizzabili 2 <mm> 14
Elenco diametri utilizzabili 3 <mm> 16
Elenco diametri utilizzabili 4 <mm>
Elenco diametri utilizzabili 5 <mm>
Elenco diametri utilizzabili 6 <mm>
Elenco diametri utilizzabili 7 <mm>
Numero minimo ferri 2.00
Interferro minimo <cm> 10.00
-Aggiungi staffe chiuse Si
-Stesso diametro armatura diffusa orizzontale x
-Diametro imposto
-Stesso passo armatura diffusa orizzontale x
-Passo imposto

Armatura secondaria

Diametro ferri di collegamento <mm> 8.00
Numero ferri di collegamento (a mq) 6.00
Lunghezza ancoraggio ferri di collegamento <cm> 10.00

Dati per progettazione agli stati limite

Gruppo di esigenza
-Ambiente poco aggressivo
-Ambiente moderatamente aggressivo x
-Ambiente molto aggressivo
Usa dominio N-M per flessioni rette No
-Ricerca della sicurezza con sforzo normale costante
-Ricerca della sicurezza con eccentricità costante
Controllo rapporto X/D No
Barre da considerare tese per verifiche a taglio
-Solo le barre con deformazione percentuale rispetto
alla barra più tesa non inferiore al <%> 30.00
-Tutte le barre in trazione

Solette/Platee

Generali

Parametri di progetto

Controllo resistenza a taglio allo S.L.U. No
Calcolo armature con metodo di Wood No
Accoppia pilastri per calcolo punzonamento Si
-Massima distanza come un moltiplicatore dello spessore 1.50

Parametri di disegno

Disposizione disegno 2A
Particolari nel disegno principale
-Eliminare le quotature No
-Eliminare le campiture No
-Eliminare la numerazione dei pilastri No
-Eliminare la numerazione delle travi e dei muri No
Particolari nei disegni secondari
-Eliminare le quotature Si
-Eliminare le campiture Si
-Eliminare la numerazione dei pilastri Si
-Eliminare la numerazione delle travi e dei muri Si
Disegno armatura diffusa No
Posizione particolari punzonamento In automatico
Copriferro per calcolo lunghezza ferri <cm> 3.50
Risvoltare al bordo i ferri
-Inferiori Si
-Superiori Si
Lunghezza risvolti ferri al bordo Pari all'altezza meno due volte il copriferro
Disegno particolare ferri al bordo Si
Scala disegno particolare ferri al bordo 20.00
Calcolo lunghezza ferri semplificato No

Stampe

Tipo di relazione Sintetica

Specifici

Materiali

Calcestruzzo	
-Tipo di calcestruzzo	C32/40
-Rck calcestruzzo <daN/cmq>	400.00
-Modulo elastico <daN/cmq>	336428.00
-Resistenza caratteristica cilindrica (Fck) <daN/cmq>	332.00
-Resistenza caratteristica a trazione (Fctk) <daN/cmq>	21.69
-Riduci Fcd per tutte le verifiche secondo il D.M. 08	Si
-γ_c per stati limite ultimi	
-Automatico	x
-Pari a	
-σ amm. calcestruzzo <daN/cmq>	122.50
-τc0 <daN/cmq>	7.30
-τc1 <daN/cmq>	21.10
Acciaio	
-D.M. 92/96	
-Tipo di acciaio (Fe B 22÷44 k)	44
-Modulo elastico <daN/cmq>	2.06E+006
-Tensione caratteristica di snervamento (Fyk) <daN/cmq>	4300.00
-Sigma amm. acciaio <daN/cmq>	2600.00
-Sigma amm. reti e tralicci <daN/cmq>	2600.00
-D.M. 08	
-Tipo di acciaio (B450A÷B450C)	B450C
-Modulo elastico <daN/cmq>	2.06E+006
-Tensione caratteristica di snervamento (Fyk) <daN/cmq>	4500.00
-γ_s per stati limite ultimi	
-Automatico	x
-Pari a	
Coeff. di omogeneizzazione	15.00

Armatura a flessione

Angolo d'armatura <grad>	0.00
Copriferro teorico superiore <cm>	5.00
Copriferro teorico inferiore <cm>	5.00
Tipo di progetto in doppia armatura	
-Tensione pari ai valori amm.	
-Tensione pari ai valori amm. con AfComp/AfTesa minore o pari a	1.00
-Tensione pari ai valori amm. con AfComp/AfTesa pari a	
Min. percentuale di regolamento	
-Platee di fondazione su suolo elastico	No
-Solette di elevazione	Si
Controlla min. armatura di ripartizione	No
Elenco diametri utilizzabili 1 <mm>	10
Elenco diametri utilizzabili 2 <mm>	12
Elenco diametri utilizzabili 3 <mm>	14
Elenco diametri utilizzabili 4 <mm>	16
Elenco diametri utilizzabili 5 <mm>	
Elenco diametri utilizzabili 6 <mm>	
Elenco diametri utilizzabili 7 <mm>	
Passi utilizzabili	
-Minimo <cm>	15.00
-Massimo <cm>	30.00
-Incremento <cm>	5.00
Uniformizzazione interassi armatura	No
-Sempre	
-Nella stessa direzione	
-Nella stessa posizione	
Uniformizzazione diametri armatura	No
-Sempre	
-Nella stessa direzione	
-Nella stessa posizione	
Tipo di ottimizzazione armatura a flessione	
-Minimizza il numero dei ferri	
-Minimizza il peso complessivo dei ferri	x

Ancoraggi

Fattore di riduzione per ancoraggio ferri	1.00
Lunghezza ancoraggi armature	
-Calcolata in funzione della Sigmaf	x
-Imposta come multiplo del diametro	
Lunghezza ancoraggi ferri punzonamento	
-Calcolata in funzione della Sigmaf	x
-Imposta come multiplo del diametro	

Armatura a punzonamento

Fattore di riduzione altezza soletta/platea	0.90
Modifica altezza soletta/platea	Si

Allargamento piastra pilastri in acciaio <cm>		5.00
Distanza dal bordo libero		
-Distanza come un moltiplicatore dello spessore		1.00
-Distanza imposta a <cm>		
Moltiplicatore altezza utile per valutare perimetro efficace (D.M. 08)		2.00
Tolleranza di posizionamento barre		
-Distanza come un moltiplicatore dello spessore		0.10
-Distanza imposta a <cm>		
Elenco diametri utilizzabili 1 <mm>	12	
Elenco diametri utilizzabili 2 <mm>	14	
Elenco diametri utilizzabili 3 <mm>	16	
Elenco diametri utilizzabili 4 <mm>	18	
Elenco diametri utilizzabili 5 <mm>	20	
Elenco diametri utilizzabili 6 <mm>		
Elenco diametri utilizzabili 7 <mm>		
Passi utilizzabili		
-Minimo <cm>		10.00
-Massimo <cm>		20.00
-Incremento <cm>		2.00
Tipo di ottimizzazione armatura a punzonamento		
-Minimizza il numero dei ferri	x	
-Minimizza il peso complessivo dei ferri		

Dati per progettazione agli stati limite

Gruppo di esigenza		
-Ambiente poco aggressivo		
-Ambiente moderatamente aggressivo	x	
-Ambiente molto aggressivo		
Usa dominio N-M per flessioni rette	No	
-Ricerca della sicurezza con sforzo normale costante		
-Ricerca della sicurezza con eccentricità costante		
Controllo rapporto X/D	No	
Barre da considerare tese per verifiche a taglio		
-Solo le barre con deformazione percentuale rispetto		
Incremento <%>		30.00
-Tutte le barre in trazione		

Verifiche e armature solette/platee

Simbologia

Nodo = Numero del nodo
X = Coordinata X del nodo
Y = Coordinata Y del nodo
DV = Direzione di verifica
  XX = Verifica per momento Mxx
  YY = Verifica per momento Myy
CC = Numero della combinazione delle condizioni di carico elementari
TCC = Tipo di combinazione di carico
  SLU = Stato limite ultimo
  SLU S = Stato limite ultimo (azione sismica)
  SLE R = Stato limite d'esercizio, combinazione rara
  SLE F = Stato limite d'esercizio, combinazione frequente
  SLE Q = Stato limite d'esercizio, combinazione quasi permanente
  SLD = Stato limite di danno
  SLV = Stato limite di salvaguardia della vita
  SLC = Stato limite di prevenzione del collasso
  SLO = Stato limite di operatività
  SLU I = Stato limite di resistenza al fuoco
c = Ricoprimento dell'armatura
s = Distanza minima tra le barre
K3 = Coefficiente di forma del diagramma delle tensioni prima della fessurazione
s_{rm} = Distanza media tra le fessure
Φ = Diametro della barra
A_s = Area complessiva dei ferri nell'area di calcestruzzo efficace
$A_{c\ eff}$ = Area di calcestruzzo efficace
σ_s = Tensione nell'acciaio nella sezione fessurata
σ_{sr} = Tensione nell'acciaio corrispondente al raggiungimento della resistenza a trazione nel calcestruzzo
ε_{sm} = Deformazione unitaria media dell'armatura (*1000)
Wk = Apertura delle fessure
AfE S = Area di ferro effettiva totale presente nel punto di verifica, superiore
AfE I = Area di ferro effettiva totale presente nel punto di verifica, inferiore
Mom = Momento flettente
Mu = Momento ultimo
Sic. = Sicurezza a rottura
Vsdu = Taglio agente nella direzione del momento ultimo
Vrdu = Taglio ultimo assorbibile dal solo calcestruzzo
σ_c = Tensione nel calcestruzzo

σ_f = Tensione nel ferro
Spess. = Spessore
Cf sup = Copriferro superiore
Cf inf = Copriferro inferiore
Cls = Tipo di calcestruzzo
Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
Fctk = Resistenza caratteristica a trazione del calcestruzzo
Fcd = Resistenza di calcolo a compressione del calcestruzzo
Fctd = Resistenza di calcolo a trazione del calcestruzzo
Acc. = Tipo di acciaio
Fyk = Tensione caratteristica di snervamento dell'acciaio
Fyd = Resistenza di calcolo dell'acciaio

Armatura soletta a quota 0.00

Caratteristiche delle sezioni e dei materiali utilizzati

Spess. <cm>	Cf sup <cm>	Cf inf <cm>	Cls	Fck <daN/cmq>	Fctk <daN/cmq>	Fcd <daN/cmq>	Fctd <daN/cmq>	Acc.	Fyk <daN/cmq>	Fyd <daN/cmq>
100.00	5.00	5.00	C32/40	332.00	21.69	188.13	14.46	B450C	4500.00	3913.04

Stato limite ultimo - Ferri longitudinali - Verifiche armatura

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Mom <daNm>	Mu <daNm>	Sic.
-67	7.02	0.00	XX	9	SLV	7.70	7.70	-5217.62	-28240.10	5.412
-233	0.00	4.74	XX	10	SLD	7.70	7.70	3360.24	32594.60	9.700
-198	12.74	3.95	XX	19	SLU	7.70	7.70	-6024.29	-28240.10	4.688
-147	7.02	2.37	XX	2	SLD	7.70	7.70	-3254.18	-32594.60	10.016
-198	12.74	3.95	YY	19	SLU	7.70	7.70	-5624.70	-28240.10	5.021
-194	1.30	3.95	YY	14	SLD	7.70	7.70	-2824.98	-32594.60	11.538
-67	7.02	0.00	YY	18	SLU	7.70	7.70	3884.49	28240.10	7.270
-257	7.02	5.24	YY	6	SLD	7.70	7.70	2156.33	32594.60	15.116

Stato limite ultimo - Verifica a taglio del calcestruzzo

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Vsdu <daN>	Vrdu <daN>
-127	13.35	1.60	XX	18	SLU	7.70	7.70	20192.10	33757.40
-127	13.35	1.60	XX	10	SLD	7.70	7.70	11691.20	34693.10
-208	12.90	4.28	YY	19	SLU	7.70	7.70	31947.10	33757.40
-208	12.90	4.28	YY	2	SLD	7.70	7.70	16679.90	34693.10

Stato limite d'esercizio - Ferri longitudinali - Verifiche armatura

Nodo	X <m>	Y <m>	DV	CC	TCC	AfE S <cmq>	AfE I <cmq>	Mom <daNm>	σ_c <daN/cmq>	σ_f <daN/cmq>
-348	3.06	7.36	XX	20	SLE R	7.70	7.70	3540.17	5.40	507.76
-348	3.06	7.36	XX	23	SLE Q	7.70	7.70	2219.57	3.38	318.35
-198	12.74	3.95	XX	21	SLE R	7.70	7.70	-4210.86	6.42	603.96
-194	1.30	3.95	XX	23	SLE Q	7.70	7.70	-3012.93	4.59	432.14
-198	12.74	3.95	YY	21	SLE R	7.70	7.70	-3900.91	5.95	559.51
-198	12.74	3.95	YY	23	SLE Q	7.70	7.70	-2735.14	4.17	392.30
-67	7.02	0.00	YY	20	SLE R	7.70	7.70	2709.84	4.13	388.67
-262	12.98	5.25	YY	23	SLE Q	7.70	7.70	1909.86	2.91	273.93

Verifiche stato limite di formazione delle fessure

Nodo	X <m>	Y <m>	DV	CC	TCC	c <mm>	s <mm>	K3	s_{rm} <mm>	Φ	A_s <cmq>	$A_{c\ eff}$ <cmq>	σ_s <daN/cmq>	σ_{sr} <daN/cmq>	ε_{sm}	Wk <mm>
-348	3.06	7.36	XX	23	SLE Q	43.00	196.00	0.21	311.83	14.00	1.54	240.76	318.35	9388.39	0.06	0.03
-229	0.59	4.67	XX	22	SLE F	43.00	196.00	0.21	311.83	14.00	1.54	240.76	351.13	9388.40	0.07	0.04
-194	1.30	3.95	XX	23	SLE Q	43.00	196.00	0.21	311.83	14.00	1.54	240.76	432.14	9388.39	0.08	0.04
-194	1.30	3.95	XX	22	SLE F	43.00	196.00	0.21	311.83	14.00	1.54	240.76	441.80	9388.40	0.09	0.05
-198	12.74	3.95	YY	23	SLE Q	43.00	196.00	0.21	311.83	14.00	1.54	240.76	392.30	9388.39	0.08	0.04
-198	12.74	3.95	YY	22	SLE F	43.00	196.00	0.21	311.83	14.00	1.54	240.76	404.95	9388.40	0.08	0.04
-262	12.98	5.25	YY	23	SLE Q	43.00	196.00	0.21	311.83	14.00	1.54	240.76	273.93	9388.40	0.05	0.03
-257	7.02	5.24	YY	22	SLE F	43.00	196.00	0.21	311.83	14.00	1.54	240.76	286.00	9388.39	0.06	0.03

Verifiche aste in acciaio

Simbologia

Sez. = Numero della sezione
Cod. = Codice
Tipo = Tipologia
- 2C = Doppia C lato labbri
- 2Cdx = Doppia C lato costola
- 2I = Doppia I
- 2L = Doppia L lato labbri
- 2Ldx = Doppia L lato costole
- C = C
- Cdx = C destra
- Cir. = Circolare

Cir.c = Circolare cava
I = I
L = L
Ldx = L destra
Om. = Omega
Pg = Pi greco
Pr = Poligono regolare
Prc = Poligono regolare cavo
Pc = Per coordinate
Ia = Inerzie assegnate
R = Rettangolare
Rc = Rettangolare cava
T = T
U = U
Ur = U rovescia
V = V
Vr = V rovescia
Z = Z
Zdx = Z destra
Ts = T stondata
Ls = L stondata
Cs = C stondata
Is = I stondata
Dis. = Disegnata

D	<cm>	= Distanza
Area	<cmq>	= Area
Anet	<cmq>	= Area netta per compressione
Aeff	<cmq>	= Area effettiva per trazione
Jy	<cm4>	= Momento d'inerzia rispetto all'asse Y
Jz	<cm4>	= Momento d'inerzia rispetto all'asse Z
Iy	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Y
Iz	<cm>	= Raggio giratorio d'inerzia rispetto all'asse Z
Wymin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Y
Wzmin	<cmc>	= Modulo di resistenza minimo rispetto all'asse Z
Wy,plas	<cmc>	= Modulo di resistenza plastico intorno all'asse Y
Wz,plas	<cmc>	= Modulo di resistenza plastico intorno all'asse Z
Atag,y	<cmq>	= Area resistente a taglio in dir. Y
Atag,z	<cmq>	= Area resistente a taglio in dir. Z
Jω	<cm6>	= Costante di ingobbamento
L_{cr}	<m>	= Lunghezza di libera inflessione laterale fra ritegni torsionali
α-imp		= Coefficiente di imperfezione
k_c		= Coeff. di correzione momento flettente per stabilità laterale membrature inflesse
ψ		= Coeff. di correzione momento critico per stabilità laterale membrature inflesse
M,cr	<daNm>	= Momento critico per instabilità flesso torsionale
λ_{LT}		= Coefficiente di imperfezione per stabilità laterale membrature inflesse
$\lambda_{LT,0}$		= Coefficiente di imperfezione di confronto per stabilità laterale membrature inflesse
β_{LT}		= Coefficiente per calcolo Φ_{LT}
Φ_{LT}		= Coefficiente Φ per stabilità laterale membrature inflesse
f		= Fattore di modifica per il coefficiente di riduzione
χ_{LT}		= Coefficiente di riduzione per stabilità laterale membrature inflesse
My,Ed	<daNm>	= Momento flettente di calcolo intorno all'asse Y
My,b,Rd	<daNm>	= Resistenza di calcolo a flessione ridotta per stabilità laterale membrature inflesse
CC		= Numero della combinazione delle condizioni di carico elementari
N,Ed	<daN>	= Forza assiale di calcolo
Nc,Rd	<daN>	= Resistenza a compressione
My,c,Rd	<daNm>	= Resistenza di calcolo a flessione intorno all'asse Y
L		= lunghezza dell'asta
αmy, αmz, αLT		= Coefficienti correttivi per il momento flettente
λ_y		= Snellezza per inflessione intorno all'asse y(c)
Ncr,y	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse y(c)
λ^*_y		= Snellezza adimensionale per inflessione intorno all'asse y(c)
Curva		= Curva di instabilità adottata
Φ_y		= Coefficiente Φ per inflessione intorno all'asse y(c)
χ_y		= Coefficiente χ di riduzione per instabilità intorno all'asse y(c)
λ_z		= Snellezza per inflessione intorno all'asse z(e)
Ncr,z	<daN>	= Sforzo normale critico euleriano per inflessione intorno all'asse z(e)
λ^*_z		= Snellezza adimensionale per inflessione intorno all'asse z(e)
Φ_z		= Coefficiente Φ per inflessione intorno all'asse z(e)
χ_z		= Coefficiente χ di riduzione per instabilità intorno all'asse z(e)
Kyy, Kyz, Kzy, Kzz		= Coefficienti di interazione
Xl	<m>	= Coordinata progressiva (dal nodo iniziale dell'asta) in cui viene effettuato il progetto/verifica
N	<daN>	= Sforzo normale
Tz	<daN>	= Taglio in dir. Z
My	<daNm>	= Momento flettente intorno all'asse Y
σ_N	<daN/cmq>	= Tensione normale per sforzo normale
σ_M	<daN/cmq>	= Tensione normale per momento flettente
τ	<daN/cmq>	= Tensione tangenziale per taglio e/o torsione
$\sigma_{ID,max}$	<daN/cmq>	= Tensione ideale massima
V,Ed,G	<daN>	= Forza di taglio per azioni non sismiche
V,Ed,M	<daN>	= Forza di taglio dovuta all'applicazione dei momenti resistenti
V,Ed	<daN>	= Forza di taglio di calcolo
Vc,Rd	<daN>	= Resistenza a taglio
MNy,c,Rd	<daNm>	= Resistenza di calcolo a pressoflessione intorno all'asse Y
$f_{Z,L}$	<cm>	= Freccia in direzione Z locale
$f_{Z,G}$	<cm>	= Freccia in direzione Z globale

Caratteristiche profilati utilizzati

Sez.	Cod.	Tipo	D <cm>	Area <cmq>	Anet <cmq>	Aeff <cmq>	Jy <cm4>	Jz <cm4>	Iy <cm>	Iz <cm>	Wymin <cmc>	Wzmin <cmc>
1	HEA280	Is	--	97.27	97.27	97.27	13673.70	4762.65	11.86	7.00	1012.87	340.19
2	HEB280	Is	--	131.37	131.37	131.37	19270.70	6594.53	12.11	7.09	1376.48	471.04
3	IPE180	Is	--	23.95	23.95	23.95	1316.99	100.85	7.42	2.05	146.33	22.16

Caratteristiche profilati utilizzati

Sez.	Cod.	Wy,plas <cmc>	Wz,plas <cmc>	Atag,y <cmq>	Atag,z <cmq>	Jω <cm6>
1	HEA280	1117.45	518.72	81.59	31.75	785367.00
2	HEB280	1539.66	718.22	110.79	41.10	1130150.00
3	IPE180	166.93	34.64	16.21	11.25	7431.22

Asta n. 101 (101 102) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 18 My,Ed=-857.51 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-4366.56
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.13 = 0.42
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.07 (L/1129)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=5011.54 M_y=-4366.56
  Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 σ_{max}=-1376.11
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=271.65 τ_{max}=271.65
  Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 $\sigma_{ID,max}$=1376.11

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.35
  Sollecitazioni: T_z=11558.10
  V,Ed=11558.10 (V,Ed,G=794.45, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.19

Asta n. 101 (102 103) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1206500.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-1622.66 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-8276.49
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1207080.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.25 = 0.54
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1501)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=2894.20 M_y=-8276.49
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 σ_{max}=-1762.13
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=156.88 τ_{max}=156.88
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 $\sigma_{ID,max}$=1762.13

Asta n. 101 (103 104) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001010.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.59
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001090.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.28 = 0.57

Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/4474)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=567.11 M_y=-9463.59
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.34
Tensioni: σ_N=-945.00 σ_M=0.00 τ=30.74 τ_{max}=30.74
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.34

Asta n. 101 (104 105) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019570.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.58
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019740.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211010.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.28 = 0.57
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/3485)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
Sollecitazioni: N=-91917.70 T_z=-865.24 M_y=-9463.58
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.33
Tensioni: σ_N=-945.00 σ_M=0.00 τ=46.90 τ_{max}=46.90
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.33

Asta n. 101 (105 106) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1252230.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=-1554.59 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-7927.64
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1253090.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.24 = 0.53
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.08 (L/1408)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
Sollecitazioni: N=-91917.70 T_z=-3192.33 M_y=-7927.64
Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 σ_{max}=-1727.69
Tensioni: σ_N=-945.00 σ_M=0.00 τ=173.04 τ_{max}=173.04
Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 $\sigma_{ID,max}$=1727.69

Asta n. 101 (106 107) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
CC 19 My,Ed=-721.36 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-3668.90
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95

L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.11 = 0.40
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.06 (L/1117)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
Sollecitazioni: N=-91917.70 T_z=-5219.78 M_y=-3668.90
Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 σ_{max}=-1307.23
Tensioni: σ_N=-945.00 σ_M=0.00 τ=282.94 τ_{max}=282.94
Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 $\sigma_{ID,max}$=1307.23

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.67
Sollecitazioni: T_z=9959.74
V,Ed=9959.74 (V,Ed,G=-803.90, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.16

Asta n. 101 (107 108) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650940.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
CC 18 My,Ed=-721.36 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-3668.89
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650940.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703100.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211010.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.11 = 0.40
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.06 (L/1118)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=5219.78 M_y=-3668.89
Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 σ_{max}=-1307.23
Tensioni: σ_N=-945.00 σ_M=0.00 τ=282.94 τ_{max}=282.94
Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 $\sigma_{ID,max}$=1307.23

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.50
Sollecitazioni: T_z=11567.50
V,Ed=11567.50 (V,Ed,G=803.90, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.19

Asta n. 101 (108 109) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1252230.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 18 My,Ed=-1554.59 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-7927.64
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1253090.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.24 = 0.53
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/1410)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=3192.33 M_y=-7927.64
Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 σ_{max}=-1727.69

Tensioni: σ_N=-945.00 σ_M=0.00 τ=173.04 τ_{max}=173.04
Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 $\sigma_{ID,max}$=1727.69

Asta n. 101 (109 110) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019570.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 18 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.58
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019740.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.28 = 0.57
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/3500)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=865.24 M_y=-9463.58
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.33
Tensioni: σ_N=-945.00 σ_M=0.00 τ=46.90 τ_{max}=46.90
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.33

Asta n. 101 (110 111) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001010.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.59
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001090.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.28 = 0.57
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/4451)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
Sollecitazioni: N=-91917.70 T_z=-567.11 M_y=-9463.59
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.34
Tensioni: σ_N=-945.00 σ_M=0.00 τ=30.74 τ_{max}=30.74
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.34

Asta n. 101 (111 112) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1206500.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=-1622.66 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-8276.49
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1207080.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.25 = 0.54
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.08 (L/1498)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-2894.20 M_y=-8276.49
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 σ_{max}=-1762.13
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=156.88 τ_{max}=156.88
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 $\sigma_{ID,max}$=1762.13

Asta n. 101 (112 113) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 19 My,Ed=-857.51 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-4366.56
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.13 = 0.42
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.07 (L/1128)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-5011.54 M_y=-4366.56
  Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 σ_{max}=-1376.11
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=271.65 τ_{max}=271.65
  Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 $\sigma_{ID,max}$=1376.11

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.82
  Sollecitazioni: T_z=9969.19
  V,Ed=9969.19 (V,Ed,G=-794.45, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.16

Asta n. 102 (114 115) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.02 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.09 (L/920)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.35 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=491.40
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.35
  Sollecitazioni: T_z=1644.74
  V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 102 (115 116) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1448)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (116 117) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.03 (L/4453)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (117 118) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.03 (L/3470)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (118 119) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.09 (L/1344)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (119 120) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-66.70
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.01 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.08 (L/890)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=401.51
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1638.00
  V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 102 (120 121) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-67.25
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00

λ_z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.01 = 0.31
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/890)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.50 - Classe 2
Sollecitazioni: N=-22630.70 T_z=401.51
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.50
Sollecitazioni: T_z=1638.00
V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 102 (121 122) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.09 (L/1345)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (122 123) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/3475)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (123 124) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1

L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/4445)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (124 125) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.08 (L/1445)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 102 (125 126) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.02 = 0.31
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.09 (L/920)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=491.40
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1644.74
  V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 103 (127 128) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.02 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.09 (L/915)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.35 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=491.40
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.35
  Sollecitazioni: T_z=1644.74
  V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 103 (128 129) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1437)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (129 130) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00

αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/4421)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (130 131) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/3446)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (131 132) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.09 (L/1334)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (132 133) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-66.70
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.01 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.08 (L/885)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=401.51
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1638.00
  V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 103 (133 134) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-67.25
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.01 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/885)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.50 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=401.51
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.50
  Sollecitazioni: T_z=1638.00
  V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 103 (134 135) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33

Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.09 (L/1334)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (135 136) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/3451)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (136 137) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/4421)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (137 138) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1436)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 103 (138 139) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.02 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,G}$=0.09 (L/915)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=491.40
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1644.74
  V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 104 (140 141) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 18 My,Ed=-1238.82 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-8256.92
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
  Verifica YY: 0.29 + 0.15 = 0.45
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.07 (L/1104)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.35 - Classe 1
  Sollecitazioni: N=-124143.00 T_z=10607.50
  N,Ed=-124143.00 Nc,Rd=-444147.00 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.35
  Sollecitazioni: T_z=15957.60
  V,Ed=15957.60 (V,Ed,G=1127.12, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.20

Asta n. 104 (141 142) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1721890.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-2342.41 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-15648.80
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1723140.00 λ_{LT}=0.18
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
  Verifica YY: 0.29 + 0.29 = 0.59
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1467)

- Verifica a pressoflessione retta - CC 17 Xl=1.17 - Classe 1
  Sollecitazioni: N=-124143.00 T_z=5550.65 M_y=-15648.80
  My,Ed=-15648.80 My,c,Rd=52055.10
  N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.37

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=15591.30 M_y=-865.66
  V,Ed=15591.30 (V,Ed,G=760.80, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.19

Asta n. 104 (142 143) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1428890.00 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-2677.58 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-17892.80
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1429060.00 λ_{LT}=0.20
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
  Verifica YY: 0.29 + 0.33 = 0.63
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.03 (L/4362)

- Verifica a pressoflessione retta - CC 17 Xl=1.17 - Classe 1
  Sollecitazioni: N=-124143.00 T_z=1150.48 M_y=-17892.80
  My,Ed=-17892.80 My,c,Rd=52055.10
  N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.42

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=15132.60 M_y=-1636.54
  V,Ed=15132.60 (V,Ed,G=302.04, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.19

Asta n. 104 (143 144) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1455320.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-2677.58 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-17892.80
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00

αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1455690.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.66 Ncr,y=29177300.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
Verifica YY: 0.29 + 0.33 = 0.63
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/3412)

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 1
Sollecitazioni: N=-124143.00 T_z=-1714.23 M_y=-17892.80
My,Ed=-17892.80 My,c,Rd=52055.10
N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.42

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=14673.80 M_y=-1870.68
V,Ed=14673.80 (V,Ed,G=-156.72, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.18

Asta n. 104 (144 145) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1786970.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 18 My,Ed=-2244.36 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
Sollecitazioni: N,Ed=-124143.00 My,Ed=-14989.30
Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1788820.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
Verifica YY: 0.29 + 0.28 = 0.57
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/1378)

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 1
Sollecitazioni: N=-124143.00 T_z=-6114.40 M_y=-14989.30
My,Ed=-14989.30 My,c,Rd=52055.10
N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.35

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=14215.00 M_y=-1568.08
V,Ed=14215.00 (V,Ed,G=-615.48, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.18

Asta n. 104 (145 146) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
CC 18 My,Ed=-1042.73 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
Sollecitazioni: N,Ed=-124143.00 My,Ed=-6937.82
Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
Verifica YY: 0.29 + 0.13 = 0.42
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.06 (L/1092)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.67 - Classe 1
Sollecitazioni: N=-124143.00 T_z=-10794.60
N,Ed=-124143.00 Nc,Rd=-444147.00 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=13801.20 M_y=-728.73
  V,Ed=13801.20 (V,Ed,G=-1029.29, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.17

Asta n. 104 (146 147) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 18 My,Ed=-1042.73 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-6937.82
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=9.66 Ncr,y=29177300.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
  Verifica YY: 0.29 + 0.13 = 0.42
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.06 (L/1092)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.50 - Classe 1
  Sollecitazioni: N=-124143.00 T_z=10794.60
  N,Ed=-124143.00 Nc,Rd=-444147.00 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.50
  Sollecitazioni: T_z=15976.50
  V,Ed=15976.50 (V,Ed,G=1146.02, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.20

Asta n. 104 (147 148) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1786970.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-2244.36 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-14989.30
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1788820.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
  Verifica YY: 0.29 + 0.28 = 0.57
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1378)

- Verifica a pressoflessione retta - CC 17 Xl=1.17 - Classe 1
  Sollecitazioni: N=-124143.00 T_z=6114.40 M_y=-14989.30
  My,Ed=-14989.30 My,c,Rd=52055.10
  N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.35

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=15649.80 M_y=-728.72
  V,Ed=15649.80 (V,Ed,G=819.32, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.20

Asta n. 104 (148 149) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1455320.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-2677.58 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-17892.80
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1455690.00 λ_{LT}=0.19

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
Verifica YY: 0.29 + 0.33 = 0.63
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/3412)

- Verifica a pressoflessione retta - CC 17 Xl=1.17 - Classe 1
Sollecitazioni: N=-124143.00 T_z=1714.23 M_y=-17892.80
My,Ed=-17892.80 My,c,Rd=52055.10
N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.42

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=15191.10 M_y=-1568.07
V,Ed=15191.10 (V,Ed,G=360.56, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.19

Asta n. 104 (149 150) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1428890.00 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 18 My,Ed=-2677.58 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
Sollecitazioni: N,Ed=-124143.00 My,Ed=-17892.80
Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1429060.00 λ_{LT}=0.20
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
Verifica YY: 0.29 + 0.33 = 0.63
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/4362)

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 1
Sollecitazioni: N=-124143.00 T_z=-1150.48 M_y=-17892.80
My,Ed=-17892.80 My,c,Rd=52055.10
N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.42

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=14732.30 M_y=-1870.68
V,Ed=14732.30 (V,Ed,G=-98.20, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.18

Asta n. 104 (150 151) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1721890.00 λ_{LT}=0.18
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 18 My,Ed=-2342.41 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
Sollecitazioni: N,Ed=-124143.00 My,Ed=-15648.80
Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1723140.00 λ_{LT}=0.18
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
Verifica YY: 0.29 + 0.29 = 0.59
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/1467)

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 1
Sollecitazioni: N=-124143.00 T_z=-5550.65 M_y=-15648.80
My,Ed=-15648.80 My,c,Rd=52055.10
N,Ed=-124143.00 Nc,Rd=444147.00 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=42443.30 My,Ed/MNy,c,Rd = 0.37

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=14273.60 M_y=-1636.54
  V,Ed=14273.60 (V,Ed,G=-556.96, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.18

Asta n. 104 (151 152) HEB280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 18 My,Ed=-1238.82 My,b,Rd=49689.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 1
  Sollecitazioni: N,Ed=-124143.00 My,Ed=-8256.92
  Resistenze: Nc,Rd=423959.00 My,c,Rd=49689.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=2356720.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=9.66 Ncr,y=29177200.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.51 Ncr,z=9984610.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.54, 0.00, 0.90
  Verifica YY: 0.29 + 0.15 = 0.45
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.07 (L/1104)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.82 - Classe 1
  Sollecitazioni: N=-124143.00 T_z=-10607.50
  N,Ed=-124143.00 Nc,Rd=-444147.00 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=13846.30 M_y=-865.66
  V,Ed=13846.30 (V,Ed,G=-984.25, V,Ed,M=14830.50) Vc,Rd=80224.50 V,Ed/Vc,Rd=0.17

Asta n. 105 (153 154) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.02 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.09 (L/914)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.35 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=491.40
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.35
  Sollecitazioni: T_z=1644.74
  V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 105 (154 155) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00

λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.08 (L/1435)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (155 156) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/4413)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (156 157) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/3451)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (157 158) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1

L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.09 (L/1335)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (158 159) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-66.70
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.01 = 0.31
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/884)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=401.51
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1638.00
V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 105 (159 160) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-67.25
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.01 = 0.31
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/884)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.50 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=401.51
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.50
  Sollecitazioni: T_z=1638.00
  V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 105 (160 161) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.09 (L/1334)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (161 162) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.03 (L/3441)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (162 163) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00

αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/4429)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (163 164) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/1436)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 105 (164 165) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.02 = 0.31
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.09 (L/914)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=491.40
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1644.74
V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 106 (166 167) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.02 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.09 (L/920)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.35 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=491.40
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.35
  Sollecitazioni: T_z=1644.74
  V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 106 (167 168) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.08 (L/1446)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (168 169) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33

Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/4429)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (169 170) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.03 (L/3475)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (170 171) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.09 (L/1345)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (171 172) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-66.70
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.01 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/890)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=401.51
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1638.00
  V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 106 (172 173) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-7.41 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-67.25
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.01 = 0.31
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.08 (L/889)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.50 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=401.51
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.50
  Sollecitazioni: T_z=1638.00
  V,Ed=1638.00 (V,Ed,G=30.12, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 106 (173 174) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.09 (L/1344)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (174 175) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.03 (L/3465)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (175 176) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
  λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
  Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
  Verifica YY: 0.29 + 0.04 = 0.33
  Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.03 (L/4445)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=701.14
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=1660.48
  V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (176 177) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  CC 18 My,Ed=-22.59 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-205.08
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
  λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00

λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.04 = 0.33
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.08 (L/1448)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=701.14
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1660.48
V,Ed=1660.48 (V,Ed,G=52.59, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.08

Asta n. 106 (177 178) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
CC 18 My,Ed=-11.10 My,b,Rd=5353.59 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-100.74
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=26222.40 λ_{LT}=0.48
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.60 β_{LT}=0.75 f=0.98 χ_{LT}=0.99
λ_Y=15.78 Ncr,y=1994020.00 λ^*_y=0.21 Curva a: Φ_y=0.52 χ_y=1.00
λ_Z=57.01 Ncr,z=152695.00 λ^*_z=0.75 Curva b: Φ_z=0.87 χ_z=0.76
Kyy, Kyz, Kzy, Kzz = 0.95, 0.77, 0.00, 1.28
Verifica YY: 0.29 + 0.02 = 0.31
Verifica ZZ: 0.39 = 0.39

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.09 (L/921)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=491.40
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=1644.74
V,Ed=1644.74 (V,Ed,G=36.86, V,Ed,M=1607.89) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.07

Asta n. 107 (179 180) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
CC 19 My,Ed=-857.51 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-4366.56
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.13 = 0.42
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,G}$=0.07 (L/1128)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=5011.54 M_y=-4366.56
Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 σ_{max}=-1376.11
Tensioni: σ_N=-945.00 σ_M=0.00 τ=271.65 τ_{max}=271.65
Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 $\sigma_{ID,max}$=1376.11

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.35
Sollecitazioni: T_z=11558.10
V,Ed=11558.10 (V,Ed,G=794.45, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.19

Asta n. 107 (180 181) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1206500.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 19 My,Ed=-1622.66 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-8276.49
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1207080.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.25 = 0.54
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.08 (L/1499)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=2894.20 M_y=-8276.49
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 σ_{max}=-1762.13
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=156.88 τ_{max}=156.88
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 $\sigma_{ID,max}$=1762.13

Asta n. 107 (181 182) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001010.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 19 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.59
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001090.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.28 = 0.57
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.03 (L/4442)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=567.11 M_y=-9463.59
  Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.34
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=30.74 τ_{max}=30.74
  Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.34

Asta n. 107 (182 183) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019570.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.58
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019740.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211010.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.28 = 0.57
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.03 (L/3500)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-865.24 M_y=-9463.58
  Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.33
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=46.90 τ_{max}=46.90
  Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.33

Asta n. 107 (183 184) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1252230.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-1554.59 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-7927.64
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1253090.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.24 = 0.53
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1410)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-3192.33 M_y=-7927.64
  Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 σ_{max}=-1727.69
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=173.04 τ_{max}=173.04
  Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 $\sigma_{ID,max}$=1727.69

Asta n. 107 (184 185) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 18 My,Ed=-721.36 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-3668.90
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.11 = 0.40
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.06 (L/1117)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-5219.78 M_y=-3668.90
  Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 σ_{max}=-1307.23
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=282.94 τ_{max}=282.94
  Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 $\sigma_{ID,max}$=1307.23

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.67
  Sollecitazioni: T_z=9959.74
  V,Ed=9959.74 (V,Ed,G=-803.90, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.16

Asta n. 107 (185 186) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650940.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 19 My,Ed=-721.36 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-3668.89
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95

L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650940.00 λ_{LT}=0.15
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703100.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211010.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.11 = 0.40
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,G}$=0.06 (L/1116)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=5219.78 M_y=-3668.89
Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 σ_{max}=-1307.23
Tensioni: σ_N=-945.00 σ_M=0.00 τ=282.94 τ_{max}=282.94
Tensioni: σ_N=-945.00 σ_M=-362.23 τ=0.00 $\sigma_{ID,max}$=1307.23

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.50
Sollecitazioni: T_z=11567.50
V,Ed=11567.50 (V,Ed,G=803.90, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.19

Asta n. 107 (186 187) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1252230.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=-1554.59 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-7927.64
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.33 M,cr=1253090.00 λ_{LT}=0.17
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.24 = 0.53
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.08 (L/1408)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=3192.33 M_y=-7927.64
Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 σ_{max}=-1727.69
Tensioni: σ_N=-945.00 σ_M=0.00 τ=173.04 τ_{max}=173.04
Tensioni: σ_N=-945.00 σ_M=-782.69 τ=0.00 $\sigma_{ID,max}$=1727.69

Asta n. 107 (187 188) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 3
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019570.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.58
Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.08 M,cr=1019740.00 λ_{LT}=0.19
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
Verifica YY: 0.29 + 0.28 = 0.57
Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.03 (L/3485)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=1.17 - Classe 3
Sollecitazioni: N=-91917.70 T_z=865.24 M_y=-9463.58
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.33
Tensioni: σ_N=-945.00 σ_M=0.00 τ=46.90 τ_{max}=46.90
Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.33

Asta n. 107 (188 189) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001010.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-1855.02 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.06

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-9463.59
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.06 M,cr=1001090.00 λ_{LT}=0.19
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.48 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.28 = 0.57
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.03 (L/4465)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-567.11 M_y=-9463.59
  Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 σ_{max}=-1879.34
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=30.74 τ_{max}=30.74
  Tensioni: σ_N=-945.00 σ_M=-934.34 τ=0.00 $\sigma_{ID,max}$=1879.34

Asta n. 107 (189 190) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1206500.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=-1622.66 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.05

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-8276.49
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.28 M,cr=1207080.00 λ_{LT}=0.17
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.25 = 0.54
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.08 (L/1502)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-2894.20 M_y=-8276.49
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 σ_{max}=-1762.13
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=156.88 τ_{max}=156.88
  Tensioni: σ_N=-945.00 σ_M=-817.13 τ=0.00 $\sigma_{ID,max}$=1762.13

Asta n. 107 (190 191) HEA280 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 3
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  CC 18 My,Ed=-857.51 My,b,Rd=32688.00 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 3
  Sollecitazioni: N,Ed=-91917.70 My,Ed=-4366.56
  Resistenze: Nc,Rd=313908.00 My,c,Rd=32688.00 L=117.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=1.17 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=1650930.00 λ_{LT}=0.15
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.47 β_{LT}=0.75 f=1.00 χ_{LT}=1.00
  λ_Y=9.87 Ncr,y=20703000.00 λ^*_y=0.13 Curva b: Φ_y=0.50 χ_y=1.00
  λ_Z=16.72 Ncr,z=7211000.00 λ^*_z=0.22 Curva c: Φ_z=0.53 χ_z=0.99
  Kyy, Kyz, Kzy, Kzz = 0.97, 0.99, 0.00, 0.99
  Verifica YY: 0.29 + 0.13 = 0.42
  Verifica ZZ: 0.29 = 0.29

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.07 (L/1129)

- Verifica in termini tensionali (4.2.5) - CC 17 Xl=0.00 - Classe 3
  Sollecitazioni: N=-91917.70 T_z=-5011.54 M_y=-4366.56
  Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 σ_{max}=-1376.11
  Tensioni: σ_N=-945.00 σ_M=0.00 τ=271.65 τ_{max}=271.65
  Tensioni: σ_N=-945.00 σ_M=-431.11 τ=0.00 $\sigma_{ID,max}$=1376.11

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.82
  Sollecitazioni: T_z=9969.19
  V,Ed=9969.19 (V,Ed,G=-794.45, V,Ed,M=10763.60) Vc,Rd=61972.50 V,Ed/Vc,Rd=0.16

Asta n. 108 (101 114) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.36 M,cr=72367.30 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 19 My,Ed=3.88 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-5.01
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.81 M,cr=86110.40 λ_{LT}=0.26
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.00 = 0.29
  Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.57 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-16.06
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2387.05
  V,Ed=2387.05 (V,Ed,G=5.75, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 108 (114 127) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.44 M,cr=44240.20 λ_{LT}=0.37
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 19 My,Ed=3.01 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=4.88
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.01 M,cr=30941.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.00 = 0.29
  Verifica ZZ: 0.33 = 0.33

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=10.13 M_y=4.88
  My,Ed=4.88 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.00

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2389.03 M_y=1.58
  V,Ed=2389.03 (V,Ed,G=7.73, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 108 (127 140) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 5 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.23 M,cr=68400.10 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 5 My,Ed=2.46 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-11.07
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95

L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.88 M,cr=88313.90 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.29 - Classe 2
Sollecitazioni: N=-22630.70 T_z=28.81
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2391.84 M_y=1.88
V,Ed=2391.84 (V,Ed,G=10.54, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 108 (140 153) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.09 M,cr=64089.50 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 19 My,Ed=4.23 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-10.36
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.97 M,cr=91244.20 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.47 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-27.22
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2386.13
V,Ed=2386.13 (V,Ed,G=4.83, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 108 (153 166) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.69 M,cr=52006.80 λ_{LT}=0.34
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 19 My,Ed=4.35 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=4.67
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.04 M,cr=31965.90 λ_{LT}=0.43
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.57 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=10.54 M_y=4.67
My,Ed=4.67 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.00

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.79 M_y=1.25
V,Ed=2388.79 (V,Ed,G=7.49, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 108 (166 179) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 13 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.09 M,cr=64175.20 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 13 My,Ed=2.88 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-4.70
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=3.03 M,cr=92934.60 λ_{LT}=0.25
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.00 = 0.29
  Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.24 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=15.64
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2390.48 M_y=1.63
  V,Ed=2390.48 (V,Ed,G=9.18, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 109 (102 115) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.17 = 0.46
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/4945)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1222.61
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2493.03
  V,Ed=2493.03 (V,Ed,G=111.73, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 109 (115 128) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.17 = 0.46
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.00 (L/31860)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-959.92
  My,Ed=-959.92 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.19

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00

Sollecitazioni: T_z=2388.73 M_y=-82.40
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 109 (128 141) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/5082)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1222.61
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2284.43 M_y=-82.40
V,Ed=2284.43 (V,Ed,G=-96.88, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 109 (141 154) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.01 (L/5310)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1222.61
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2493.03
V,Ed=2493.03 (V,Ed,G=111.73, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 109 (154 167) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88

Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.00 (L/27891)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-959.92
My,Ed=-959.92 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.19

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-82.40
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 109 (167 180) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/4760)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1222.61
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2284.43 M_y=-82.40
V,Ed=2284.43 (V,Ed,G=-96.88, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 110 (103 116) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4194)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2508.76
V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 110 (116 129) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.00 (L/25102)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-1125.62
  My,Ed=-1125.62 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-94.83
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 110 (129 142) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/4589)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2268.69 M_y=-94.83
  V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 110 (142 155) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/4760)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2508.76
  V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 110 (155 168) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.00 (L/22090)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-1125.62
  My,Ed=-1125.62 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-94.83
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 110 (168 181) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/4060)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2268.69 M_y=-94.83
  V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 111 (104 117) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00

CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/4131)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2508.76
V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 111 (117 130) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,G}$=0.00 (L/24010)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-1125.62
My,Ed=-1125.62 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-94.83
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 111 (130 143) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4653)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2268.69 M_y=-94.83
  V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 111 (143 156) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.02 (L/4816)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2508.76
  V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 111 (156 169) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,G}$=0.00 (L/21799)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-1125.62
  My,Ed=-1125.62 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-94.83
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 111 (169 182) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64

Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4011)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2268.69 M_y=-94.83
V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 112 (105 118) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/4162)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2508.76
V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 112 (118 131) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.00 (L/25024)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-1125.62
My,Ed=-1125.62 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-94.83
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 112 (131 144) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/4551)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2268.69 M_y=-94.83
  V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 112 (144 157) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.02 (L/4706)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2508.76
  V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 112 (157 170) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00

λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.00 (L/22695)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-1125.62
My,Ed=-1125.62 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-94.83
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 112 (170 183) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4060)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2268.69 M_y=-94.83
V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 113 (106 119) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.15 = 0.45
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/5259)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1132.72
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2486.28
V,Ed=2486.28 (V,Ed,G=104.98, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 113 (119 132) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.15 = 0.45
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,G}$=0.00 (L/33811)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-888.91
  My,Ed=-888.91 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.18

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-77.07
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 113 (132 145) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.15 = 0.45
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.01 (L/5414)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1132.72
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2291.17 M_y=-77.07
  V,Ed=2291.17 (V,Ed,G=-90.13, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 113 (145 158) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.15 = 0.45

Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.01 (L/5597)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1132.72
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2486.28
V,Ed=2486.28 (V,Ed,G=104.98, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 113 (158 171) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.15 = 0.45
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.00 (L/30122)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-888.91
My,Ed=-888.91 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.18

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-77.07
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 113 (171 184) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.15 = 0.45
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/5113)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1132.72
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2291.17 M_y=-77.07
V,Ed=2291.17 (V,Ed,G=-90.13, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 114 (107 120) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.46 M,cr=75451.50 λ_{LT}=0.28

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 18 My,Ed=2.76 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-6.78
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.39 M,cr=73487.10 λ_{LT}=0.28
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.57 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-17.71
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.74
V,Ed=2388.74 (V,Ed,G=7.44, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 114 (120 133) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.31 M,cr=40351.40 λ_{LT}=0.38
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 19 My,Ed=3.29 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=7.91
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.18 M,cr=36361.00 λ_{LT}=0.40
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.56 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=13.38 M_y=7.91
My,Ed=7.91 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.00

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2391.29 M_y=2.80
V,Ed=2391.29 (V,Ed,G=9.99, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 114 (133 146) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.47 M,cr=75835.40 λ_{LT}=0.28
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=3.82 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-18.28
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.75 M,cr=84552.70 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.30
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.29 - Classe 2
Sollecitazioni: N=-22630.70 T_z=43.96
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2395.57 M_y=3.04
V,Ed=2395.57 (V,Ed,G=14.27, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 114 (146 159) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.22 M,cr=68134.50 λ_{LT}=0.29
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 18 My,Ed=3.32 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-13.52
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.85 M,cr=87478.30 λ_{LT}=0.26
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.00 = 0.30
  Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.47 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-33.56
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.09
  V,Ed=2388.09 (V,Ed,G=6.79, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 114 (159 172) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.32 M,cr=40640.90 λ_{LT}=0.38
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=4.40 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=8.36
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.43 M,cr=43776.50 λ_{LT}=0.37
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.00 = 0.29
  Verifica ZZ: 0.33 = 0.33

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=16.99 M_y=8.36
  My,Ed=8.36 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.00

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2392.77 M_y=2.79
  V,Ed=2392.77 (V,Ed,G=11.47, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 114 (172 185) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 13 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.46 M,cr=75657.20 λ_{LT}=0.28
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  CC 13 My,Ed=5.32 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-10.32
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.90 M,cr=89037.20 λ_{LT}=0.26
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.00 = 0.29
  Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.32 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=26.51
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2395.93 M_y=3.86
  V,Ed=2395.93 (V,Ed,G=14.63, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 115 (108 121) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.15 = 0.45
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.02 (L/5259)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1132.72
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2486.28
  V,Ed=2486.28 (V,Ed,G=104.98, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 115 (121 134) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.15 = 0.45
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,G}$=0.00 (L/33811)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-888.91
  My,Ed=-888.91 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.18

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-77.07
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 115 (134 147) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.15 = 0.45
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.01 (L/5414)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1132.72
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2291.17 M_y=-77.07
V,Ed=2291.17 (V,Ed,G=-90.13, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 115 (147 160) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.15 = 0.45
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.01 (L/5616)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1132.72
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2486.28
V,Ed=2486.28 (V,Ed,G=104.98, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 115 (160 173) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.15 = 0.45
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.00 (L/30122)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-888.91
My,Ed=-888.91 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.18

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-77.07
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 115 (173 186) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-111.80 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-886.93
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.15 = 0.45
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/5113)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1132.72
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2291.17 M_y=-77.07
  V,Ed=2291.17 (V,Ed,G=-90.13, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 116 (109 122) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.02 (L/4131)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2508.76
  V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 116 (122 135) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49

Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.00 (L/24550)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-1125.62
My,Ed=-1125.62 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-94.83
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 116 (135 148) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4551)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2268.69 M_y=-94.83
V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 116 (148 161) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/4693)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2508.76
V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 116 (161 174) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.00 (L/22695)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-1125.62
My,Ed=-1125.62 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-94.83
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 116 (174 187) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4060)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2268.69 M_y=-94.83
V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 117 (110 123) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/4090)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2508.76
  V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 117 (123 136) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.00 (L/23271)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-1125.62
  My,Ed=-1125.62 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-94.83
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 117 (136 149) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/4653)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2268.69 M_y=-94.83
  V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 117 (149 162) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2

Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/4774)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2508.76
V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 117 (162 175) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.00 (L/21799)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-1125.62
My,Ed=-1125.62 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-94.83
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 117 (175 188) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4011)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2268.69 M_y=-94.83
  V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 118 (111 124) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.02 (L/4121)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2508.76
  V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 118 (124 137) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.00 (L/23956)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
  Sollecitazioni: N=-22630.70 M_y=-1125.62
  My,Ed=-1125.62 My,c,Rd=5643.68
  N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
  MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2388.73 M_y=-94.83
  V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 118 (137 150) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4576)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2268.69 M_y=-94.83
V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 118 (150 163) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/4693)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1432.35
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2508.76
V,Ed=2508.76 (V,Ed,G=127.46, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 118 (163 176) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.19 = 0.49
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,G}$=0.00 (L/22090)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-1125.62
My,Ed=-1125.62 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.22

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-94.83
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 118 (176 189) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-137.87 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.03

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-1123.64
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.19 = 0.49
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
  $f_{Z,L}$=0.02 (L/4060)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=-1432.35
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2268.69 M_y=-94.83
  V,Ed=2268.69 (V,Ed,G=-112.61, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 119 (112 125) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.17 = 0.46
  Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
  $f_{Z,L}$=0.02 (L/4844)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
  Sollecitazioni: N=-22630.70 T_z=1222.61
  N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
  Sollecitazioni: T_z=2493.03
  V,Ed=2493.03 (V,Ed,G=111.73, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 119 (125 138) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
  Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
  Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
  αmy, αmz, αLT = 0.95, 0.95, 0.95
  L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
  $\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
  λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
  λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
  Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
  Verifica YY: 0.29 + 0.17 = 0.46

Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.00 (L/29503)

- Verifica a pressoflessione retta - CC 17 Xl=0.39 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-959.92
My,Ed=-959.92 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.19

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-82.40
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 119 (138 151) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/5082)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1222.61
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2284.43 M_y=-82.40
V,Ed=2284.43 (V,Ed,G=-96.88, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 119 (151 164) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.40 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 21
$f_{Z,L}$=0.02 (L/5226)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=1222.61
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2493.03
V,Ed=2493.03 (V,Ed,G=111.73, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 119 (164 177) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44

$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.00 M,cr=30695.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.00 (L/27931)

- Verifica a pressoflessione retta - CC 17 Xl=0.40 - Classe 2
Sollecitazioni: N=-22630.70 M_y=-959.92
My,Ed=-959.92 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.19

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.73 M_y=-82.40
V,Ed=2388.73 (V,Ed,G=7.43, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 119 (177 190) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=-119.62 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.02

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-957.94
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.75 M,cr=53716.50 λ_{LT}=0.33
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.53 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.17 = 0.46
Verifica ZZ: 0.33 = 0.33

- Verifica freccia massima carichi totali - CC 20
$f_{Z,L}$=0.02 (L/4774)

- Verifica a compressione (4.2.10) - CC 17 Xl=0.79 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-1222.61
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2284.43 M_y=-82.40
V,Ed=2284.43 (V,Ed,G=-96.88, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.10

Asta n. 120 (113 126) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.33 M,cr=71502.50 λ_{LT}=0.29
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 18 My,Ed=3.71 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-5.01
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.81 M,cr=86111.40 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.57 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-16.06

N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2387.05
V,Ed=2387.05 (V,Ed,G=5.75, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 120 (126 139) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.37 M,cr=42004.80 λ_{LT}=0.38
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.55 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=2.84 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=4.88
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.01 M,cr=30941.10 λ_{LT}=0.44
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.58 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=10.13 M_y=4.88
My,Ed=4.88 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.00

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2389.03 M_y=1.58
V,Ed=2389.03 (V,Ed,G=7.73, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 120 (139 152) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 19 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.22 M,cr=68277.60 λ_{LT}=0.29
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.51 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
CC 19 My,Ed=2.68 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-11.07
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.88 M,cr=88314.10 λ_{LT}=0.26
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.29 - Classe 2
Sollecitazioni: N=-22630.70 T_z=28.81
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2391.84 M_y=1.88
V,Ed=2391.84 (V,Ed,G=10.54, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 120 (152 165) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.05 M,cr=62829.20 λ_{LT}=0.31
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=3.91 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-10.36
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.97 M,cr=91244.20 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08

Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.47 - Classe 2
Sollecitazioni: N=-22630.70 T_z=-27.22
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2386.13
V,Ed=2386.13 (V,Ed,G=4.83, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Asta n. 120 (165 178) IPE180 Crit. 1

- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 18 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.63 M,cr=49982.00 λ_{LT}=0.34
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.54 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 18 My,Ed=3.91 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=4.67
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=1.04 M,cr=31965.90 λ_{LT}=0.43
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.57 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373670.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a pressoflessione retta - CC 17 Xl=0.00 - Classe 2
Sollecitazioni: N=-22630.70 T_z=10.54 M_y=4.67
My,Ed=4.67 My,c,Rd=5643.68
N,Ed=-22630.70 Nc,Rd=80966.20 n= N,Ed/Nc,Rd = 0.28
MNy,c,Rd=5057.53 My,Ed/MNy,c,Rd = 0.00

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2388.79 M_y=1.25
V,Ed=2388.79 (V,Ed,G=7.49, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

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- Verifica di stabilità aste inflesse (4.2.4.1.3.2) CC 5 - Classe 1
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=2.09 M,cr=64174.50 λ_{LT}=0.30
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.52 β_{LT}=0.75 f=0.98 χ_{LT}=1.00
CC 5 My,Ed=2.88 My,b,Rd=5387.15 My,Ed/My,b,Rd=0.00

- Verifica di stabilità aste presso-inflesse (C4.2.4.1.3.3.2) - CC 17 - Classe 2
Sollecitazioni: N,Ed=-22630.70 My,Ed=-4.70
Resistenze: Nc,Rd=77285.90 My,c,Rd=5387.15 L=79.00
αmy, αmz, αLT = 0.95, 0.95, 0.95
L_{cr}=0.79 Curva b: α-imp=0.34 k_c=0.94 ψ=3.03 M,cr=92934.30 λ_{LT}=0.25
$\lambda_{LT,0}$=0.40 β_{LT}=0.75 Φ_{LT}=0.50 β_{LT}=0.75 f=0.99 χ_{LT}=1.00
λ_Y=10.65 Ncr,y=4373680.00 λ^*_y=0.14 Curva a: Φ_y=0.50 χ_y=1.00
λ_Z=38.50 Ncr,z=334922.00 λ^*_z=0.50 Curva b: Φ_z=0.68 χ_z=0.88
Kyy, Kyz, Kzy, Kzz = 0.93, 0.65, 0.00, 1.08
Verifica YY: 0.29 + 0.00 = 0.29
Verifica ZZ: 0.33 = 0.33

- Verifica a compressione (4.2.10) - CC 17 Xl=0.24 - Classe 2
Sollecitazioni: N=-22630.70 T_z=15.64
N,Ed=-22630.70 Nc,Rd=-80966.20 N,Ed/Nc,Rd=0.28

- Verifica a taglio dir. Z (4.2.17) - CC 1 Xl=0.00
Sollecitazioni: T_z=2390.48 M_y=1.63
V,Ed=2390.48 (V,Ed,G=9.18, V,Ed,M=2381.30) Vc,Rd=21964.00 V,Ed/Vc,Rd=0.11

Verifiche e armature pareti

Simbologia

CC = Numero della combinazione delle condizioni di carico elementari
Zona = Zona di verifica
Zv = Coordinata Z di verifica
Xi = Coordinata X iniziale
Xf = Coordinata X finale
Xv = Coordinata X di verifica
TCC = Tipo di combinazione di carico

SLU = Stato limite ultimo
SLU S = Stato limite ultimo (azione sismica)
SLE R = Stato limite d'esercizio, combinazione rara
SLE F = Stato limite d'esercizio, combinazione frequente
SLE Q = Stato limite d'esercizio, combinazione quasi permanente
SLD = Stato limite di danno
SLV = Stato limite di salvaguardia della vita
SLC = Stato limite di prevenzione del collasso
SLO = Stato limite di operatività
SLU I = Stato limite di resistenza al fuoco

N = Sforzo normale
My = Momento flettente intorno all'asse Y
Nu = Sforzo normale ultimo
Myu = Momento ultimo intorno all'asse Y
Sic. = Sicurezza a rottura
σ_c = Tensione nel calcestruzzo
σ_f = Tensione nel ferro
c = Ricoprimento dell'armatura
s = Distanza minima tra le barre
K3 = Coefficiente di forma del diagramma delle tensioni prima della fessurazione
s_{rm} = Distanza media tra le fessure
Φ = Diametro della barra
A_s = Area complessiva dei ferri nell'area di calcestruzzo efficace
$A_{c\ eff}$ = Area di calcestruzzo efficace
σ_s = Tensione nell'acciaio nella sezione fessurata
σ_{sr} = Tensione nell'acciaio corrispondente al raggiungimento della resistenza a trazione nel calcestruzzo
ε_{sm} = Deformazione unitaria media dell'armatura (*1000)
Wk = Apertura delle fessure
Ty = Taglio in dir. Y
Vsdu = Taglio agente nella direzione del momento ultimo
VRsd = Taglio ultimo lato armatura
VRcd = Taglio ultimo lato calcestruzzo
$V_{Rd,s}$ = Taglio ultimo per scorrimento lungo piani orizzontali
V_{dd} = Contributo effetto spinotto
V_{fd} = Contributo resistenza per attrito
Vrdu = Taglio ultimo assorbibile dal solo calcestruzzo
Sic.T = Sicurezza a rottura per taglio
Sez. = Sezione di verifica
Spess. = Spessore
Cf = Copriferro
Cls = Tipo di calcestruzzo
Fck = Resistenza caratteristica cilindrica a compressione del calcestruzzo
Fctk = Resistenza caratteristica a trazione del calcestruzzo
Fcd = Resistenza di calcolo a compressione del calcestruzzo
Fctd = Resistenza di calcolo a trazione del calcestruzzo
Acc. = Tipo di acciaio
Fyk = Tensione caratteristica di snervamento dell'acciaio
Fyd = Resistenza di calcolo dell'acciaio

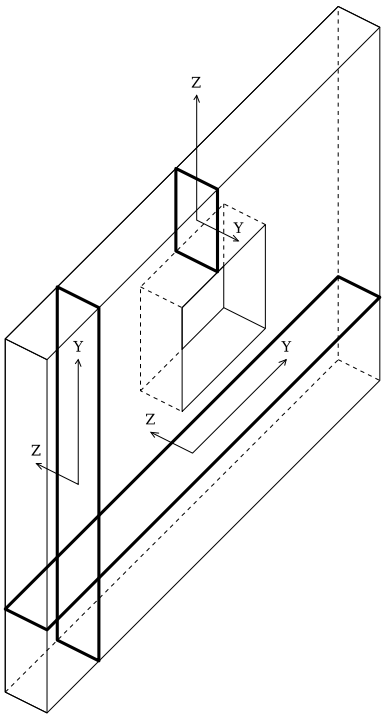

Figura numero 3: Riferimenti sezione

Parete 102

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Spess. <cm>	Cf <cm>	Cls	Fck <daN/cmq>	Fctk <daN/cmq>	Fcd <daN/cmq>	Fctd <daN/cmq>	Acc.	Fyk <daN/cmq>	Fyd <daN/cmq>
Oriz.	100.00	5.20	C32/40	332.00	21.69	188.13	14.46	B450C	4500.00	3913.04

Snellezza massima = 18.36 (CC 17) - Snellezza limite (4.1.2.1.7.2) = 277.30

Verifiche su sezioni orizzontali

Stato limite ultimo - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	Nu <daN>	Myu <daNm>	Sic.
9	SLV	Diff.	0.00	0.00	5.74	-76412.50	81597.10	-76412.80	208565.00	2.556
10	SLD	Diff.	0.00	0.00	5.74	-76412.50	45247.70	-76417.50	237466.00	5.248
9	SLV	Diff.	1.33	0.00	5.74	-63736.60	66761.30	-63741.00	202782.00	3.037
10	SLD	Diff.	1.33	0.00	5.74	-63736.60	37020.80	-63740.50	231642.00	6.257
9	SLV	Diff.	2.65	0.00	5.74	-51060.80	51925.40	-51063.10	196994.00	3.794
10	SLD	Diff.	2.65	0.00	5.74	-51060.80	28794.00	-51063.90	225816.00	7.842
9	SLV	Diff.	3.98	0.00	5.74	-25709.10	22253.80	-25713.80	185412.00	8.332
10	SLD	Diff.	3.98	0.00	5.74	-25709.10	12340.30	-25711.80	214158.00	17.354
9	SLV	Diff.	5.30	0.00	5.74	-13033.30	7417.89	-13035.30	179620.00	24.214
10	SLD	Diff.	5.30	0.00	5.74	-13033.30	4113.41	-13035.80	208330.00	50.647
9	SLV	Loc.	0.00	0.00	5.74	-76344.30	81542.00	-76345.60	208528.00	2.557
10	SLD	Loc.	0.00	0.00	5.74	-76349.40	45217.10	-76354.30	237428.00	5.251

Stato limite d'esercizio - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	σ_c <daN/cmq>	σ_f <daN/cmq>
20	SLE R	Diff.	0.00	0.00	5.74	-76412.50	12.83	1.30	19.51
23	SLE Q	Diff.	0.00	0.00	5.74	-76412.50	8.59	1.30	19.51
20	SLE R	Diff.	1.33	0.00	5.74	-63736.60	10.49	1.09	16.28
23	SLE Q	Diff.	1.33	0.00	5.74	-63736.60	7.02	1.08	16.27
20	SLE R	Diff.	2.65	0.00	5.74	-51060.80	8.16	0.87	13.04
23	SLE Q	Diff.	2.65	0.00	5.74	-51060.80	5.46	0.87	13.04
20	SLE R	Diff.	3.98	0.00	5.74	-25709.10	3.50	0.44	6.56
23	SLE Q	Diff.	3.98	0.00	5.74	-25709.10	2.34	0.44	6.56
20	SLE R	Diff.	5.30	0.00	5.74	-13033.30	1.17	0.22	3.33
23	SLE Q	Diff.	5.30	0.00	5.74	-13033.30	0.78	0.22	3.33
20	SLE R	Loc.	0.00	0.00	5.74	-76289.60	12.65	1.30	19.50
20	SLE R	Loc.	5.30	0.00	5.74	-13025.00	1.16	0.22	3.33
23	SLE Q	Loc.	0.00	0.00	5.74	-76355.40	8.45	1.30	19.51

Parete 103

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Spess. <cm>	Cf <cm>	Cls	Fck <daN/cmq>	Fctk <daN/cmq>	Fcd <daN/cmq>	Fctd <daN/cmq>	Acc.	Fyk <daN/cmq>	Fyd <daN/cmq>
Oriz.	70.00	5.20	C32/40	332.00	21.69	188.13	14.46	B450C	4500.00	3913.04

Snellezza massima = 26.23 (CC 17) - Snellezza limite (4.1.2.1.7.2) = 268.11

Verifiche su sezioni orizzontali

Stato limite ultimo - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	Nu <daN>	Myu <daNm>	Sic.
1	SLV	Diff.	0.00	0.00	5.74	-52054.70	46606.60	-52057.50	135427.00	2.906
2	SLD	Diff.	0.00	0.00	5.74	-52054.70	33279.50	-52059.30	156120.00	4.691
9	SLV	Diff.	1.33	0.00	5.74	-43181.60	-28539.90	-43183.20	-132705.00	4.650
10	SLD	Diff.	1.33	0.00	5.74	-43181.60	-17635.90	-43185.30	-153373.00	8.697
17	SLU	Diff.	2.65	0.00	5.74	-56589.90	-36110.30	-56591.10	-136818.00	3.789
10	SLD	Diff.	2.65	0.00	5.74	-25435.50	-23263.00	-25435.70	-147872.00	6.357
17	SLU	Diff.	3.98	0.00	5.74	-44611.20	-25955.50	-44613.70	-133144.00	5.130
10	SLD	Diff.	3.98	0.00	5.74	-16562.40	-15924.60	-16564.40	-145121.00	9.113
9	SLV	Diff.	5.30	0.00	5.74	-7689.29	-6214.68	-7691.78	-121818.00	19.602
10	SLD	Diff.	5.30	0.00	5.74	-7689.29	-5003.13	-7692.00	-142387.00	28.460
9	SLV	Loc.	0.00	0.15	0.85	-5332.31	5760.35	-5334.47	17457.80	3.031
10	SLD	Loc.	0.00	0.15	0.85	-6219.46	4156.17	-6224.34	20458.70	4.923
9	SLV	Loc.	0.00	0.94	1.64	-5292.27	5659.56	-5292.64	17445.00	3.082
10	SLD	Loc.	0.00	0.94	1.64	-5700.96	4044.62	-5704.71	20298.30	5.019
9	SLV	Loc.	0.00	1.73	2.43	-5631.75	5634.22	-5633.71	17549.40	3.115
10	SLD	Loc.	0.00	1.73	2.43	-5825.53	3992.99	-5828.29	20336.50	5.093
9	SLV	Loc.	0.00	2.53	3.23	-5905.44	5674.49	-5907.86	17633.20	3.107
10	SLD	Loc.	0.00	2.53	3.23	-5934.37	4034.85	-5936.75	20370.00	5.049
1	SLV	Loc.	0.00	3.31	4.01	-5434.49	5658.40	-5438.94	17489.80	3.091
2	SLD	Loc.	0.00	3.31	4.01	-5652.04	4028.60	-5655.92	20283.30	5.035
1	SLV	Loc.	0.00	4.10	4.80	-4995.87	5600.98	-4999.35	17355.30	3.099
2	SLD	Loc.	0.00	4.10	4.80	-5424.27	3985.67	-5427.13	20212.60	5.071
1	SLV	Loc.	0.00	4.89	5.59	-5058.40	5708.24	-5062.29	17374.50	3.044
2	SLD	Loc.	0.00	4.89	5.59	-5915.01	4099.52	-5918.10	20364.20	4.967

Stato limite d'esercizio - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	σ_c <daN/cmq>	σ_f <daN/cmq>
21	SLE R	Diff.	0.00	0.00	5.74	-52054.70	16468.60	6.51	121.52
23	SLE Q	Diff.	0.00	0.00	5.74	-52054.70	16693.20	6.64	127.19
20	SLE R	Diff.	1.33	0.00	5.74	-43181.60	-4250.10	1.88	26.35
23	SLE Q	Diff.	1.33	0.00	5.74	-43181.60	-4065.34	1.85	25.89
20	SLE R	Diff.	2.65	0.00	5.74	-25435.50	-15826.40	7.33	306.27
23	SLE Q	Diff.	2.65	0.00	5.74	-25435.50	-15723.80	7.28	302.75
20	SLE R	Diff.	3.98	0.00	5.74	-16562.40	-11462.60	5.36	239.27
23	SLE Q	Diff.	3.98	0.00	5.74	-16562.40	-11401.00	5.33	237.14
20	SLE R	Diff.	5.30	0.00	5.74	-7689.29	-3515.82	1.56	50.05
23	SLE Q	Diff.	5.30	0.00	5.74	-7689.29	-3495.29	1.54	49.39
21	SLE R	Loc.	0.00	0.15	0.85	-12741.90	2201.66	6.33	86.00
21	SLE R	Loc.	3.98	0.15	0.85	-2176.63	-1408.38	5.37	214.53
23	SLE Q	Loc.	0.00	0.15	0.85	-7197.47	2158.00	6.73	108.28
21	SLE R	Loc.	0.00	0.94	1.64	-8492.22	2037.38	5.91	77.27
21	SLE R	Loc.	3.98	0.94	1.64	-2201.55	-1393.38	5.24	208.04
23	SLE Q	Loc.	0.00	0.94	1.64	-6149.71	2033.72	6.57	128.43
20	SLE R	Loc.	2.65	1.73	2.43	-4442.40	-1719.91	5.83	146.61
21	SLE R	Loc.	3.98	1.73	2.43	-2067.08	-1385.21	5.17	214.50
23	SLE Q	Loc.	0.00	1.73	2.43	-6039.39	1950.19	6.24	116.66
21	SLE R	Loc.	0.00	2.53	3.23	-5968.54	1955.79	6.28	120.83
21	SLE R	Loc.	3.98	2.53	3.23	-1884.50	-1391.34	5.20	228.73
23	SLE Q	Loc.	0.00	2.53	3.23	-5969.75	1994.39	6.45	128.49
20	SLE R	Loc.	0.00	3.31	4.01	-4949.39	1984.17	6.81	179.13
21	SLE R	Loc.	2.65	3.31	4.01	-2695.02	-1732.88	6.48	261.12
23	SLE Q	Loc.	0.00	3.31	4.01	-5894.14	1999.90	6.52	133.29
20	SLE R	Loc.	0.00	4.10	4.80	-3832.65	1950.61	7.13	240.39
21	SLE R	Loc.	2.65	4.10	4.80	-2883.27	-1746.01	6.56	252.40
23	SLE Q	Loc.	0.00	4.10	4.80	-5894.36	1974.62	6.42	128.29
20	SLE R	Loc.	0.00	4.89	5.59	-1803.63	2072.59	8.40	421.41
21	SLE R	Loc.	0.00	4.89	5.59	-1250.60	2025.22	8.34	452.00
23	SLE Q	Loc.	0.00	4.89	5.59	-6856.29	2095.91	6.59	110.43

Verifiche stato limite di formazione delle fessure

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	c <mm>	s <mm>	K3	s_{rm} <mm>	Φ	A_s <cmq>	$A_{c\ eff}$ <cmq>	σ_s <daN/cmq>	σ_{sr} <daN/cmq>	ε_{sm}	Wk <mm>
23	SLE Q	Diff.	0.00	0.00	5.74	-52054.70	16693.20	45.00	194.35	0.16	272.65	14.00	46.18	7227.62	127.19	2295.66	0.02	0.01

22	SLE	F	Diff.	0.00	0.00	5.74	-58567.50	20444.50	45.00	194.35	0.17	276.20	14.00	46.18	7227.62	187.57	2634.11	0.04	0.02
23	SLE	Q	Diff.	2.65	0.00	5.74	-25435.50	-15723.80	45.00	194.35	0.18	289.70	14.00	46.18	7227.55	302.75	4488.40	0.06	0.03
22	SLE	F	Diff.	2.65	0.00	5.74	-31948.20	-19434.70	45.00	194.35	0.18	289.47	14.00	46.18	7227.55	369.49	4449.48	0.07	0.04
23	SLE	Q	Diff.	3.98	0.00	5.74	-16562.40	-11401.00	45.00	194.35	0.19	291.11	14.00	46.18	7227.55	237.14	4730.97	0.05	0.02
22	SLE	F	Diff.	3.98	0.00	5.74	-23075.10	-14016.30	45.00	194.35	0.18	289.44	14.00	46.18	7227.55	266.16	4445.87	0.05	0.03
23	SLE	Q	Diff.	5.30	0.00	5.74	-7689.29	-3495.29	45.00	194.35	0.18	284.09	14.00	46.18	7227.55	49.39	3611.02	0.01	0.00
22	SLE	F	Diff.	5.30	0.00	5.74	-14202.00	-3223.40	45.00	194.35	0.14	247.41	14.00	46.18	7227.55	8.89	1109.27	0.00	0.00
23	SLE	Q	Loc.	3.98	0.15	0.85	-2077.69	-1403.02	45.00	194.35	0.18	277.95	14.00	6.16	888.74	220.22	4393.53	0.04	0.02
22	SLE	F	Loc.	3.98	0.15	0.85	-2816.95	-1731.55	45.00	194.35	0.18	276.75	14.00	6.16	888.74	253.78	4192.08	0.05	0.02
23	SLE	Q	Loc.	3.98	0.94	1.64	-2033.79	-1387.58	45.00	194.35	0.18	279.26	14.00	6.16	895.26	218.44	4400.19	0.04	0.02
22	SLE	F	Loc.	3.98	0.94	1.64	-2768.79	-1702.58	45.00	194.35	0.18	277.94	14.00	6.16	895.26	248.69	4181.13	0.05	0.02
23	SLE	Q	Loc.	3.98	1.73	2.43	-2040.88	-1378.80	45.00	194.35	0.18	279.80	14.00	6.16	898.51	214.68	4364.94	0.04	0.02
22	SLE	F	Loc.	3.98	1.73	2.43	-2898.18	-1689.20	45.00	194.35	0.18	277.85	14.00	6.16	898.51	235.30	4045.94	0.05	0.02
23	SLE	Q	Loc.	3.98	2.53	3.23	-2032.15	-1384.10	45.00	194.35	0.18	280.03	14.00	6.16	899.07	216.32	4375.08	0.04	0.02
22	SLE	F	Loc.	3.98	2.53	3.23	-2944.95	-1707.07	45.00	194.35	0.18	277.91	14.00	6.16	899.07	236.34	4028.63	0.05	0.02
23	SLE	Q	Loc.	3.98	3.31	4.01	-2004.28	-1379.72	45.00	194.35	0.18	279.80	14.00	6.16	897.48	217.93	4408.55	0.04	0.02
22	SLE	F	Loc.	3.98	3.31	4.01	-2857.37	-1689.97	45.00	194.35	0.18	277.84	14.00	6.16	897.48	238.70	4085.16	0.05	0.02
23	SLE	Q	Loc.	3.98	4.10	4.80	-1961.17	-1389.58	45.00	194.35	0.19	279.24	14.00	6.16	892.81	224.62	4480.73	0.04	0.02
22	SLE	F	Loc.	3.98	4.10	4.80	-2688.65	-1704.93	45.00	194.35	0.18	277.91	14.00	6.16	892.81	255.38	4254.53	0.05	0.02
23	SLE	Q	Loc.	3.98	4.89	5.59	-1974.63	-1405.67	45.00	194.35	0.19	276.85	14.00	6.16	878.89	229.03	4508.27	0.04	0.02
22	SLE	F	Loc.	3.98	4.89	5.59	-2706.21	-1734.24	45.00	194.35	0.18	275.61	14.00	6.16	878.89	263.02	4292.97	0.05	0.02

Parete 104

Caratteristiche delle sezioni e dei materiali utilizzati

Sez.	Spess. <cm>	Cf <cm>	Cls	Fck <daN/cmq>	Fctk <daN/cmq>	Fcd <daN/cmq>	Fctd <daN/cmq>	Acc.	Fyk <daN/cmq>	Fyd <daN/cmq>
Oriz.	70.00	5.20	C32/40	332.00	21.69	188.13	14.46	B450C	4500.00	3913.04

Snellezza massima = 26.23 (CC 17) - Snellezza limite (4.1.2.1.7.2) = 268.13

Verifiche su sezioni orizzontali

Stato limite ultimo - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	Nu <daN>	Myu <daNm>	Sic.
9	SLV	Diff.	0.00	0.00	5.74	-52054.70	-46615.30	-52057.60	-135425.00	2.905
10	SLD	Diff.	0.00	0.00	5.74	-52054.70	-33288.10	-52058.20	-156117.00	4.690
1	SLV	Diff.	1.33	0.00	5.74	-43181.60	28532.90	-43184.70	132709.00	4.651
2	SLD	Diff.	1.33	0.00	5.74	-43181.60	17628.90	-43185.50	153377.00	8.700
17	SLU	Diff.	2.65	0.00	5.74	-56589.90	36105.10	-56592.00	136821.00	3.790
2	SLD	Diff.	2.65	0.00	5.74	-25435.50	23259.10	-25440.30	147878.00	6.358
17	SLU	Diff.	3.98	0.00	5.74	-44611.20	25952.40	-44611.80	133147.00	5.130
2	SLD	Diff.	3.98	0.00	5.74	-16562.40	15922.20	-16565.80	145126.00	9.115
1	SLV	Diff.	5.30	0.00	5.74	-7689.29	6213.90	-7690.47	121821.00	19.605
2	SLD	Diff.	5.30	0.00	5.74	-7689.29	5002.35	-7691.66	142391.00	28.465

Stato limite d'esercizio - Armatura a flessione

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	σ_c <daN/cmq>	σ_f <daN/cmq>
20	SLE	R	Diff.	0.00	0.00	5.74	-52054.70	-16480.20	6.52	121.81
23	SLE	Q	Diff.	0.00	0.00	5.74	-52054.70	-16701.80	6.64	127.41
21	SLE	R	Diff.	1.33	0.00	5.74	-43181.60	4247.82	1.88	26.35
23	SLE	Q	Diff.	1.33	0.00	5.74	-43181.60	4058.31	1.84	25.87
21	SLE	R	Diff.	2.65	0.00	5.74	-25435.50	15825.10	7.33	306.22
23	SLE	Q	Diff.	2.65	0.00	5.74	-25435.50	15719.90	7.28	302.62
21	SLE	R	Diff.	3.98	0.00	5.74	-16562.40	11461.90	5.36	239.24
23	SLE	Q	Diff.	3.98	0.00	5.74	-16562.40	11398.70	5.33	237.06
21	SLE	R	Diff.	5.30	0.00	5.74	-7689.29	3515.56	1.56	50.05
23	SLE	Q	Diff.	5.30	0.00	5.74	-7689.29	3494.51	1.54	49.36

Verifiche stato limite di formazione delle fessure

CC	TCC	Zona	Zv <m>	Xi <m>	Xf <m>	N <daN>	My <daNm>	c <mm>	s <mm>	K3	s_{rm} <mm>	Φ	A_s <cmq>	$A_{c\ eff}$ <cmq>	σ_s <daN/cmq>	σ_{sr} <daN/cmq>	ε_{sm}	Wk <mm>
23	SLE	Q	Diff.	0.00	0.00	5.74	-52054.70	-16701.80	45.01	194.35	0.16	272.70	14.00	46.18	7227.96	127.41	2297.70	0.02	0.01
22	SLE	F	Diff.	0.00	0.00	5.74	-58567.50	-20452.90	45.01	194.35	0.17	276.24	14.00	46.18	7227.96	187.80	2635.72	0.04	0.02
23	SLE	Q	Diff.	2.65	0.00	5.74	-25435.50	15719.90	44.99	194.35	0.18	289.68	14.00	46.18	7227.22	302.62	4487.79	0.06	0.03
22	SLE	F	Diff.	2.65	0.00	5.74	-31948.20	19430.90	44.99	194.35	0.18	289.44	14.00	46.18	7227.22	369.36	4448.98	0.07	0.04
23	SLE	Q	Diff.	3.98	0.00	5.74	-16562.40	11398.70	44.99	194.35	0.19	291.09	14.00	46.18	7227.22	237.06	4730.51	0.05	0.02
22	SLE	F	Diff.	3.98	0.00	5.74	-23075.10	14014.00	44.99	194.35	0.18	289.42	14.00	46.18	7227.22	266.08	4445.45	0.05	0.03
23	SLE	Q	Diff.	5.30	0.00	5.74	-7689.29	3494.51	44.99	194.35	0.18	284.07	14.00	46.18	7227.22	49.36	3610.27	0.01	0.00
22	SLE	F	Diff.	5.30	0.00	5.74	-14202.00	3222.64	44.99	194.35	0.14	247.37	14.00	46.18	7227.22	8.88	1108.69	0.00	0.00